



December 21, 2015

FOUNDATION INVESTIGATION REPORT

TIFFIN STREET OVERPASS REPLACEMENT STRUCTURE SITE NO. 30-176/1 & 2 BARRIE, ONTARIO G.W.P. 2159-11-00

Submitted to:

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GEOCRES No. 31D-630

Report Number: 1532543-1

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REPORT





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1.0 INTRODUCTION

Golder Associates Ltd. (Golder) has been retained by Morrison Hershfield Limited (MH) on behalf of the Ministry of Transportation, Ontario (MTO) to provide foundation engineering services to support the detail design for the proposed replacement of the Highway 400-Tiffin Street overpasses in the City of Barrie. This report addresses the foundation investigation carried out for the proposed construction of the following structures:

- New overpass structure that will permit the Highway 400 Northbound Lanes (NBL) to cross over the widened Tiffin Street corridor.
- Replacement of the existing overpass structure for the Highway 400 Southbound Lanes (SBL) to cross over the widened Tiffin Street corridor.

The purpose of this investigation is to establish the subsurface conditions at the location of the proposed replacement structures, approach embankments and wing walls, by means of a limited borehole investigation and geotechnical laboratory testing on selected samples.

Golder has completed the foundation engineering services in accordance with Proposal No. GEOTETOB22161AA, dated March 13, 2015, originally provided to MH by Coffey Geotechnics Inc. (Coffey).

2.0 SITE DESCRIPTION

The existing overpass structure carrying Highway 400 over Tiffin Street is located between the Dunlop Street and Essa Road interchanges, in Barrie, Ontario, at the location shown on the Key Plan on the Borehole Location and Soil Strata drawings contained in the Contract Documents.

This portion of Highway 400, including the existing Tiffin Street overpass, was built between 1950 and 1955. The existing structure consists of a 15.5 m long, single-span, concrete rigid frame structure supported on spread footings. The overpass carries six lanes of Highway 400 traffic. The existing overpass structure is approximately 30 m wide and currently lies at a 22.5 degree skew to the Highway 400 centreline.

At the site, Tiffin Street is two lanes wide where it passes beneath Highway 400; the highway is constructed on fill / raised embankments. The existing Highway 400 / Tiffin overpass structure surface level is at about Elevation 240.5 m; the new Highway 400 grade at the north and south abutments is proposed to be at about Elevation 243.5 m, requiring a grade raise of approximately 3 m.

3.0 INVESTIGATION PROCEDURES

3.1 Previous Investigation by Others

Coffey completed a preliminary foundation investigation for the Highway 400 / Tiffin Street overpass structures involving the advancement of a total of four boreholes (F1, F2, F3 and F4) in October 2014; the records for these boreholes are provided in Appendix A. The locations of these boreholes are shown on the Borehole Location and Soil Strata drawings contained in the Contract Documents.

Boreholes F1 and F2 were advanced as part of the SBL overpass structure investigation; Boreholes F3 and F4 were advanced as part of the new NBL overpass structure investigation.

The results of the MTO investigation are presented in Coffey's Preliminary Foundation Investigation and Design Report (GEOCREs No. 31D-587), dated February 2015.



3.2 Current Investigation

The field work for the subsurface investigation for the Highway 400 / Tiffin Street overpass structures was carried out between June 25 and July 13, 2015, during which time a total of six boreholes were advanced using a track-mounted drill rig, supplied and operated by specialist drilling subcontractors. The locations of the six boreholes advanced at the NBL and SBL structures are shown on the Borehole Location and Soil Strata drawings contained in the Contract Documents.

The boreholes were advanced to depths ranging from 10.1 m to 19.8 m below existing ground surface using hollow stem auger drilling methods. Soil samples were obtained in the boreholes at 0.75 m and 1.5 m intervals of depth using 50 mm outer diameter split-spoon samplers driven by an automatic hammer, in accordance with the Standard Penetration Test (SPT) procedure. Each of the boreholes was terminated at the depths provided in the Coffey proposal, in order to avoid penetrating into a trichloroethylene (TCE) plume that is present in the vicinity of the site.

The groundwater conditions were observed in the open boreholes during and immediately following the drilling operations, and monitoring wells were installed in three boreholes (Boreholes 15-2, 15-4 and HF4) to permit monitoring of the groundwater levels at these locations. The monitoring wells consist of 50 mm diameter PVC pipe, with a slotted screen sealed within a sand filter pack at a selected depth interval within the borehole. The monitoring well installation details and water level readings are indicated on the borehole records contained in Appendix A. All remaining boreholes were backfilled with bentonite upon completion, in accordance with Ontario Regulation 903 (as amended).

The field work was supervised on a full-time basis by a member of Golder's staff who observed the drilling, sampling and in situ testing operations, and logged the subsurface conditions encountered in the boreholes. The soil samples were identified in the field, placed in labelled containers and transported to Golder's laboratory in Mississauga for further examination and laboratory testing. Index and classification tests consisting of water contents, Atterberg limits and grain size distributions were carried out on selected soil samples.

The borehole locations and ground surface elevations were obtained from the digital terrain model provided by MH. The borehole locations, including MTM NAD83 and UTM NAD83 northing and easting coordinates and ground surface elevations referenced to geodetic datum, are summarized below and are shown on the Borehole Location and Soil Strata drawings contained in the Contract Documents.

Borehole No.	NAD83 MTM Zone 10 Coordinates		Ground Surface Elevation (m)	Borehole Depth (m)
	Northing (m)	Easting (m)		
15-1	4914534.5	288258.2	240.5	19.8
15-2	4914565.9	288247.2	239.8	19.8
15-3	4914544.2	288286.9	240.7	19.8
15-4	4914580.1	288286.1	233.6	14.0
15-5	4914575.3	288233.7	239.5	13.7
HF4	4914537.7	288309.6	236.5	10.1



4.0 SITE GEOLOGY AND SUBSURFACE CONDITIONS

4.1 Regional Geology

This section of Highway 400 lies within the Simcoe Lowlands, as delineated in *The Physiography of Southern Ontario* (Chapman and Putnam, Third Edition, 1984). The soil deposits are typically interlayered, non-cohesive sand and silt layers, with occasional cohesive clayey silt to silty clay layers.

4.2 Subsurface Conditions

The detailed soil and groundwater conditions encountered in the boreholes, and the results of in situ and geotechnical laboratory testing, are summarized on the borehole records in Appendix A. The results of the laboratory tested samples from Golder's current borehole investigation are shown on Figures B1 to B5 in Appendix B. The stratigraphic boundaries shown on the borehole records and on the interpreted stratigraphic profile and cross sections on the Borehole Location and Soil Strata drawings contained in the Contract Documents are inferred from non-continuous sampling and, therefore, represent the transitions between soil types rather than exact planes of geological change. The subsoil conditions will vary between and beyond the borehole location.

In summary, the subsoils encountered in the boreholes consist of fill overlying interlayered native strata comprised of silt, sand, and clayey silt. A more detailed description of the subsurface conditions encountered in the boreholes is provided in the following sections.

4.2.1 Fill

An approximately 100 mm to 400 mm thick layer of asphalt was encountered immediately below the ground surface in Boreholes 15-1 to 15-3, 15-5, F1, F2 and F4.

