

DOCUMENT MICROFILMING IDENTIFICATION

GEOCREs No. 52E-21

DIST. 20 REGION _____

W.P. No. 18-77-18

CONT. No. 88-450

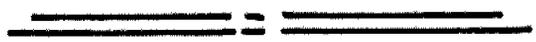
W. O. No. _____

STR. SITE No. 41S-133

HWY. No. 807

LOCATION Gibson Creek & Hwy 807
(Bending dare Rd)

No of PAGES - _____



OVERSIZE DRAWINGS TO BE INCLUDED WITH THIS REPORT. _____

REMARKS: _____

G.I.-30 SEPT. 1976

FOUNDATION INVESTIGATION REPORT

CONTRACT NO 88 - 450



Ontario

Ministry of
Transportation and
Communications

INDEX

<u>Page No.</u>	<u>DESCRIPTION</u>
1	Index
2	Abbreviations & Symbols
3 - 15	Foundation Investigation Report Gibson Creek Culvert W.P. 18-77-18, Site 41S-133 District 20, Kenora

Note: For purposes of the contract this report supercedes all other Foundation Reports prepared by or for the Ministry in connection with the above-mentioned project.

EXPLANATION OF TERMS USED IN REPORT

2

N VALUE: THE STANDARD PENETRATION TEST (SPT) N VALUE IS THE NUMBER OF BLOWS REQUIRED TO CAUSE A STANDARD 51mm O.D SPLIT BARREL SAMPLER TO PENETRATE 0.3m INTO UNDISTURBED GROUND IN A BOREHOLE WHEN DRIVEN BY A HAMMER WITH A MASS OF 63.5kg, FALLING FREELY A DISTANCE OF 0.76m FOR PENETRATIONS OF LESS THAN 0.3m N VALUES ARE INDICATED AS THE NUMBER OF BLOWS FOR THE PENETRATION ACHIEVED AVERAGE N VALUE IS DENOTED THUS \bar{N} .

DYNAMIC CONE PENETRATION TEST: CONTINUOUS PENETRATION OF A CONICAL STEEL POINT (51mm O.D. 60° CONE ANGLE) DRIVEN BY 475 J IMPACT ENERGY ON 'A' SIZE DRILL RODS. THE RESISTANCE TO CONE PENETRATION IS MEASURED AS THE NUMBER OF BLOWS FOR EACH 0.3m ADVANCE OF THE CONICAL POINT INTO THE UNDISTURBED GROUND

SOILS ARE DESCRIBED BY THEIR COMPOSITION AND CONSISTENCY OR DENSENESS

CONSISTENCY: COHESIVE SOILS ARE DESCRIBED ON THE BASIS OF THEIR UNDRAINED SHEAR STRENGTH (c_u) AS FOLLOWS:

c_u (kPa)	0 - 12	12 - 25	25 - 50	50 - 100	100 - 200	> 200
	VERY SOFT	SOFT	FIRM	STIFF	VERY STIFF	HARD

DENSENESS: COHESIONLESS SOILS ARE DESCRIBED ON THE BASIS OF DENSENESS AS INDICATED BY SPT N VALUES AS FOLLOWS:

N (BLOWS/0.3m)	0 - 5	5 - 10	10 - 30	30 - 50	> 50
	VERY LOOSE	LOOSE	COMPACT	DENSE	VERY DENSE

ROCKS ARE DESCRIBED BY THEIR COMPOSITION AND STRUCTURAL FEATURES AND/OR STRENGTH.

RECOVERY: SUM OF ALL RECOVERED ROCK CORE PIECES FROM A CORING RUN EXPRESSED AS A PERCENT OF THE TOTAL LENGTH OF THE CORING RUN

MODIFIED RECOVERY: SUM OF THOSE INTACT CORE PIECES, 100mm+ IN LENGTH EXPRESSED AS A PERCENT OF THE LENGTH OF THE CORING RUN. THE ROCK QUALITY DESIGNATION (RQD), FOR MODIFIED RECOVERY, IS:

RQD (%)	0 - 25	25 - 50	50 - 75	75 - 90	90 - 100
	VERY POOR	POOR	FAIR	GOOD	EXCELLENT

JOINTING AND BEDDING:

SPACING	50mm	50 - 300mm	0.3m - 1m	1m - 3m	> 3m
JOINTING	VERY CLOSE	CLOSE	MOD. CLOSE	WIDE	VERY WIDE
BEDDING	VERY THIN	THIN	MEDIUM	THICK	VERY THICK

ABBREVIATIONS AND SYMBOLS

FIELD SAMPLING

SS SPLIT SPOON	TP THINWALL PISTON
WS WASH SAMPLE	OS OSTERBERG SAMPLE
ST SLOTTED TUBE SAMPLE	RC ROCK CORE
BS BLOCK SAMPLE	PH TW ADVANCED HYDRAULICALLY
CS CHUNK SAMPLE	PM TW ADVANCED MANUALLY
TW THINWALL OPEN	FS FOIL SAMPLE

STRESS AND STRAIN

u_w	kPa	PORE WATER PRESSURE
r_u	1	PORE PRESSURE RATIO
σ	kPa	TOTAL NORMAL STRESS
σ'	kPa	EFFECTIVE NORMAL STRESS
τ	kPa	SHEAR STRESS
$\sigma_1, \sigma_2, \sigma_3$	kPa	PRINCIPAL STRESSES
ϵ	%	LINEAR STRAIN
$\epsilon_1, \epsilon_2, \epsilon_3$	%	PRINCIPAL STRAINS
E	kPa	MODULUS OF LINEAR DEFORMATION
G	kPa	MODULUS OF SHEAR DEFORMATION
μ	1	COEFFICIENT OF FRICTION

MECHANICAL PROPERTIES OF SOIL

m_v	kPa^{-1}	COEFFICIENT OF VOLUME CHANGE
C_c	1	COMPRESSION INDEX
C_s	1	SWELLING INDEX
C_α	1	RATE OF SECONDARY CONSOLIDATION
c_v	m^2/s	COEFFICIENT OF CONSOLIDATION
H	m	DRAINAGE PATH
T_v	1	TIME FACTOR
U	%	DEGREE OF CONSOLIDATION
σ'_{v0}	kPa	EFFECTIVE OVERBURDEN PRESSURE
σ'_p	kPa	PRECONSOLIDATION PRESSURE
τ_f	kPa	SHEAR STRENGTH
c'	kPa	EFFECTIVE COHESION INTERCEPT
ϕ'	-°	EFFECTIVE ANGLE OF INTERNAL FRICTION
c_u	kPa	APPARENT COHESION INTERCEPT
ϕ_u	-°	APPARENT ANGLE OF INTERNAL FRICTION
τ_R	kPa	RESIDUAL SHEAR STRENGTH
τ_r	kPa	REMOULDED SHEAR STRENGTH
S_t	1	SENSITIVITY = $\frac{c_u}{\tau_r}$

PHYSICAL PROPERTIES OF SOIL

ρ_s	kg/m^3	DENSITY OF SOLID PARTICLES	e	1, %	VOID RATIO	e_{min}	1, %	VOID RATIO IN DENSEST STATE
γ_s	kn/m^3	UNIT WEIGHT OF SOLID PARTICLES	n	1, %	POROSITY	I_D	1	DENSITY INDEX = $\frac{e_{max} - e}{e_{max} - e_{min}}$
ρ_w	kg/m^3	DENSITY OF WATER	w	1, %	WATER CONTENT	D	mm	GRAIN DIAMETER
γ_w	kn/m^3	UNIT WEIGHT OF WATER	S_r	%	DEGREE OF SATURATION	D_n	mm	n PERCENT - DIAMETER
ρ	kg/m^3	DENSITY OF SOIL	w_l	%	LIQUID LIMIT	C_u	1	UNIFORMITY COEFFICIENT
γ	kn/m^3	UNIT WEIGHT OF SOIL	w_p	%	PLASTIC LIMIT	h	m	HYDRAULIC HEAD OR POTENTIAL
ρ_d	kg/m^3	DENSITY OF DRY SOIL	w_s	%	SHRINKAGE LIMIT	q	m^3/s	RATE OF DISCHARGE
γ_d	kn/m^3	UNIT WEIGHT OF DRY SOIL	I_p	%	PLASTICITY INDEX = $w_l - w_p$	v	m/s	DISCHARGE VELOCITY
ρ_{sat}	kg/m^3	DENSITY OF SATURATED SOIL	I_L	1	LIQUIDITY INDEX = $\frac{w - w_p}{I_p}$	i	1	HYDRAULIC GRADIENT
γ_{sat}	kn/m^3	UNIT WEIGHT OF SATURATED SOIL	I_C	1	CONSISTENCY INDEX = $\frac{w_l - w}{I_p}$	k	m/s	HYDRAULIC CONDUCTIVITY
ρ'	kg/m^3	DENSITY OF SUBMERGED SOIL	e_{max}	1, %	VOID RATIO IN LOOSEST STATE	j	kn/m^3	SEEPAGE FORCE
γ'	kn/m^3	UNIT WEIGHT OF SUBMERGED SOIL						

FOUNDATION INVESTIGATION REPORT
For
W.P. 18-77-18, Site #41S-133
Gibson Creek Culvert
Highway #807, (Bending Lake Road)
District #20, Kenora

INTRODUCTION

This report contains the information obtained from a foundation investigation carried out at the above-noted site.

