

G.I.-30 SEPT. 1976

GEOCRES No. 420-16DIST. 18 REGION W.P. No. 195-87-01(B)CONT. No. W. O. No. STR. SITE No. 48E-46HWY. No. 17LOCATION Hwy 17 & McKellar Creek  
(Approaches)No of PAGES - =====OVERSIZE DRAWINGS TO BE INCLUDED WITH THIS REPORT. REMARKS:



Ministry  
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Transportation

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## **FOUNDATION DESIGN SECTION**

# **foundation investigation and design report**

ENGINEERING MATERIALS OFFICE  
FOUNDATION DESIGN SECTION

WP 195-87-01 (B) DIST 18  
HWY 17 STR SITE 48 E - 46  
McKellar Creek Culvert at Highway 17

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FOUNDATION INVESTIGATION REPORT  
For  
McKellar Creek Culvert at Highway 17  
W.P. 195-87-01 (B), Site 48 E - 46  
District 18, Sault Ste. Marie

INTRODUCTION

This report summarizes the results of a foundation investigation conducted near McKellar Creek, just north of Highway 17. The investigation was carried out upon the request of the Northwestern Region Geotechnical Section. A previous investigation carried out for the Structural Section on the proposed McKellar Creek culvert structure has revealed potential stability and settlement problems on the approaches. The current investigation intends to address these concerns. This report should therefore be read in conjunction with the Foundation Investigation Report W.P. 195-87-01 dated 91 04 25 on the McKellar Creek Culvert.

SITE DESCRIPTION

The site is located along the proposed new Highway 17 alignment at the approaches to the McKellar Creek crossing, approximately 34.5 km east of Terrace Bay in the Township of Walsh, District of Sault Ste. Marie. The area is undulating and heavily vegetated with trees.

According to the Geological Map S265 in Ontario Geological Survey Report GR 164, the site consists largely of deposits of varved or massive clay and silt and bare bedrock.

INVESTIGATION PROCEDURES

The field investigation for this project was conducted between 91 04 09 and 91 04 12 and consisted of fourteen (14) sampled boreholes generally accompanied by dynamic cone penetration tests. BH 10 was located on exposed bedrock and no drilling was carried out at this location. The grade elevation was noted. The boreholes are generally staggered evenly along the centreline and 30 m offset lines on both sides. Due to the existing terrain, some hole locations had to be adjusted from this pattern.

Trailer mounted and muskeg vehicle mounted continuous flight drilling machines equipped with hollow stem augers were used to advance the boreholes. A bulldozer was also employed to remove surficial obstructions, and to move the trailer mounted machine around the site.

The locations of the boreholes are shown on Drawing No. 1958701(B)-A. A total of 59 split spoon samples and 13 shelby tube samples were collected. The shelby tube samples provided generally undisturbed samples for detailed laboratory evaluation of the relatively soft cohesive overburden. The split spoon samples provided material for visual classification purposes and Standard Penetration Tests values for assessment of the strength of the subsoil. In addition, 18 field vane tests were carried out to determine the in situ shear strengths and sensitivity values of the cohesive material. Groundwater elevations were determined by measuring in the open boreholes.

The following laboratory tests were carried out on representative samples to identify and determine the physical properties and strength of the overburden.

- Natural Moisture Content Determinations
- Atterberg Limits
- Consolidation Tests
- Unit Weight Tests
- Unconfined Compressive Tests

#### SUBSURFACE CONDITIONS

The Record of Borehole sheets in the Appendix illustrates the subsurface conditions at the borehole locations. The locations and elevations of the boreholes, along with stratigraphical profiles based on the borehole data are shown on Drawing No. 1958701(B)-A.

The subsurface stratigraphy typically comprises a layer (up to 3 m) of organic material overlying silty clay to a maximum depth of 9.9 m, which is in turn underlain by a major silty sand deposit.

### Organics

Organic material was contacted in most of the boreholes at the ground surface. The thickness of the material is very variable across the site. It was an organic silty sand with rootlets or woodchips in BH 5, BH 7, BH 9, BH 12 and BH 14, and an organic silty clay in BH 1, BH 3, BH 8, BH 11 and BH 13. The thickness of this organic layer is 0.8 to 3.0 m.

### Silty Clay

This cohesive deposit was encountered at the ground surface or below the organic layer in the boreholes between Sta. 14+600 to 14+750 approximately, as shown in Drawing No. 1958701(B)-A. It is described as silty clay to clay. It extended to a maximum depth of 9.9 m (elevation 185.3 m) in BH 7.

The results of the laboratory testing carried out on the soil samples are as follows:

<u>Property</u>	<u>Range</u>
Natural Moisture Content (%)	27-54
Liquid Limit (%)	35-57
Plastic Limit (%)	16-28
Unit Weight (kN/cu.m)	15.9-18.5

Two consolidation tests were carried out and they indicated an average void ratio of 1.485 and an average compression index of 0.663.

An unconfined compressive test was carried out on a silty clay sample and the unconfined shear strength obtained was 20 kPa.

Field vane tests carried out on the material indicated undrained shear strengths of 19 to 39 kPa, but typically between 20 and 25 kPa. Based on this information, the consistency of the material can be described as soft to firm.

### Silty Sand

This non-cohesive deposit was contacted in all boreholes underlying the organic or silty clay stratum except in BH 10 where the overburden was absent. The material was described as a fine to coarse sand with trace of gravel. It was generally in a loose to compact state, as determined by the Standard Penetration Tests and Dynamic Cone Tests. The deposit was not penetrated at the termination depths in BH 3, BH 6, BH 9 and BH 13.

