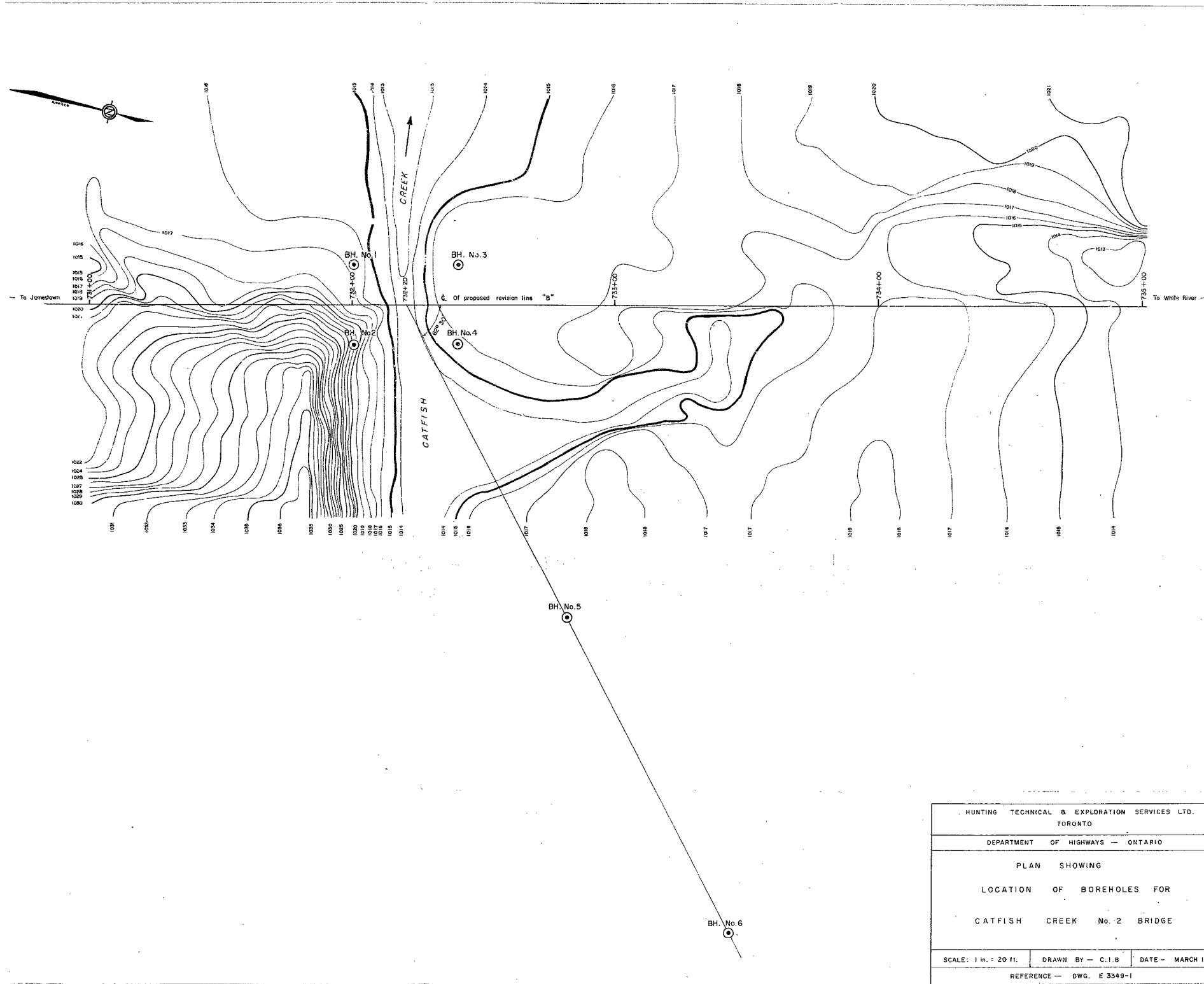


58-F-289C  
W.P. 931-57  
Hwy. #17  
CATFISH CREEK  
#2 BRIDGE



# HUNTING TECHNICAL AND EXPLORATION SERVICES LIMITED

RESOURCES AND DEVELOPMENT STUDIES

1450 O'CONNOR DRIVE  
TORONTO 16, CANADA  
PLYMOUTH 5-1141

MONTRÉAL  
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CALGARY  
OTTAWA

NEW YORK  
CARACAS  
RIO DE JANEIRO

March 24th., 1958.

WP-931-57

Mr. S. McCombie,  
Bridge Officer,  
Department of Highways - Ontario.

Dear Sir;

We are transmitting herewith four (4) copies of our report entitled "Preliminary Site Investigation for the Proposed Catfish Creek No. 2 Bridge".

We trust that this report will be to your satisfaction and that we may have the pleasure of working for you again.

Yours very truly,

HUNTING TECHNICAL AND EXPLORATION SERVICES LIMITED

D. R. Lueder,  
Chief,  
Engineering Division.

DRL/ko



ASSOCIATE OF THE WORLD-WIDE HUNTING GROUP

*BR717*

58-F-289C

W.P. 931-57

**PRELIMINARY SITE INVESTIGATION  
for the  
PROPOSED CATFISH CREEK NO. 2 BRIDGE  
near  
JAMESTOWN, ONTARIO**

**for the  
DEPARTMENT OF HIGHWAYS - ONTARIO**

**by the  
ENGINEERING DIVISION  
HUNTING TECHNICAL AND EXPLORATION SERVICES LIMITED**

**March, 1958**

**Toronto, Ontario.**

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### Section 1.1

#### PURPOSE OF REPORT

##### 1.11 General

The purpose of this report is to present the results of a subsurface soil investigation for the proposed Catfish Creek No. 2 Bridge near Jamestown, Ontario.

## Section 1.2

### DISCUSSION OF PROCEDURES

#### 1.21 Location of Boreholes

The borehole locations for this investigation were established by Department of Highways' surveyors. At the completion of the work, each borehole was marked with a large stake denoting the hole number for future reference. The borehole locations are shown on the plan in Appendix 1.51.

#### 1.22 Subsurface Drilling and Sampling

A primary program, specified by the client, of 4 soil borings was initiated in the vicinity of the proposed site of the Catfish Creek No. 2 Bridge. The program was later enlarged to include 2 additional holes along the route of a proposed channel improvement in connection with the bridge construction.

A skid mounted, hydraulic head junior Longyear diamond drilling rig was used on this project. All boring and sampling operations were completed by an experienced soil sampling crew under the supervision of a geologist experienced in soil sampling procedures.

In the first boring, an attempt was made to advance the hole by the standard wash boring method. In this procedure, drill casing is driven into the soil by a 350 lb. hammer to a depth of 5 feet. All the contained soil is thoroughly washed out to the bottom of the casing. Sampling tools are then lowered on the ends of the rods to the bottom of the hole. The sample is taken and the sampling tools removed from the hole. An additional 5 foot length of casing is added and the procedure is repeated. However, in the loose material in the first hole, it was found that the impact method of advancing the casing caused the material to "flow" into the casing. As a result, the soil at the bottom of the casing was considered unlikely to be in its natural state. Thus, the field boring supervisor decided to advance the casing by diamond drilling techniques. In this procedure, the bottom end of the casing is fitted with a diamond shoe bit, and is fed into the ground by the diamond drill. Water is used in this method to clean and cool the diamond drill bit as well as carry the sludge out of the hole during the actual drilling operations. It was found that this method allowed the hole to be advanced with a minimum of disturbance to the loose sand. An additional advantage with this method is that, whenever large boulders or glacial till were encountered they were easily penetrated with the diamond shoe bit.

Wherever possible, split spoon samples were obtained in cohesionless materials by means of a 2 inch O.D. standard split spoon sampler. The standard penetration test using a 140 lb. hammer falling 30 inches was recorded for each foot of sample taken with the split spoon sampler. Great difficulties were encountered in obtaining a split spoon sample in the loose sand, even though trap valves, spring type sample retainers, and basket shoes were used to help retain the sample. In this material, it was found necessary to take the penetration tests with the split spoon sampler then lower a side slit sampler to recover the sample.

### 1.23 Soil Testing

All disturbed representative samples, i.e., split spoon samples and side slit samples, were visually examined and classified on the site, then placed in jars and forwarded to the engineering office. Selective samples from each strata were forwarded to the laboratory as a check on the visual field classification.

The results of all tests are given in the Appendices. The laboratory tests on the samples were performed by:

Donald Inspection Ltd.,  
340 Richmond St. West,  
Toronto, Ontario.

### Section 1.3

#### DISCUSSION OF SITE

##### 1.31 Geographic Location

The proposed bridge site is located on Catfish Creek at the proposed crossing of the King's Highway No. 17, (revision line "B"). The site is in the District of Algoma approximately 9 miles north of the village of Jamestown. The bridge site location is shown on the airphoto in Appendix 1.54.

##### 1.32 Bedrock Geology

The bedrock in the vicinity of the bridge site is entirely Precambrian in age, and appears to consist generally of assorted gneisses and greywacke.

### 1.33 Overburden Geology

The landform in the general area of the proposed site consists of a relatively flat river valley bounded on the east and west by Precambrian hills of low relief under a shallow to moderately deep glacial till mantle. The valley is partially filled with post-glacial lacustrine deposits of a lake that once filled the entire valley. Catfish Lake is one of the remnants of this glacial lake (see Appendix 1.54).

The soil deposits within the valley are typical of a post-glacial emergent landform. A glacial till overlies the bedrock which in turn is overlain by glacio-lacustrine deposits. On top of these we find beach or glacio-fluvial material as shown in the soil profiles in Appendix 1.52.