Each of the boreholes encountered fill materials of variable composition and thickness. As boreholes were advanced from the Highway 400 embankment grade, as well as at the Tiffin Street level, the elevations of the surface of the fill materials are variable. The elevations of the surface and base of the fill and the thickness of the fill materials as encountered in the boreholes are summarized below.

Borehole No.	Fill Surface Depth	Fill Surface Elevation	Fill Thickness	Base of Fill Elevation
15-1	0.3 m	240.2 m	6.9 m	233.3 m
15-2	0.1 m	239.7 m	8.6 m	231.1 m
15-3	0.3 m	240.4 m	9.9 m	230.5 m
15-4	0.0 m	233.6 m	2.2 m	231.4 m
15-5	0.4 m	239.1 m	9.8 m	229.2 m
HF-4	0.0 m	236.5 m	3.9 m	232.6 m
F1	0.2 m	240.6 m	7.0 m	233.4 m
F2	0.4 m	239.1 m	5.0 m	234.1 m
F3	0.0 m	234.1 m	1.4 m	232.7 m
F4	0.2 m	239.7 m	7.0 m	232.7 m



The fill materials vary in composition from gravelly sand containing some silt and trace clay, to silty sand containing trace to some gravel. Clayey silt to silty clay layers were observed in Boreholes 15-3 and 15-5 from the current investigation, as well as in Borehole F1. Organics were found between 5.6 m and 7.2 m depth in Boreholes 15-1 and 15-2, as well as in Borehole F3. The results of grain size distribution tests completed on two selected samples of the fill from the current investigation are shown on Figure B1.

The measured Standard Penetration Test (SPT) “N”-values within the non-cohesive fill materials range from 3 blows to 74 blows per 0.3 m of penetration, indicating that the fill materials are very loose to very dense, but typically compact. The measured SPT “N”-value within the clayey silt to silty clay fill layers in Boreholes 15-5 and F1 range from 8 blows to 14 blows per 0.3 m of penetration, suggestive of a stiff consistency.

4.2.2 Sand to Silt

A deposit of sand to silt was encountered below the fill in Boreholes 15-1 to 15-4, HF4, and F1 to F4, and below an upper clayey silt layer in Borehole 15-5. The deposit varies in composition from sand containing some silt, to silty sand, to sandy silt, to silt containing trace to some sand, with variable amounts of gravel and trace clay. The results of grain size distribution tests carried out on three selected samples of the sand to silty sand portions of the deposit from the current investigation are shown on Figure B2, and the results of grain size distribution tests carried out on seven selected samples of the silt to sandy silt portions of the deposit are shown on Figure B3 in Appendix B.

The elevations of the surface and base of the sand to silt deposit and the deposit thickness encountered at the borehole locations are summarized below.

Borehole No.	Sand to Silt Surface Depth	Sand to Silt Surface Elevation	Sand to Silt Thickness	Sand to Silt Base Elevation
15-1	7.2 m	233.3 m	11.5 m	221.8 m
15-2	8.7 m	231.1 m	7.7 m	223.4 m
15-3	10.2 m	230.5 m	8.8 m	221.7 m
15-4	2.2 m	231.4 m	9.5 m	221.9 m
15-5	11.7 m	227.7 m	>2.0 m	Below 225.7 m
HF4	3.9 m	232.6 m	>6.2 m	Below 226.4 m
F1	7.2 m	233.4 m	>8.6 m	Below 224.8 m
F2	5.4 m	234.1 m	>10.4 m	Below 223.7 m
F3	1.4 m	232.7 m	>8.3 m	Below 224.4 m
F4	7.2 m	232.7 m	>8.6 m	Below 224.1 m

The measured SPT “N”-values in the sand to silt deposit range from 7 blows to 42 blows per 0.3 m of penetration, indicating this deposit is loose to dense material, but typically compact to dense.

4.2.3 Clayey Silt

An upper layer of clayey silt was encountered underlying the fill in Borehole 15-5, and a lower layer of clayey silt to silty clay was encountered below the sand to silt deposit in Boreholes 15-1 to 15-4. Boreholes 15-1 to 15-4



were terminated in the lower clayey silt deposit. The elevation of the surface and base of the deposit and the thickness of the stratum as encountered in the boreholes are summarized below.

Borehole No.	Clayey Silt to Silty Clay Surface Depth	Clayey Silt to Silty Clay Surface Elevation	Clayey Silt to Silty Clay Thickness	Clayey Silt to Silty Clay Base Elevation
15-1	18.7 m (Lower)	221.8 m	>1.1 m	Below 220.7 m
15-2	16.3 m (Lower)	223.4 m	>3.5 m	Below 219.9 m
15-3	19.1 m (Lower)	221.7 m	>0.8 m	Below 220.9 m
15-4	11.7 m (Lower)	221.9 m	>2.4 m	Below 219.5 m
15-5	10.2 m (Upper)	229.2 m	1.5 m	227.7 m

The measured SPT “N”-values within the clayey silt to silty clay deposit range from 9 blows to 37 blows per 0.3 meters of penetration, suggesting a stiff to hard consistency.

The results of a grain size distribution test completed on one selected samples of the clayey silt to silty clay deposit is shown on Figure B4 in Appendix B. Atterberg limits testing was carried out on one selected sample of the deposit and measured a plastic limit of 15 per cent, a liquid limit of 19 per cent and a plasticity index of 4 per cent. This result, which is plotted on the plasticity chart on Figure B5 in Appendix B, confirms that the tested sample of the deposit consists of clayey silt of low plasticity.

4.3 Groundwater Conditions

The observed water levels in the open boreholes following completion of drilling, and the water levels measured the three piezometers installed at this site, are summarized in the following table. The table also provides the groundwater elevations in Borehole F3, which was installed by Coffey Geotechnics Inc. as part of the preliminary investigation at this site.

Bridge Structure	Foundation Element	Borehole No.	Ground Surface Elevation (m)	Groundwater Elevation (m)	Date of Measurement	Notes
SBL	South Abutment	15-1	240.5	226.8	June 29, 2015	Open Borehole
	North Abutment	15-2	239.8	230.7	June 25, 2015	Open Borehole Monitoring Well
				230.1	November 8, 2015	
	North Approach	15-5	239.5	236.0	June 29, 2015	Open Borehole
NBL	South Abutment	15-3	240.7	232.9	June 28, 2015	Open Borehole
		F3	234.1	229.7	November 6, 2015	Monitoring Well
	North Abutment	15-4	233.6	227.0 229.6 229.5	July 13, 2015 August 11, 2015 November 6, 2015	Open Borehole Monitoring Well Monitoring Well



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OVERPASS REPLACEMENT, GWP 2159-11-00**

Bridge Structure	Foundation Element	Borehole No.	Ground Surface Elevation (m)	Groundwater Elevation (m)	Date of Measurement	Notes
	South Approach	HF4	236.5	228.0 231.7 231.6	July 7, 2015 August 11, 2015 November 6, 2015	Open Borehole Monitoring Well Monitoring Well

The groundwater level at the site is expected to fluctuate seasonally in response to changes in precipitation and snow melt, and is expected to be higher during the spring and other wet periods of the year.

5.0 CLOSURE

This Foundation Investigation Report was prepared by Mr. Nick La Posta, P. Eng., and reviewed by Ms. Lisa Coyne, P.Eng., a Designated MTO Foundations Contact for Golder.

