

**FOUNDATION INVESTIGATION AND DESIGN REPORT
GWP 392-98-00
PROPOSED EMBANKMENT WIDENING
HIGHWAY 17 FROM STATION 10+400 TO 10+675
TOWNSHIP OF ROLPH**

**December 19, 2005
TG04221**

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1.0 INTRODUCTION

DST Consulting Engineers Inc. (DST) has been retained by JMC Transportation Group to conduct foundation investigations at nine locations for the proposed embankment widening for the passing lanes of Highway 17 and a culvert extension in the Townships of Head and Rolph. This report summarizes the factual information and provides recommendations for one of these sites.

Authorization to proceed with this work was received from JMC Transportation Group. This work was carried out as part of their Total Project Management for the Ministry of Transportation of Ontario (MTO) under G.W.P. 392-98-00.

The project is located on Highway 17, from 6.2 km west of Renfrew County, Road 635, easterly 18.6 km. As part of this project, it is proposed to construct one new east bound passing lane from Station 28+250 to Station 30+850, Twp of Head, one new west bound passing lane from Station 29+120 Twp of Head to Station 12+250 Twp of Rolph and to extend the Colton Creek culvert. Within the alignment for the passing lanes, Detailed Foundation Investigation and Design are required at nine locations for embankment widening and for a culvert extension. The specified locations for detailed foundation design are as follows:

| | |
|-------------------|--------------------------|
| Township of Head | Station 28+475 to 28+700 |
| Township of Head | Station 29+175 to 29+350 |
| Township of Head | Station 30+025 to 30+150 |
| Township of Head | Station 30+450 to 30+600 |
| Township of Head | Station 30+750 to 31+100 |
| Township of Rolph | Station 10+400 to 10+675 |
| Township of Rolph | Station 11+250 to 11+550 |

Township of Rolph Station 11+725 to 11+825

Township of Rolph Station 12+050 to 12+250

At the proposed passing lane locations, the through lanes and the passing lanes will be 3.75 m wide. Shoulder widths at the passing lanes will be 3.0 m on the side of the new passing lane and 2.3 m on the opposite side. The shoulder rounding on the side of the new passing lane will be 1.0 m.

This report addresses the field investigation, laboratory testing program and design for the proposed widening at the Township of Rolph, Station 10+400 to 10+675, as defined by the Ministry as the Foundation Investigation and Design Report.

2.0 SITE DESCRIPTION

Along this section of highway under investigation for the proposed widening, the existing embankment varies in height from approximately 1 m to 2.2 m within the proposed construction. Colton Lake is located on the south side of the highway.

Colton Lake Road begins at the east-most section of investigation limits. A ditch is located approximately 13.6 m north of the centreline of the highway. Overhead wires running along a tree line are located 4.6 m north of the ditch, and Colton Lake Road is another 10.7 m north of the overhead wires. A tree line is noted 7.6 m north of the north edge of Colton Lake Road. The ditch is approximately 2 m wide, and is sloped towards the east. A 760 x 25.87 CSP culvert exists at Station 10+600. There do not appear to be any rock outcrops in the study area.

A picture of the site taken from Station 10+400 looking east is shown below. On the south side of the road is Colton Lake.



3.0 INVESTIGATION PROCEDURES AND LABORATORY TESTING

Site work was carried out between November 12 and December 8, 2004 utilizing a CME 750 and track mounted CME 75 drill rig equipped for geotechnical drilling and operated by DST. Thirteen boreholes were put down to depths ranging between 0.65 to 6.4 m.

Borehole locations and a stratigraphic profile and section are shown on the Borehole Location Plan, Drawing No. 1. Boreholes 9, 4 and 4A are located in the shoulder of the roadway while Boreholes 1 to 3, 5 to 8, 9A, 10 and 11 are located between the toes of the existing and proposed embankments.

The boreholes were advanced with hollow stem augers to auger refusal which varied from 0.65 to 6.4 m below existing grade. At Borehole 4, attempted through the embankment, auger refusal occurred at 0.72 m. The borehole was moved 3 m to the east where penetration through the embankment was achieved. The Borehole was identified as 4A.

Soil samples were obtained from the auger flights and from the split spoon sampler used for the standard penetration test (SPT). The SPT involves driving a 50 mm diameter thick-walled sampler into the soil under the energy of a 63.5 kg weight falling through 760 mm. The number of blows required to drive the sampler 300 mm is known as the standard penetration blow count (N) which provides an indication of the denseness or consistency of the soil. Representative soil samples are obtained from within the sampler. Borehole Logs are presented as Enclosures 1 to 13.

Ground surface elevations at the borehole locations were surveyed by K. Smart Associates Limited.

The fieldwork was supervised on a full-time basis by DST personnel who located the boreholes in the field, supervised the drilling, sampling and in-situ testing, and logged the boreholes. The soil

samples were identified in the field, placed in labelled containers and transported to DST's laboratory in Thunder Bay for further analysis.

Classification and index tests were subsequently performed in the laboratory on samples collected from the boreholes to aid in the selection of engineering properties. Laboratory tests included natural moisture contents and gradation analyses. Laboratory test results are presented on the Borehole Logs and Enclosure 14. Where samples were non-plastic, grainsize analyses were carried out above the 0.075 mm sieve which is adequate for the purposes of soil classification and assessment of frost susceptibility. Other analyses of the finer fractions of non-plastic soils were not carried out given that soil permeability estimates were not required.