### 1.34 Soil Conditions

Soils encountered at the site consisted primarily of three structural types. Overlying the bedrock, a medium dense to dense glacial till was found. A medium dense sand with silt strata was encountered on top of the till. The sand with silt was in turn overlain by several feet of loose sand topped by a few feet of loose sand and gravel.

The physical properties of each type of soil encountered at the site are summarized below in the order of their occurrence above bedrock.

#### 1. - Medium Dense to Dense Gravel with Sand, some Silt (till texture)

This soil was encountered immediately above bedrock over the entire site. The physical properties for this soil are listed below:

##### Gradation (M.I.T. Classification)

Gravel        50% - 67%

Sand        22% - 35%

Silt        10% - 16%

Specific Gravity (Ave.)        2.68 (range 2.66 to 2.70)

Average Depth        21.2 feet

Top Elevation Range        965 feet to 982 feet

Bottom Elevation Range        946 feet to 955 feet

Penetration Resistance average        33 blows/foot

Range        23 to 50 blows/foot

Nomenclature        Medium dense to dense grey gravel with sand, some silt, occasional boulder (till texture)

#### 2. Medium Dense Sand with Silt

This material overlies the glacial till and is found in all boreholes except No. 3. This stratum contains a layer of sand. However, for structural purposes, in this investigation, they can be treated as one stratum. The physical properties for this soil are listed below:

##### Gradation (M.I.T. Classification)

Gravel        None

Sand        65% to 87%

Silt        13% to 35%

Specific Gravity (Ave.)	2.64 (range 2.63 to 2.66)
Average Depth	28.8 feet
Top Elevation Range	992 feet to 998 feet
Bottom Elevation Range	965 feet to 970 feet
Penetration Resistance average	18 blows/foot
Range	10 to 38 blows/foot
Nomenclature	Medium dense grey sand with silt.

### 3. Loose Sand

This material overlies the medium dense sand with silt and is found in all the boreholes. The physical properties for this stratum are listed below:

#### Gradation (M.I.T. Classification)

Gravel	0% to 5%
Sand	92% to 100%
Silt	0% to 8%
Specific Gravity (Ave.)	2.66 (range 2.62 to 2.70)
Average Depth	17.5 feet
Top Elevation Range	1005 feet to 1012 feet
Bottom Elevation Range	982 feet to 999 feet
Penetration Resistance average	3.75 blows/foot
Range	1 to 12 blows/foot
Nomenclature	Loose grey sand, trace of silt.

### 4. Loose Gravel with Sand

This material is found at ground surface as a capping on top of the loose sand. The physical properties for this material are listed below:

**Gradation (M.I.T. Classification)**

Gravel	69%
Sand	21%
Silt	None
Specific Gravity	2.68
Average Depth	7 feet
Top Elevation Range	1015 feet to 1020 feet
Bottom Elevation Range	1005 feet to 1012 feet
Penetration Resistance Average	6 blows/foot
Range (unfrozen state)	3 to 10 blows/foot
Nomenclature	loose brown gravel, some sand.

### 1.35 Comments

Our understanding of the initial bridge design is that abutments are contemplated at chainages 732+00 and 732+40. The approaches to the bridge are to be made on fill, contained and protected by wing walls.

With reference to this proposal, we would like to make the following comments for your consideration:

1. Considering the possibility of using spread footings for the base of the abutments and wing walls, we estimate the bearing capacity of the soil beneath the base of the footing to be in the order of 350 lbs. per square foot. It can therefore be concluded that the soil does not have adequate bearing capacity for this type of foundation.
2. It appears that it will be necessary to support the bridge abutments and wing walls on pile foundations. Since pipe piles and H piles are rarely used unless they reach a stratum of exceptionally high supporting capacity, and the soil profile does not indicate an exceptionally firm strata within a reasonable depth from surface, we recommend that consideration be given to friction piles of the compaction type for the abutment and wing wall foundations.
3. We have assumed that wooden friction piles will prove to be the most economical and convenient type of pile to use on this structure. As the ultimate bearing capacity of piles in sand increases roughly with the square of the depth of penetration, we assume that the wooden piles will be driven as deep as possible without injuring the pile.

Assuming that the pile foundation will be designed on the basis of pile driving formula, in order to assist the designer in determining the required pile length, we have enclosed a graph (Fig. 1) roughly indicating the depth of pile penetration versus the blows per inch for the loose sand and for the medium dense sand shown in the soil profiles.

4. With reference to horizontal loads on the vertical piles beneath the structure, we would not recommend the use of loads greater than 1000 lbs. at the top of each pile.

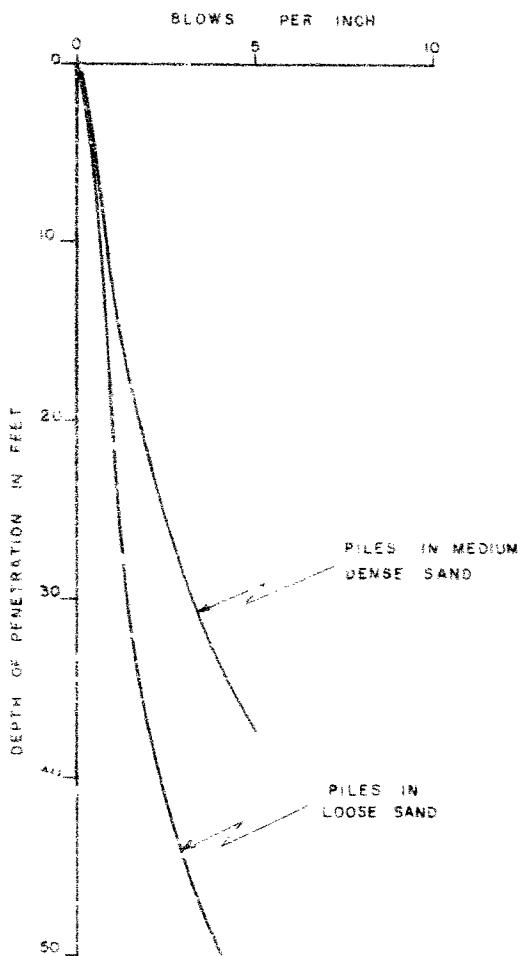


FIG. 1

RELATION BETWEEN BLOWS PER INCH OF PENETRATION

AND TOTAL DEPTH OF PENETRATION FOR WOOD PILES

after TERZAGHI and PECK

Section 1.4PERSONNEL

The field work was performed under the supervision of  
Mr. D. G. Fraser.

This report was written by J. Kilgour, P. Eng., with the  
assistance of P. Arkema, P. Eng.