GOLDER ASSOCIATES LTD.



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FOUNDATION REPORT - HIGHWAY 400-TIFFIN STREET OVERPASS REPLACEMENT, GWP 2159-11-00

REFERENCES

Chapman, L.J., and Putnam, D.F., 1984. *The Physiography of Southern Ontario*, 3rd Edition. Ontario Geological Survey, Special Volume 2. Ontario Ministry of Natural Resources.



APPENDIX A

Borehole Records



LIST OF SYMBOLS

Unless otherwise stated, the symbols employed in the report are as follows:

I.	GENERAL	(a)	Index Properties (continued)
π	3.1416	w	water content
$\ln x$,	natural logarithm of x	w_l or LL	liquid limit
\log_{10}	x or log x, logarithm of x to base 10	w_p or PL	plastic limit
g	acceleration due to gravity	I_p or PI	plasticity index = $(w_l - w_p)$
t	time	w_s	shrinkage limit
FoS	factor of safety	I_L	liquidity index = $(w - w_p) / I_p$
		I_C	consistency index = $(w_l - w) / I_p$
		e_{max}	void ratio in loosest state
		e_{min}	void ratio in densest state
		I_D	density index = $(e_{max} - e) / (e_{max} - e_{min})$ (formerly relative density)
II.	STRESS AND STRAIN	(b)	Hydraulic Properties
γ	shear strain	h	hydraulic head or potential
Δ	change in, e.g. in stress: $\Delta \sigma$	q	rate of flow
ε	linear strain	v	velocity of flow
ε_v	volumetric strain	i	hydraulic gradient
η	coefficient of viscosity	k	hydraulic conductivity (coefficient of permeability)
ν	Poisson's ratio	j	seepage force per unit volume
σ	total stress	(c)	Consolidation (one-dimensional)
σ'	effective stress ($\sigma' = \sigma - u$)	C_c	compression index (normally consolidated range)
σ'_{vo}	initial effective overburden stress	C_r	recompression index (over-consolidated range)
$\sigma_1, \sigma_2, \sigma_3$	principal stress (major, intermediate, minor)	C_s	swelling index
σ_{oct}	mean stress or octahedral stress = $(\sigma_1 + \sigma_2 + \sigma_3)/3$	C_α	secondary compression index
τ	shear stress	m_v	coefficient of volume change
u	porewater pressure	C_v	coefficient of consolidation (vertical direction)
E	modulus of deformation	C_h	coefficient of consolidation (horizontal direction)
G	shear modulus of deformation	T_v	time factor (vertical direction)
K	bulk modulus of compressibility	U	degree of consolidation
		σ'_p	pre-consolidation stress
III.	SOIL PROPERTIES	OCR	over-consolidation ratio = σ'_p / σ'_{vo}
(a)	Index Properties	(d)	Shear Strength
$\rho(\gamma)$	bulk density (bulk unit weight)*	τ_p, τ_r	peak and residual shear strength
$\rho_d(\gamma_d)$	dry density (dry unit weight)	ϕ'	effective angle of internal friction
$\rho_w(\gamma_w)$	density (unit weight) of water	δ	angle of interface friction
$\rho_s(\gamma_s)$	density (unit weight) of solid particles	μ	coefficient of friction = $\tan \delta$
γ'	unit weight of submerged soil ($\gamma' = \gamma - \gamma_w$)	c'	effective cohesion
D_R	relative density (specific gravity) of solid particles ($D_R = \rho_s / \rho_w$) (formerly G_s)	C_u, S_u	undrained shear strength ($\phi = 0$ analysis)
e	void ratio	p	mean total stress $(\sigma_1 + \sigma_3)/2$
n	porosity	p'	mean effective stress $(\sigma'_1 + \sigma'_3)/2$
S	degree of saturation	q	$(\sigma_1 - \sigma_3)/2$ or $(\sigma'_1 - \sigma'_3)/2$
		q_u	compressive strength $(\sigma_1 - \sigma_3)$
		S_t	sensitivity

* Density symbol is ρ . Unit weight symbol is γ where $\gamma = \rho g$ (i.e. mass density multiplied by acceleration due to gravity)

Notes: 1
2

$\tau = c' + \sigma' \tan \phi'$
shear strength = (compressive strength)/2



LIST OF ABBREVIATIONS

The abbreviations commonly employed on Records of Boreholes, on figures and in the text of the report are as follows:

I. SAMPLE TYPE

AS	Auger sample
BS	Block sample
CS	Chunk sample
DS	Denison type sample
FS	Foil sample
RC	Rock core
SC	Soil core
SS	Split-spoon
ST	Slotted tube
TO	Thin-walled, open
TP	Thin-walled, piston
WS	Wash sample

II. PENETRATION RESISTANCE

Standard Penetration Resistance (SPT), N:

The number of blows by a 63.5 kg. (140 lb.) hammer dropped 760 mm (30 in.) required to drive a 50 mm (2 in.) drive open sampler for a distance of 300 mm (12 in.)

Dynamic Cone Penetration Resistance; N_d :

The number of blows by a 63.5 kg (140 lb.) hammer dropped 760 mm (30 in.) to drive uncased a 50 mm (2 in.) diameter, 60° cone attached to "A" size drill rods for a distance of 300 mm (12 in.).

PH: Sampler advanced by hydraulic pressure

PM: Sampler advanced by manual pressure

WH: Sampler advanced by static weight of hammer

WR: Sampler advanced by weight of sampler and rod

Piezo-Cone Penetration Test (CPT)

A electronic cone penetrometer with a 60° conical tip and a project end area of 10 cm² pushed through ground at a penetration rate of 2 cm/s. Measurements of tip resistance (Q_t), porewater pressure (PWP) and friction along a sleeve are recorded electronically at 25 mm penetration intervals.

III. SOIL DESCRIPTION

(a) Non-Cohesive (Cohesionless) Soils

Density Index	N
Relative Density	Blows/300 mm or Blows/ft
Very loose	0 to 4
Loose	4 to 10
Compact	10 to 30
Dense	30 to 50
Very dense	over 50

(b) Cohesive Soils Consistency

	kPa	C_u, S_u	psf
Very soft	0 to 12		0 to 250
Soft	12 to 25		250 to 500
Firm	25 to 50		500 to 1,000
Stiff	50 to 100		1,000 to 2,000
Very stiff	100 to 200		2,000 to 4,000
Hard	over 200		over 4,000

IV. SOIL TESTS

w	water content
w _p	plastic limit
w _l	liquid limit
C	consolidation (oedometer) test
CHEM	chemical analysis (refer to text)
CID	consolidated isotropically drained triaxial test ¹
CIU	consolidated isotropically undrained triaxial test with porewater pressure measurement ¹
D _R	relative density (specific gravity, G _s)
DS	direct shear test
M	sieve analysis for particle size
MH	combined sieve and hydrometer (H) analysis
MPC	Modified Proctor compaction test
SPC	Standard Proctor compaction test
OC	organic content test
SO ₄	concentration of water-soluble sulphates
UC	unconfined compression test
UU	unconsolidated undrained triaxial test
V	field vane (LV-laboratory vane test)
γ	unit weight

Note: 1 Tests which are anisotropically consolidated prior to shear are shown as CAD, CAU.