### GROUNDWATER CONDITIONS

Groundwater levels were measured in open boreholes after completion of the investigation. The groundwater table was typically found to be within 2 m below the ground surface, between elevations 190 to 194 m from Sta. 14+600 to 14+800 and 194 to 202 m from Sta. 14+500 to 14+600. Seasonal variation is expected.

## DISCUSSIONS AND RECOMMENDATIONS

It is proposed to replace the existing timber box culvert at McKellar Creek with a concrete box culvert. The new culvert will be located under a new alignment of Highway 17 about 75 m maximum to the north of the existing alignment.

Recommendations for the construction of the structure were given in the Foundation Investigation Report W.P. 195-87-01 dated 91 04 25. A layer of soft silty clay of substantial thickness was revealed in the previous investigation. the design height of embankment is up to about 14 m as indicated in the E-plan. there are concerns on potential stability and settlement problems along the new alignment of Highway 17. In response to this, the Northwestern Region Geotechnical Section requested this office to carry out an investigation on the approaches between Sta. 14+500 to 14+800 to cover the fill portion of the new alignment. The profile of the new alignment in relation to the existing grades is shown in the longitudinal sections of Drawing No. 1958701(B)-A.

According to the field investigation data, the silty clay deposit exists approximately from Sta. 14+600 to Sta. 14+750 as indicated in Drawing No. 1958701(B)-A. It extends to depths of 3.7 to 9.9 m. A surficial layer of organic material was found over most of the site area. Based on the laboratory and in situ test results, the silty clay is soft to firm, highly compressible and in a normally consolidated state. Constructing the embankment over this material will create stability as well as settlement problems.

### Excavation

All surficial organic material should be completely excavated. In addition, the silty clay should be removed as far as possible in order to minimize consolidation settlement. Excavation should be ideally carried down to the sand stratum, and be then brought up to the design grades with rockfill material. Considerations could be given to backfilling with free draining granular material if rockfill is not available. No dewatering is required during excavation and backfilling. For preliminary planning purposes, the estimated bottom of the soft clay stratum is given in Table 1.



Table 1

<u>Highway 17 Centreline</u>	<u>Estimated Bottom of Excavation Elevation</u>
14+500	202.5
14+550	197.0
14+600	192.5
14+650	187.5
14+700	186.5
14+750	189.0
14+800	190.0
 <u>Highway 17 Left 30 m</u>	
14+500	not required
14+550	198.5
14+600	191.5
14+650	187.5
14+700	186.5
14+750	not required
14+800	not required
 <u>Highway 17 Right 30 m</u>	
14+500	not required
14+550	not required
14+600	195.0
14+650	190.0
14+700	184.5
14+750	188.0
14+800	190.0

Excavation should be carried down to remove as much of the soft material as possible. The geometry of the excavation should be as shown in Figure 1. It is anticipated that the maximum depth of excavation is about 6 m to 7 m due to limitations in equipment. Based on the investigation results, the weak material between Sta. 14+600 and Sta. 14+710 approximately may extend beyond the excavation depth limits of a standard excavating machine. Any remaining soft material will have to be preloaded by the weight of the backfill and an additional surcharge to eliminate most of the consolidation settlement.

It is recommended that a 2 m rockfill surcharge be placed on top of the new embankment from Sta. 14+600 to 14+710 during the early stage of construction and be left there as long as possible. The surcharge should extend over the entire width of the roadway and this may necessitate minor steepening of the top portion of the embankment slope. The surcharge should taper off smoothly at a gradient of 5H:1V at both ends of the loaded area to minimize differential settlements. The preloading period should preferably be 3 months or longer. If not enough time is allowed for the preloading, excessive settlements would take place in the future and maintenance of the highway would be required.

#### Embankment Slopes

Following the removal of the soft clay and organic material to the sand stratum, the excavation should be backfilled and the embankment be constructed with rockfill or suitable fill material. If earth fill is used, the slopes should be formed at 2H:1V gradient with a 1 to 2 m wide berm incorporated at 9 m for embankment heights above 9 m to a maximum height of 18 m. In our opinion, 2 m wide berms may be more practical to construct. For rockfill slopes, they should be formed at 1.25H:1V up to 6 m and with a 2 m wide berm every 6 m up to a maximum height of 18 m so that no uninterrupted slope is greater than 6 m. Alternatively, rockfill slopes may be formed to 1.5H:1V gradients up to 10 m and with a 2 m wide berm every 10 m up to a maximum height of 18 m.

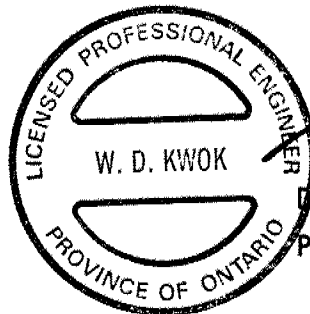
#### Foundation

Detailed recommendations for foundation construction are given in the Foundation Investigation Report W.P. 195-87-01 dated 91 04 25. As requested by the

Structural Section, deep foundation recommendations were also given in the report as an alternative to shallow footings. The current investigation has concluded that excavation for removal of soft clay is required in the approaches to the structure. It is therefore not recommended to employ deep foundations at this site due to concerns about possible differential settlements between the structure and the approaches.

#### MISCELLANEOUS

The field work for this investigation was carried out by D. Kwok, Project Foundation Engineer, and G. Dare, Engineering Student. The drilling equipment was owned and operated by Dominion Soil Investigation Ltd. The report was prepared by D. Kwok. It was reviewed by Mr. D. Dundas, Senior Foundation Engineer, and approved by Mr. M. Devata, Chief Foundation Engineer.