D. R. Lueder, P. Eng., provided administrative supervision  
of the work.

Section 1.5

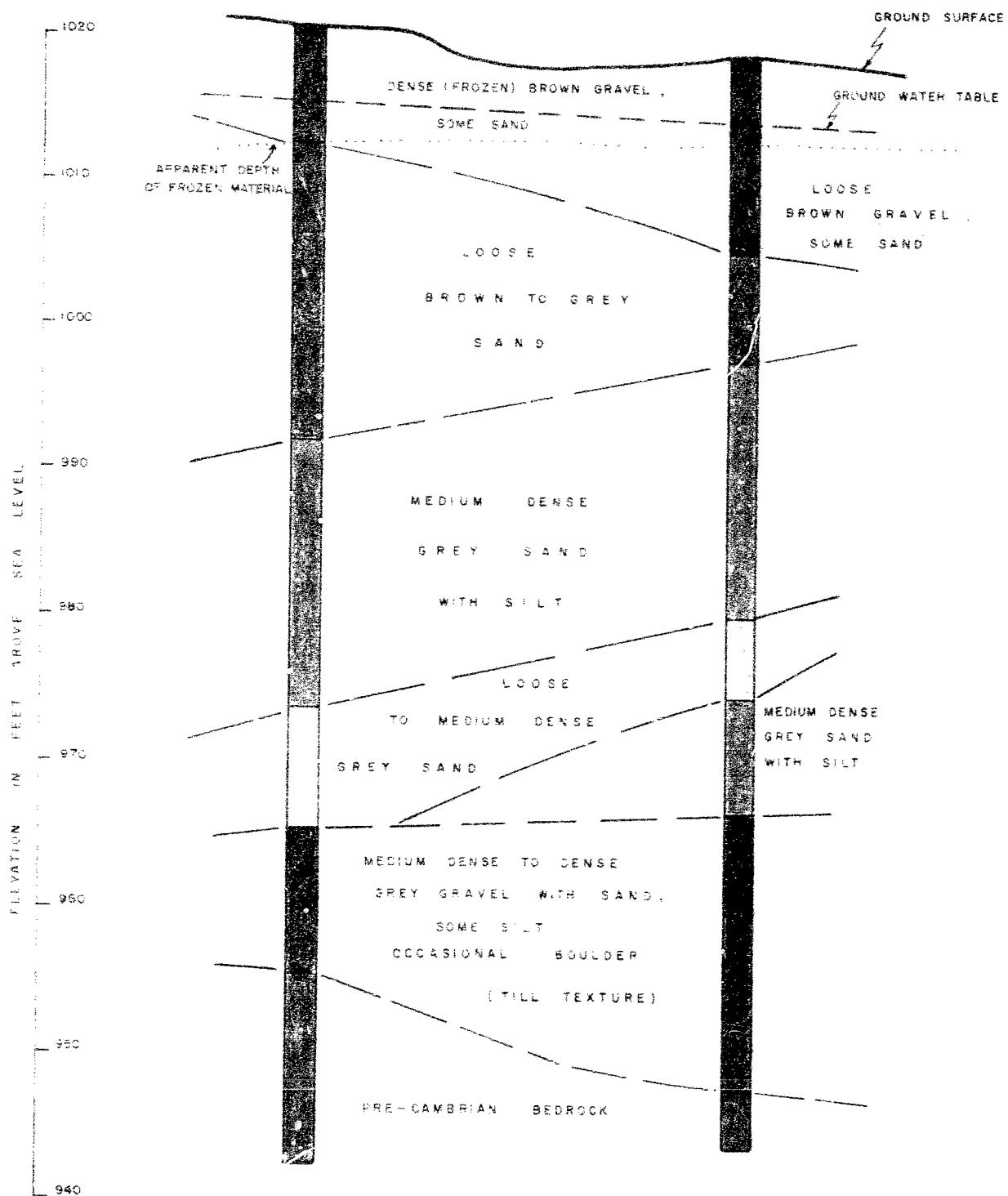
APPENDICES

1.51 GENERAL PLAN OF SITE

**1.52 SUBSURFACE SECTIONS**

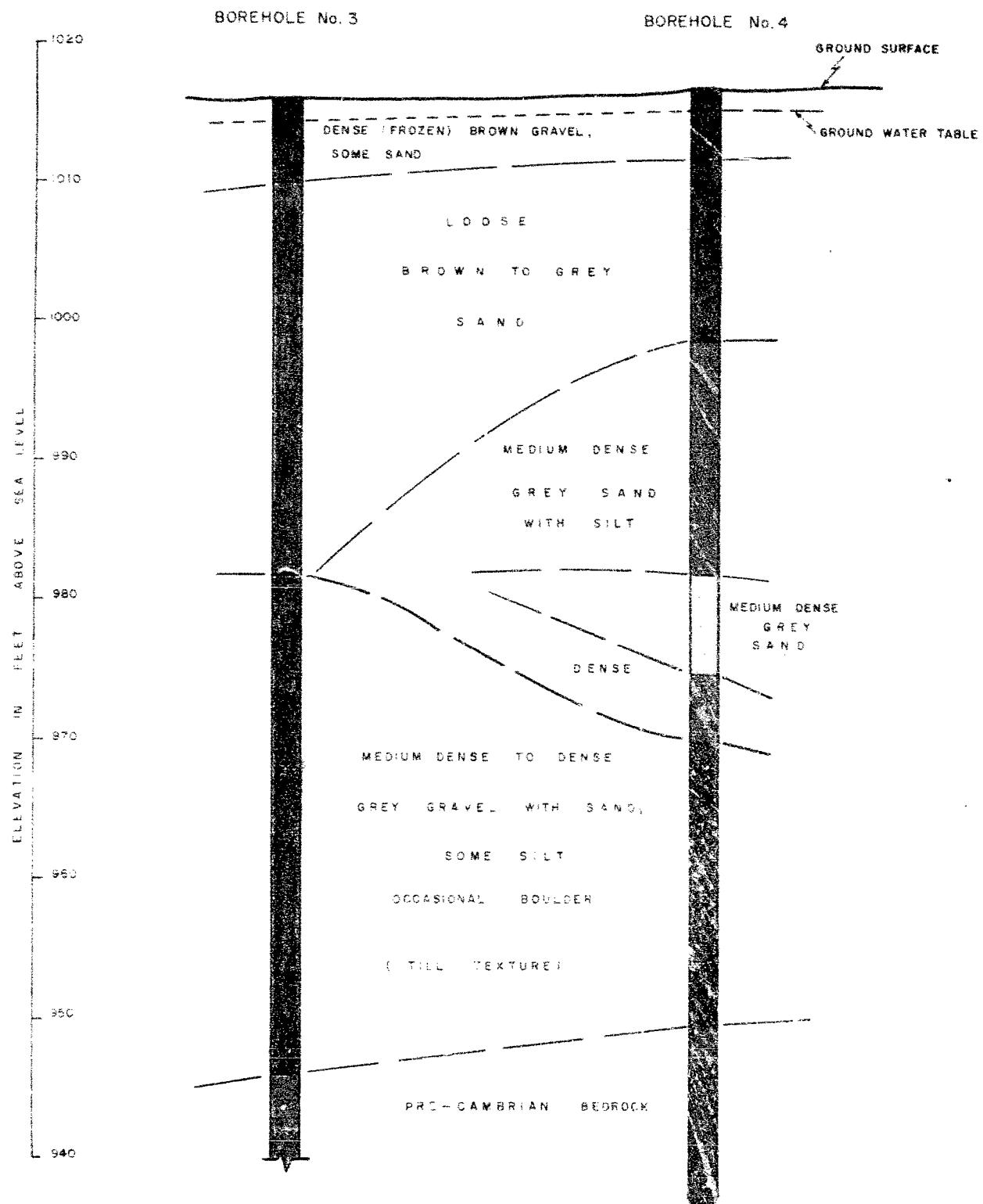
BOREHOLE No. 2

BOREHOLE No. 1



S U B - S U R F A C E   S E C T I O N   A L O N G   P R O P O S E D   S O U T H  
A B U T M E N T   C E N T R E   L I N E -   L O O K I N G   S O U T H

Scale - 1" - 10'



SUB-SURFACE SECTION ALONG PROPOSED NORTH ABUTMENT CENTRE LINE - LOOKING NORTH.

Scale - 1" = 10'



**1.53 OFFICE LOG OF BOREHOLES**

# **HUNTING TECHNICAL and EXPLORATION SERVICES**

JOB NO. H273/57 LOCATION CATFISH CREEK No 2  
CLIENT DEPARTMENT OF HIGHWAYS - ONTARIO  
COORDINATES CH. 732 + 00 - 15' LEFT

ELEV. (Surface) 1018.4' (Collar) Datum D.H.O.

## **BOREHOLE NUMBER**

Datum D.H.O.

## BOREHOLE NUMBER

Date (Started) Jan. 21, 1958 (Finished) Jan. 23, 1958

RIG NO.                    TYPE                    CONSTRUCTION OF A

C = Consolidation test  
 $\delta_d$  = dry density  
 $\delta_f$  = field density  
 M = mechanical analysis

Q - unconsol un'nt shear  
 Qc - consol drained shear  
 S - drained shear  
 V - vane shear (in situ)

C — core  
 K — Permeability  
 $w_f$  — field moisture content  
 $wp$  — plastic limit  
 $w_l$  — liquid limit  
 U — unconfined compressive stress

Up—approx. U as indicated  
by calibrated penetrometer  
P — field penetration tests  
x — standard penet. 2 S.S.  
o — cone penetration (60 24)  
— other

E.S.	- chunk
S.S.	- split spoon
S.L.	- sleeve <i>seɪpl̩z</i>
S.T.	- shelby tube
B.A.	- barrel sugar
S.C.	- scalding

T.W. --thin walled, open  
 T.W.P. --thin walled piston  
 D.P. --drive piston  
 D.F.V. --drive foot valve  
 D.B. --diamond bit

F.T.	-fish-tail
W.O.	-wash-out
	-undisturbed
	-disturbed
	-but represent

# **HUNTING TECHNICAL and EXPLORATION SERVICES**

OB H27 157  
ORI HOLE 2  
COMPILED J.K.  
CHECKED P.A.  
  
PAGE 1.  
  
F.7. -fish-tail  
W.O. -wash-out  
-undisturbed  
-disturbed -  
but represe-  
nted  
-lost

JOB NO. H273/57 LOCATION CATFISH CREEK No 2  
CLIENT DEPARTMENT OF HIGHWAYS - ONTARIO  
COORDINATES CHNG. 732 + 00 - 15' Right  
FL.EV. (Surface) 1020.4 (Collar) Datum D.H.

## BOREHOLE NUMBER 3

**BORROWER NUMBER** 2  
Date Started Feb 6, 1958 Date Due Feb 10, 1958

RIG NO. 1 TYPE LONGYEAR Jr. A

**ANSWER** *What is the name of the author of the book?*

BORING LOG

**BOILING SPRINGS**

silt	gravel	C - Consolidation test
clay	peat	d - dry density
sand	limestone	$\delta_f$ - Field density
	rock	M - mechanical analysis
	fill	
	igneous	
	igneous rock	
	WEIGHT OF HAMMER	

Q -- unconsol undr. shear  
 Qc -- consol drained shear  
 S -- drained shear  
 V -- vane shear (in situ)  
 ER 140 lb DROP 30 IN.

C — core  
 K — Permeability  
 $w_n$  — field moisture content  
 $w_p$  — plastic limit  
 $w_l$  — liquid limit  
 U — unconfined compressive strength

- Up—approx. U as indicated by calibrated penetrometer
- P—field penetration tests
- \*—standard penet. 2 S.S.
- cone penetration (60 2 1/4)
- others

E.S.	--chunk	T.W.
S.S.	--split spoon	T.L.
S.L.	--slieve sample	D.J.
S.T.	--shelby tube	D.J.
B.A.	--barrel auger	D.R.
G.C.	--Gardner cone	D.R.

<b>W.</b> —thin, walled, open	<b>F.7.</b> —S
<b>W.P.</b> —thin walled piston	<b>W.C.</b> —w
<b>P.</b> —drive piston	<b>C.</b> —u
<b>F.V.</b> —drive foot valve	<b>D.</b> —d
<b>B.</b> —diamond bit	<b>H.</b> —h

BORING		LOG		TESTS												SAMPLES								REMARKS					
SCALED DEPTH IN FEET	ELEV.	LOG NO.	DESCRIPTION	FIELD						LABORATORY						No.				COND.	DEPTH	TYPE	RECOVERY	HYD.	PENET.	SCALE			
				ft	5	15	25	50	100	150					I	H	O	Oc	S	C	M	Other	No.	From	To	Length Rec.	Hyd. Press	Penet. Resis.	Scale
WATER OBSERVATION																													
11	ft	11																											
					</td																								

# **HUNTING TECHNICAL and EXPLORATION SERVICES**

JOB NO. H273/57 LOCATION CATFISH CREEK No 2  
CLIENT DEPARTMENT OF HIGHWAYS - ONTARIO  
COORDINATES CHNG. 732 +00 - 15' Right

EL-FV (Surface) 10294 (Collected) Datum 9-18-00

E.G.E.V. (Surface) 1020.4 (Collar) Datum 5.H.U.