The fieldwork for this project was carried out during the period from 86 05 26 to 86 05 30 utilizing a diamond drill equipped with 60 mm I.D. B-Casing. The investigation consisted of 8 sampled boreholes which ranged in depth from 0.9 m to 3.6 m. BX-size (41 mm) rock core was recovered from all 8 boreholes to prove bedrock.

SITE DESCRIPTION

The site is located approximately 33.4km south of Highway #17 on proposed Bending Lake Road, Highway #807. Due to the isolated nature of the site, it was accessible only from Snake Bay Road (a Great Lakes Paper Company Road) which intersects Highway #17 approximately 9 km west of Borups Corners, Gibson Creek is located approximately 66 km south west of Highway #17 along Snake Bay Road.

The topography of the site is gently rolling with some hills in the vicinity. Gibson Creek is a fairly small shallow creek with rapidly flowing water; it runs in a north west direction and drains Gibson Lake located to the east of the site. The area is extensively forested; there is a logging camp located approximately 500 m north along Snake Bay Road. The Ministry right-of-way is visible to the north where trees have been cleared for the road.

The existing bridge, built by the paper company, is a small structure supported by timber cross-braces and logs embedded into each embankment. It is sufficient strong to support fully loaded logging trucks which cross it several times each day. The approaches to the bridge consist of up to 2 m of sand, gravel, and boulder fill material.

SUBSURFACE CONDITIONS

General

Bedrock was very close to the surface at all borehole locations as illustrated by the Record of Borehole Sheets (Appendix, BH #1 to BH #8). Overburden consisted mainly of boulders, cobbles and gravel with silty sand interstitial material. The locations and elevations of the boreholes are shown on Sheet No. 2 of the Contract Drawings.

Overburden

The overburden at this site is very dense, consisting of a thin layer (0.15 to 0.6 m) of boulders, cobbles, gravel and sand.

Bedrock

The bedrock was proved at each borehole location. The upper portion of the granite type bedrock was found to be moderately weathered. The rock core samples were examined by Mr. E.R. Magni, Geologist and his description is appended to this report.

Groundwater Conditions

No groundwater level observations were carried out in Borehole No. 1, 2, 5 and 6. For construction purposes the groundwater level may be assumed to be at the same level as the prevailing water surface in the creek.



P. Payer

P. Payer, P. Eng.

Sr. Foundations Engineer

K. G. Selby

K.G. Selby, P. Eng.

Chief Foundations Engineer

APPENDIX

DESCRIPTION OF ROCK CORE - W.P.

18-77-18

BOREHOLE NUMBER				CORE DESCRIPTION	
	DEPTH (m)	% CR*	% RQD*	DEPTH (m)	DESCRIPTION
1	0.30 - 1.30	77	18	0.30 - 0.63	GRANITE, pink mottled black, moderately weathered, very closely spaced
	1.30 - 2.06	97	80	0.63 - 1.12	GRANITE, grey mottled pink, slightly weathered, closely spaced joints
	2.06 - 3.58	98	78		GRANITE, grey mottled pink, unweathered, medium spaced joints
					1.12 - 3.58
2	0.15 - 0.76	83	21	0.15 - 1.37	GRANITE, white mottled black and pink, slightly weathered, closely to medium spaced joints, near vertical oxidized joint from 0.15 to 0.38
	0.76 - 1.37	96	0		
3	0.30 - 1.22	64	0	0.30 - 0.94	GRANITE, grey mottled pink, moderately weathered, very closely spaced joints
	1.22 - 1.98	93	50	0.94 - 1.98	GRANITE, grey mottled pink, unweathered, medium spaced joints
4	0.08 - 0.76	100	100	0.08 - 0.23	BOULDER
				0.23 - 0.76	GRANITE, white mottled black, unweathered, medium spaced joints
5	0.46 - 0.76	100	0	0.46 - 0.76	GRANITE, pink mottled black, medium weathered, very closely spaced joints
	0.76 - 1.52	93	37		
	1.52 - 1.98	94	67		
6	0.46 - 0.91	89	0	0.46 - 0.61	BOULDERS
	0.91 - 1.37	94	89	0.61 - 0.91	GRANITE, white mottled black, medium weathered, very closely spaced joints
	1.37 - 1.83	100	94		
	1.83 - 2.59	90	57	0.91 - 2.59	GRANITE, white mottled black, unweathered, medium spaced joints

* CR = CORE RECOVERY ; RQD = ROCK QUALITY DESIGNATION

DESCRIPTION OF ROCK CORE - W.P.

18-77-18

BOREHOLE NUMBER				CORE DESCRIPTION	
	DEPTH (m)	% CR *	% RQD *	DEPTH (m)	DESCRIPTION
7	0.15 - 0.91	77	0	0.15 - 0.46	GRANITE, white mottled black and brown, slightly weathered, vertical joint along length of core
				0.46 - 0.91	GRANITE, white mottled black and pink, unweathered, vertical joint along length of core, closely spaced joints
8	0.23 - 0.84	92	50	0.23 - 0.84	GRANITE, white mottled pink, unweathered, closely spaced joints

* CR = CORE RECOVERY ; RQD = ROCK QUALITY DESIGNATION

ENGINEERING MATERIALS OFFICE
FOUNDATION DESIGN SECTION

WP 18-77-18

DIST 20

HWY 807

STR SITE 41S-133

Gibson Creek Bridge
Highway #807
(Bending Lake Road)

DISTRIBUTION

O. Ramakko (3)
J. B. MacMaster
G. D. Jewell
C. E. Pritchard
K. Bassi
J. H. Peer
T. Yakutchuk
D. E. Moorhouse (Cover Only)
M. MacLean (Cover Only)
File Copy

FOUNDATION INVESTIGATION REPORT
For
W.P. 18-77-18, Site #41S-133
Gibson Creek Bridge, Highway #807 (Bending Lake Road)
District #20, Kenora

INTRODUCTION

This report contains the information obtained from a foundation investigation carried out at the above-noted site, together with recommendations for design and construction of a new structure and approaches.

The fieldwork for this project was carried out during the period from 86 05 26 to 86 05 30 utilizing a diamond drill equipped with 60 mm I.D. B-Casing. The investigation consisted of 8 sampled boreholes which ranged in depth from 0.9 m to 3.6 m. BX-size (41 mm) rock core was recovered from all 8 boreholes to prove bedrock.

SITE DESCRIPTION

The site is located approximately 33.4 km south of Highway #17 on proposed Bending Lake Road, Highway #807. Due to the isolated nature of the site, it was accessible only from Snake Bay Road (a Great Lakes Paper Company Road) which intersects Highway #17 approximately 9 km west of Borups Corners; Gibson Creek is located approximately 66 km south west of Highway #17 along Snake Bay Road.

The topography of the site is gently rolling with some hills in the vicinity. Gibson Creek is a fairly small shallow creek with rapidly flowing water; it runs in a north west direction and drains Gibson Lake located to the east of the site. The area is extensively forested; there is a logging camp located approximately 500 m north along Snake Bay Road. The Ministry right-of-way is visible to the north where trees have been cleared for the road.

The existing bridge, built by the paper company, is a small structure supported by timber cross-braces and logs embedded into each embankment. It is sufficiently strong to support fully loaded logging trucks which cross it several times each day. The approaches to the bridge consist of up to 2 m of sand, gravel, and boulder fill material.

SUBSURFACE CONDITIONS

General

Bedrock was very close to the surface at all borehole locations as illustrated by the Record of Borehole Sheets (Appendix, BH #1 to BH #8). Overburden consisted mainly of boulders, cobbles and gravel with silty sand interstitial material. The locations and elevations of the boreholes and the bedrock elevations are shown on Drawing No. 187718-A.

Overburden

The overburden at this site is very dense, consisting of a thin layer (0.15 m to 0.6 m) of boulders, cobbles, gravel and sand.

Bedrock

The bedrock is moderately weathered to unweathered, precambrian granite.

Groundwater

At the time of the field investigation, the groundwater elevation was at the creek surface (elev. 411.5 m on 86 05 27 at the south side of the bridge and elev. 410.9 m on 86 05 27 at the north side of the bridge).

DISCUSSION AND RECOMMENDATIONS

The region has proposed to replace the timber structure at this location with one of the following alternatives:

- a. 6.1 m span concrete culvert
- b. Twin 3.048 m C.S.P.'s
- c. 18 m single span bridge

The new grade will be at el. 413.8 m, which is 0.6 m above the existing bridge deck and 2.8 m above the creek bed.

18 m Single Span Bridge

For the 18 m single span bridge, the abutments should be constructed on sound bedrock.

A safe bearing pressure of up to 5 MPa may be assumed for design purposes.