*[Signature]*  
D. Kwok, P.Eng.  
Project Foundation Engineer

*[Signature]*  
M. Devata, P.Eng.  
Chief Foundation Engineer

RECORD OF BOREHOLE No 1

1 OF 1

METRIC

W.P. 195-87-018 LOCATION McKellar Creek, Sta 14+500 Centreline ORIGINATED BY DK  
DIST 18 HWY 17 BOREHOLE TYPE Hollow Stem Auger COMPILED BY GD  
DATUM Geodetic DATE 1991 04 11 CHECKED BY DD

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT NATURAL MOISTURE CONTENT LIQUID LIMIT			UNIT WEIGHT 7 kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			'N' VALUES	20	40	60	80	100	W <sub>P</sub>	W		
203.6	Ground Surface															
0.0	Organic Clay and Silt, Trace of Gravel, Brown and Grey		1	SS	13											
202.2																
1.4	Fine Sand, Compact, Brown		2	SS	12											
201.3																
2.3	End of Borehole Probable Bedrock															

# RECORD OF BOREHOLE No 2

1 OF 1

METRIC

W.P. 195-87-01B LOCATION McKellar Creek, Sta 14+525 Lt. 30m ORIGINATED BY GD  
 DIST 18 HWY 17 BOREHOLE TYPE Hollow Stem Auger COMPILED BY GD  
 DATUM Geodetic DATE 1991 04 11 CHECKED BY DD

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT NATURAL MOISTURE CONTENT LIQUID LIMIT			UNIT WEIGHT 7 kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			'N' VALUES	20	40	60	80	100	W <sub>p</sub>	W		
203.1	Ground Surface															
0.0	Fine to Medium Sand, Some Gravel Silt, Trace Sand and Clay, Compact Brown, Loose		1	SS	17											
200.7			2	SS	7											
2.4	End of Borehole Probable Bedrock															

# RECORD OF BOREHOLE No 3

1 OF 1

METRIC

W.P. 195-87-018 LOCATION McKellar Creek, Sta. 14+575 Centreline ORIGINATED BY GD  
 DIST 18 HWY 17 BOREHOLE TYPE Hollow Stem Augers COMPILED BY OK  
 DATUM Geodetic DATE 1991 04 12 CHECKED BY DD

SOIL PROFILE			SAMPLES			GROUND WATER • CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT w <sub>p</sub>	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w <sub>L</sub>	UNIT WEIGHT γ kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			20	40					
197.6	Ground Surface													
0.0	Silty Clay, Some Organics Soft, Brown		1	SS	3									
194.9			2	TW	PH									
2.7	Fine to Medium Sand Brown, Loose		3	SS	8									
192.9			4	SS	70									
4.7	End of Borehole • Silty Sand with Gravel													

# RECORD OF BOREHOLE No 4

1 OF 1

METRIC

W.P. 195-87-01B LOCATION McKellar Creek, Sta 14+636.5 Rt 30 m ORIGINATED BY GD  
 DIST 18 HWY 17 BOREHOLE TYPE Hollow Stem Auger, Cone COMPILED BY DK  
 DATUM Geodetic DATE 91 04 11 CHECKED BY DD

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT 20 40 60 80 100	SHEAR STRENGTH kPa ○ UNCONFINED + FIELD VANE ● QUICK TRIAXIAL x LAB VANE 10 20 30 40 50	PLASTIC LIMIT W <sub>P</sub> NATURAL MOISTURE CONTENT W LIQUID LIMIT W <sub>L</sub> WATER CONTENT (%) 20 40 60	UNIT WEIGHT γ kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES							
198.5	Ground Surface											
0.0			1	SS	7		198				18.5	
	Brown Grey Silty Clay to Clay Soft to Firm		2	TW	PH		196				16.2	
			3	TW	PH		194				15.9	
191.6			4	SS	3		192					
6.9	Fine to Coarse Sand, Traces of Clay Very Loose to Compact		5	SS	2		190					
	Sandy Silt with Gravel some rock fragment		6	SS	13							
188.6			7	SS	80							
9.9	End of Borehole Probable Bedrock											

# RECORD OF BOREHOLE No 5

1 OF 1

METRIC

W.P. 195-87-018 LOCATION McKellar Creek, Sta 14+637.5 Centreline ORIGINATED BY DK  
 DIST 18 HWY 17 BOREHOLE TYPE Hollow Stem, Cone COMPILED BY DK  
 DATUM Geodetic DATE 91 04 09 CHECKED BY DD