V. MINOR SOIL CONSTITUENTS

Per cent by Weight	Modifier	Example
0 to 5	Trace	Trace sand
5 to 12	Trace to Some (or Little)	Trace to some sand
12 to 20	Some	Some sand
20 to 30	(ey) or (y)	Sandy
over 30	And (non-cohesive (cohesionless)) or With (cohesive)	Sand and Gravel Silty Clay with sand / Clayey Silt with sand



RECORD OF BOREHOLE No 15-2 2 OF 2 **METRIC**

PROJECT 1532543 G.W.P. 2159-11-00 LOCATION N 4914565.9; E 288247.2 ORIGINATED BY AK

DIST Central HWY 400 BOREHOLE TYPE 200 mm Diameter Hollow Stem Augers COMPILED BY NLP

DATUM GEODETIC DATE June 25, 2015 CHECKED BY LCC

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)								
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20	40	60	80						100	20	40	60	80	100	10	20
223.4	SILTY SAND, trace clay Compact Grey Moist to wet	[Strat Plot: Dotted pattern]	14	SS	19																			
16.3	CLAYEY SILT, trace sand Stiff to very stiff Grey	[Strat Plot: Diagonal lines]	15	SS	16																			
			16	SS	13																			
219.9			17	SS	9																			
19.8	END OF BOREHOLE NOTE: 1. Groundwater measured at a depth of 9.1 m (Elev. 230.7 m) during drilling operations.																							

SUD-MTO 001 1532543.GPJ GAL-MISS.GDT 07/10/15 DATA INPUT:

+³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

PROJECT <u>1532543</u>	RECORD OF BOREHOLE No 15-3	2 OF 2 METRIC
G.W.P. <u>2159-11-00</u>	LOCATION <u>N 4914544.2; E 288286.9</u>	ORIGINATED BY <u>D.M</u>
DIST <u>Central</u> HWY <u>400</u>	BOREHOLE TYPE <u>200 mm Diameter Hollow Stem Augers</u>	COMPILED BY <u>NLP</u>
DATUM <u>GEODETIC</u>	DATE <u>June 28, 2015</u>	CHECKED BY <u>LCC</u>

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20	40	60	80					
	--- CONTINUED FROM PREVIOUS PAGE ---															
221.7	SILTY SAND, trace clay Compact Brown becoming grey below a depth of 13.7 m Wet		12	SS	15											
			13	SS	18											
			14	SS	16											
19.1	CLAYEY SILT, trace fine sand Stiff Grey		15	SS	10											0 1 86 13
220.9																
19.8	END OF BOREHOLE NOTES: 1. Groundwater encountered at 10.7 m (Elev. 230.0 m) during drilling. 2. Groundwater measured in augers at 7.8 m (Elev. 232.9 m) upon completion. 3. Borehole sloughed to 11.6 m (Elev. 229.1 m) upon removal of augers.															

SUD-MTO 001 1532543.GPJ GAL-MISS.GDT 07/10/15 DATA INPUT:

PROJECT <u>1532543</u>	RECORD OF BOREHOLE No 15-4		1 OF 2 METRIC
G.W.P. <u>2159-11-00</u>	LOCATION <u>N 4914580.1; E 288286.1</u>	ORIGINATED BY <u>AK</u>	
DIST <u>Central</u> HWY <u>400</u>	BOREHOLE TYPE <u>200 mm Diameter Hollow Stem Augers</u>	COMPILED BY <u>NLP</u>	
DATUM <u>GEODETIC</u>	DATE <u>July 13, 2015</u>	CHECKED BY <u>LCC</u>	

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)		
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	SHEAR STRENGTH kPa						WATER CONTENT (%)	
233.6	GROUND SURFACE														
0.0	Sand to silty sand, trace gravel (FILL) Loose to very dense Brown Moist	[Hatched]	1	SS	8										
			2	SS	74										
			3	SS	11										
231.4	2.2														
	SILT, trace to some sand, trace clay Compact Light brown Moist to wet	[Vertical Lines]	4	SS	23				○						
			5	SS	29										
			6	SS	15				H ○			0	10	89	10
			7	SS	26										
227.9	5.6														
	SILTY SAND Compact Grey Moist to wet	[Vertical Lines]	8A	SS	25				○						
227.0	6.6														
	SILT, trace to some sand to sandy, trace clay Compact to dense Grey Wet	[Vertical Lines]	8B						○						
			9	SS	16										
			10	SS	29				○			0	8	91	1
			11A	SS	43										
			11B												
221.9	11.7														
	SILTY CLAY, trace sand Very stiff to hard Grey	[Hatched]	12	SS	17				○						
			13	SS	37										
219.5	14.0														

SUD-MTO 001 1532543.GPJ GAL-MISS.GDT 07/10/15 DATA INPUT:

Continued Next Page

 +³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE



RECORD OF BOREHOLE No 15-4 2 OF 2 **METRIC**

PROJECT 1532543

G.W.P. 2159-11-00 LOCATION N 4914580.1; E 288286.1 ORIGINATED BY AK

DIST Central HWY 400 BOREHOLE TYPE 200 mm Diameter Hollow Stem Augers COMPILED BY NLP

DATUM GEODETIC DATE July 13, 2015 CHECKED BY LCC

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC NATURAL LIQUID LIMIT MOISTURE LIMIT CONTENT			UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT NUMBER	TYPE	"N" VALUES			20	40	60	80	100	W _p	W	W _L		
	END OF BOREHOLE															
	NOTE: 1. Groundwater measured at a depth of 6.6 m (Elev. 227.0 m) during drilling.															

SUD-MTO 001 1532543.GPJ GAL-MISS.GDT 07/10/15 DATA INPUT:

+³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

GEOTETOB22161AA; Hwy 400/ Tiffin Street

RECORD OF BOREHOLE No BH F1

1 OF 2

METRIC

GWP 2074-11-00 LOCATION 29+721, 2.6 m LI C/L (N 4914538.6, E286270.5) ORIGINATED BY LG
 DIST HWY 400 BOREHOLE TYPE Hollow Stem Auger COMPILED BY MP
 DATUM Geodetic DATE 15/10/2014 CHECKED BY SH

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT W _L	UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV. DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			T _N VALUES	20	40	60	80					
240.8	GROUND SURFACE															
240.6	220 mm ASPHALT															
239.8	PAVEMENT GRANULAR FILL: 0.2 m Sand and Gravel 0.4 m Sand, some gravel		1	SS	24											
239.6	FILL: Silty Sand trace to some gravel trace silty clay lenses grey to brown, compact to loose moist very loose silty clay lenses silty clay lenses		2	SS	22											
239.4			3	SS	8											
239.2			4	SS	3											
239.0			5	SS	5											
238.8			6	SS	8											
238.6			7	SS	13											
238.4			8	SS	20											
238.2			9	SS	10											
238.0			10	SS	14											
233.4		SILTY SAND brown, compact, moist		11	SS	29										
230.4	SILT trace sand, trace clay brown, compact, moist		12	SS	19											
230.2			13	SS	18											
228.9	SANDY SILT grey, compact, wet		14	SS	15											
228.7			15	SS	15											
225.6																wet spoon