The east abutment should be constructed at or below elev. 410.3 m and the west abutment at or below elev. 411.3 m because of the slightly higher bedrock surface. Please refer to Drawing No. 187718-A for bedrock elevations of the borehole locations. For estimation purposes, bedrock elevations have been interpolated between these points.

The following design values are recommended, for purposes of the O.H.B.D.C.:

FACTORED BEARING CAPACITY AT ULS-10,000 kPa
BEARING CAPACITY AT SLS TYPE II - Not Applicable

Lateral earth pressures should be computed in accordance with Section 6-6.1.2 of the O.H.B.D.C. the 'at rest' condition should be assumed to apply for granular backfill for which the following properties are applicable:

Gran 'A': $\gamma = 22.8 \text{ kN/m}^3$, $\phi = 35^\circ$, $K_o = 0.43$
 Gran 'B': $\gamma = 21.1 \text{ kN/m}^3$, $\phi = 30^\circ$, $K_o = 0.50$

A coefficient of friction of TAN 35° may be assumed to apply between the base of footings and sound granite bedrock.

Differential settlements will be negligible for foundations mounted on solid bedrock.

Frost protection is not required.

Dewatering should not pose any problems.

6.1 m Span Concrete Culvert

For the 6.1 m span concrete culvert, footings should be constructed on sound bedrock at or below el. 410.3 m.

Safe bearing pressures up to 5 MPa may be assumed for design purposes.

The following design values are recommended, for purposes of the O.H.B.D.C.:

FACTORED BEARING CAPACITY AT ULS - 10,000 kPa
 BEARING CAPACITY AT SLS TYPE II - Not Applicable

Lateral earth pressures should be computed in accordance with Section 6-6.1.2 of the O.H.B.D.C. The 'at rest' condition should be assumed to apply for granular backfill for which the following properties are applicable:

Gran 'A': $\gamma = 22.8 \text{ kN/m}^3$, $\phi = 35^\circ$, $K_o = 0.43$
 Gran 'B': $\gamma = 21.1 \text{ kN/m}^3$, $\phi = 30^\circ$, $K_o = 0.50$

A coefficient of friction of TAN 35° may be assumed to apply between the base of footings and sound granite bedrock.

Bedding and backfilling should be in accordance with the appropriate Ministry Standards.

Differential settlements will be negligible.

Frost protection is not required.

Dewatering should not pose any problems.

Twin 3.048 m C.S.P.'s

Twin 3.048 m C.S.P.'s may be used at this site if they are large enough to perform in spring flooding. Bedding and backfill should be in accordance with the appropriate Ministry Standards.

MISCELLANEOUS

The drilling portion of the fieldwork for this project was carried out under the supervision of Mr. W. Dumanski, Student Engineer.

The report was written by Mr. Dumanski, and reviewed by Mr. K.G. Selby, Chief Foundations Engineer.

The drilling equipment used was owned and operated by N. Morissette Drilling Co. Ltd..

W.M. Dumanski

W.M. Dumanski
Project Foundations Engineer

K.G. Selby

K.G. Selby, P.Eng.
Chief Foundations Engineer
(West)

APPENDIX



RECORD OF BOREHOLE No 1

METRIC

W P 18-77-18 LOCATION STA. 36 + 534.0 °/s 5.9 m Rt. ORIGINATED BY W.D.
 DIST 20 HWY 807 BOREHOLE TYPE Washboring, BXL Rock Coring COMPILED BY W.D.
 DATUM Geodetic DATE 86 05 27 CHECKED BY

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			20	40	60	80	100		
421.9	Ground Level													
411.6	Boulders with Sand, Trace Silt, cobbles, gravel	[Handwritten Stratigraphic Column]												
0.3	Weathered Sound		1	RC BXL	77%									RQD 18%
	Bedrock Granite		2	RC BXL	97%									RQD 80%
			3	RC BXL	98%									RQD 78%
408.3	End of Borehole													
3.6														

RT ON SOIL EXPLORATION



RECORD OF BOREHOLE No 2

METRIC

W P 18-77-18 LOCATION STA. 36 + 534.5 o/s 9.0 m Lt. ORIGINATED BY W.D.
 DIST 20 HWY 807 BOREHOLE TYPE Washboring, BQ Rock Coring COMPILED BY W.D.
 DATUM Geodetic DATE 86 05 29 CHECKED BY [Signature]

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			20	40	60	80	100					
411.8	Ground Level																
411.65	cobbles with Sand Some	80%															
0.15	Weathered Sound		1	RC BQ	80%											RQD 21%	
	Bedrock Granite		2	RC BQ	96%											RQD 0%	
410.4																	
1.4	End of Borehole																



RECORD OF BOREHOLE No 3

METRIC

W P 18-77-18 LOCATION STA. 36 + 542.3 °/s 6.8 m Rt. ORIGINATED BY W.D.
 DIST 20 HWY 807 BOREHOLE TYPE Washboring, BXL Rock Coring COMPILED BY W.D.
 DATUM Geodetic DATE 86 05 27 CHECKED BY [Signature]

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			20	40	60	80	100					
411.5	Creek Water Level																
411.3	Creek Bottom																
410.9	Boulders, cobbles, gravel						411										
0.5	Weathered																
	Bedrock Sound Granite		1	RC BXL	64%		410									RQD 0%	
			2	RC BXL	93%											RQD 50%	
409.3	End of Borehole						409										
2.2																	



RECORD OF BOREHOLE No 4

METRIC

W P 18-77-18 LOCATION STA. 36 + 543.5 o/s 7.0 m Lt. ORIGINATED BY W.D.
 DIST 20 HWY 807 BOREHOLE TYPE Washboring, BXL Rock Coring COMPILED BY W.D.
 DATUM Geodetic DATE 86 05 29 CHECKED BY [Signature]

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			SHEAR STRENGTH									
410.9	Creek Water Level																
410.7	Creek Bottom																
410.5	Boulders, cobbles, gravel																
0.4	Bedrock Sound		1	RC	100%		410									RQD 100%	
409.9	Granite			BXL													
1.0	End of Borehole						409										



RECORD OF BOREHOLE No 5

METRIC

W P 18-77-18 LOCATION STA. 36 + 550.0 o/s 8.2 m Rt. ORIGINATED BY W.D.
 DIST 20 HWY 807 BOREHOLE TYPE Washboring, BXL Rock Coring COMPILED BY W.D.
 DATUM Geodetic DATE 86 05 27 CHECKED BY [Signature]

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			20	40	60	80	100					
411.9	Ground Level																
0.0	Boulders, cobbles																
411.45	gravel with Sand																
0.45	Weathered Sound		1	RC BXL	100%												RQD 0%
	Bedrock Granite		2	RC BXL	93%												RQD 37%
409.9			3	RC BXL	94%												RQD 67%
2.0	End of Borehole																
							409										

RT ON SOIL EXPLORATION



RECORD OF BOREHOLE No 6

METRIC

W P 18-77-18 LOCATION STA. 36 + 553.1 °/s 5.4 m Lt. ORIGINATED BY W.D.
 DIST 20 HWY 807 BOREHOLE TYPE Washboring, BXL Rock Coring COMPILED BY W.D.
 DATUM Geodetic DATE 86 05 28 CHECKED BY [Signature]

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL		
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			20	40	60	80	100						SHEAR STRENGTH ○ UNCONFINED + FIELD VANE ● QUICK TRIAXIAL x LAB VANE	
410.9	Ground Level																		
0.0	Boulders, cobbles gravel with Sand Trace																		
410.3	Silt																		
0.6	Weathered Sound		1	RC BXL	89%	410											RQD 0%		
	Bedrock Granite		2	RC BXL	94%													RQD 89%	
			3	RC BXL	100%		409												RQD 94%
			4	RC BXL	90%														
408.3																			
2.6	End of Borehole						408												



RECORD OF BOREHOLE No 7

METRIC

W P 18-77-18 LOCATION STA. 36 + 547.0 °/s 7.3 m Lt. ORIGINATED BY W.D.
 DIST 20 HWY 807 BOREHOLE TYPE Washboring, BXL Rock Coring COMPILED BY W.D.
 DATUM Geodetic DATE 86 05 29 CHECKED BY [Signature]

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			SHEAR STRENGTH ○ UNCONFINED + FIELD VANE ● QUICK TRIAXIAL x LAB VANE									
410.9	Creek Water Level																
410.7	Creek Bottom																
0.2	cobbles, and gravel																
0.3	Bedrock Granite <u>Weathered</u>																
409.8	Sound		1	RC BXL	77%		410									RQD 0%	
1.1	End of Borehole						409										

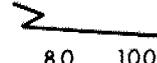
RT ON SOIL EXPLORATION



RECORD OF BOREHOLE No 8

METRIC

W P 18-77-18 LOCATION STA. 36 + 539.3 °/s 6.5 m Rt. ORIGINATED BY W.D.
 DIST 20 HWY 807 BOREHOLE TYPE Washboring, BQ Rock Coring COMPILED BY W.D.
 DATUM Geodetic DATE 86 05 30 CHECKED BY [Signature]

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT 					UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL			
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			20	40	60	80	100			PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L
411.4	Creek Water Level																
411.3	Creek Bottom	SOIL															
411.1	cobbles, and gravel																
0.3	Bedrock weathered Sound	SOIL	1	RC BQ	92%												RQD 50%
410.5	Granite																
0.9	End of Borehole																
							411										
							410										

EXPLANATION OF TERMS USED IN REPORT

N VALUE: THE STANDARD PENETRATION TEST (SPT) N VALUE IS THE NUMBER OF BLOWS REQUIRED TO CAUSE A STANDARD 51mm O.D. SPLIT BARREL SAMPLER TO PENETRATE 0.3m INTO UNDISTURBED GROUND IN A BOREHOLE WHEN DRIVEN BY A HAMMER WITH A MASS OF 63.5kg, FALLING FREELY A DISTANCE OF 0.76m. FOR PENETRATIONS OF LESS THAN 0.3m N VALUES ARE INDICATED AS THE NUMBER OF BLOWS FOR THE PENETRATION ACHIEVED. AVERAGE N VALUE IS DENOTED THUS \bar{N} .