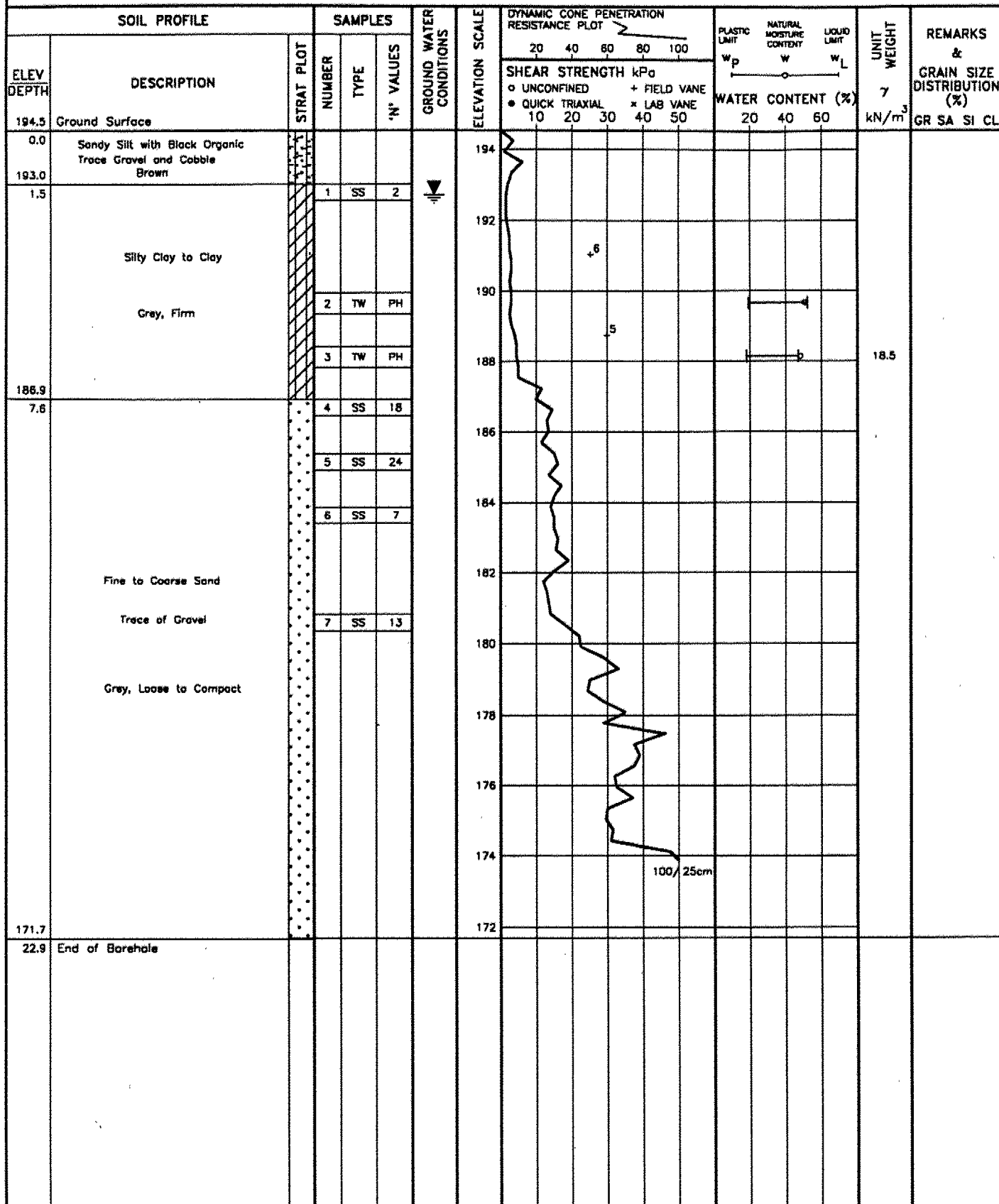
SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC NATURAL LIQUID LIMIT MOISTURE CONTENT LIMIT			UNIT WEIGHT $\gamma$ kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			20 40 60 80 100	W <sub>p</sub> W W <sub>L</sub>	WATER CONTENT (%)	20 40 60			
195.3	Ground Surface													
0.0	Organic Silty Sand													
194.3	Some Rootlets, Black													
1.0	Brown Grey		1	SS	4									
	Silty Clay to Clay		2	TW	PH									
	Soft to Firm		3	TW	PH									
			4	SS	2									
188.5														
6.9	Fine to Medium Sand		5	SS	0									
	Some Silt, Trace of Gravel													
186.4	Loose, Grey		6	SS	44									
9.0	End of Borehole Probable Bedrock													



# RECORD OF BOREHOLE No 6

1 OF METRIC

W.P. 195-87-01B LOCATION McKellar Creek, Sta 14+705.7 Lt 30 m ORIGINATED BY DK  
 DIST 18 HWY 17 BOREHOLE TYPE Hollow Stem Auger, Cone COMPILED BY GD  
 DATUM Geodetic DATE 1991 04 10 CHECKED BY DD



# RECORD OF BOREHOLE No 7

1 OF 1

METRIC

W.P. 195-87-01B LOCATION McKellar Creek, Sta 14+675 Centreline ORIGINATED BY DK  
 DIST 18 HWY 17 BOREHOLE TYPE Hollow Stem Auger, Cone COMPILED BY GD  
 DATUM Geodetic DATE 1991 04 09 CHECKED BY DD

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT w <sub>p</sub>	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w <sub>L</sub>	UNIT WEIGHT γ kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			20 40 60 80 100						
195.2	Ground Surface													
0.0	Organic Silty Sand Some Wood Fibres and Gravel Black		1	SS	7		194							
193.6			2	SS	1		192							
1.5	Silty Clay to Clay  Soft to Firm  Grey		3	TW	PH		190						17.3	
			4	TW	PH		188							
185.3			5	SS	2		186							
8.9			6	SS	2		184							
	Fine Grained		7	SS	5		182							
	Fine to Medium Sand		8	SS	1		180							
	Grey, Loose		9	SS	4									
			10	SS	3									
178.4														
16.8	End of Borehole Probable Bedrock													

+3, x<sup>3</sup>: Numbers refer to  
Sensitivity

20  
15-5 (%) STRAIN AT FAILURE  
10

# RECORD OF BOREHOLE No 8

1 OF 1

METRIC

W.P. 195-87-018 LOCATION McKellar Creek, Sta 14+700 Rt 30 m ORIGINATED BY GD  
DIST 18 HWY 17 BOREHOLE TYPE Hollow Stem Auger, Cone COMPILED BY DK  
DATUM Geodetic DATE 1991 04 10 CHECKED BY DD

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W <sub>p</sub>	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W <sub>L</sub>	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)	
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			20	40						60
190.6	Ground Surface														
0.0	Organic Clay with Rootlets Grey		1	SS	15		190								
189.1			2	SS	5										
1.5	Trace of Organic														
	Silty Clay														
	Grey, Firm		3	TW	PH										
184.5															
6.1			4	SS	6										
	Fine to Coarse Sand														
	Brown and Grey														
	Loose to Compact		5	SS	8										
	with Gravel and Rock Fragment														
175.6															
15.0	End of Borehole														