Continued Next Page

+³, X³: Numbers refer to Sensitivity 20 15-5 10 (%) STRAIN AT FAILURE

GEOTETOB22181AA: Hwy 400/ Tiffin Street

RECORD OF BOREHOLE No BH F1

2 OF 2

METRIC

GWP 2074-11-00 LOCATION 29+721, 2.6 m Lt C/L (N 4914538.5, E288270.5) ORIGINATED BY LG
 DIST _____ HWY 400 BOREHOLE TYPE Hollow Stem Auger COMPILED BY MP
 DATUM Geodetic DATE 15/10/2014 CHECKED BY SH

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT			PLASTIC LIMIT W _P	NATURAL MOISTURE CONTENT w	LIQUID LIMIT W _L	UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	SHEAR STRENGTH (kPa)						
						20	40	60	80	100				
225.8 15.0	SANDY SILT grey, compact, wet		15	SS	10	225								
224.8 15.9														
	End of Borehole wet cave- in @10.7 m													

+³, X³: Numbers refer to Sensitivity $\frac{20}{15} \times \frac{5}{10}$ (%) STRAIN AT FAILURE

GEOTETOB22161AA: Hwy 400/ Tiffin Street

RECORD OF BOREHOLE No BH F2

1 OF 2

METRIC

GWP 2074-11-00 LOCATION 10+030, 10.8 m LI C/L (N 4914566.2, E 288234.3) ORIGINATED BY JD
 DIST HWY 400 BOREHOLE TYPE Hollow Stem Auger COMPILED BY MP
 DATUM Geodetic DATE 23/10/2014 CHECKED BY SH

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL	
ELEV. DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			T _N VALUES	SHEAR STRENGTH (kPa)						WATER CONTENT (%)
						20	40	60	80	100	W P	W	W L	
239.6	GROUND SURFACE													
0.0	400 mm ASPHALT													
239.1														
0.4	PAVEMENT GRANULAR FILL: 0.3 m Sand and Gravel 0.2 m Sand, some gravel		1	SS	48						○			
238.6			2	SS	24						○			
0.9	FILL: Silty Sand brown to grey, dense to compact, moist trace clay		3	SS	27						○			
			4	SS	24						○			
			5	SS	29						○			
			6	SS	11						○			
			7	SS	24						○			
234.1			8	SS	27						○			
5.4	SILTY SAND trace gravel, trace clay brown to grey, compact, moist to wet		9	SS	24						○			
			10	SS	11						○			
			11	SS	39						○			
229.3			12	SS	13						○			
10.2	SILT some sand, trace clay, dilatant grey, compact, wet		13	SS	16						○			
			14	SS	23						○			
224.5														

Continued Next Page

+³, ×³: Numbers refer to Sensitivity
 20
 15-φ-5
 10 (%) STRAIN AT FAILURE

GEOTETOB22181AA: Hwy 400/ Tiffin Street

RECORD OF BOREHOLE No BH F2

2 OF 2

METRIC

GWP 2074-11-00 LOCATION 10+030, 10.8 m Lt C/L (N 4914569.2, E 288234.3) ORIGINATED BY JD
 DIST _____ HWY 400 BOREHOLE TYPE Hollow Stem Auger COMPILED BY MP
 DATUM Geodetic DATE 23/10/2014 CHECKED BY SH

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT W _L	UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20	40	60	80					
224.5 15.0	SILT some sand, trace clay, dilatant grey, compact, wet		15	SS	20	224										
223.7 15.9																
	End of Borehole cave-in @ 9.1 m Water level @ 9.1 m (not stabilized)* upon completion.															

+³, ×³: Numbers refer to Sensitivity 20
15-10-5 (% STRAIN AT FAILURE
10

GEOTETO22161AA: Hwy 400/ Tiffin Street

RECORD OF BOREHOLE No BH F3

1 OF 1

METRIC

GWP 2074-11-00 LOCATION 29+712, 31.6 m Rt C/L (N 4914553.7, E288302.4) ORIGINATED BY LG
 DIST HWY 400 BOREHOLE TYPE Hollow Stem Auger COMPILED BY MP
 DATUM Geodetic DATE 02/10/2014 CHECKED BY SH

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT				PLASTIC LIMIT W P	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)						
ELEV. DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			T _N VALUES	SHEAR STRENGTH (kPa)								WATER CONTENT (%)					
						20	40	60	80	100	20	40	60	80	100	10	20	30		GR SA SI CL	
234.1 0.0	GROUND SURFACE 0.1 m TOPSOIL FILL: Silty Sand to Sand and Silt trace to some gravel trace rootlets trace organics brown, loose, moist		1	SS	7																
232.7 1.4	SILTY SAND trace gravel, trace clay brown, loose to dense, moist to wet		2	SS	4																
			3	SS	23																
			4	SS	29																0 77 20 3
			5	SS	17																
			6	SS	34																wet spoon
			7	SS	8																
			8	SS	16																
			9	SS	17																
			10	SS	11																
			11	SS	7																
224.4 9.8	End of Borehole Water level upon completion @ 4.2 m Piezometer installed to 9.1 m. Piezometer water level records : Oct. 31, 2014 4.1 m (El. 230 m)																				

+³, x³: Numbers refer to Sensitivity
 (% STRAIN AT FAILURE

GEOTETOB22181AA: Hwy 400/ Tiffin Street

RECORD OF BOREHOLE No BH F4

1 OF 2

METRIC

GWP 2074-11-00 LOCATION 10+012, 11.9 m Rt C/L (N 4914570.4, E 288282.9) ORIGINATED BY LG
 DIST HWY 400 BOREHOLE TYPE Hollow Stem Auger COMPILED BY MP
 DATUM Geodetic DATE 02/10/2014 CHECKED BY SH

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	DYNAMIC CONE PENETRATION RESISTANCE PLOT				PLASTIC LIMIT W _P	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT Y kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE		"N" VALUES	SHEAR STRENGTH (kPa)							
						20	40	60	80	100				
239.9	GROUND SURFACE													
239.9	230 mm ASPHALT													
0.2	PAVEMENT GRANULAR FILL: 0.4 m Sand and Gravel 0.3 m Sand, some gravel		1	SS	40									
239.0	FILL: Silty Sand trace to some gravel brown to grey, very loose to dense, moist		2	SS	13									
0.9			3	SS	7									
			4	SS	8									4 84 9 3
			5	SS	10									
			6	SS	14									
			7	SS	3									
			8	SS	6									
			9	SS	11									
232.7	SILTY SAND trace gravel, trace clay brown to grey, compact, moist to wet		10	SS	19									
7.2			11	SS	32									wet spoon 0 9 85 6
			12	SS	26									
			13	SS	22									
			14	SS	16									
224.9														

Continued Next Page

+³, X³: Numbers refer to Sensitivity $\frac{20}{15-5}$ (%) STRAIN AT FAILURE

GEOTETOB22161AA: Hwy 400/ Tiffin Street

RECORD OF BOREHOLE No BH F4

2 OF 2

METRIC

GWP 2074-11-00 LOCATION 10+012, 11.9 m Rt C/L (N 4914570.4, E 288262.9) ORIGINATED BY LG
 DIST HWY 400 BOREHOLE TYPE Hollow Stem Auger COMPILED BY MP
 DATUM Geodetic DATE 02/10/2014 CHECKED BY SH