DYNAMIC CONE PENETRATION TEST: CONTINUOUS PENETRATION OF A CONICAL STEEL POINT (51mm O.D. 60° CONE ANGLE) DRIVEN BY 475 J IMPACT ENERGY ON 'A' SIZE DRILL RODS. THE RESISTANCE TO CONE PENETRATION IS MEASURED AS THE NUMBER OF BLOWS FOR EACH 0.3m ADVANCE OF THE CONICAL POINT INTO THE UNDISTURBED GROUND.

SOILS ARE DESCRIBED BY THEIR COMPOSITION AND CONSISTENCY OR DENSENESS.

CONSISTENCY: COHESIVE SOILS ARE DESCRIBED ON THE BASIS OF THEIR UNDRAINED SHEAR STRENGTH (c_u) AS FOLLOWS:

c_u (kPa)	0 - 12	12 - 25	25 - 50	50 - 100	100 - 200	> 200
	VERY SOFT	SOFT	FIRM	STIFF	VERY STIFF	HARD

DENSENESS: COHESIONLESS SOILS ARE DESCRIBED ON THE BASIS OF DENSENESS AS INDICATED BY SPT N VALUES AS FOLLOWS:

N (BLOWS/0.3m)	0 - 5	5 - 10	10 - 30	30 - 50	> 50
	VERY LOOSE	LOOSE	COMPACT	DENSE	VERY DENSE

ROCKS ARE DESCRIBED BY THEIR COMPOSITION AND STRUCTURAL FEATURES AND / OR STRENGTH.

RECOVERY: SUM OF ALL RECOVERED ROCK CORE PIECES FROM A CORING RUN EXPRESSED AS A PERCENT OF THE TOTAL LENGTH OF THE CORING RUN.

MODIFIED RECOVERY: SUM OF THOSE INTACT CORE PIECES, 100mm+ IN LENGTH EXPRESSED AS A PERCENT OF THE LENGTH OF THE CORING RUN. THE ROCK QUALITY DESIGNATION (R Q D), FOR MODIFIED RECOVERY, IS:

RQD (%)	0 - 25	25 - 50	50 - 75	75 - 90	90 - 100
	VERY POOR	POOR	FAIR	GOOD	EXCELLENT

JOINTING AND BEDDING:

SPACING	50mm	50 - 300mm	0.3m - 1m	1m - 3m	> 3m
JOINTING	VERY CLOSE	CLOSE	MOD. CLOSE	WIDE	VERY WIDE
BEDDING	VERY THIN	THIN	MEDIUM	THICK	VERY THICK

ABBREVIATIONS AND SYMBOLS

FIELD SAMPLING

SS	SPLIT SPOON	TP	THINWALL PISTON
WS	WASH SAMPLE	OS	OSTERBERG SAMPLE
ST	SLOTTED TUBE SAMPLE	RC	ROCK CORE
BS	BLOCK SAMPLE	PH	TW ADVANCED HYDRAULICALLY
CS	CHUNK SAMPLE	PM	TW ADVANCED MANUALLY
TW	THINWALL OPEN	FS	FOIL SAMPLE

STRESS AND STRAIN

u_w	kPa	PORE WATER PRESSURE
r_u	1	PORE PRESSURE RATIO
σ	kPa	TOTAL NORMAL STRESS
σ'	kPa	EFFECTIVE NORMAL STRESS
τ	kPa	SHEAR STRESS
$\sigma_1, \sigma_2, \sigma_3$	kPa	PRINCIPAL STRESSES
ϵ	%	LINEAR STRAIN
$\epsilon_1, \epsilon_2, \epsilon_3$	%	PRINCIPAL STRAINS
E	kPa	MODULUS OF LINEAR DEFORMATION
G	kPa	MODULUS OF SHEAR DEFORMATION
μ	1	COEFFICIENT OF FRICTION

MECHANICAL PROPERTIES OF SOIL

m_v	kPa^{-1}	COEFFICIENT OF VOLUME CHANGE
C_c	1	COMPRESSION INDEX
C_s	1	SWELLING INDEX
C_α	1	RATE OF SECONDARY CONSOLIDATION
c_v	m^2/s	COEFFICIENT OF CONSOLIDATION
H	m	DRAINAGE PATH
T_v	1	TIME FACTOR
U	%	DEGREE OF CONSOLIDATION
σ'_{v0}	kPa	EFFECTIVE OVERBURDEN PRESSURE
σ'_p	kPa	PRECONSOLIDATION PRESSURE
τ_f	kPa	SHEAR STRENGTH
c'	kPa	EFFECTIVE COHESION INTERCEPT
ϕ'	-°	EFFECTIVE ANGLE OF INTERNAL FRICTION
c_u	kPa	APPARENT COHESION INTERCEPT
ϕ_u	-°	APPARENT ANGLE OF INTERNAL FRICTION
τ_R	kPa	RESIDUAL SHEAR STRENGTH
τ_r	kPa	REMOULDED SHEAR STRENGTH
S_t	1	SENSITIVITY = $\frac{c_u}{\tau_r}$

PHYSICAL PROPERTIES OF SOIL

ρ_s	kg/m^3	DENSITY OF SOLID PARTICLES	e	1, %	VOID RATIO	e_{min}	1, %	VOID RATIO IN DENSEST STATE
γ_s	kN/m^3	UNIT WEIGHT OF SOLID PARTICLES	n	1, %	POROSITY	I_D	1	DENSITY INDEX = $\frac{e_{max} - e}{e_{max} - e_{min}}$
ρ_w	kg/m^3	DENSITY OF WATER	w	1, %	WATER CONTENT	D	mm	GRAIN DIAMETER
γ_w	kN/m^3	UNIT WEIGHT OF WATER	S_r	%	DEGREE OF SATURATION	D_n	mm	n PERCENT - DIAMETER
ρ	kg/m^3	DENSITY OF SOIL	w_L	%	LIQUID LIMIT	C_u	1	UNIFORMITY COEFFICIENT
γ	kN/m^3	UNIT WEIGHT OF SOIL	w_p	%	PLASTIC LIMIT	h	m	HYDRAULIC HEAD OR POTENTIAL
ρ_d	kg/m^3	DENSITY OF DRY SOIL	w_s	%	SHRINKAGE LIMIT	q	m^3/s	RATE OF DISCHARGE
γ_d	kN/m^3	UNIT WEIGHT OF DRY SOIL	I_p	%	PLASTICITY INDEX = $\frac{w_L - w_p}{w - w_p}$	v	m/s	DISCHARGE VELOCITY
ρ_{sat}	kg/m^3	DENSITY OF SATURATED SOIL	I_L	1	LIQUIDITY INDEX = $\frac{w - w_p}{I_p}$	i	1	HYDRAULIC GRADIENT
γ_{sat}	kN/m^3	UNIT WEIGHT OF SATURATED SOIL	I_C	1	CONSISTENCY INDEX = $\frac{w_L - w}{I_p}$	k	m/s	HYDRAULIC CONDUCTIVITY
ρ'	kg/m^3	DENSITY OF SUBMERGED SOIL	e_{max}	1, %	VOID RATIO IN LOOSEST STATE	j	kN/m^3	SEEPAGE FORCE
γ'	kN/m^3	UNIT WEIGHT OF SUBMERGED SOIL						

METRIC
DIMENSIONS ARE IN METRES
AND/OR MILLIMETRES UNLESS
OTHERWISE SHOWN. STATIONS
IN KILOMETRES + METRES.