# RECORD OF BOREHOLE No 9

1 OF 1

METRIC

W.P. 195-87-018 LOCATION McKellar Creek, Sta 14+770.6 Rt 30 m ORIGINATED BY DK  
 DIST 18 HWY 17 BOREHOLE TYPE Hollow Stem Auger, Cone COMPILED BY DK  
 DATUM Geodetic DATE 1991 04 12 CHECKED BY DD

SOIL PROFILE			SAMPLES			GROUND WATER % CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT NATURAL MOISTURE CONTENT LIQUID LIMIT			UNIT WEIGHT $\gamma$ kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			20 40 60 80 100	W <sub>p</sub> W W <sub>L</sub>	WATER CONTENT (%)	20 40 60			
191.6	Ground Surface													
0.0	Organic Silty Sand Numerous Woodchips		1	SS	23									
190.0			2	SS	15									
1.5	Coarse Sand and Gravel Brown and Grey, Compact		3	SS	15									
	Some Silt, Grey		4	SS	8									
	Medium to Coarse Sand Grey and Brown		5	SS	19									
			6	SS	14									
	with Cobbles and Boulders													
180.4														
11.1	End of Borehole													

## METRIC

[illegible]

20  
15-5 (X) STRAIN AT FAILURE  
10

RECORD OF BOREHOLE No 11

1 of 1

METRIC

W.P. 195-87-01B LOCATION McKellar Creek, Sta 14+563.38 Rt 14.45 m ORIGINATED BY DK  
DIST 18 HWY 17 BOREHOLE TYPE Hollow Stem Auger, Cone COMPILED BY DK  
DATUM Geodetic DATE 1991 04 11 CHECKED BY DD

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT 20 40 60 80 100	PLASTIC LIMIT W <sub>P</sub>	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W <sub>L</sub>	UNIT WEIGHT γ kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES								
197.9	Ground Surface												
0.0 197.1	Silty Clay with Organics Brown and Black												
0.8	Sand and Silt Brown		1	SS	10								
195.8	Compact to Very Dense		2	SS	45	/25cm	196						
2.3	End of Borehole Probable Bedrock												

# RECORD OF BOREHOLE No 12

1 OF 1

METRIC

W.P. 195-87-018 LOCATION McKellar Creek, Sta 14+600 Lt 30 m ORIGINATED BY GD  
 DIST 18 HWY 17 BOREHOLE TYPE Hollow Stem Auger, Cone COMPILED BY DK  
 DATUM Geodetic DATE 1991 04 12 CHECKED BY DD



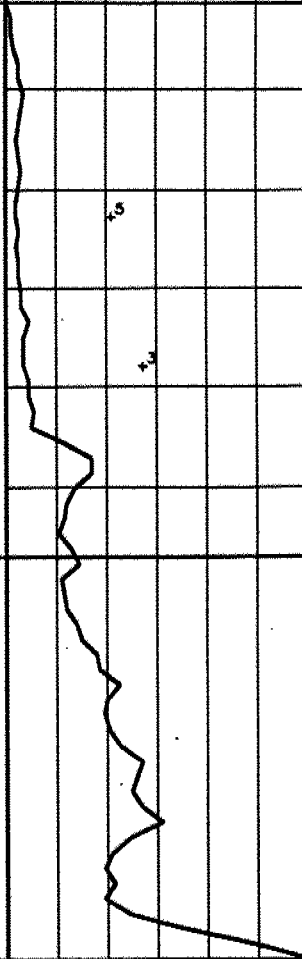



SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W <sub>p</sub>	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W <sub>L</sub>	UNIT WEIGHT γ kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			20	40					
188.0	Ground Surface													
0.0	Organic Sand		1	SS	8									
197.1														
0.9			2	SS	2									
	Brown													
	Grey													
	Silty Clay		3	TW	PH									
	Soft to Firm		4	SS	7									
191.0			5	SS	7.8									
190.4	Sandy Silt with Gravel, Grey													
7.8	End of Borehole Probable Bedrock													

# RECORD OF BOREHOLE No 13

1 OF 1

METRIC

W.P. 195-87-018 LOCATION McKellar Creek, Sta 14+885.8 Lt 30 m ORIGINATED BY GD  
 DIST 18 HWY 17 BOREHOLE TYPE Hollow Stem Auger, Cone COMPILED BY OK  
 DATUM Geodetic DATE 1991 04 12 CHECKED BY DD

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT w <sub>p</sub>	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w <sub>L</sub>	UNIT WEIGHT γ kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL			
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			20 40 60 80 100	SHEAR STRENGTH kPa ○ UNCONFINED      + FIELD VANE ● QUICK TRIAXIAL    x LAB VANE						WATER CONTENT (%) 20 40 60		
185.7	Ground Surface																
0.0	Silty Clay with Organics Grey to Dark Grey, Soft		1	SS	3								16.7				
			2	SS	4												
192.7			3	SS	1												
3.0			4	SS	1												
	Silty Clay to Clay Soft to Firm Grey		5	TW	PH												
186.8	Clayey Silt, Trace Sand		6	SS	10												
9.1	Fine to Coarse Sand Grey Loose to Compact		7	SS	6												
184.6			8	SS	13												
11.1	End of Borehole																
	Probable Sand																
176.5																	
19.2	End of Cone Test																





# RECORD OF BOREHOLE No 15

1 OF 1

METRIC

W.P. 195-87-018 LOCATION McKellar Creek, Sta 14+725 Lt 30 m ORIGINATED BY DK  
 DIST 18 HWY 17 BOREHOLE TYPE Hollow Stem Auger COMPILED BY DK  
 DATUM Geodetic DATE 1991 04 12 CHECKED BY DD