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT	NATURAL MOISTURE CONTENT	LIQUID LIMIT	UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			T _N VALUES	20	40	60	80					
224.8 15.0	SILTY SAND trace gravel brown to grey, compact, moist to wet		15	SS	20											
224.1 15.9			End of Borehole cave-in @ 11.6 m Water level upon completion @ 9.8 m													

+³, X³: Numbers refer to Sensitivity
 20
 15-5
 10 (%) STRAIN AT FAILURE



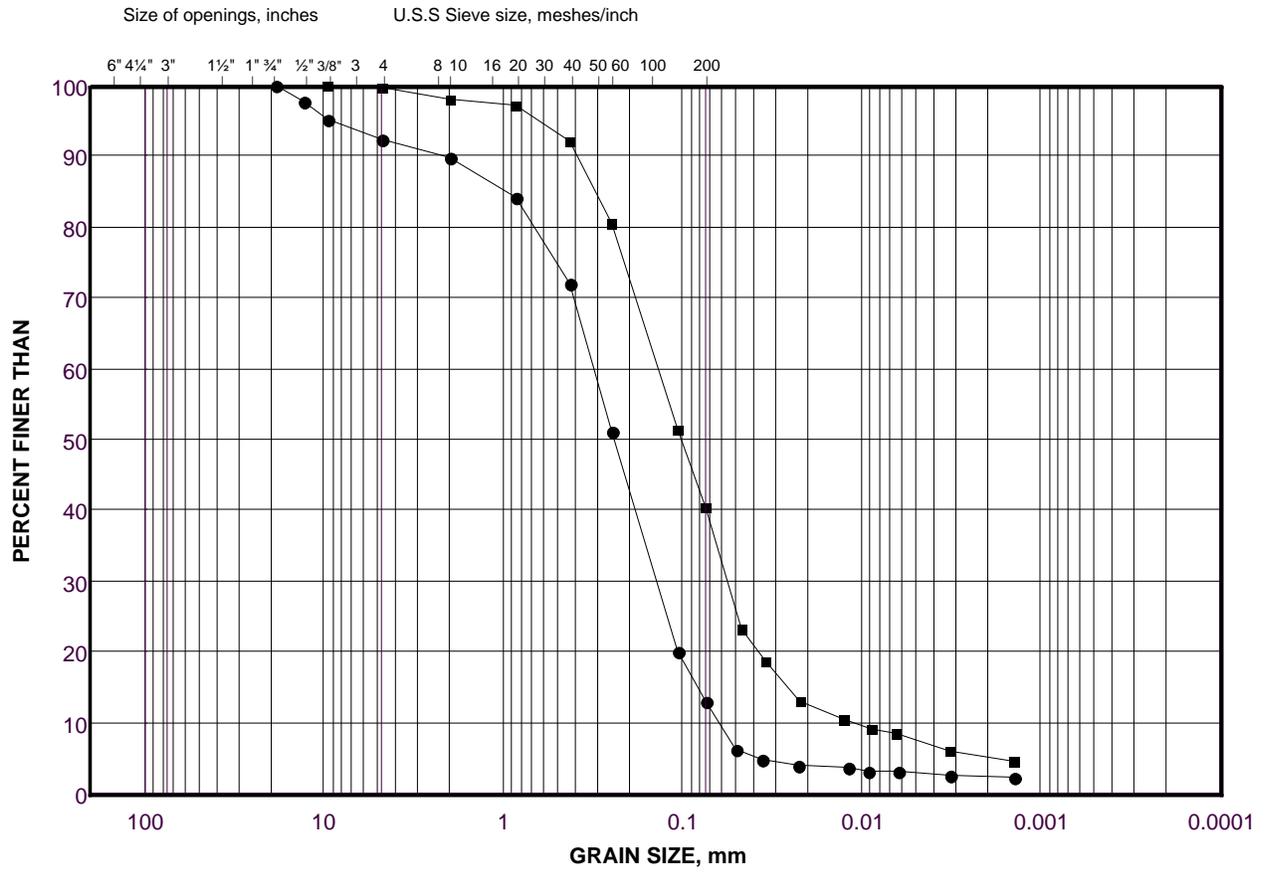
APPENDIX B

Geotechnical Laboratory Test Results

GRAIN SIZE DISTRIBUTION

Silty Sand to Sand Fill

FIGURE B1



COBBLE	COARSE	FINE	COARSE	MEDIUM	FINE	SILT AND CLAY SIZES
	GRAVEL SIZE		SAND SIZE			
SIZE						FINE GRAINED

LEGEND

SYMBOL	BOREHOLE	SAMPLE	ELEVATION(m)