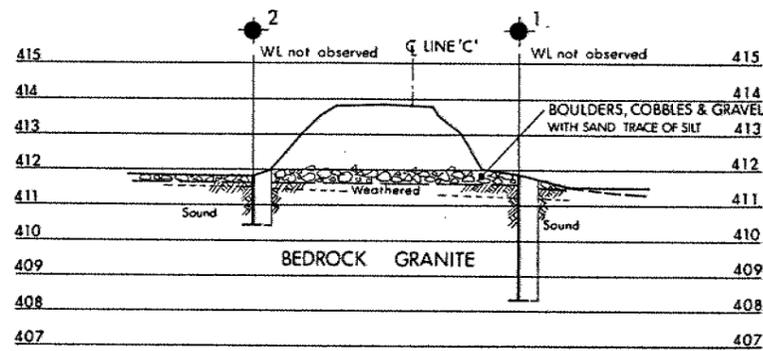
CONT No
WP No 18-77-18



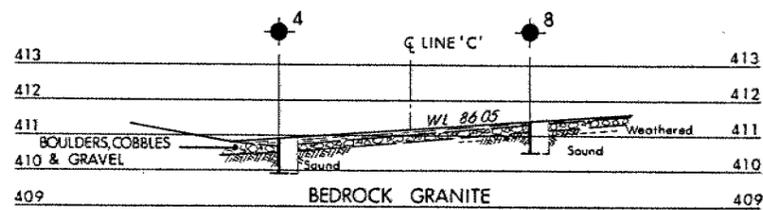
GIBSON CREEK

SHEET

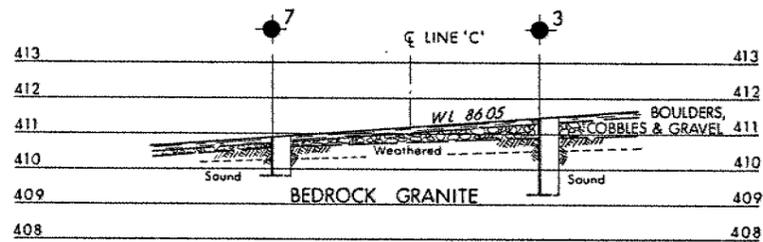
BORE HOLE LOCATIONS & SOIL STRATA



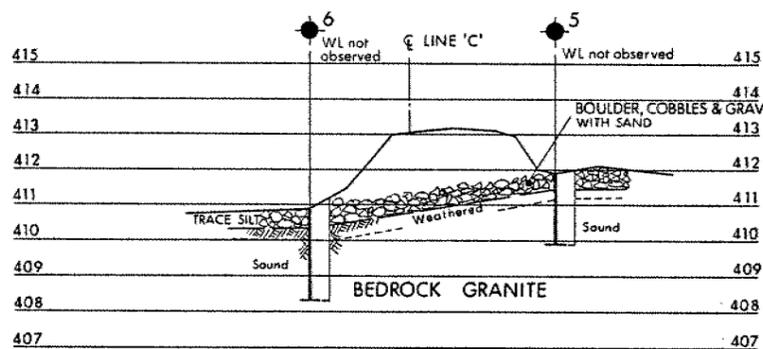
A-A



B-B

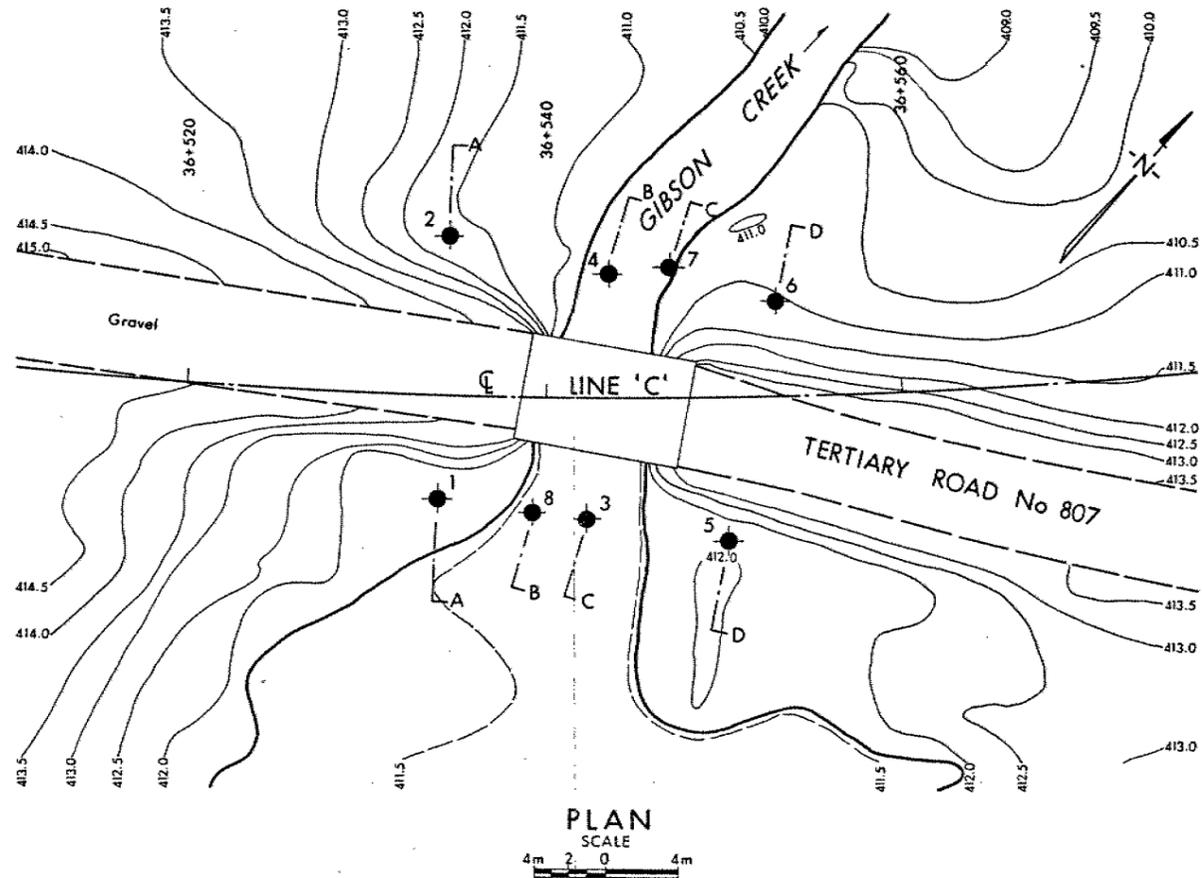
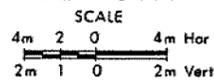


C-C

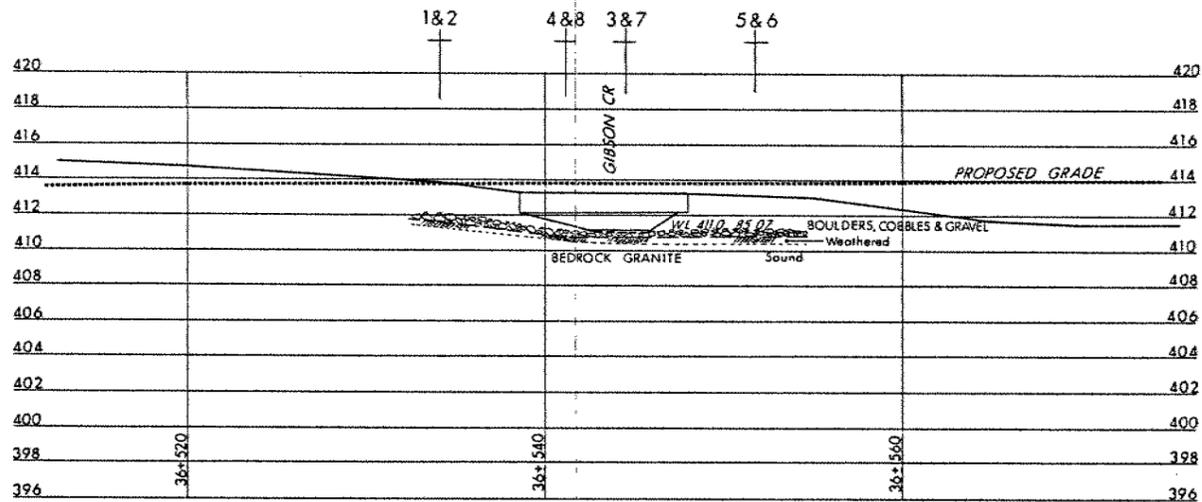
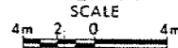


D-D

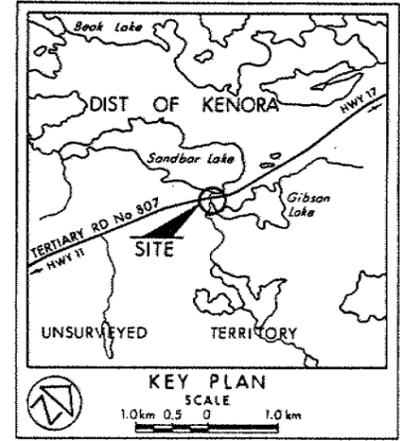
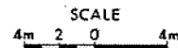
SECTIONS



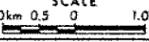
PLAN



PROFILE LINE 'C'



KEY PLAN



LEGEND

- Bore Hole
- ⊕ Dynamic Cone Penetration Test (Cone)
- ⊕ Bore Hole & Cone
- N Blows/0.3m (Srd Pen Test, 475 J/blow)
- CONE Blows/0.3m (60° Cone, 475 J/blow)
- ⊕ WL at time of investigation 1986 05
- ⊕ WL not observed in BHs 1, 2, 5 & 6

No	ELEVATION	STATION	OFFSET
1	411.9	36+534.0	5.9 m RT
2	411.8	36+534.5	9.0 m LT
3	411.5	36+542.3	6.8 m RT
4	410.9	36+543.5	7.0 m LT
5	411.9	36+550.0	8.2 m RT
6	410.9	36+553.1	5.4 m LT
7	410.9	36+547.0	7.3 m LT
8	411.4	36+539.3	6.5 m RT

NOTE
The boundaries between soil strata have been established only at Bore Hole locations. Between Bore Holes the boundaries are assumed from geological evidence.