4.0 DESCRIPTION OF SUBSURFACE CONDITIONS

4.1 Published Engineering Geology

The Quaternary and bedrock geology of the area under investigation as reported by John F. Gartner and P.F. VanDine in the Northern Ontario Engineering Geology Terrain Study 103, Deep River Area (NTS31K/SW) District of Nipissing and County of Renfrew consists of a discontinuous veneer of ground moraine till over the bedrock. During deglaciation, a number of glaciofluvial deposits were formed (Chapman 1975). Precambrian rocks of the Grenville Structural Province underlie the Deep River map area. The oldest and most abundant rocks of the metamorphic complex are metasediments derived largely from siliceous sandstone and siltstones. These metasediments consist of a variety of gneisses and can be found throughout most of the map area.

The mapping associated with the above report indicates that the soil, landform, topography and drainage generally consist of sand and gravel outwash plain with moderate local relief and dry.

4.2 Field Observations

The generalized stratigraphy of the site based on the borehole locations off the highway consist of organics overlying a sand. Auger refusal occurred in all boreholes. The refusal material was not confirmed by diamond drilling techniques, therefore could be boulders or bedrock. At Borehole 7 location, the refusal occurred at 0.65 m. An area one meter square was excavated down to the refusal depth and found to be bedrock. Bedrock knobs exist throughout the area of investigation.

The highway fill, as identified by Boreholes 4, 4A and 9, consists of granular fill to about 2.4 m. A trace of organics was found in the split spoon sample at 2.4 m in Borehole 4A and 9. Below the granular fill to auger refusal of 3.3 m and 6.4 m a sand and/or silt exists.

4.3 Embankment Fill

The fill in the highway embankment consists of sand and gravel. The sand and gravel comprises the base and subbase materials. The base materials vary in thickness from 0.15 to 0.28 m. The subbase varies in thickness from 2.1 to 2.3 m. The bottom of the fill varies between elevations 172.1 m and 172.3 m.

The Standard Penetration Test (SPT) results generally indicate very loose to compact state of denseness (N values vary from 3 blows/0.3 m to 16 blows/0.3 m).

Gradation analyses (Enclosure 14) conducted on samples from Boreholes 9 at 0.7 m and 1.5 m indicate the percent fines (silt and clay fraction) varies from 7 to 8%, 89% sand and 7 to 8% gravel.

4.4 Organics

An organic layer is present at surface in all boreholes located off the Highway varying from Elevation 174.5 to 173.1 m. The organic layer is generally less than 0.3 m thick except at Boreholes 06-02 and 06-03 where peat and sand was found to extend to depths of up to 0.7 m. In general, the organic layers consist of a mixture of root mat, inorganic soil and peat.

Primary and secondary consolidation properties of the peat and sand have been estimated based on published correlations for peat.

A trace of organics was also found in the split spoon sample from Borehole 06-04A and 9 beneath the road fill at 2.4 m depth.

4.5 Sand and/or Silt

From beneath the fill and/or organics noted above, a sand and/or silt exists to auger refusal varying between 0.65 and 6.4 m below existing grade. Gradation analyses conducted on representative samples retrieved from the field investigation at Boreholes 1, 5 and 11 indicate 0% gravel content, 20% to 94% sand and 6 to 80% silt (Enclosure 14).

The Standard Penetration Test (SPT) results generally indicate a very loose to compact state of denseness (N values vary from 2 blows/0.3 m to 16 blows/0.3 m).

4.6 Groundwater

The groundwater levels taken on completion of drilling are noted on the Borehole Logs, Enclosures 1 to 3. Colton Lake exists on the south side of the highway at this location. The groundwater level in this area will generally be affected by the existing lake level or run along the existing bedrock surface where the bedrock is at a higher elevation. The groundwater level in the off road boreholes noted during our field investigation varied between 0.6 m and 1.5 m below existing grade. For design purposes, the high groundwater level should be taken at the natural ground surface outside the embankment.

Groundwater levels may fluctuate seasonally and in response to climatic conditions.

5.0 DISCUSSION

DST Consulting Engineers Inc. (DST) has been retained by JMC Transportation Group to conduct a foundation investigation for proposed westbound passing lane of Highway 17 in the Township of Rolph between Stations 10+400 and 10+675. It is understood that no significant change in grade is expected. The existing embankment width (shoulder to shoulder) is understood to be 12.1 m. With the addition of a new passing lane and the proposed modifications to the lane and shoulder widths, it is understood that the new embankment width from end of shoulder to end of shoulder will be 16.55 m. With a 1.0 m rounding proposed for the passing lane side of the embankment, the distance from existing centerline to end of rounding on the passing lane side will be 11.5 m ($3.75 + 3.75 + 3.0 + 1$). Along the proposed passing lane side, the existing height of the embankment varies from 1.0 to 2.2 m with side slope grades between 2.1 and 6.8 horizontal to 1 vertical.

The subsurface conditions below the existing embankment shoulder consists of up to 2.4 m of granular fills overlying sands and silts. In general, the subsurface conditions beyond the existing toe of the embankment were found to consist of up to 0.7 m topsoil and/or peat with sand overlying sands and silts.

Engineering properties for embankment fill have been estimated as follows:

- Unit Weight, $\gamma = 20 \text{ kN/m}^3$
- Drained Angle of Internal Friction, $\phi' \geq 30^\circ$
- Drained Cohesion Intercept, $c' = 0 \text{ kPa}$

For the normally consolidated organics outside of the existing embankment the following consolidation properties have been estimated based on highest natural moisture content measured

of 35%:

- Void Ratio (e) varies from 1 to 1.5.
- Compression Index (C_c) varies from 1 to 1.5.
- Secondary Compression Index (C_α) varies from 0.1 to 0.15.
- Unit Weight (γ) = varies from 12 to 13 kN/m³.