●	15-1	2	238.0
■	15-1	4	236.5

Project Number: 1532543

Checked By: _____

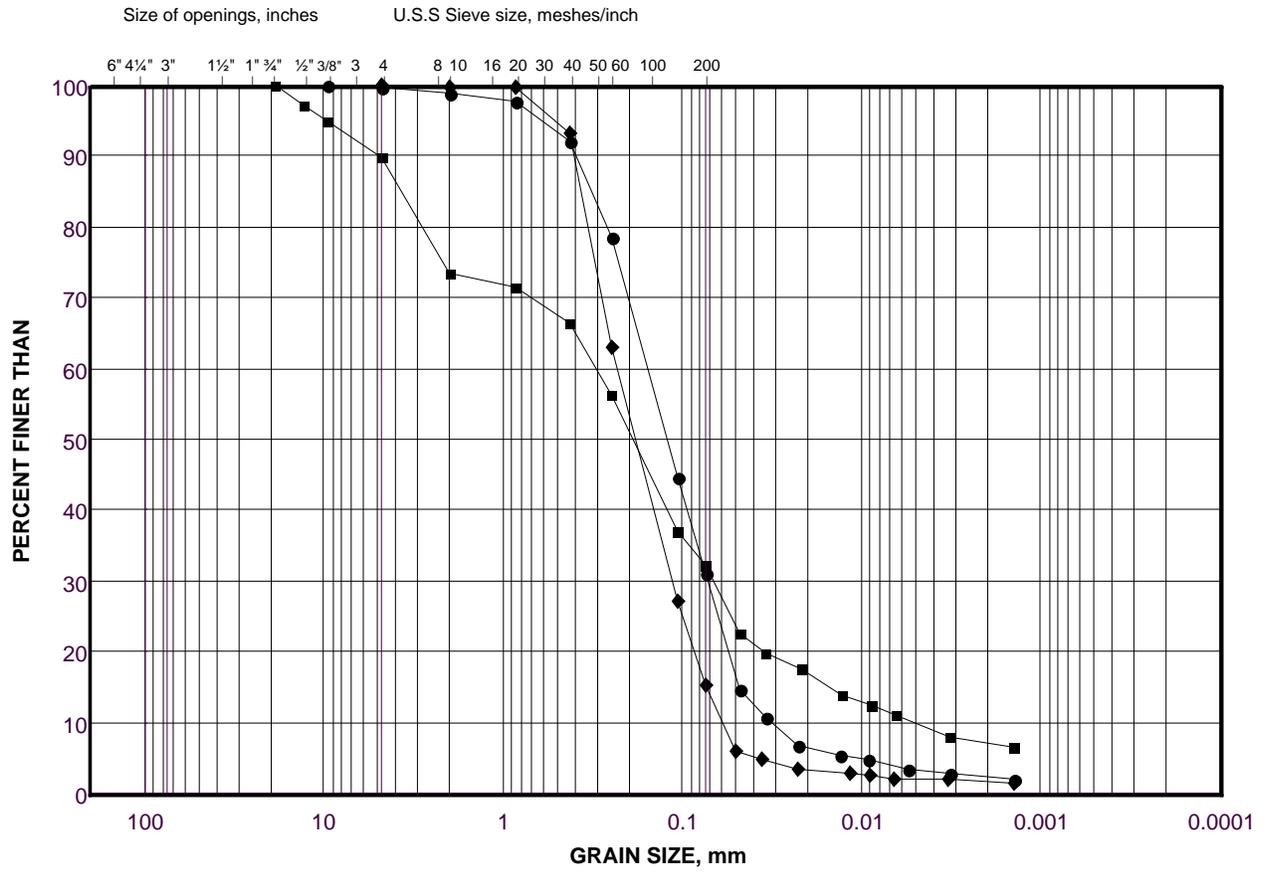
Golder Associates

Date: 04-Sep-15

GRAIN SIZE DISTRIBUTION

Silty Sand to Sand

FIGURE B2



COBBLE SIZE	COARSE	FINE	COARSE	MEDIUM	FINE	SILT AND CLAY SIZES
	GRAVEL SIZE		SAND SIZE			

LEGEND

SYMBOL	BOREHOLE	SAMPLE	ELEVATION(m)
●	15-3	4	236.6
■	15-2	6	235.6
◆	15-1	7	232.6

Project Number: 1532543

Checked By: _____

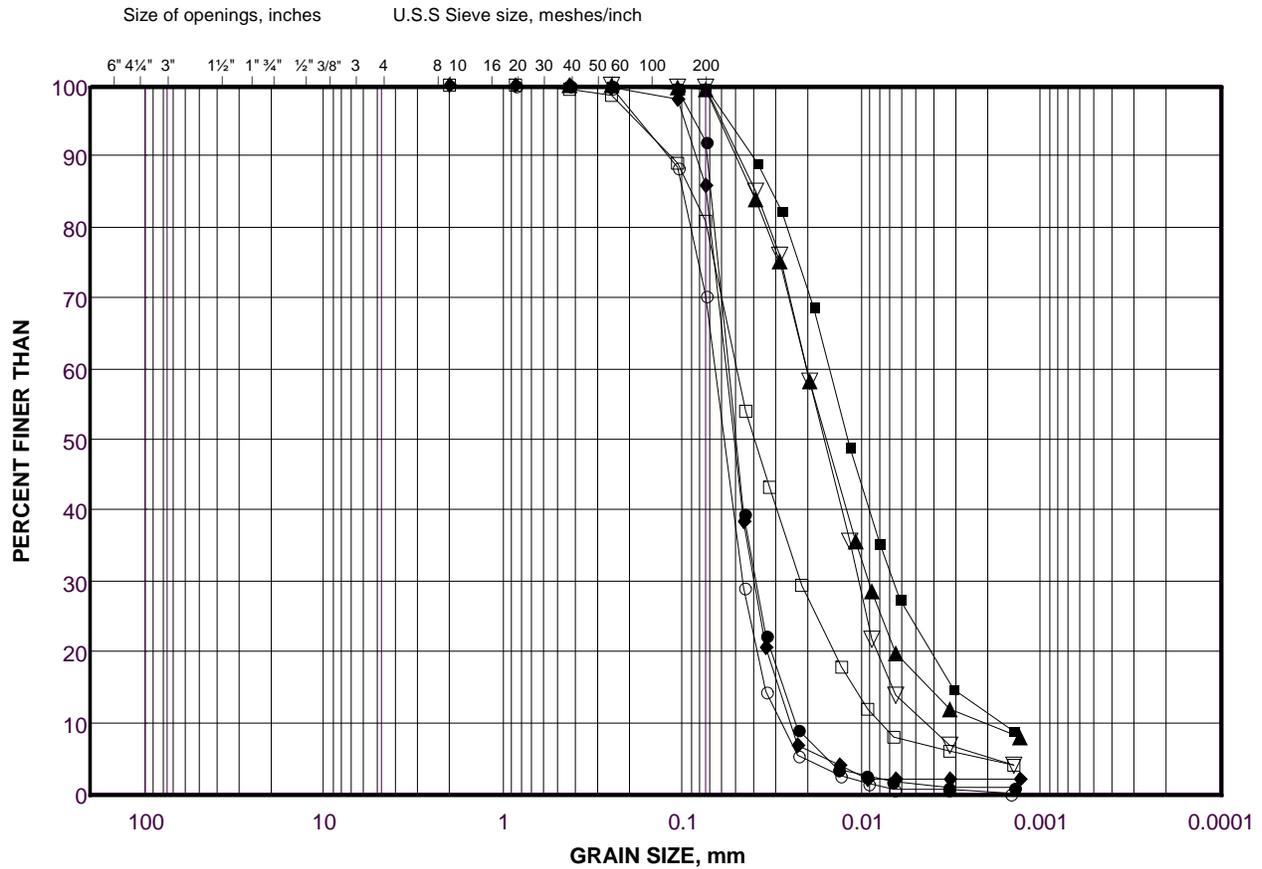
Golder Associates

Date: 04-Sep-15

GRAIN SIZE DISTRIBUTION

Silt to Sandy Silt

FIGURE B3



LEGEND

SYMBOL	BOREHOLE	SAMPLE	DEPTH(m)
●	15-4	10	224.2
■	15-2	11	228.8
◆	15-1	12	225.0
▲	15-4	6	229.5
▽	HF4	7	231.7
○	HF4	9	228.6
□	15-3	9	229.8