**BOREHOLE NUMBER** 2

Date (Started) Feb 5, 1958 (Finished) Feb 10, 1958

Date Started: Feb 5, 1958 (Finished) Feb 10, 1958  
RIG No. 1 TYPE LONGYEAR Jr.

RIG NO. TYPE LONGYEAR JP A

Digitized by srujanika@gmail.com

III III III salt  
H H H H clay

gravel	limestone	Con.
pool	rock	dry
fill	igneous	field
		M.

solidation test  
density  
d density  
mechanical analysis

ndr. shear      C - core  
 ed shear      K - Permeability  
 ar              w<sub>f</sub> - field moisture content  
 n situ)        w<sub>p</sub> - plastic limit  
 w<sub>l</sub> - liquid limit  
 M - moisture

Up = approx. U as indicated  
 by calibrated penetrometer  
 P = field penetration test  
 \* = standard penet. 2 S.E.  
 o = cone penetration (60°)

ted	E.S.	--chunk
cometar	S.S.	--split spoon
sts	S.L.	--sleeve sample
S.	S.T.	--shelby tube
2½,	B.A.	--barrel auger

- T.W. —thin walled, open
- T.W.P.—thin walled piston
- D.P. —drive piston
- D.F.V.—drive foot valve
- D.B.—diamond bit

F.T. — fish-tail  
W.O. — wash-out  
— undisturbed  
— disturbed —  
but represent.

BORING LOG			TESTS												SAMPLES						REMARKS								
SCALE	DEPTH	ELEV.	LOG			DESCRIPTION			FIELD			LABORATORY						No.			COND	DEPTH	TYPE	RECOVERY	HYD.	PENET.	SCALE		
ft	ft	ft																Id	St	O	C	M	Other	From	To	Length Rec.	Press	Resis.	
																		From	To	Length Rec.	Press	Resis.							
																		Dist.	Dist.	Dist.	Dist.	Dist.	Dist.	SAMPLE	BLOWS	PEN	FOOT		

# HUNTING TECHNICAL and EXPLORATION SERVICES

JOB NO. H273/57 LOCATION CATFISH CREEK No. 2  
CLIENT DEPARTMENT OF HIGHWAYS - ONTARIO  
COORDINATES CH 732440, 15' LEFT

ELEV. (Surface) 1016.0' (Collar) Datum D.H.O.

BOREHOLE NIV

Datum D.H.O.

**BOREHOLE NUMBER**

Date (Started) Jan 24, 1958 (Finished) Jan. 29, 1958

RIG NO. 1 TYPE LONGYEAR JR.

[View Details](#) | [Edit](#) | [Delete](#)

C Consolidation  
 d dry density  
 f field density  
 M mechanical c  
 WEIGHT OF HAM

O -- unconsoled undr.  
 Oe -- consol drained  
 S -- drained shear  
 V -- vane shear (in situ)

C —cohesion  
 K —Permeability  
 $w_f$  —field moisture content  
 $w_p$  —plastic limit  
 $w_l$  —liquid limit  
 U —unconfined compressive strength

Up--approx. U as indicated  
 by calibrated penetrometers  
 P --field penetration tests  
 = --standard penet. 2 S.S.  
 ? --cone penetration (50 2½)

S.S.	-chunk
S.S.	-split spoon
S.L.	-sieve sample
S.T.	-shabby tube
B.A.	-barrel sugar

—thin walled, open	F.T.	—fish-tail
P.—thin walled piston	W.O.	—wash-out
—drive piston		—undisturbed
V.—drive foot valve		—disturbed
—diamond kit		—last represent.

# HUNTING TECHNICAL and EXPLORATION SERVICES

JOB NO. H273/57 LOCATION CATFISH CREEK No. 2  
 CLIENT DEPARTMENT OF HIGHWAYS - ONTARIO  
 COORDINATES CH. 732440 , 15' LEFT

ELEV. (Surface) 1016.0' (Collar) Datum D.H.C

## BOREHOLE NUMBER

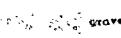
3

Date (Started) Jun 24, 1958 (Finished) Jun 29, 1958

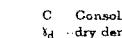
RIG NO. TYPE LONGYEAR JR. A



sand  
silt  
clay



gravel  
pebbles  
rock



limestone  
igneous  
organic rock



fill  
sound



unconsolidated  
consolidated



undrained  
drained



shear  
vane shear (in situ)



core  
permeability



moisture content  
density



plastic limit  
liquid limit



standard penetration test  
cone penetration (60.2%)



other



thin-walled open piston  
thin-walled piston



drive piston  
drive foot valve



barrel auger  
diamond bit



rock bit  
spiral auger

WEIGHT OF HAMMER 140 lb DROP 30 IN.

PAGE 2.

JOB H273/57  
 BOREHOLE 3  
 COMPILED J.K.  
 CHECKED P.A.

BORING LOG			TESTS										SAMPLES					REMARKS							
SCALE	DEPTH	ELEV.	LOG			DESCRIPTION			FIELD			LABORATORY						TESTS			SAMPLES			REMARKS	
ft	ft	ft							D	I	O	Oc	S	C	M	Other	No.	COND	DEPTH	TYPE	RECOVERY	HYD.	PENET.	SCALE	
			WATER OBSERVATION															From	To	Length	Re.	Hyd.	Penet.	Scale	
																		Dist.	Rev.	Dist.	Res.				
												DENSITY and NATURAL WATER CONTENT (in % of dry weight)													
												<input type="checkbox"/> DENSITY <input checked="" type="radio"/> NATURAL WATER CONTENT													
												ATTERBERG LIMITS wp = wl = (plf) (plf)													



## **HUNTING TECHNICAL and EXPLORATION SERVICES**

JOB NO. H273/57 LOCATION CATFISH CREEK No. 2

**CLIENT** DEPARTMENT OF HIGHWAYS - ONTARIO

**COORDINATES** CHNG 732 + 40 - 15 Right

ELEV. (Surface) 1016.7 (Collar) Datum D.H.O.

## **BOREHOLE NUMBER**

Date (Started) Jul.

RIG NO. 1 TYPE LONGYEAR Jr.

	silt		gravel	C -- consolidation test	Q - unconstr. undr. shear
	clay		peat	d - dry density	Qc - consol. drained shear
	sand		rock	f - field density	S - drained shear
	till		lignite rock	M - mechanical analysis	V - vane shear (in situ)
				WEIGHT OF HAMMER 140 lb	DROP 30 in.

C	—core	Up	—approx. U as indicated
K	—Permeability		by calibrated penetrometer
wn	—field moisture content	P	—field penetration tests
wp	—plastic limit	x	—standard penet. 2 S.S.
wl	—liquid limit	u	—cone penetration (60 2½")
U	—unconfined compressive strength	A	—other

E.S.	-chunk	T.W.	-thin, walled, open
S.S.	-split spoon	T.W.P.	-thin walled piston
S.L.	-sleeve sample	D.P.	-drive piston
S.T.	-shelby tube	D.F.V.	-drive foot valve
B.A.	-barrel auger	D.B.	-diamond bit
S.A.	-Spiral auger	R.B.	-Rock bit

F.T. — fish-tail  
 W.O. — wash-out  
 undisturbed  
 disturbed  
 best represent.  
 fair  
 lost

# **HUNTING TECHNICAL and EXPLORATION SERVICES**

JOB NO. H-2-5/57 LOCATION CATFISH CREEK ! 2

**CLIENT** DEPARTMENT OF HIGHWAYS - ONTARIO

**COORDINATES** CHNG. 772+81 '17 right

ELEV. (Surface) 1018.0 (Coring) Datum 04.0.

## **BOREHOLE NUMBER**

**BUREAU NUMBER**  
Date (Stamp) Feb 17 1958

Date (Started) Feb. 11, 1990

RIG NO. 1

---

BOB

BURGESS & BURGESS

ING

III

gravel  
peat

**Limestone** rock C - Consolid.  
 rock d - dry tensile  
 rock f - field den.  
 M - mechanical

ation test  
ity  
sity  
cal analysis

unconsol undr. shear  
 consol drained shear  
 drained shear  
 vane shear (in situ)

C --core  
 K --Permeability  
 wn --field moisture content  
 wp --plastic limit  
 wl --liquid limit  
 U --unconfined compressive strength

Up—approx. U as indicated  
     by calibrated penetrometers  
 P —field penetration tests  
 \* —standard penet. 2 S.S.  
 o —cone penetration (60 2/4)

E.S.	-ch
S.S.	-sp
S.L.	-sh
S.T.	-sh
B.A.	-ba
S.A.	-sa

hunk  
split spoon  
leove sample  
helby tube  
arrel auger  
piral auger

T.W. —thin walled sp.  
 T.W.P.—thin walled pist  
 D.P. —drive piston  
 D.F.V.—drive foot valve  
 D.B. —diamond bit  
 R.B. —Rock bit

F.T.	- fresh-trail
W.O.	- wash-out
<input type="checkbox"/>	- undisturbed
<input checked="" type="checkbox"/>	- disturbed
<input type="checkbox"/>	- but represent.
<input type="checkbox"/>	- fair
<input type="checkbox"/>	- lost

# HUNTING TECHNICAL and EXPLORATION SERVICES

JOB H 273/57  
BOREHOLE 6  
COMPILED J.K.  
CHECKED P.A.