Engineering properties for sand and/or silt have been estimated as follows:

- Unit Weight, $\gamma = 20 \text{ kN/m}^3$
- Drained Angle of Internal Friction, $\phi' \geq 28^\circ$
- Drained Cohesion Intercept, $c' = 0 \text{ kPa}$

Based on the findings of the field and laboratory programs preliminary engineering assessment of various construction alternatives were carried out to identify the most feasible construction option. The results of this preliminary assessment have been discussed in Section 5.1, Preliminary Assessment of Construction Alternatives. Assessments for stability and settlement have been carried out for static conditions and are reported in subsequent sections of this report for the preferred option.

As indicated in the Draft Supplemental Pavement Design Report, G.W.P. 392-98-00, carried out for this project by Golder Associates Ltd., it is understood that are no settlement areas identified within this section of the highway.

5.1 Preliminary Assessment of Foundation Alternatives

Based on the findings of the field investigation works and engineering assessment, the following

table has been prepared summarizing and comparing various foundation alternatives. Through this exercise of comparing the various foundation alternatives, DST has selected a preferred option.

DST recommends subexcavation and replacement of the topsoil and any peat below the proposed embankment widening (Foundation Alternative 2 in the following table). Given relatively shallow and variable organic thickness found below the proposed widening, removal is recommended to avoid potential differential and long term embankment settlements. As the topsoil/peat thickness is generally less than 0.7 m, costs associated with its removal are considered to be relatively small given the much improved settlement performance. The subsequent sections of this report address this foundation alternative in detail.

| Foundation Alternative | Advantages | Disadvantages | Costs | Risks/Consequences |
|--|---|---|---|--|
| 1) Fill placement without peat excavation | Lowest cost alternative. | Poor settlement performance with differential and short and long term settlements. Within the embankment widening, maximum settlements due to primary consolidation of the peat has been estimated at less than 230 mm, most of which will occur over a period of 1 to 2 months (regrading will be required to account for settlement during this period). Additional settlement due to secondary consolidation of the peat over a 25 year period has been estimated to be in the order of 90 mm. Side slopes flatter than 1.25:1 for rockfill and 2:1 for earth fill would likely be required. Possible peat displacement during fill placement at localized areas; however this risk can be reduced through the use of a geotextile. Typically, staged construction may be required where embankment fills over peat exceed 1.2 m which could add to construction delays. | Lowest cost for construction. Some additional construction costs associated with geotextile and staged construction may be warranted to avoid peat displacement. Highest long term maintenance costs. | High risk of poor settlement performance (both short and long term). Instability and displaced peat will need to be addressed during construction. Zones where peat has been displaced can lead to more severe differential settlements. Risk of higher long term maintenance costs associated with settlements. |
| 2) Fill placement with peat sub-excavation | Short and long term settlement below widening associated with primary and secondary consolidation of the peat is mitigated. Settlements associated with native soils below peat are expected to be negligible. Conventional side slopes of 1.25:1 for rockfill and 2:1 for earth fill will likely prove adequate. | Excavation of the peat will likely be required in the wet with subsequent fill placement. Fill placement below water will require the use of rockfill or 19 mm stone and a geotextile separator. | Costs associated with topsoil/peat excavation are considered are expected to be minimal given the topsoil/peat thickness is generally less than 0.3 m and up to 0.6 m at one location (as indicated on the test hole logs). It is expected that excavation can be carried out without utilizing specialized equipment such as a drag line. Long term maintenance costs will be reduced given improved settlement performance. | It will be important to ensure all peat is removed especially where excavation in the wet is required. Where zones of peat are left in-place localized areas of differential settlement can be expected. Should peat be found at depths deeper than expected special measures may be required for subexcavation. Potential instability and/or settlement of existing embankment due to subexcavation |

| Foundation Alternative | Advantages | Disadvantages | Costs | Risks/Consequences |
|---|---|--|--|--|
| 3) Lightweight fills without peat excavation | Can be used to mitigate/reduce potential settlement issues. | Unless costly rigid foam type insulation is considered for lightweight fill, settlement reduction will be negligible. Foam type insulation is not recommended below the water level. Some fill will be required above and below the insulation which will lead to primary and secondary consolidation of the peat. For up to 1.0 m of fill placement primary consolidation in the order of 150 mm can be expected with secondary consolidation settlements in the order of 90 mm over 25 years. Regrading will be required during the period of primary consolidation. | Construction utilizing rigid foam type insulation is likely cost prohibitive and not warranted. Some increased long term maintenance cost may be realized to address some differential settlement due to secondary consolidation of the peat. | Black ice formation is a known problem where rigid foam type insulations are used. |
| 4) Preload with or without surcharge or wick drains | Preloading without wickdrains may be considered to reduce/mitigate primary consolidation of the peat. | Given the relatively small settlements expected, preloading is not considered feasible. Wickdrains would not prove economical to accelerate preload duration. Light surcharge loads may be considered. | Additional cost associated with additional regrading required after preloading and for construction delays. Long term maintenance cost will be higher than that of peat removal given some long term settlement can be expected due to secondary consolidation (unless a surcharge is considered). Displacement of the peat may be incurred during construction. | Preload may not prove adequate in eliminating all long term consolidation of the peat which can be highly differential leading to increased maintenance costs. |
| 5) Retained Soil System | Can be useful to permit construction with steeper than conventional slopes. However, given embankment toes are expected to be within existing ROW, an RSS is not warranted. | High costs, not warranted. Would likely require peat removal to provide necessary foundation capacity and improve settlement performance. | High cost, not warranted. | A retained soil system does not improve settlement performance, not warranted. |

5.2 Stability Analysis For Proposed Passing Lane

The grade of the proposed new passing lane and associated shoulder will approximately match the height of the existing roadway (approximately 1.0 to 2.2 m height) and be 6.75 m in width. The existing side slope is constructed at a slope of 4.0 to 6.8 H:1V utilizing granular fill. At this time it is not known if the proposed new widening will utilize rockfill (if available), or granular fill. As such, recommendations for both construction materials have been provided. Peat subexcavation is proposed by DST as per OPSD 203.030, or OPSD 203.020 (Appendix 'B') with a side slope of 1.25H:1V for rockfill, or 2.0H:1V for granular fill. The peat subexcavation is to be extended as per Note 1 of these standards.