NOTE: The complete foundation investigation and design report for this project and other related documents may be examined at the Engineering Materials Office, Downsview. Information contained in this report and related documents is specifically excluded in accordance with the conditions of Section 102-2 of Form 100.

REV	DATE	BY	DESCRIPTION

Geocres No 52E-21

HWY No TERTIARY RD No 807	DIST 20
SUBM'D WD [CHECKED] DATE 1986 08 12	SITE 415-133
DRAWN SO [CHECKED] APPROVED	DWG 187718-A

DOCUMENT MICROFILMING IDENTIFICATION

G.I.-30 SEPT. 1976

GEOCRES No. 52E-21

DIST. 20 REGION _____

W.P. No. _____

CONT. No. _____

W. O. No. 78-12003

STR. SITE No. _____

HWY. No. LOC.

LOCATION 5.0 MILES NORTH

OF KENORA - ANDERSON ROAD BRIDGE

NO OF PAGES -



OVERSIZE DRAWINGS TO BE INCLUDED WITH THIS REPORT. _____

REMARKS: _____

FILE
COPY



Ontario

Ministry of
Transportation and
Communications

foundation investigation and design report

ENGINEERING MATERIALS OFFICE
SOIL MECHANICS SECTION

WO 78-12003

DIST 20

HWY Mun.

STR SITE 41S-26

Anderson Road Bridge

DISTRIBUTION

W. Kulmatickas (2)

C.M. Smith

D.R. Hogg (2)

E. Van Beilen

G.A. Wrong

R. Hore

N. Maluzinsky)

J. Anderson) cover only

G. Sloan

Files

MUNICIPAL FOUNDATION INVESTIGATION REPORT

For

Anderson Road Bridge
W.O. 78-12003, Site 41S-26
District 20, Kenora

INTRODUCTION

This report contains the results of a foundation investigation which was carried out at the site of the above mentioned project during the period of January 20-24, 1979. The fieldwork was done by utilizing a conventional diamond drilling equipment using NX (3 inch I.D.) and BX (2 3/8 inch I.D.) size casings.

SITE DESCRIPTION

The proposed bridge replacement site is situated at the crossing of Anderson Road and Winnipeg River system, approximately 3.1 miles northwest of the junction of Secondary Hwy. 666 and Anderson Road in the Township of Melick. The junction of Anderson Road and Secondary Hwy. 666 is located some 1.2 miles north of Kenora's Townline. The structure site is located in a relatively steeply sloping (2:1) valley having a width of about 70 feet measured along the existing river water level (elev. 66+). Frequent rock outcrops with a vertical or near vertical face are visible adjacent to the crossing. The immediate vicinity of the site is covered with trees. Residential dwellings in a scattered pattern were observed along Anderson Road.

SUBSURFACE CONDITIONS

In general the overburden in the borings was found to consist of a surficial deposit of organic silt to a maximum thickness of about 5 feet below the existing river bed level. The consistency of this stratum (when it is not frozen) is estimated to be in the very soft state. Below the organic silt, a compact to dense gravelly sand with some silt was encountered to varying depths, the maximum thickness being about 19 feet at the approximate

centre of the valley. Partially weathered, pink coloured, friable, gneiss type bedrock was found to underlie the overburden.

References should be made to the Record of Borehole Sheets and Drawing No. 7812003-A contained in the Appendix of this report for the different subsoil boundaries and also for the locations and elevations of the individual borings. The groundwater is assumed to be the same as the existing river water level at a given time.

DISCUSSION AND RECOMMENDATIONS

General

It is proposed to replace the existing 8 span, approximately 115 foot long single lane timber bridge supported on pile bents. Some of these bents have moved towards the river. The flow in the river is minimal at this location. Design requirements for the structure replacement are as follows:

Horizontal Alignment: as existing

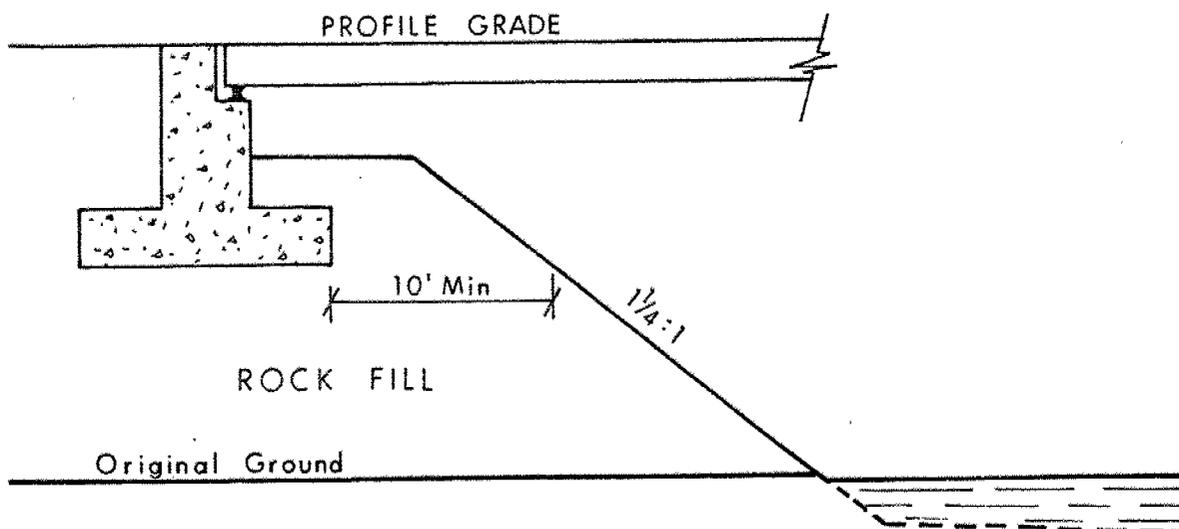
Vertical Alignment: Up to 4 feet grade raise over the existing

Navigational Clearance: 6 feet vertical by 8 feet horizontal.

The 6 feet vertical clearance should be taken from an average H.W.L. of Elev. 71+.

Structure Foundations

In view of the site conditions and the proposed design criteria, the most practical type of solution appears to be the erection of C.S.P. culvert or culverts. According to the information of Northwestern Region's Structural Section, the Federal Ministry of Transport would not approve the construction of C.S.P. culvert (s). As an alternative, the abutments of the proposed structure may be founded on spread footings placed within rock fill approach embankments. Design pressures up to 2 tsf may be assumed. The footings should be placed so as to have at least 8 feet of cover to provide for frost protection. The rock fill approach embankments should be built initially to profile grade with $1\frac{1}{4}:1$ side and forward slopes at the structure location, then excavated for the structure foundation as shown on the sketch below.



NTS

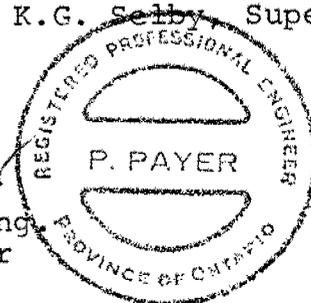
It would be advantageous to provide for shimming up the bridge deck to accommodate settlements which may occur after completion of the project. The encountered very soft organic silt deposit should be removed from toe to toe and at least 10 feet in front of the forward slopes to its full vertical extent prior to the placement of the rock fill approach embankments.

As a second alternative the abutments may be founded on the bedrock some 10 feet behind the rock face. The footings should be keyed into the bedrock for a minimum distance of about 1 foot. Should a multi-span structure be considered at this location, it is recommended that steel 'H' pile bents be constructed. This will eliminate the dewatering problems which arise if the pile caps would be formed below the prevailing river water level. The steel 'H' piles should be driven to bedrock in which case the maximum allowable load for the particular steel section adopted may be used for design purposes. Due to the steeply sloping nature of the bedrock and the shallow overburden at some locations within the construction area, it is recommended that the piles be fitted with Oslo points (SS3-4) and keyed into the rock to safeguard against sliding.

MISCELLANEOUS

The supervision of the fieldwork, together with the preparation of this report, was carried out by Mr. P. Payer, Senior Engineer. Equipment was owned and operated by Morton and Partners, Ltd., Thunder Bay. The report was reviewed by Mr. K.G. Selby, Supervising Engineer.