**JOB NO.** H 273/57 **LOCATION** CATFISH CREEK No. 2  
**CLIENT** DEPARTMENT OF HIGHWAYS - ONTARIO

**CLIENT** DEPARTMENT OF HIGHWAYS - ONTARIO  
**COORDINATES** CHNG. 733 + 43 236' Right

ENTR. (2.4) 1018.2' (G. H.) 1031.0 Datum = 2 H. G.

ELEV. (Surface) 1019.0' (Collar) 1021.0 Datum D.H.O.

## BOREHOLE NUMBER 6

**BUREAU NUMBER** \_\_\_\_\_  
B.I. (Bull.) No. Feb. 17, 1958 (Finished) Feb. 17, 1958

Date (Started) Feb. 17, 1958 (Finished) Feb. 17, 1958

RIG NO. 1 TYPE LONGYEAR JR.

REC NO. 1445

C	—Consolidation test	O	—unconsol. undr. shear
d <sub>d</sub>	—dry density	O <sub>c</sub>	—consol drained shear
d <sub>b</sub>	—field density	S	—drained shear
M	—mechanical analysis	V	—vane shear (in situ)
L	—lithology	WEIGHT OF HAMMER	140 lb
R	—rock	DROP	30 IN.
I	—igneous		
S	—igneous rock		

C --core  
 K --Permeability  
 w<sub>n</sub> --field moisture content  
 w<sub>p</sub> --plastic limit  
 w<sub>l</sub> --liquid limit  
 U --unconfined compressive strength

- Up - approx. U as indicated by calibrated penetrometer
- P - field penetration tests
- \* - standard penet. 2 S.S.
- o - cone penetration (60 2 1/4)
- x - other

E.S.	--chunk
S.S.	--split spoon
S.L.	--sleeve sample
S.T.	--shelby tube
B.A.	--barrel auger
S.A.	--Spiral auger

.W. —thin, walled, open  
 .W.P.—thin walled piston  
 .P. —drive piston  
 .F.V.—drive foot valve  
 .B. —diamond bit  
 .B. —Rock bit

F.T.	-fish-tail
W.O.	-wash-out
	-undisturbed
	-disturbed
	-but represent.
	-fair
	-lost

1.54 AIR-PHOTO WITH INTERPRETED GEOLOGY

CATFISH CREEK

Jamestown Ont.

scale - 1" = 1 mile

- — prop. Hwy. 17
- ..... boundary of valley sediments
- D - rock controlled areas
- R - bedrock



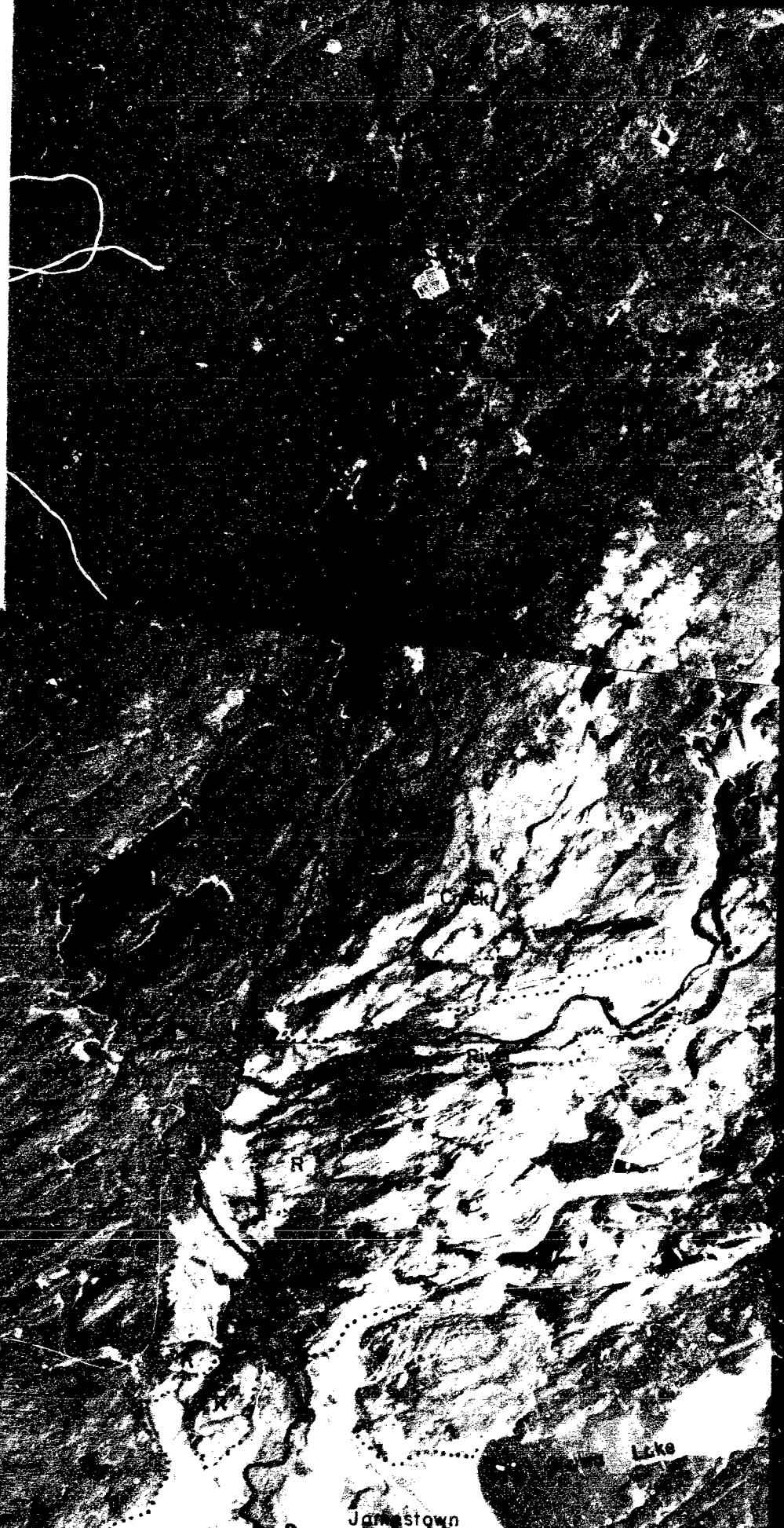
CATFISH CREEK

Jamestown Ont

scale - 1" = 1 mile

— — — prop. Hwy. 17  
- - - boundary of valley sediments  
O - rock controlled areas  
R - bedrock

N



1.55 PHOTOS OF SITE AND RIG



STEREOPHOTO PAIR SHOWING GENERAL VIEW  
OF SITE FROM CHAINAGE 738+00 LOOKING SOUTH,  
DRILL IS SET UP AT HOLE NO. 1.

SUPER IMPOSED DOCUMENT MAY  
APPEAR AS MULTI-FEED ON FILM.



STEREOGRAPHIC PHOTO PAIR SHOWING GENERAL VIEW  
OF SITE FROM CHAINAGE 738+00 LOOKING SOUTH,  
DRILL IS SET UP AT HOLE NO. 1.

SUPERIMPOSED DOCUMENT MAY  
APPEAR AS MULTIFEED ON FILM.



GENERAL VIEW OF SOUTH ABUTMENT AREA  
DRILL SETUP AT HOLE NO. 2



VIEW SHOWING OVERTBURDEN MATERIALS  
VICINITY BOREHOLE NO. 2

SUPER IMPOSED DOCUMENT MAY  
APPEAR AS MULTIFEED ON FILM.



GENERAL VIEW OF SOUTH ABUTMENT AREA  
DRILL SETUP AT HOLE NO. 2



VIEW SHOWING OVERTBURDEN MATERIALS  
VICINITY BOREHOLE NO. 2



GENERAL VIEW OF SOUTH ABUTMENT LOOKING EAST  
DRILL SETUP AT HOLE NO. 1



GENERAL VIEW OF SOUTH ABUTMENT LOOKING WEST  
DRILL SETUP AT HOLE NO. 1.

SUPER IMPOSED DOCUMENT MAY  
APPEAR AS MULTIFEED ON FILM.