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT NATURAL MOISTURE CONTENT			UNIT WEIGHT 7 kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			20	40	60	80	100	w <sub>p</sub>	w	w <sub>L</sub>		
194.5	Ground Surface																
0.0	Coarse Sand Cobble and Boulder		1	SS	7												
	Silty Clay																
	Grey																
	Firm																
190.8			2	TW	PH												
190.2	Medium to Coarse Sand		3	SS	1												
4.3	End of Borehole																

# RECORD OF BOREHOLE No 1A

1 OF 1

METRIC

W.P. 195-87-01 LOCATION Sta. 14 + 738.0, 24.4 LT. Line B ORIGINATED BY BL  
 DIST 18 HWY 17 BOREHOLE TYPE Cone Test, Hollow-Stem Auger, N Casing COMPILED BY BL  
 DATUM Geodetic DATE 90 08 21 CHECKED BY DD

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT w <sub>p</sub>	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w <sub>L</sub>	UNIT WEIGHT γ KN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			20	40					
193.0	Ground Surface		1	CS	*									
0.0			2	CS	*									
			3	CS	*									
			4	SS	2									
			5	SS	2									
			6	SS	2									
			7	SS	2									
			8	SS	2									
			9	SS	12									
			10	SS	9									
			11	SS	6									
			12	SS	4									
			13	SS	25									
			14	SS	12									
177.9			15	SS	36									
15.1	End of Borehole													
176.8														
16.2	End of Cone Test													
	• Grab sample taken by backhoe													

# RECORD OF BOREHOLE No 2A

1 OF 1

METRIC

W.P. 195-97-01 LOCATION Stn. 14 + 736.0, C/L Line B ORIGINATED BY BL  
 DIST 18 HWY 17 BOREHOLE TYPE Cone Test, Hollow-Stem Auger, N Casing COMPILED BY BL  
 DATUM Geodetic DATE 90 08 20 CHECKED BY DD

SOIL PROFILE			SAMPLES		GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W <sub>p</sub>	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W <sub>L</sub>	UNIT WEIGHT 7 kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			'N' VALUES	20					
192.7	Ground Surface												
0.0	Occ. Cobbles And Boulders		1	CS									
	Silty Clay		2	SS	9								0 2 34 64
	Trace Sand		3	SS	4								
	Soft To Firm		4	SS	2								
188.6													
4.1	Silty Sand		5	SS	9								0 87 5 8
	Trace Clay		6	SS	7								
	Loose To Compact		7	SS	7								0 81 15 4
			8	SS	17								
183.2	Occ. Gravel Very Dense		9	SS	63								
9.5	End of Borehole												
181.9													
10.8	End of Cone Test Probable Bedrock												
	* Grab sample taken by backhoe												

# RECORD OF BOREHOLE No 3A

1 OF 1

METRIC

W.P. 195-87-01 LOCATION Sta. 14 + 720.0, 47.0 RT, Line B ORIGINATED BY BL  
 DIST 18 HWY 17 BOREHOLE TYPE Cone Test, Hollow-Stem Auger COMPILED BY BL  
 DATUM Geodetic DATE 90 08 22 CHECKED BY DD

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W <sub>p</sub>	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W <sub>L</sub>	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			20 40 60 80 100	20 40 60 80 100					
190.7	Ground Surface												
0.0			1	PS									
	Silty Sand Occ. Organics Compact		2	SS		190							
			3	TW									
			4	TW		188							0 0 72 28
	Silty Clay		5	TW									
	Trace Sand		6	SS		186							0 1 50 49
	Soft To Firm		7	SS									
			8	SS		184							
182.9			9	SS									0 65 33 2
7.8			10	SS		182							
	Silty Sand		11	SS		180							
	Trace Clay												
	Compact		12	SS									1 78 12 5
178.1													
12.8	End of Borehole												
172.1													
18.6	End of Cone Test = Grab sample taken by backhoe												

+3, x5: Numbers refer to  
Sensitivity

20  
15-25 (%) STRAIN AT FAILURE  
10

# RECORD OF BOREHOLE No 4A

1 OF 1

METRIC

W.P. 195-87-01 LOCATION Sta. 14 + 727.8, 23.6 RT. Line B ORIGINATED BY BL  
 DIST 18 HWY 17 BOREHOLE TYPE Cone Test COMPILED BY BL  
 DATUM Geodetic DATE 90 08 22 CHECKED BY DD

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT NATURAL MOISTURE CONTENT LIQUID LIMIT			UNIT WEIGHT	REMARKS & GRAIN SIZE DISTRIBUTION (%)
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			20	40	60	80	100		
181.3	Ground Surface													
0.0														
	Probable Silty Clay													
	Soft To Firm													
186.4														
4.9														
	Probable Silty Sand													
	Loose To Compact													
176.4														
14.9	End of Cone Test										120	10cm		

1 OF 1

METRIC

LOCATION Sta. 14 + 740.0, 14.0 LT. Line B

ORIGINATED BY SL

BOREHOLE TYPE Cone Test

COMPILED BY BL

DATUM Geodetic

DATE 90 08 22

CHECKED BY     DC    

+3, x5: Numbers refer to Sensitivity

## EXPLANATION OF TERMS USED IN REPORT

**N VALUE:** THE STANDARD PENETRATION TEST (SPT) N VALUE IS THE NUMBER OF BLOWS REQUIRED TO CAUSE A STANDARD 51mm O.D. SPLIT BARREL SAMPLER TO PENETRATE 0.3m INTO UNDISTURBED GROUND IN A BOREHOLE WHEN DRIVEN BY A HAMMER WITH A MASS OF 63.5kg, FALLING FREELY A DISTANCE OF 0.76m. FOR PENETRATIONS OF LESS THAN 0.3m N VALUES ARE INDICATED AS THE NUMBER OF BLOWS FOR THE PENETRATION ACHIEVED. AVERAGE N VALUE IS DENOTED THUS  $\bar{N}$ .