P. Payer
P. Payer, P. Eng.
Senior Engineer



K.G. Selby
K.G. Selby, P. Eng.
Supervising Engineer

APPENDIX

RECORD OF BOREHOLE No 1

WO 78-12003 LOCATION Sta. 13+39; E Anderson Road ORIGINATED BY PP
 DIST 20 HWY Loc. BOREHOLE TYPE Washbore-NX Casing COMPILED BY PP
 DATUM Assumed DATE January 20-21, 1979 CHECKED BY CP

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT Y	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL	
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			'N' VALUES	20	40	60	80						100
											○ UNCONFINED	+ FIELD VANE	WATER CONTENT (%)				
											● QUICK TRIAXIAL	x LAB VANE					
65.9	Ice Level																
0.0	River Bed																
62.3	Organic Silt																
3.6	Very Soft		1	SS	2												
56.9	Gravelly Sand Some Silt Compact to Dense		2	SS	33												
9.0			3	SS	18												
				4	SS	33											
37.6																	
28.3	Refusal Probable Bedrock End of Borehole																

RECORD OF BOREHOLE No 2

WO 78-12003 LOCATION Sta. 13+08; E Anderson Road ORIGINATED BY PP
 DIST 20 HWY Loc. BOREHOLE TYPE Proborehole-NX Casing COMPILED BY PP
 DATUM Assumed DATE January 21, 1979 CHECKED BY CP

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT Y	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			'N' VALUES	20	40	60	80					
											○ UNCONFINED	+ FIELD VANE	WATER CONTENT (%)			
											● QUICK TRIAXIAL	x LAB VANE				
65.8	Ice and Frozen Ground Level															
0.0	Organic Silt (Frozen)															
60.8	Gravelly Sand															
5.0																
56.1																
9.7	Refusal Probable Bedrock End of Hole															

RECORD OF BOREHOLE No 3

WO 78-12003 LOCATION Sta. 13+70; @ Anderson Road ORIGINATED BY PP
 DIST 20 HWY Loc. BOREHOLE TYPE Probehole-NX Casing COMPILED BY PP
 DATUM Assumed DATE January 21, 1979 CHECKED BY CP

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT Wp	NATURAL MOISTURE CONTENT W	LIQUID LIMIT Wl	UNIT WEIGHT Y	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			20	40	60	80	100					
66.6	Ground (Frozen) Level																
0.0 63.6	Organic Silt (Frozen)																
3.0	Gravelly Sand																
57.1							60										
9.5	Refusal Probable Bedrock End of Hole Note: Water Level Not Established																

RECORD OF BOREHOLE No 4

WO 78-12003 LOCATION Sta. 14+02; o/s 10' Lt. @ Anderson Road ORIGINATED BY PP
 DIST 20 HWY Loc. BOREHOLE TYPE BXL Rock Coring COMPILED BY PP
 DATUM Assumed DATE January 22, 1979 CHECKED BY CP

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT Wp	NATURAL MOISTURE CONTENT W	LIQUID LIMIT Wl	UNIT WEIGHT Y	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			20	40	60	80	100					
77.2	Ground Level																
0.0 73.1	Gravelly Sand (Frozen)																
4.1	Gneiss Bedrock Partially Weathered		1	RC BXL	Rec. 75%												
68.2			2	RC BXL	Rec. 85%												
9.0	End of Borehole Note: Water Level Not Observed						70										

OFFICE REPORT ON SOIL EXPLORATION

+3, x5: Numbers refer to Sensitivity
 20
 15 5 (%) STRAIN AT FAILURE
 10

RECORD OF BOREHOLE No 5

WO 78-12003 LOCATION Sta. 12+50; o/s 14' Rt. of Anderson Road ORIGINATED BY PP
 DIST 20 HWY Loc. BOREHOLE TYPE Rock Coring-BX Casing COMPILED BY PP
 DATUM Assumed DATE January 23, 1979 CHECKED BY *CP*

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT Y	REMARKS & GRAIN SIZE DISTRIBUTION (%)
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			20	40	60	80	100					
79.9	Ground Level																
0.0	Sand and Organic																
74.6	Recovered 4.8' of Gneiss Bedrock Sound																
5.3	End of Borehole Note: Water Level Not Established Drilled With BX Casing						70										

RECORD OF BOREHOLE No 6

WO 78-12003 LOCATION Sta. 14+12; o/s 11' Rt. of Anderson Road ORIGINATED BY PP
 DIST 20 HWY Loc. BOREHOLE TYPE BXL Rock Coring COMPILED BY PP
 DATUM Assumed DATE January 23, 1979 CHECKED BY *CP*

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT Y	REMARKS & GRAIN SIZE DISTRIBUTION (%)
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			20	40	60	80	100					
78.3	Ground Level																
0.0	Gravelly Sand																
74.1	(Frozen)																
4.2	Gneiss Bedrock		1	RC													
70.6	Sound			BXL	Rec. 97%												
7.7	End of Borehole Note: Water Level Not Established						70										

OFFICE REPORT ON SOIL EXPLORATION

EXPLANATION OF TERMS USED IN REPORT

'N' VALUE: AN INDICATOR OF SUBSOIL QUALITY. IT IS OBTAINED FROM THE STANDARD PENETRATION TEST (CSA STD. A119.1). SPT 'N' VALUE IS THE NUMBER OF BLOWS REQUIRED TO CAUSE A STANDARD 2 INCH O.D. SPLIT-BARREL SAMPLER TO PENETRATE 12 INCHES INTO UNDISTURBED GROUND IN A BOREHOLE WHEN DRIVEN BY A HAMMER WEIGHING 140 POUNDS, FALLING FREELY A DISTANCE OF 30 INCHES. FOR PENETRATIONS OF LESS THAN 12 INCHES 'N' VALUES ARE INDICATED AS THE NUMBER OF BLOWS FOR THE PENETRATION ACHIEVED. 'N' VALUES CORRECTED FOR OVERBURDEN PRESSURE ARE DENOTED THUS N.

DYNAMIC CONE PENETRATION TEST (CSA STD. A119.3): CONTINUOUS PENETRATION OF A CONICAL STEEL POINT (2" O.D. 60 CONE ANGLE) DRIVEN BY 350 FT-LB IMPACTS ON 'A' SIZE DRILL RODS. THE RESISTANCE TO CONE PENETRATION IS MEASURED AS THE NUMBER OF BLOWS FOR EACH 12 INCH ADVANCE OF THE CONICAL POINT INTO THE UNDISTURBED GROUND.

SOIL QUALITY: SOILS ARE DESCRIBED BY THEIR COMPOSITION AND CONSISTENCY OR DENSITY.

CONSISTENCY: COHESIVE SOILS ARE DESCRIBED ON THE BASIS OF THEIR UNDRAINED SHEAR STRENGTH AS FOLLOWS:

S _u (PSF)	0 - 250	250 - 500	500 - 1000	1000 - 2000	2000 - 4000	> 4000
	VERY SOFT	SOFT	FIRM	STIFF	VERY STIFF	HARD

DENSENESS: COHESIONLESS SOILS ARE DESCRIBED ON THE BASIS OF SPT 'N' VALUES AS FOLLOWS:

'N' (BLOW/FT)	0 - 5	5 - 10	10 - 30	30 - 50	> 50
	VERY LOOSE	LOOSE	COMPACT	DENSE	VERY DENSE

ROCK QUALITY: ROCKS ARE DESCRIBED BY THEIR COMPOSITION AND STRUCTURAL FEATURES AND/OR STRENGTH.

RECOVERY: SUM OF ALL RECOVERED ROCK CORE PIECES FROM A CORING RUN EXPRESSED AS A PERCENT OF THE TOTAL LENGTH DRILLED IN THAT CORING RUN.

MODIFIED RECOVERY: SUM OF THOSE NATURALLY FRACTURED CORE PIECES, 4" IN LENGTH EXPRESSED AS A PERCENT OF THE LENGTH OF THE CORING RUN. THE ROCK QUALITY DESIGNATION (RQD), FOR MODIFIED RECOVERY, IS:

RQD (%)	0 - 25	25 - 50	50 - 75	75 - 90	90 - 100
	VERY POOR	POOR	FAIR	GOOD	EXCELLENT

JOINTING AND BEDDING:

SPACING	2"	2" - 12"	1' - 3'	3' - 10'	> 10'
Jointing	VERY CLOSE	CLOSE	MOD. CLOSE	WIDE	VERY WIDE
Bedding	VERY THIN	THIN	MEDIUM	THICK	VERY THICK

ABBREVIATIONS & SYMBOLS

LABORATORY TESTING

TRIAXIAL TESTS ARE DESCRIBED IN TERMS OF WHETHER THEY ARE CONSOLIDATED (C) OR NOT (U) ISOTROPICALLY (I) OR NOT (A) AND SHEARED DRAINED (D) OR UNDRAINED (U) WITH PORE PRESSURE MEASUREMENTS (BAR OVER SYMBOLS) EG. CIU = CONSOLIDATED ISOTROPIC UNDRAINED TRIAXIAL WITH PORE PRESSURE MEASUREMENT UNLESS OTHERWISE SPECIFIED IN REPORT ALL TESTS ARE IN COMPRESSION