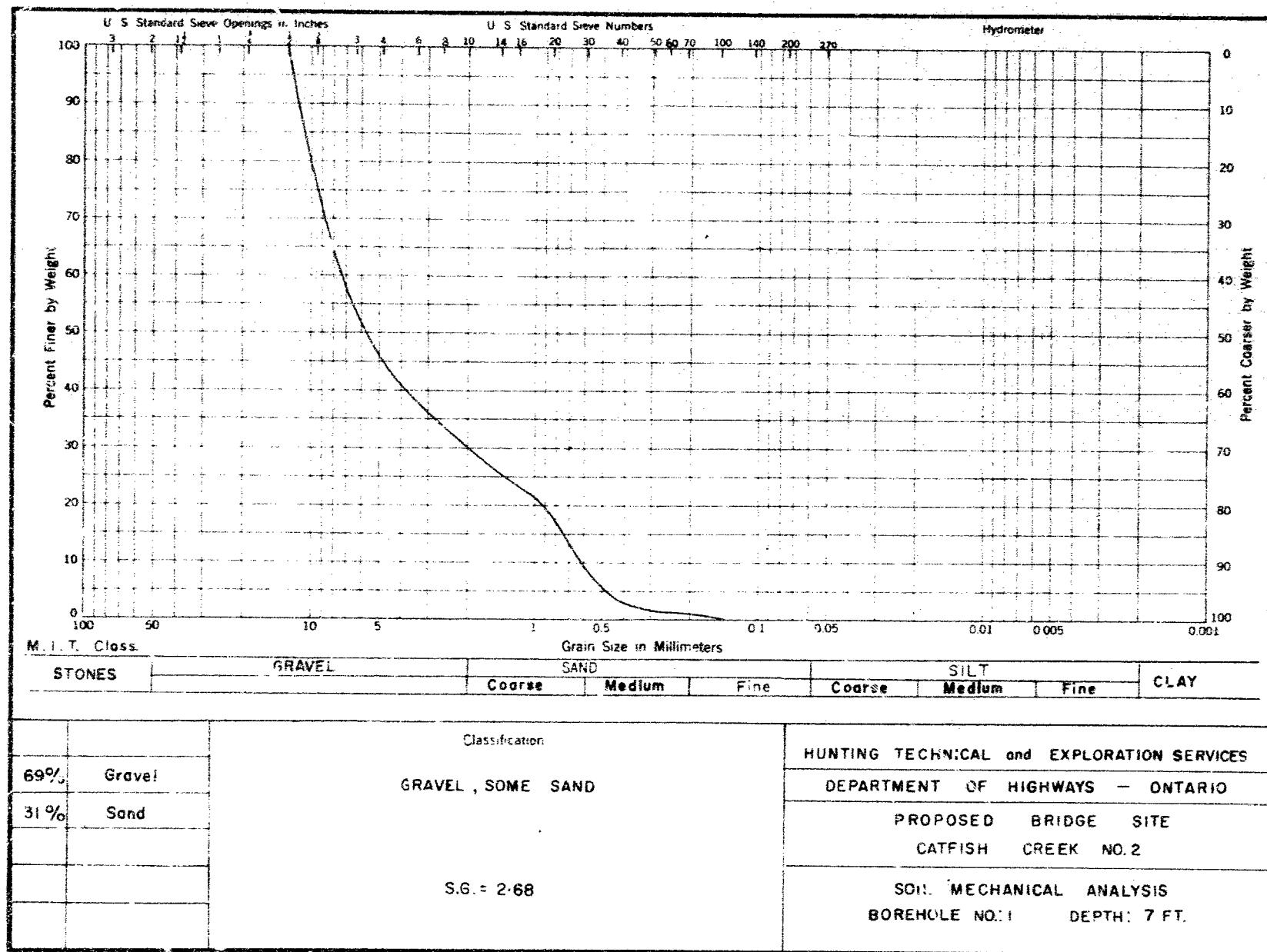


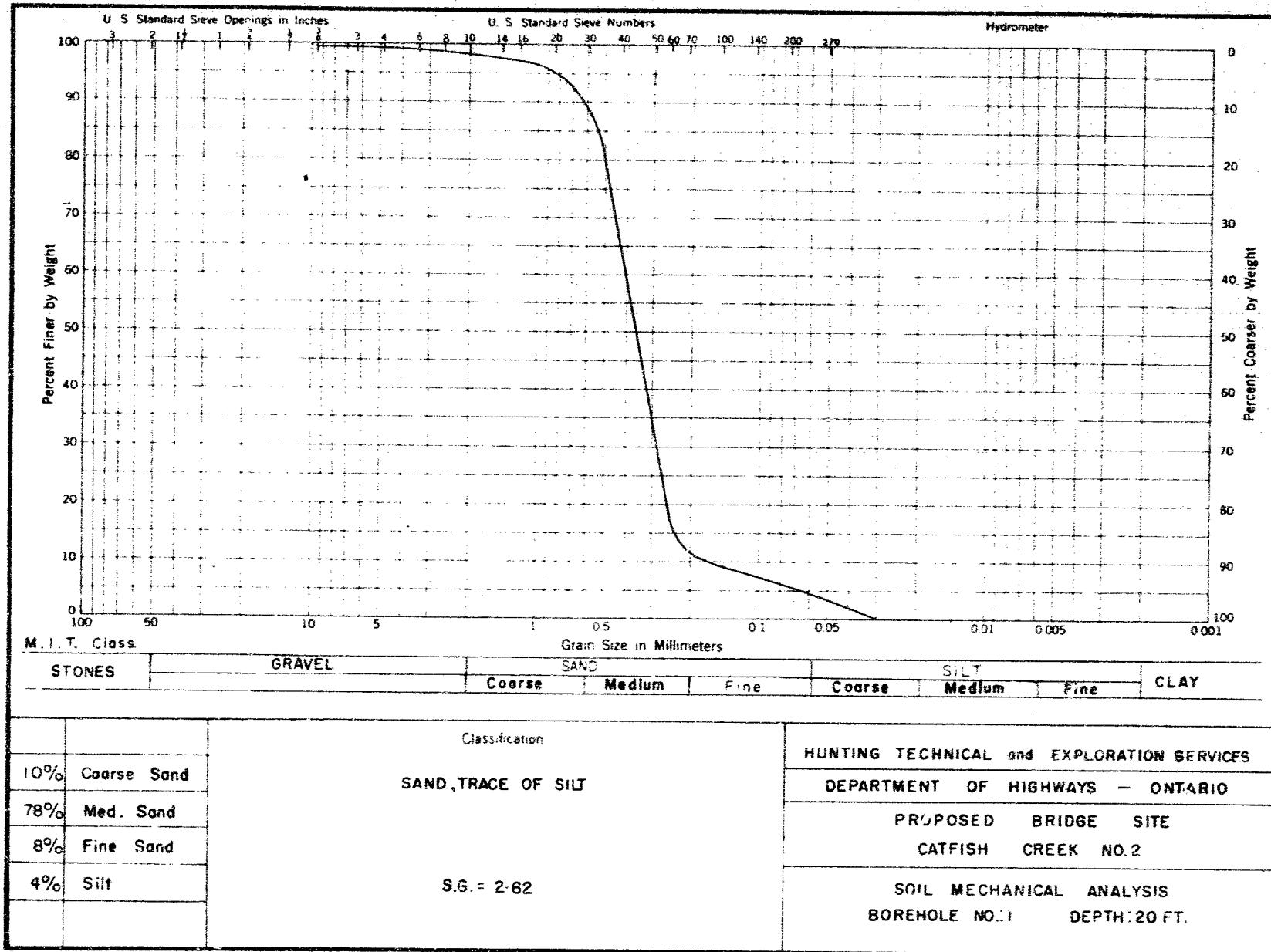
GENERAL VIEW OF SOUTH ABUTMENT LOOKING EAST  
DRILL SETUP AT HOLE NO. 1