The above noted configurations provide a minimum design target factor of safety of at least 1.3 for end of construction and final long term (drained) conditions.

Under OPSD 203.020, the existing side slopes is specified to be temporarily cut at a slope of 1 horizontal to 1 vertical starting at the existing shoulder. This is done to facilitate the removal of more peat possibly located below the existing side slope. It should be noted that sloughing of the 1 horizontal to 1 vertical slope may be experienced during construction. The degree of sloughing will be largely dependant on the duration in which it is left to stand. Backfilling of the slope to design levels should commence immediately after excavation. We recommend rapid excavation and backfilling methods be utilized. The temporary slope should be visually inspected as construction progresses. Should excessive sloughing become problematic, the temporary cut slope angle may be revised to 1.5 horizontal to 1 vertical. However, additional settlements may be incurred below the proposed new shoulder and rounding.

5.3 Settlement of Proposed Passing Lane

Maximum settlements induced by the proposed passing lane fills due to primary and secondary consolidation of any peat remaining below the existing embankment and side slope have been estimated based on two scenarios as follows:

1. During peat subexcavation, the existing side slope is maintained, as per OPSD 203.030.
2. During peat subexcavation, the existing side slope is cut at 1H:1V, as per OPSD 203.020.

The following table indicates the settlements calculated for construction as per OPSD 203.030.

| Location | Primary Consolidation of Peat (mm) | Secondary Consolidation of Peat Over 25 yrs. (mm) | Total Settlement After 25 years (mm) |
|-----------------------|---|--|---|
| C/L Existing Roadway | N/A | N/A | N/A |
| Existing Shoulder | < 5 | 25 | 30 |
| Midpoint Passing Lane | < 5 | 25 | 30 |
| Passing Lane Shoulder | 90 | 90 | 180 |

The following table indicates the settlements calculated for construction as per OPSD 203.020.

| Location | Primary Consolidation of Peat (mm) | Secondary Consolidation of Peat Over 25 yrs. (mm) | Total Settlement After 25 years (mm) |
|-----------------------|---|--|---|
| C/L Existing Roadway | N/A | N/A | N/A |
| Existing Shoulder | < 5 | 25 | 30 |
| Midpoint Passing Lane | < 5 | 25 | 30 |
| Passing Lane Shoulder | N/A | N/A | N/A |

Estimated settlements due to consolidation of organic soils for the above scenarios have been presented in the following tables. The settlements have been calculated for a passing lane embankment constructed to the same grade as the existing highway shoulder over the thickest deposit of peat found below the proposed embankment widening. Settlements have been calculated at the existing centerline, existing shoulder, approximate midpoint of passing lane, and

the approximate shoulder of the new passing lane. It is expected that most of the primary consolidation of the peat will occur over a period of 1 to 2 months. For a 2 month construction period, we expect that at least 90% of the primary consolidation will have occurred (actual degree of primary consolidation during construction will depend fill placement methods and scheduling). Secondary consolidation has been calculated over a 25 year period.

The settlements along the longitudinal profile of the passing lane will vary and be roughly proportional to the thickness of the peat deposit below the embankment.

Settlements attributed to the native sands and silts below the proposed widening have been estimated to be less than 10 mm and are expected to occur during construction.

6.0 RECOMMENDATIONS

A new westbound passing lane is proposed from Stations 10+400 to 10+675 in the Township of Rolph. The existing highway embankment is approximately 1.0 to 2.2 m in height and is to be widened to facilitate the construction of the new passing lane and shoulder. The existing native soils at the site consist of up to 0.7 m of topsoil/peat overlying sands and silts.

The additional load of the proposed passing lane does not adversely affect the stability of the existing highway embankment, nor the passing lane itself. In general, the ground level is similar on both sides of the embankment. The construction of the passing lane can therefore proceed without special considerations for stabilizing the embankment. It is recommended the passing lane be constructed in accordance with OPSD 203.020, Embankments Over Swamp, Existing Slope Excavated to 1:1. This is to avoid the estimated shoulder settlements, as per section 5.3 Settlement of Proposed Passing Lane, for construction in accordance with OPSD 203.030, Embankments Over Swamp, Existing Slopes Maintained.

It is expected that at least 90% of the primary consolidation settlements within organic soils, as provided in Section 5.3, will occur during construction. The remaining long term settlements will begin during fill placement for the passing lane and will continue at a decreasing rate. As such, some minor long term maintenance of these areas may be required as the new fills continue to settle. This may involve occasional grading/filling of shoulders and patching of asphalt.

Benching of earth slopes should be carried out in accordance with OPSD 208.010, Benching of Earth Slopes. The existing organics and deleterious material beneath the proposed widening should be excavated to the native sand which will be in the order of 0.2 to 0.6 m deep as indicated

as discrete borehole locations. The width of swamp excavation should include the additional excavation as indicated in Note 1 of OPSD 203.020.