FIELD SAMPLING

S S SPLIT SPOON
 W S WASH SAMPLE
 S T SLOTTED TUBE SAMPLE
 B S BLOCK SAMPLE
 C S CHUNK SAMPLE
 T W THINWALL OPEN
 T P THINWALL PISTON
 O S OSTERBERG SAMPLE
 F S FOIL SAMPLE
 R C ROCK CORE
 P H T.W. ADVANCED HYDRAULICALLY
 P M T.W. ADVANCED MANUALLY

EARTH PRESSURE TERMS

μ COEFFICIENT OF FRICTION
 δ ANGLE OF WALL FRICTION
 k_o COEFFICIENT OF EARTH PRESSURE AT REST
 k_A COEFFICIENT OF ACTIVE EARTH PRESSURE
 k_P COEFFICIENT OF PASSIVE EARTH PRESSURE
 i ANGLE OF INCLINATION OF SURCHARGE
 ω SLOPE ANGLE-BACKFACE OF WALL
 β ANGLE OF SLOPE
 N_y, N_q, N_c BEARING CAPACITY FACTORS
 D_f DEPTH OF FOOTING
 B, L FOOTING DIMENSIONS

INDEX PROPERTIES

γ UNIT WEIGHT OF SOIL (BULK DENSITY)
 γ_w UNIT WEIGHT OF WATER
 γ_d UNIT DRY WEIGHT OF SOIL (DRY DENSITY)
 γ' UNIT WEIGHT OF SUBMERGED SOIL
 G_s SPECIFIC GRAVITY OF SOLIDS
 e VOIDS RATIO
 e_o INITIAL VOIDS RATIO
 e_{max} e IN LOOSEST STATE
 e_{min} e IN DENSEST STATE
 D_r RELATIVE DENSITY = $\frac{e_{max} - e}{e_{max} - e_{min}}$
 n POROSITY
 w WATER CONTENT
 w_L LIQUID LIMIT
 w_p PLASTIC LIMIT
 w_s SHRINKAGE LIMIT
 I_p PLASTICITY INDEX = w_L - w_p
 I_L LIQUIDITY INDEX = $\frac{w - w_p}{I_p}$
 I_c CONSISTENCY INDEX = $\frac{w_L - w}{I_p}$
 A_c ACTIVITY = $\frac{I_p \text{ of soil}}{I_p \text{ of } 2\mu m \text{ Soil Fraction}}$
 O_m ORGANIC MATTER CONTENT
 S_r DEGREE OF SATURATION
 S SENSITIVITY = $\frac{S_o \text{ (undisturbed)}}{S_o \text{ (remoulded)}}$

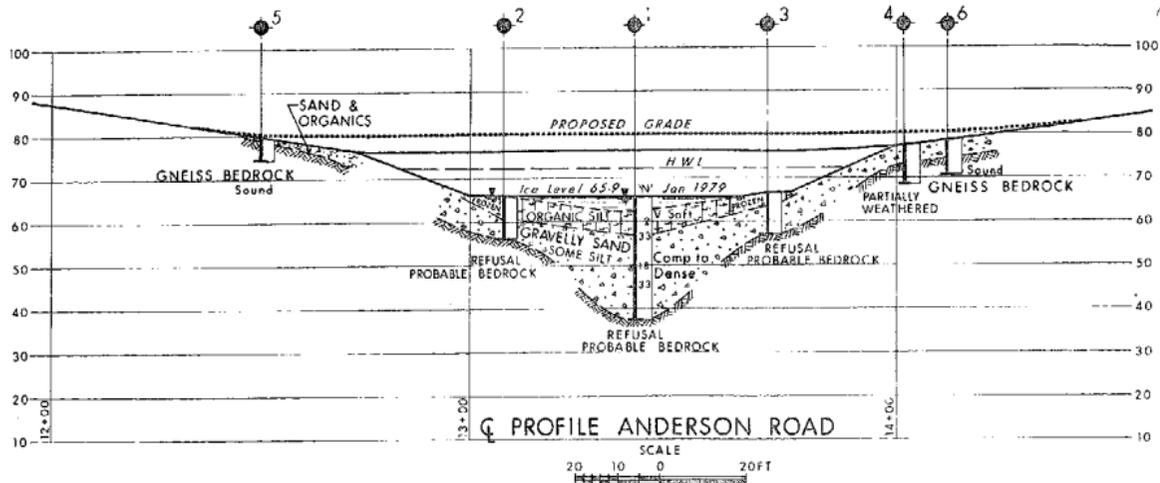
STRENGTH PARAMETERS

φ ANGLE OF SHEARING RESISTANCE
 τ_f PEAK SHEAR STRENGTH
 τ_R RESIDUAL SHEAR STRENGTH
 c COHESION INTERCEPT
 σ₁, σ₂, σ₃ NORMAL PRINCIPAL STRESSES
 u PORE WATER PRESSURE
 u_e EXCESS u
 r_u PORE PRESSURE RATIO
 q_u UNCONFINED COMPRESSIVE STRENGTH
 s_u UNDRAINED SHEAR STRENGTH
 ε LINEAR STRAIN
 γ SHEAR STRAIN
 ν POISSON'S RATIO
 E MODULUS OF ELASTICITY
 G MODULUS OF SHEAR DEFORMATION
 k_s MODULUS OF SUBGRADE REACTION
 m, n STABILITY COEFFICIENTS
 A, B PORE PRESSURE COEFFICIENTS

HYDRAULIC TERMS

h HYDRAULIC HEAD OR POTENTIAL
 q RATE OF DISCHARGE
 v VELOCITY OF FLOW
 i HYDRAULIC GRADIENT
 j SEEPAGE FORCE PER UNIT VOLUME
 η COEFFICIENT OF VISCOSITY
 k COEFFICIENT OF HYDRAULIC CONDUCTIVITY
 k_h k IN HORIZONTAL DIRECTION
 k_v k IN VERTICAL DIRECTION
 m_v COEFFICIENT OF VOLUME CHANGE
 c_v COEFFICIENT OF CONSOLIDATION
 C_c COMPRESSION INDEX
 C_r RECOMPRESSION INDEX
 d DRAINAGE PATH DISTANCE
 T TIME FACTOR
 U DEGREE OF CONSOLIDATION
 Q_c OVERCONSOLIDATION RATIO (OCR)

NOTE: EFFECTIVE STRESS PARAMETERS ARE DENOTED BY USE OF APOSTROPHE ABOVE THE SYMBOL, THUS: σ' = EFFECTIVE ANGLE OF SHEARING RESISTANCE; σ'₁ = EFFECTIVE NORMAL STRESS



NOTE:

BENCH MARK ORIGIN
 ASSUMED B.M.#1, ELEVATION 100.00
 PAINT MARK ON ROCK; STA D+17, 9/8 32' RT

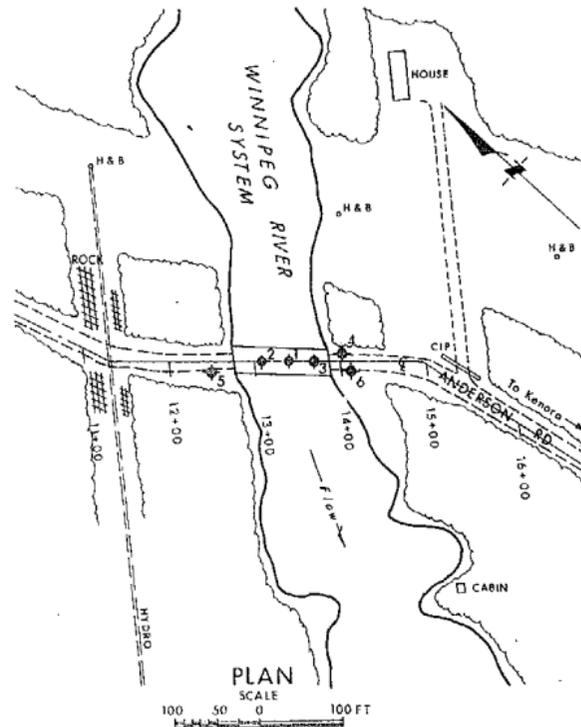
ASSUMED B.M.#2, ELEVATION 76.55
 PAINT MARK ON ROCK; STA 12+73, 9/8 20' RT

LEGEND

⊕ Bore Hole

WATER LEVEL NOT OBSERVED
 in BH#3, 4, 5 & 6

No	ELEVATION	STATION	OFFSET
1	65.9	18+3V	⊕
2	65.8	15+08	⊕
3	66.6	13+70	⊕
4	77.2	14+02	10' LT
5	79.9	12+50	14' RT
6	76.3	14+12	11' RT



Geocres No 52E-21



Ministry of
Transportation and
Communications

ANDERSON RD & WINNIPEG RIVER SYSTEM

DIST OF KENORA - MUN OF JAFFRAY & MELICK - TWP OF MELICK
 CON T LOT 17 SITE 415-26 DIST 20

DATE Feb 12, 1979

WO 78-12003

Dwg No 7812003-A