**DYNAMIC CONE PENETRATION TEST:** CONTINUOUS PENETRATION OF A CONICAL STEEL POINT (51mm O.D. 60° CONE ANGLE) DRIVEN BY 475 J IMPACT ENERGY ON 'A' SIZE DRILL RODS. THE RESISTANCE TO CONE PENETRATION IS MEASURED AS THE NUMBER OF BLOWS FOR EACH 0.3m ADVANCE OF THE CONICAL POINT INTO THE UNDISTURBED GROUND.

SOILS ARE DESCRIBED BY THEIR COMPOSITION AND CONSISTENCY OR DENSENESS.

**CONSISTENCY:** COHESIVE SOILS ARE DESCRIBED ON THE BASIS OF THEIR UNDRAINED SHEAR STRENGTH ( $c_u$ ) AS FOLLOWS:

$c_u$ (kPa)	0 - 12	12 - 25	25 - 50	50 - 100	100 - 200	> 200
	VERY SOFT	SOFT	FIRM	STIFF	VERY STIFF	HARD

**DENSENESS:** COHESIONLESS SOILS ARE DESCRIBED ON THE BASIS OF DENSENESS AS INDICATED BY SPT N VALUES AS FOLLOWS:

N (BLOWS/0.3m)	0 - 5	5 - 10	10 - 30	30 - 50	> 50
	VERY LOOSE	LOOSE	COMPACT	DENSE	VERY DENSE

ROCKS ARE DESCRIBED BY THEIR COMPOSITION AND STRUCTURAL FEATURES AND / OR STRENGTH.

**RECOVERY:** SUM OF ALL RECOVERED ROCK CORE PIECES FROM A CORING RUN EXPRESSED AS A PERCENT OF THE TOTAL LENGTH OF THE CORING RUN.

**MODIFIED RECOVERY:** SUM OF THOSE INTACT CORE PIECES, 100mm+ IN LENGTH EXPRESSED AS A PERCENT OF THE LENGTH OF THE CORING RUN. THE ROCK QUALITY DESIGNATION (RQD), FOR MODIFIED RECOVERY, IS:

RQD (%)	0 - 25	25 - 50	50 - 75	75 - 90	90 - 100
	VERY POOR	POOR	FAIR	GOOD	EXCELLENT

**JOINTING AND BEDDING:**

SPACING	50mm	50 - 300mm	0.3m - 1m	1m - 3m	> 3m
JOINTING	VERY CLOSE	CLOSE	MOD. CLOSE	WIDE	VERY WIDE
BEDDING	VERY THIN	THIN	MEDIUM	THICK	VERY THICK

## ABBREVIATIONS AND SYMBOLS

### FIELD SAMPLING

S S	SPLIT SPOON	T P	THINWALL PISTON
W S	WASH SAMPLE	O S	OSTERBERG SAMPLE
S T	SLOTTED TUBE SAMPLE	R C	ROCK CORE
B S	'BLOCK' SAMPLE	P H	T W ADVANCED HYDRAULICALLY
C S	CHUNK SAMPLE	P M	T W ADVANCED MANUALLY
T W	THINWALL OPEN	F S	FOIL SAMPLE

### STRESS AND STRAIN

$u_w$	kPa	PORE WATER PRESSURE
$r_u$	1	PORE PRESSURE RATIO
$\sigma$	kPa	TOTAL NORMAL STRESS
$\sigma'$	kPa	EFFECTIVE NORMAL STRESS
$\tau$	kPa	SHEAR STRESS
$\sigma_1, \sigma_2, \sigma_3$	kPa	PRINCIPAL STRESSES
$\epsilon$	%	LINEAR STRAIN
$\epsilon_1, \epsilon_2, \epsilon_3$	%	PRINCIPAL STRAINS
E	kPa	MODULUS OF LINEAR DEFORMATION
G	kPa	MODULUS OF SHEAR DEFORMATION
$\mu$	1	COEFFICIENT OF FRICTION

### MECHANICAL PROPERTIES OF SOIL

$m_v$	kPa <sup>-1</sup>	COEFFICIENT OF VOLUME CHANGE
$C_c$	1	COMPRESSION INDEX
$C_s$	1	SWELLING INDEX
$\alpha$	1	RATE OF SECONDARY CONSOLIDATION
$c_v$	m <sup>2</sup> /s	COEFFICIENT OF CONSOLIDATION
H	m	DRAINAGE PATH
$T_v$	1	TIME FACTOR
U	%	DEGREE OF CONSOLIDATION
$\sigma'_{vo}$	kPa	EFFECTIVE OVERBURDEN PRESSURE
$\sigma'_p$	kPa	PRECONSOLIDATION PRESSURE
$\tau_f$	kPa	SHEAR STRENGTH
$c'$	kPa	EFFECTIVE COHESION INTERCEPT
$\phi'$	-°	EFFECTIVE ANGLE OF INTERNAL FRICTION
$c_u$	kPa	APPARENT COHESION INTERCEPT
$\phi_u$	-°	APPARENT ANGLE OF INTERNAL FRICTION
$\tau_R$	kPa	RESIDUAL SHEAR STRENGTH
$\tau_r$	kPa	REMOULDED SHEAR STRENGTH
$S_t$	1	SENSITIVITY = $\frac{c_u}{\tau_r}$