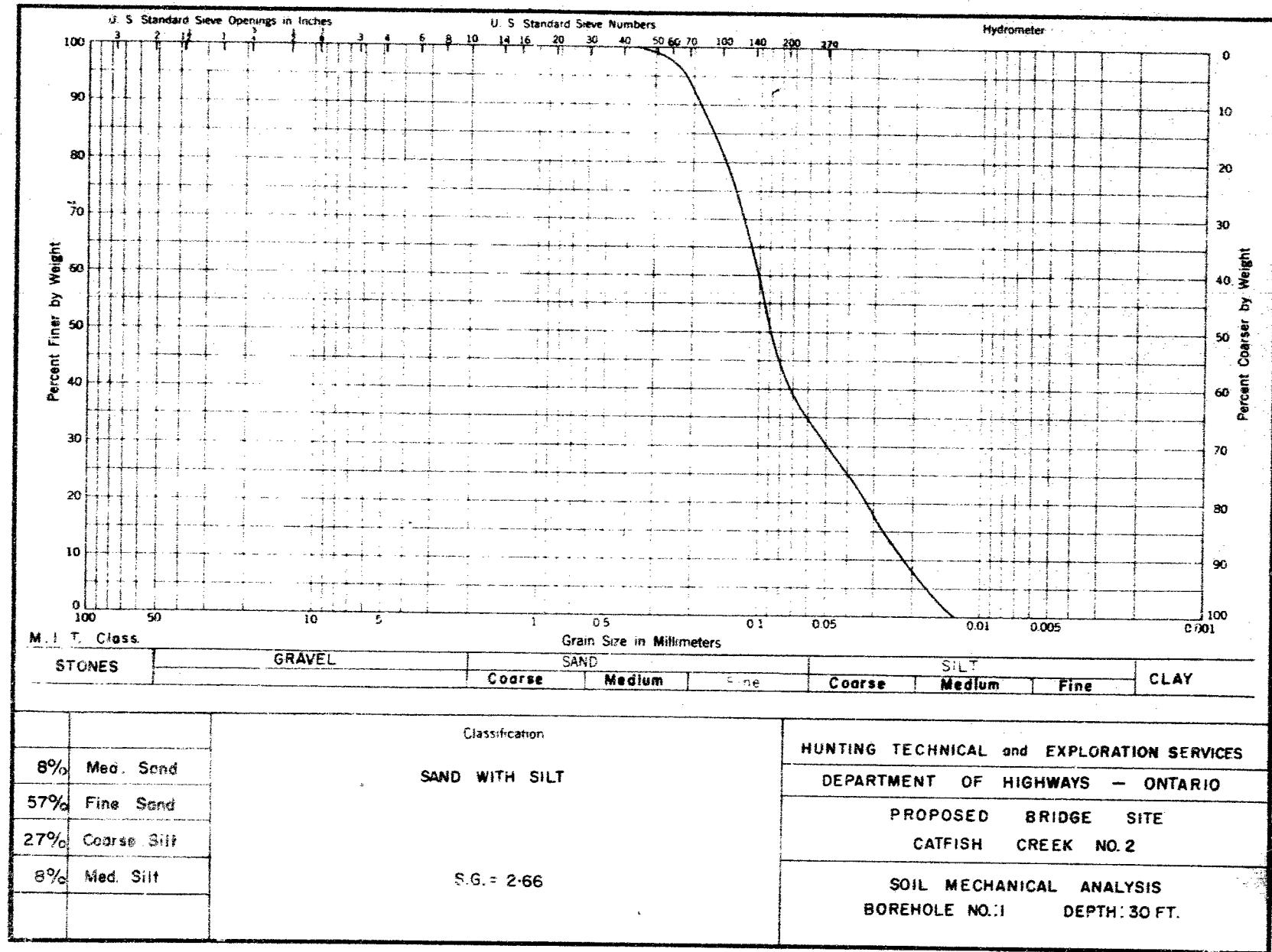


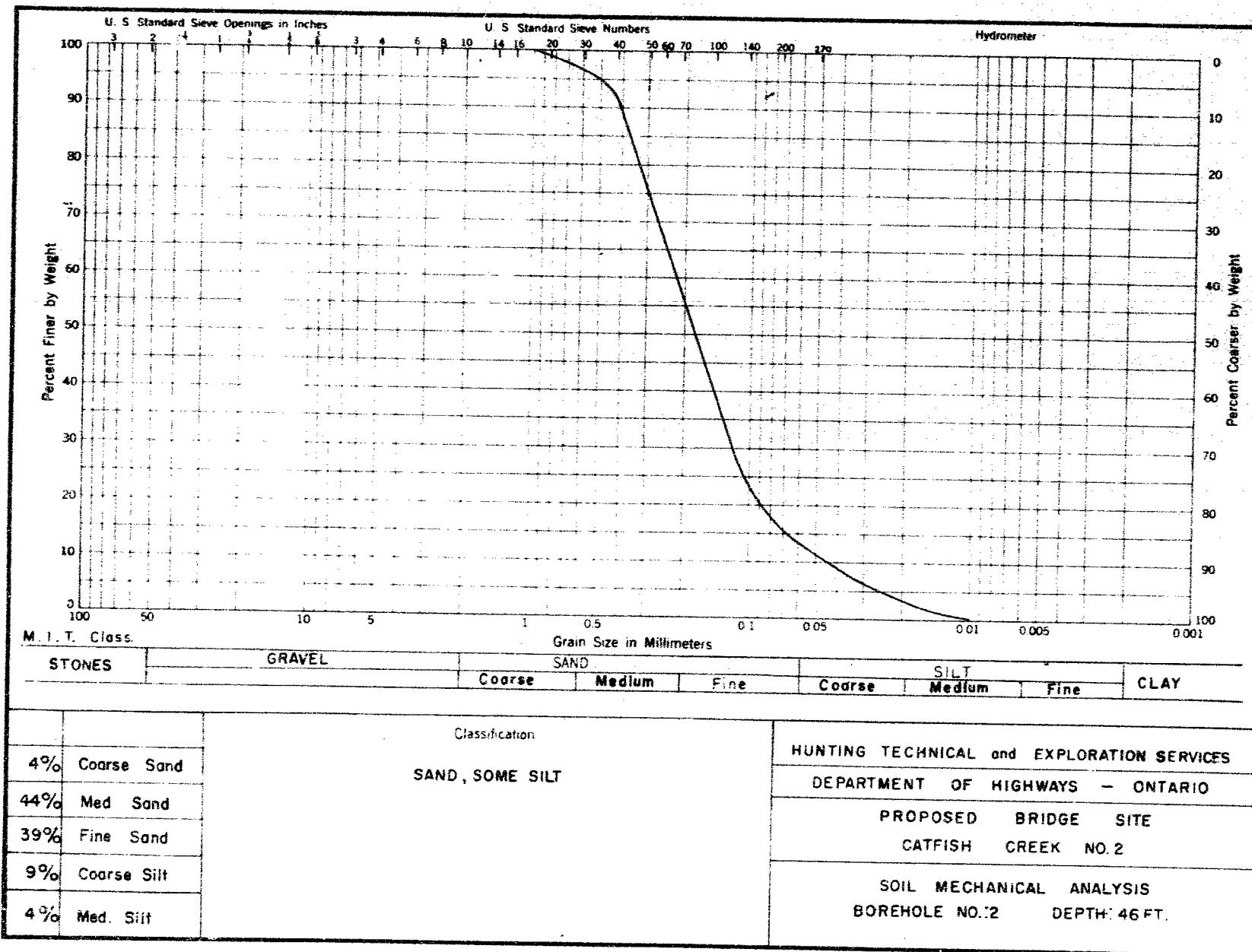
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DRILL SETUP AT HOLE NO. 1.