The native sand subgrade will likely be wet and easily disturbed through site traffic of any type. Water ingress into the excavation will need to be controlled and granular fill should be placed and compacted immediately following excavation. Where dewatering cannot be accomplished, excavation of the peat and fill placement in the wet should be considered. The use of self compacting rock fill or clear stone (such as 19mm stone) should be used below the water level.

Where the embankment material will consist of rockfill, a side slope of 1.25H:1V can be constructed. Voids on the top of the rockfill embankment should be chinked with rock fragments and spalls to form the subgrade as per OPSS 206.07.08, Rock Embankments.

Where the embankment material consists of Granular 'B', Type 1 fill in accordance with OPSS 1010, a side slope of 2:1 should be constructed. The embankment fill should be placed in lifts to the required subgrade level and compacted to a minimum 95% of standard Proctor maximum dry density. The slope should be initially overbuilt and cut back to the design slope in order to achieve the specified compaction to the slope face.

Where rockfill and/or clear stone fill is used to replace the excavated peat, a non-woven geotextile (OPSS 1860.07.05.02 Class II) should be placed between the native subgrade and fill to prevent the migration of fines into the void spaces of the fill.

6.1 Construction

The construction methodology must be in accordance with all relevant Ministry guidelines. The contractor's methods and equipment must be suitable for the site conditions and materials used.

Equipment and worker traffic over the subgrade soil should be avoided and the first lift of fill should be placed and compacted immediately after excavation to provide a working surface and protection for the subgrade. Given the design ground water level is at or near the surface of the peat, advanced dewatering methods may be required during excavation of the peat to permit excavations in the dry. It may prove more economical to carry out peat subexcavation and fill placement in the wet. Where construction in the wet is considered, tight quality control will be required to ensure adequate subexcavation has been achieved and also be required to ensure adequate fill placement to above the water level.

7.0 LIMITATIONS OF REPORT

A description of limitations which are inherent in carrying out site investigation studies is given in Appendix "A", and this forms an integral part of this report.

For DST CONSULTING ENGINEERS INC.

Prepared by:

Reviewed by:

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RFC:dm

APPENDIX 'A'
LIMITATIONS OF REPORT

LIMITATIONS OF REPORT

GEOTECHNICAL STUDIES

The data, conclusions and recommendations which are presented in this report, and the quality thereof, are based on a scope of work authorized by the Client. Note that no scope of work, no matter how exhaustive, can identify all conditions below ground. Subsurface and groundwater conditions between and beyond the testholes may differ from those encountered at the specific locations tested, and conditions may become apparent during construction which were not detected and could not be anticipated at the time of the site investigation. Conditions can also change with time. It is recommended practice that DST Consulting Engineers be retained during construction to confirm that the subsurface conditions throughout the site do not deviate materially from those encountered in the testholes. The benchmark and elevations used in this report are primarily to establish relative elevation differences between the testhole locations and should not be used for other purposes, such as grading, excavation, planning, development, etc.

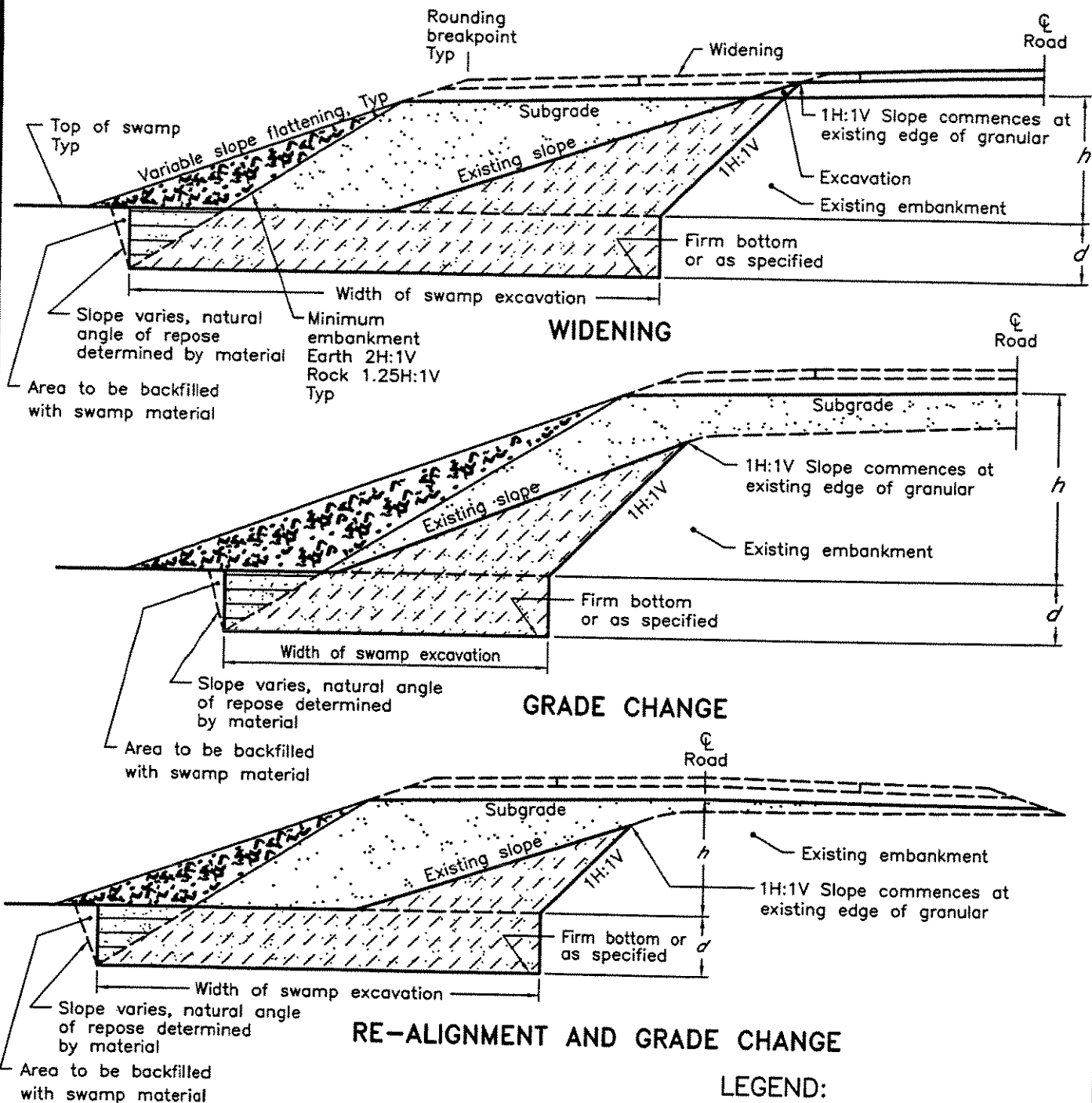
The design recommendations given in this report are applicable only to the project described in the text and then only if constructed substantially in accordance with details stated in this report. Since all details of the design may not be known, we recommend that we be retained during the final stage to verify that the design is consistent with our recommendations, and that assumptions made in our analysis are valid.