Project Number: 1532543

Checked By: _____

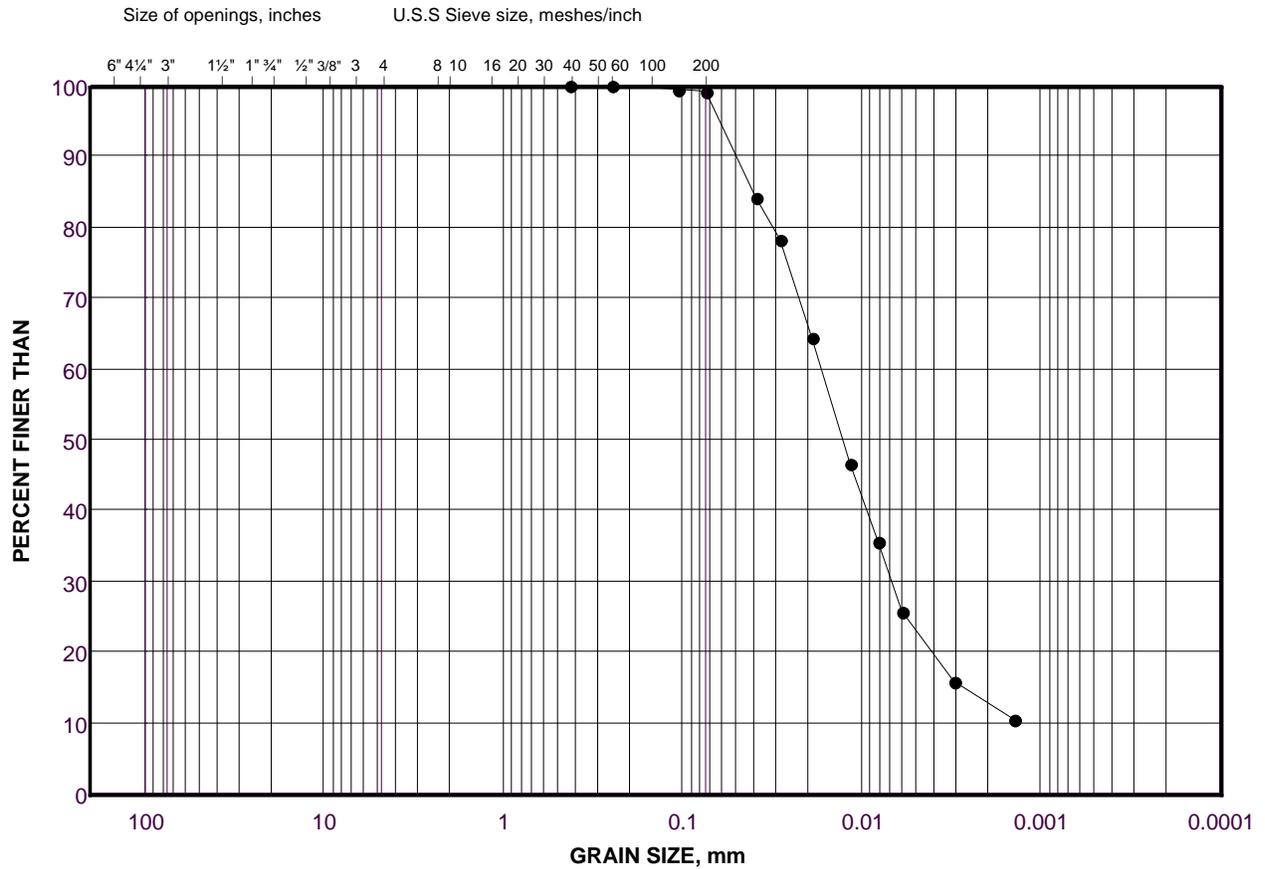
Golder Associates

Date: 07-Oct-15

GRAIN SIZE DISTRIBUTION

Clayey Silt

FIGURE B4



COBBLE	COARSE	FINE	COARSE	MEDIUM	FINE	SILT AND CLAY SIZES
SIZE	GRAVEL SIZE		SAND SIZE			FINE GRAINED

LEGEND

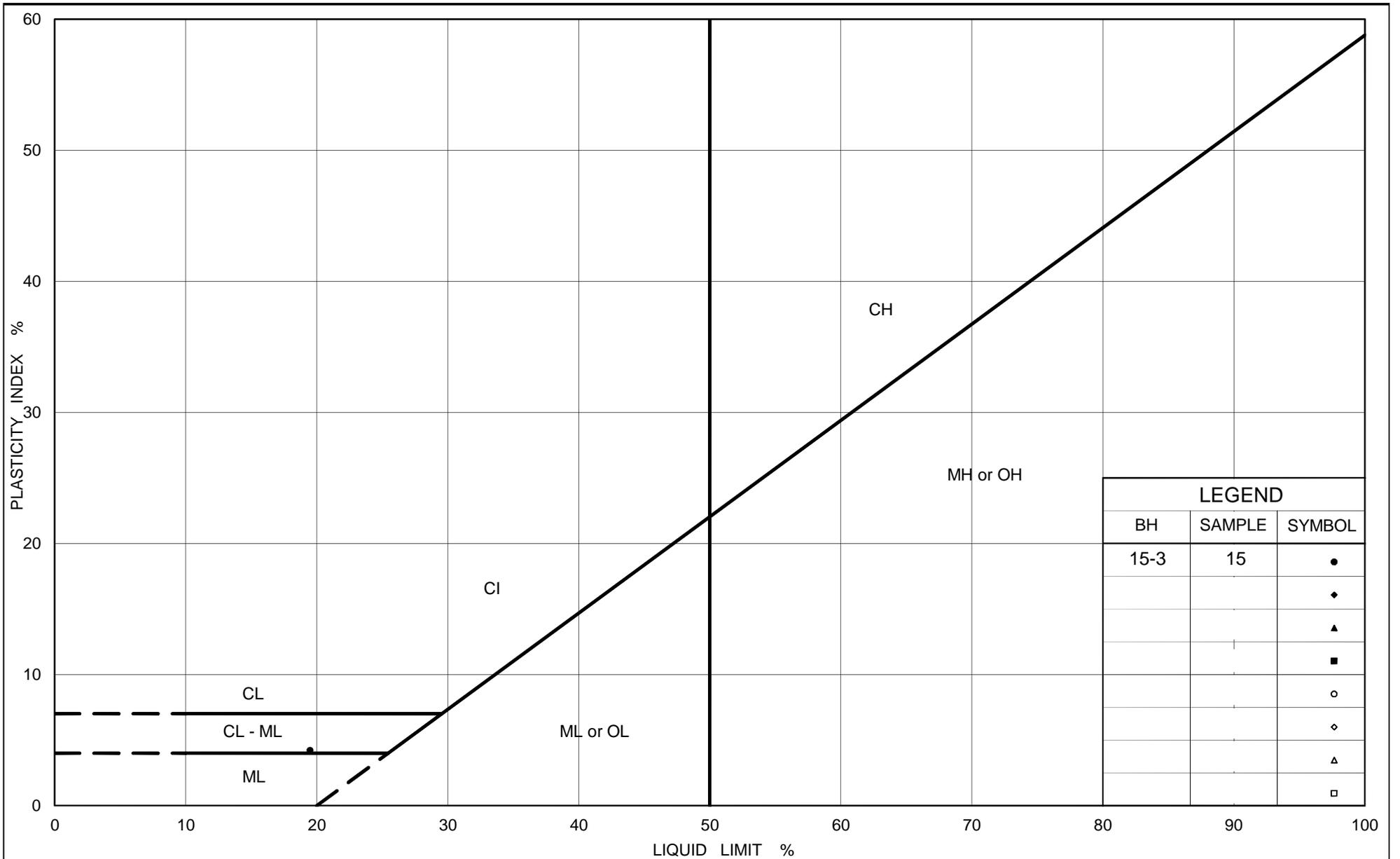
SYMBOL	BOREHOLE	SAMPLE	ELEVATION(m)
●	15-3	15	221.2

Project Number: 1532543

Checked By: _____

Golder Associates

Date: 07-Oct-15



PLASTICITY CHART
Clayey Silt

Figure No. B5

Project No. 1532543

Checked By:

At Golder Associates we strive to be the most respected global group of companies specializing in ground engineering and environmental services. Employee owned since our formation in 1960, we have created a unique culture with pride in ownership, resulting in long-term organizational stability. Golder professionals take the time to build an understanding of client needs and of the specific environments in which they operate. We continue to expand our technical capabilities and have experienced steady growth with employees now operating from offices located throughout Africa, Asia, Australasia, Europe, North America and South America.

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