### PHYSICAL PROPERTIES OF SOIL

$\rho_s$	kg/m <sup>3</sup>	DENSITY OF SOLID PARTICLES	e	1, %	VOID RATIO	$e_{min}$	1, %	VOID RATIO IN DENSEST STATE
$\gamma_s$	kN/m <sup>3</sup>	UNIT WEIGHT OF SOLID PARTICLES	n	1, %	POROSITY	$I_D$	1	DENSITY INDEX = $\frac{e_{max} - e}{e_{max} - e_{min}}$
$\rho_w$	kg/m <sup>3</sup>	DENSITY OF WATER	w	1, %	WATER CONTENT	D	mm	GRAIN DIAMETER
$\gamma_w$	kN/m <sup>3</sup>	UNIT WEIGHT OF WATER	$S_r$	%	DEGREE OF SATURATION	$D_n$	mm	n PERCENT - DIAMETER
$\rho$	kg/m <sup>3</sup>	DENSITY OF SOIL	$w_L$	%	LIQUID LIMIT	$C_u$	1	UNIFORMITY COEFFICIENT
$\gamma$	kN/m <sup>3</sup>	UNIT WEIGHT OF SOIL	$w_p$	%	PLASTIC LIMIT	h	m	HYDRAULIC HEAD OR POTENTIAL
$\rho_d$	kg/m <sup>3</sup>	DENSITY OF DRY SOIL	$w_s$	%	SHRINKAGE LIMIT	q	m <sup>3</sup> /s	RATE OF DISCHARGE
$\gamma_d$	kN/m <sup>3</sup>	UNIT WEIGHT OF DRY SOIL	$I_p$	%	PLASTICITY INDEX = $w_L - w_p$	v	m/s	DISCHARGE VELOCITY
$\rho_{sat}$	kg/m <sup>3</sup>	DENSITY OF SATURATED SOIL	$I_L$	1	LIQUIDITY INDEX = $\frac{w - w_p}{I_p}$	i	1	HYDRAULIC GRADIENT
$\gamma_{sat}$	kN/m <sup>3</sup>	UNIT WEIGHT OF SATURATED SOIL	$I_C$	1	CONSISTENCY INDEX = $\frac{w_L - w}{I_p}$	k	m/s	HYDRAULIC CONDUCTIVITY
$\rho'$	kg/m <sup>3</sup>	DENSITY OF SUBMERGED SOIL	$e_{max}$	1, %	VOID RATIO IN LOOSEST STATE	j	kN/m <sup>2</sup>	SEEPAGE FORCE
$\gamma'$	kN/m <sup>3</sup>	UNIT WEIGHT OF SUBMERGED SOIL						



## APPENDIX

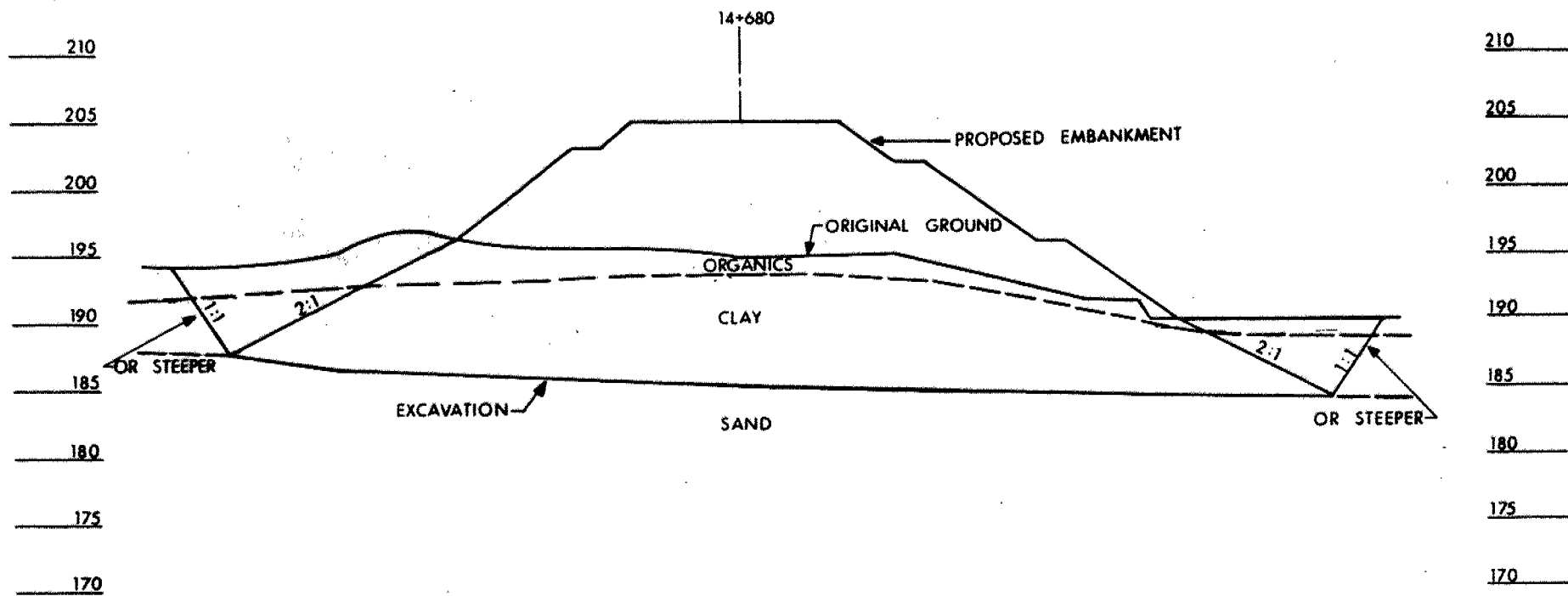


Fig 1 - EXCAVATION GEOMETRY

HWY No 17			DIST 18
SUBM'D DK	CHECKED	DATE 1991 08 01	SITE 48E-46
DRAWN KM	CHECKED	APPROVED	DWG 1958701 (B)