Unless otherwise noted, the information contained herein in no way reflects on environmental aspects of either the site or the subsurface conditions.

The comments given in this report on potential construction problems and possible methods are intended only for the guidance of the designer. The number of testholes may not be sufficient to determine all the factors that may affect construction methods and costs, e.g. the thickness of surficial topsoil or fill layers may vary markedly and unpredictably. The contractors bidding on this project or undertaking the construction should, therefore, make their own interpretation of the factual information presented and draw their own conclusion as to how the subsurface conditions may affect their work.

Any results from an analytical laboratory or other subcontractor reported herein have been carried out by others, and DST Consulting Engineers Inc. cannot warranty their accuracy. Similarly, DST cannot warranty the accuracy of information supplied by the client.

A P P E N D I X 'B'
OPSD DRAWINGS



NOTES:

- For given limits of height $h \leq 4.5\text{m}$ and depth $d \leq 6.0\text{m}$, both requirements shall be met in order to apply.
- Height of fill is the vertical difference between top of subgrade and top of swamp elevation measured at new road centreline.
- Widening of existing earth embankments shall be benched according to OPSD-208.010.
- All dimensions are in millimetres unless otherwise shown.

LEGEND:

- h - Height of fill
- d - Depth of sub-excitation
- Embankment materials as specified
- Excavated swamp material
- Excavate and backfill
- Excavate and backfill with swamp material

ONTARIO PROVINCIAL STANDARD DRAWING

EMBANKMENTS OVER SWAMP

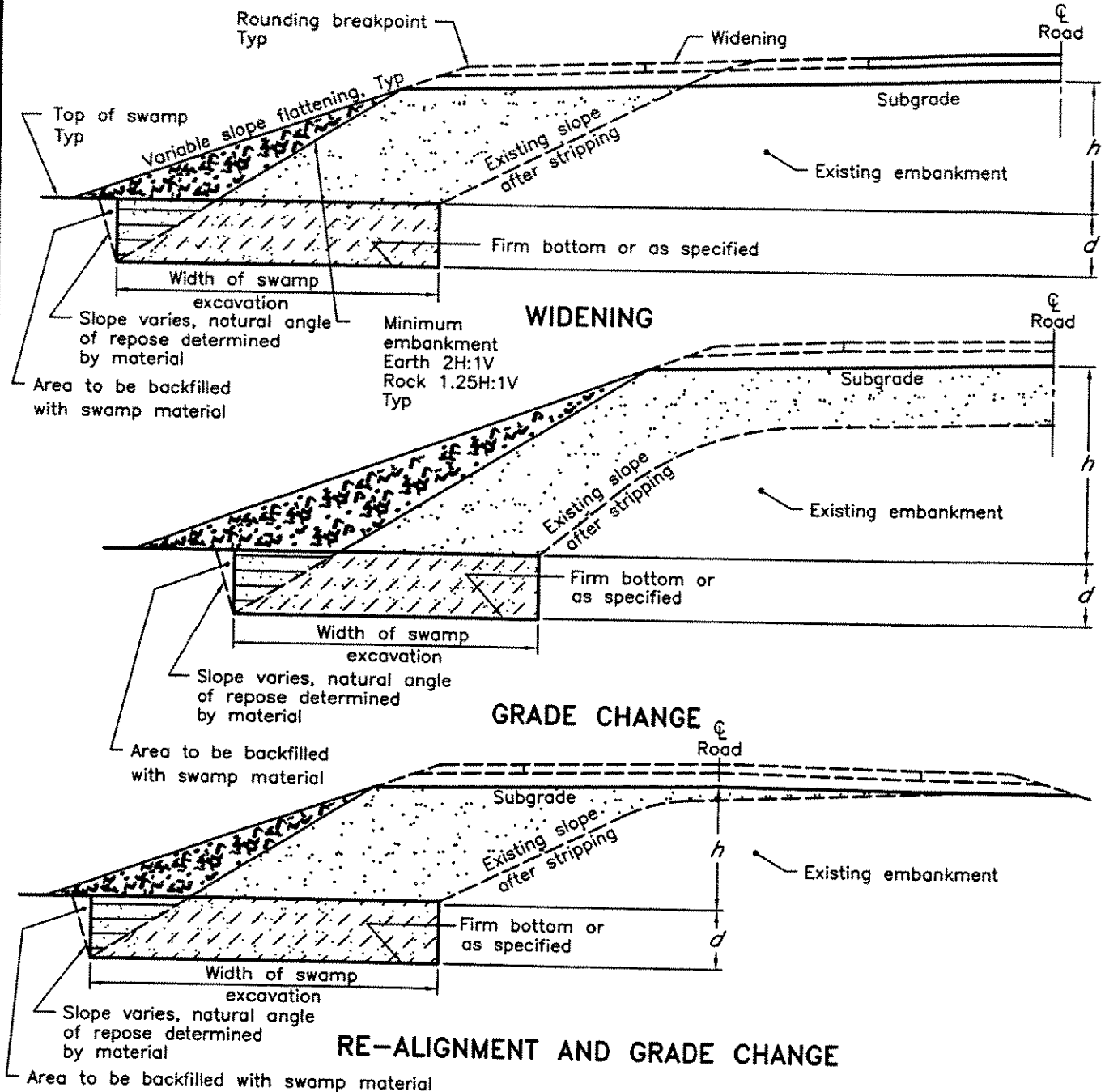
EXISTING SLOPE EXCAVATED TO 1H:1V

Nov 2004

Rev 1



OPSD - 203.020



NOTES:

- For given limits of height $h \leq 4.5\text{m}$ and depth $d \leq 6.0\text{m}$, both requirements shall be met in order to apply.
- Topsoil shall be stripped from existing slopes.
- Height of fill is the vertical difference between top of subgrade and top of swamp elevation measured at new road centreline.
- Widening of existing earth embankments shall be benched according to OPSD-208.010.
- All dimensions are in millimetres unless otherwise shown.

LEGEND:

- h - Height of fill
 d - Depth of sub-excavation
- Embankment materials as specified
 - Excavated swamp material
 - Excavate and backfill
 - Excavate and backfill with swamp material

ONTARIO PROVINCIAL STANDARD DRAWING

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EMBANKMENTS OVER SWAMP

EXISTING SLOPES MAINTAINED



OPSD - 203.030

DRAWINGS

ENCLOSURES

EXPLANATION OF TERMS USED IN REPORT

N VALUE: THE STANDARD PENETRATION TEST (SPT) N VALUE IS THE NUMBER OF BLOWS REQUIRED TO CAUSE A STANDARD 51mm O.D. SPLIT BARREL SAMPLER TO PENETRATE 0.3m INTO UNDISTURBED GROUND IN A BOREHOLE WHEN DRIVEN BY A HAMMER WITH A MASS OF 63.5kg, FALLING FREELY A DISTANCE OF 0.76m. FOR PENETRATIONS OF LESS THAN 0.3m N VALUES ARE INDICATED AS THE NUMBER OF BLOWS FOR THE PENETRATION ACHIEVED. AVERAGE N VALUE IS DENOTED THUS \bar{N} .

DYNAMIC CONE PENETRATION TEST: CONTINUOUS PENETRATION OF A CONICAL STEEL POINT (51mm O.D. 60° CONE ANGLE) DRIVEN BY 475 J IMPACT ENERGY ON 'A' SIZE DRILL RODS. THE RESISTANCE TO CONE PENETRATION IS MEASURED AS THE NUMBER OF BLOWS FOR EACH 0.3m ADVANCE OF THE CONICAL POINT INTO THE UNDISTURBED GROUND.

SOILS ARE DESCRIBED BY THEIR COMPOSITION AND CONSISTENCY OR DENSENESS.

CONSISTENCY: COHESIVE SOILS ARE DESCRIBED ON THE BASIS OF THEIR UNDRAINED SHEAR STRENGTH (c_u) AS FOLLOWS:

| c_u (kPa) | 0 - 12 | 12 - 25 | 25 - 50 | 50 - 100 | 100 - 200 | > 200 |
|-------------|-----------|---------|---------|----------|------------|-------|
| | VERY SOFT | SOFT | FIRM | STIFF | VERY STIFF | HARD |

DENSENESS: COHESIONLESS SOILS ARE DESCRIBED ON THE BASIS OF DENSENESS AS INDICATED BY SPT N VALUES AS FOLLOWS:

| N (BLOWS/0.3m) | 0 - 5 | 5 - 10 | 10 - 30 | 30 - 50 | > 50 |
|----------------|------------|--------|---------|---------|------------|
| | VERY LOOSE | LOOSE | COMPACT | DENSE | VERY DENSE |

ROCKS ARE DESCRIBED BY THEIR COMPOSITION AND STRUCTURAL FEATURES AND/OR STRENGTH.

RECOVERY: SUM OF ALL RECOVERED ROCK CORE PIECES FROM A CORING RUN EXPRESSED AS A PERCENT OF THE TOTAL LENGTH OF THE CORING RUN.

MODIFIED RECOVERY: SUM OF THOSE INTACT CORE PIECES, 100mm+ IN LENGTH EXPRESSED AS A PERCENT OF THE LENGTH OF THE CORING RUN. THE ROCK QUALITY DESIGNATION (RQD), FOR MODIFIED RECOVERY, IS:

| RQD (%) | 0 - 25 | 25 - 50 | 50 - 75 | 75 - 90 | 90 - 100 |
|---------|-----------|---------|---------|---------|-----------|
| | VERY POOR | POOR | FAIR | GOOD | EXCELLENT |

JOINTING AND BEDDING:

| SPACING | 50mm | 50 - 300mm | 0.3m - 1m | 1m - 3m | > 3m |
|----------|------------|------------|------------|---------|------------|
| JOINTING | VERY CLOSE | CLOSE | MOD. CLOSE | WIDE | VERY WIDE |
| BEDDING | VERY THIN | THIN | MEDIUM | THICK | VERY THICK |

ABBREVIATIONS AND SYMBOLS

FIELD SAMPLING

| | | | |
|-----|---------------------|-----|----------------------------|
| S S | SPLIT SPOON | T P | THINWALL PISTON |
| W S | WASH SAMPLE | O S | OSTERBERG SAMPLE |
| S T | SLOTTED TUBE SAMPLE | R C | ROCK CORE |
| B S | BLOCK SAMPLE | P H | T W ADVANCED HYDRAULICALLY |
| C S | CHUNK SAMPLE | P M | T W ADVANCED MANUALLY |
| T W | THINWALL OPEN | F S | FOIL SAMPLE |

MECHANICAL PROPERTIES OF SOIL

| | | |
|----------------|-----------------------|--------------------------------------|
| m_v | kPa^{-1} | COEFFICIENT OF VOLUME CHANGE |
| C_c | 1 | COMPRESSION INDEX |
| C_s | 1 | SWELLING INDEX |
| C_α | 1 | RATE OF SECONDARY CONSOLIDATION |
| c_v | m^2/s | COEFFICIENT OF CONSOLIDATION |
| H | m | DRAINAGE PATH |
| T_v | 1 | TIME FACTOR |
| U | % | DEGREE OF CONSOLIDATION |
| σ'_{vo} | kPa | EFFECTIVE OVERBURDEN PRESSURE |
| σ'_p | kPa | PRECONSOLIDATION PRESSURE |
| τ_f | kPa | SHEAR STRENGTH |
| c' | kPa | EFFECTIVE COHESION INTERCEPT |
| ϕ' | -° | EFFECTIVE ANGLE OF INTERNAL FRICTION |
| c_u | kPa | APPARENT COHESION INTERCEPT |
| ϕ_u | -° | APPARENT ANGLE OF INTERNAL FRICTION |
| τ_R | kPa | RESIDUAL SHEAR STRENGTH |
| τ_r | kPa | REMOULDED SHEAR STRENGTH |
| S_t | 1 | SENSITIVITY = $\frac{c_u}{\tau_r}$ |

STRESS AND STRAIN

| | | |
|--------------------------------------|-----|-------------------------------|
| u_w | kPa | PORE WATER PRESSURE |
| r_u | 1 | PORE PRESSURE RATIO |
| σ | kPa | TOTAL NORMAL STRESS |
| σ' | kPa | EFFECTIVE NORMAL STRESS |
| τ | kPa | SHEAR STRESS |
| $\sigma_1, \sigma_2, \sigma_3$ | kPa | PRINCIPAL STRESSES |
| ϵ | % | LINEAR STRAIN |
| $\epsilon_1, \epsilon_2, \epsilon_3$ | % | PRINCIPAL STRAINS |
| E | kPa | MODULUS OF LINEAR DEFORMATION |
| G | kPa | MODULUS OF SHEAR DEFORMATION |
| μ | 1 | COEFFICIENT OF FRICTION |

PHYSICAL PROPERTIES OF SOIL

| | | | | | | | | |
|----------------|------------------------|--------------------------------|-----------|------|---|-----------|------------------------|---|
| ρ_s | kg/m^3 | DENSITY OF SOLID PARTICLES | e | 1, % | VOID RATIO | e_{min} | 1, % | VOID RATIO IN DENSEST STATE |
| γ_s | kN/m^3 | UNIT WEIGHT OF SOLID PARTICLES | n | 1, % | POROSITY | I_D | 1 | DENSITY INDEX = $\frac{e_{max} - e}{e_{max} - e_{min}}$ |
| ρ_w | kg/m^3 | DENSITY OF WATER | w | 1, % | WATER CONTENT | D | mm | GRAIN DIAMETER |
| γ_w | kN/m^3 | UNIT WEIGHT OF WATER | S_r | % | DEGREE OF SATURATION | D_n | mm | n PERCENT - DIAMETER |
| ρ | kg/m^3 | DENSITY OF SOIL | w_L | % | LIQUID LIMIT | C_u | 1 | UNIFORMITY COEFFICIENT |
| γ | kN/m^3 | UNIT WEIGHT OF SOIL | w_p | % | PLASTIC LIMIT | h | m | HYDRAULIC HEAD OR POTENTIAL |
| ρ_d | kg/m^3 | DENSITY OF DRY SOIL | w_s | % | SHRINKAGE LIMIT | q | m^3/s | RATE OF DISCHARGE |
| γ_d | kN/m^3 | UNIT WEIGHT OF DRY SOIL | I_p | % | PLASTICITY INDEX = $w_L - w_p$ | v | m/s | DISCHARGE VELOCITY |
| ρ_{sat} | kg/m^3 | DENSITY OF SATURATED SOIL | I_L | 1 | LIQUIDITY INDEX = $\frac{w - w_p}{I_p}$ | i | 1 | HYDRAULIC GRADIENT |
| γ_{sat} | kN/m^3 | UNIT WEIGHT OF SATURATED SOIL | I_C | 1 | CONSISTENCY INDEX = $\frac{w_L - w}{I_p}$ | k | m/s | HYDRAULIC CONDUCTIVITY |
| ρ' | kg/m^3 | DENSITY OF SUBMERGED SOIL | e_{max} | 1, % | VOID RATIO IN LOOSEST STATE | j | kN/m^3 | SEEPAGE FORCE |
| γ' | kN/m^3 | UNIT WEIGHT OF SUBMERGED SOIL | | | | | | |