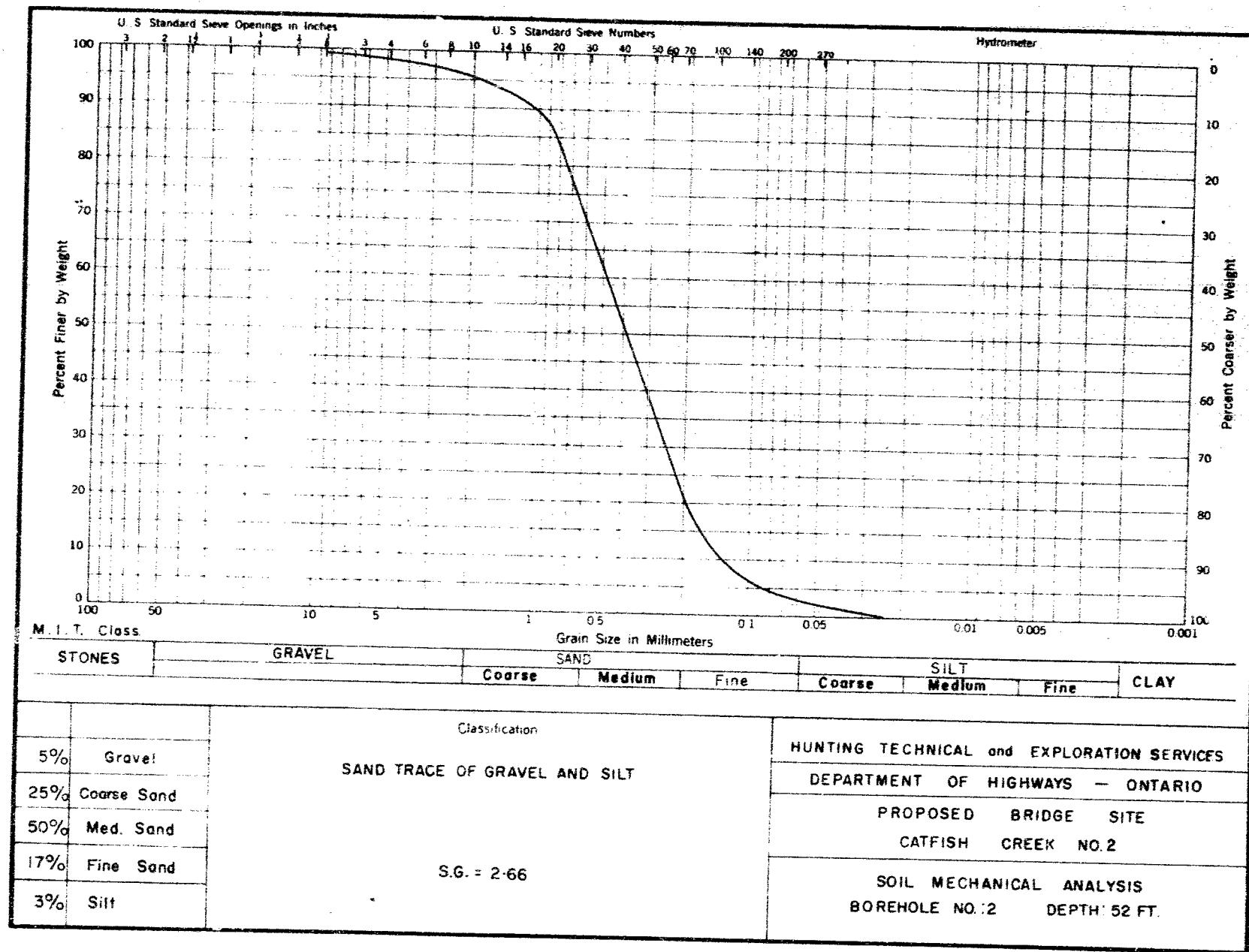
**1.56 SOIL CLASSIFICATION CHARTS**

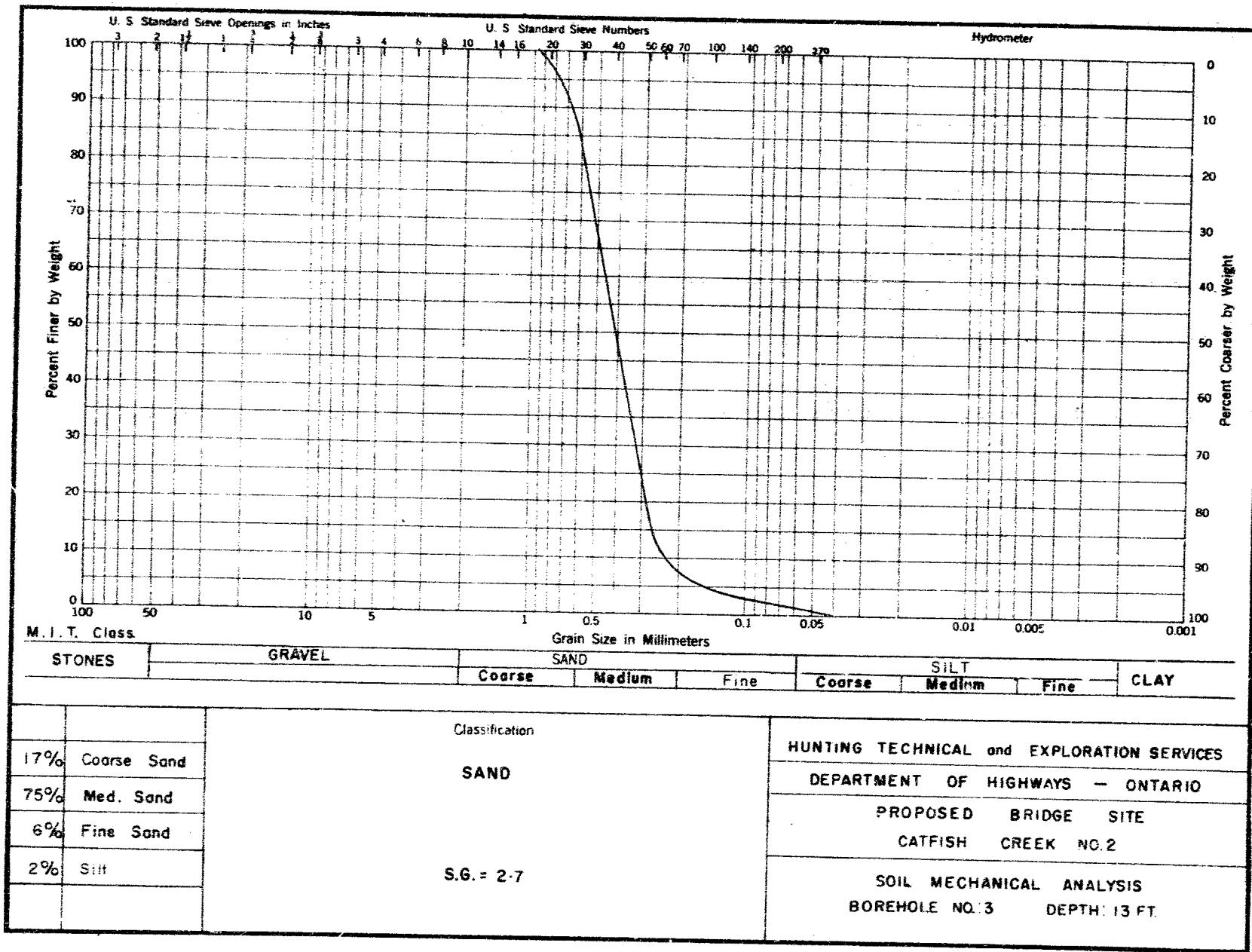


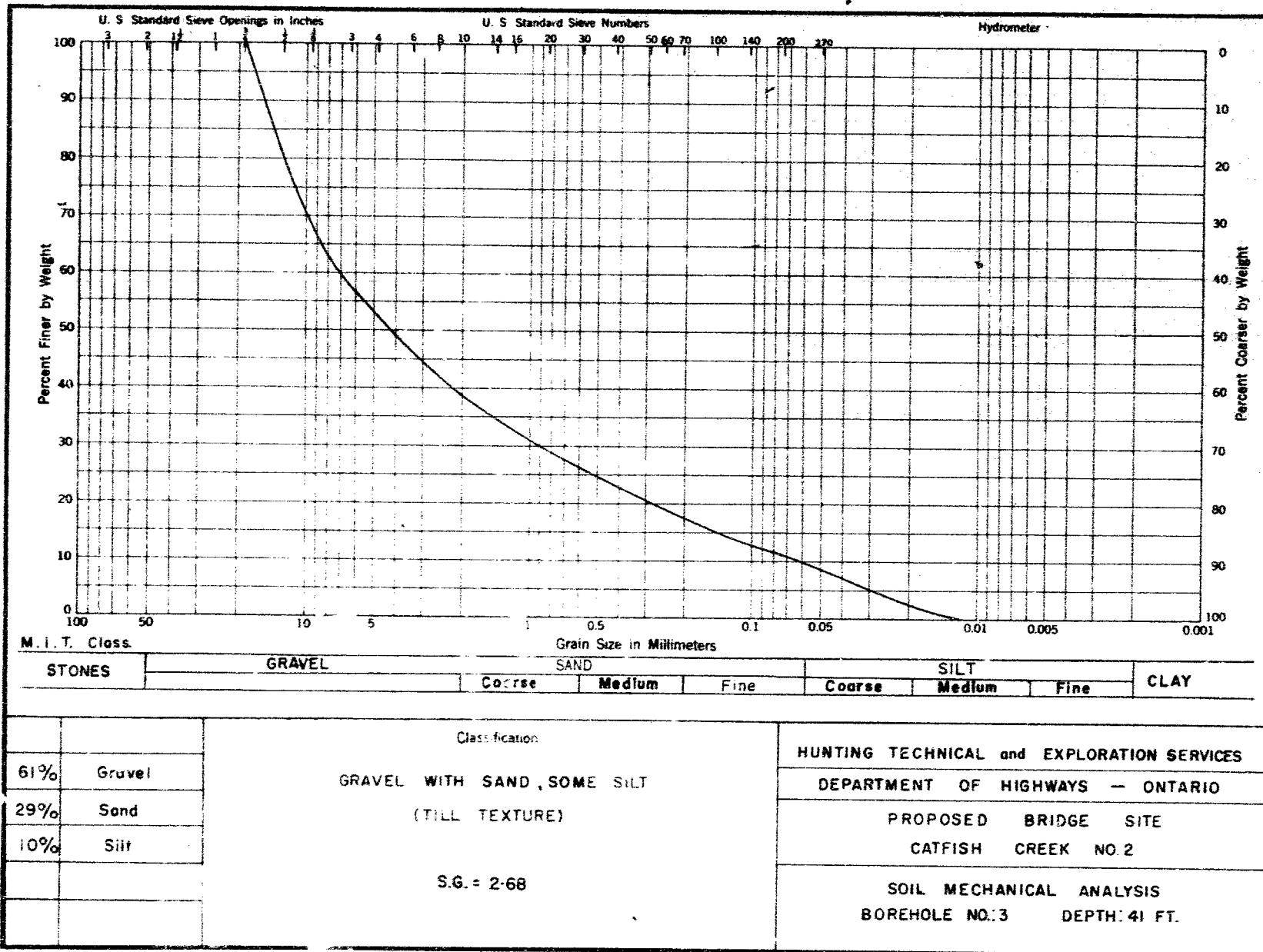


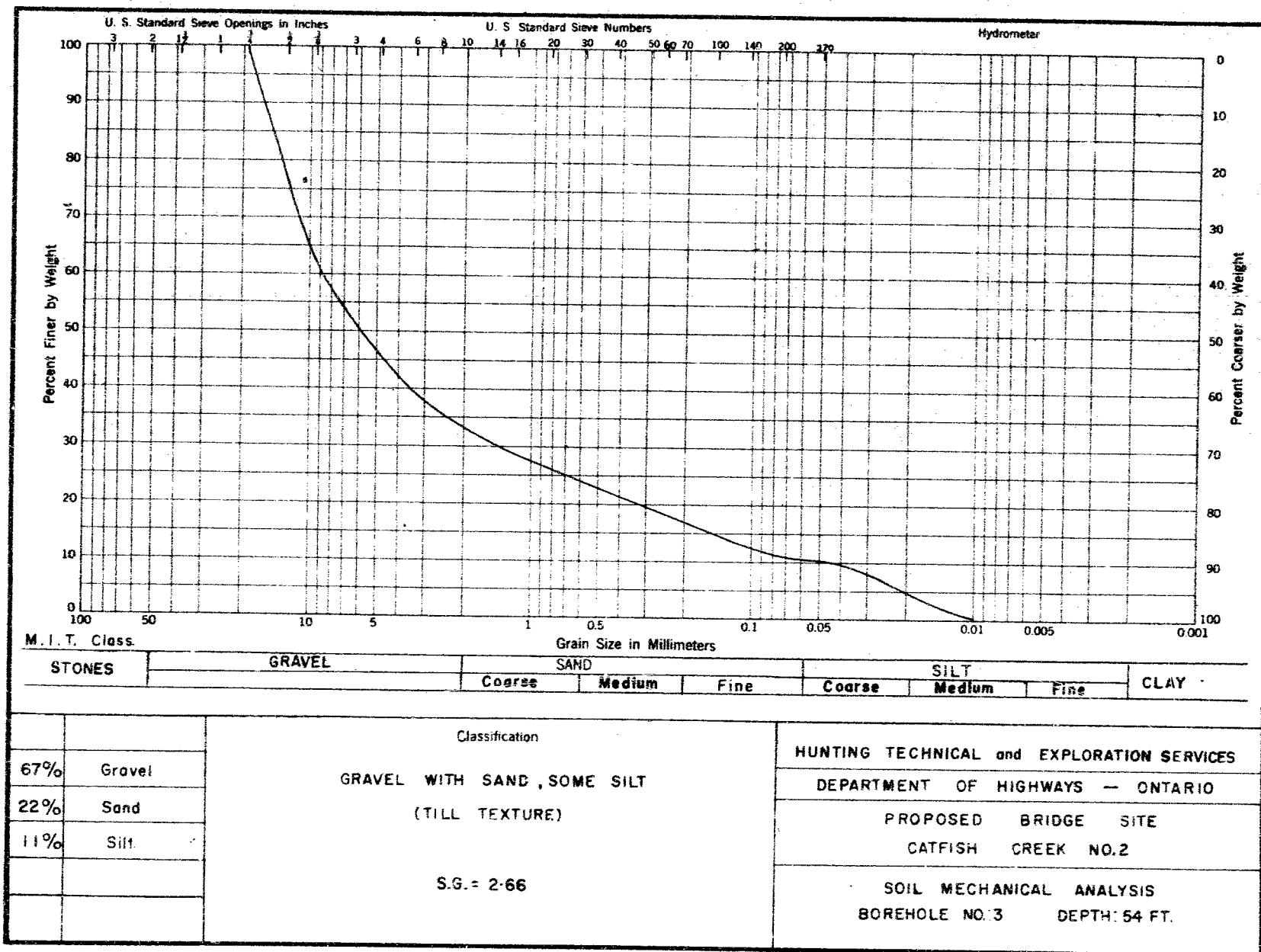


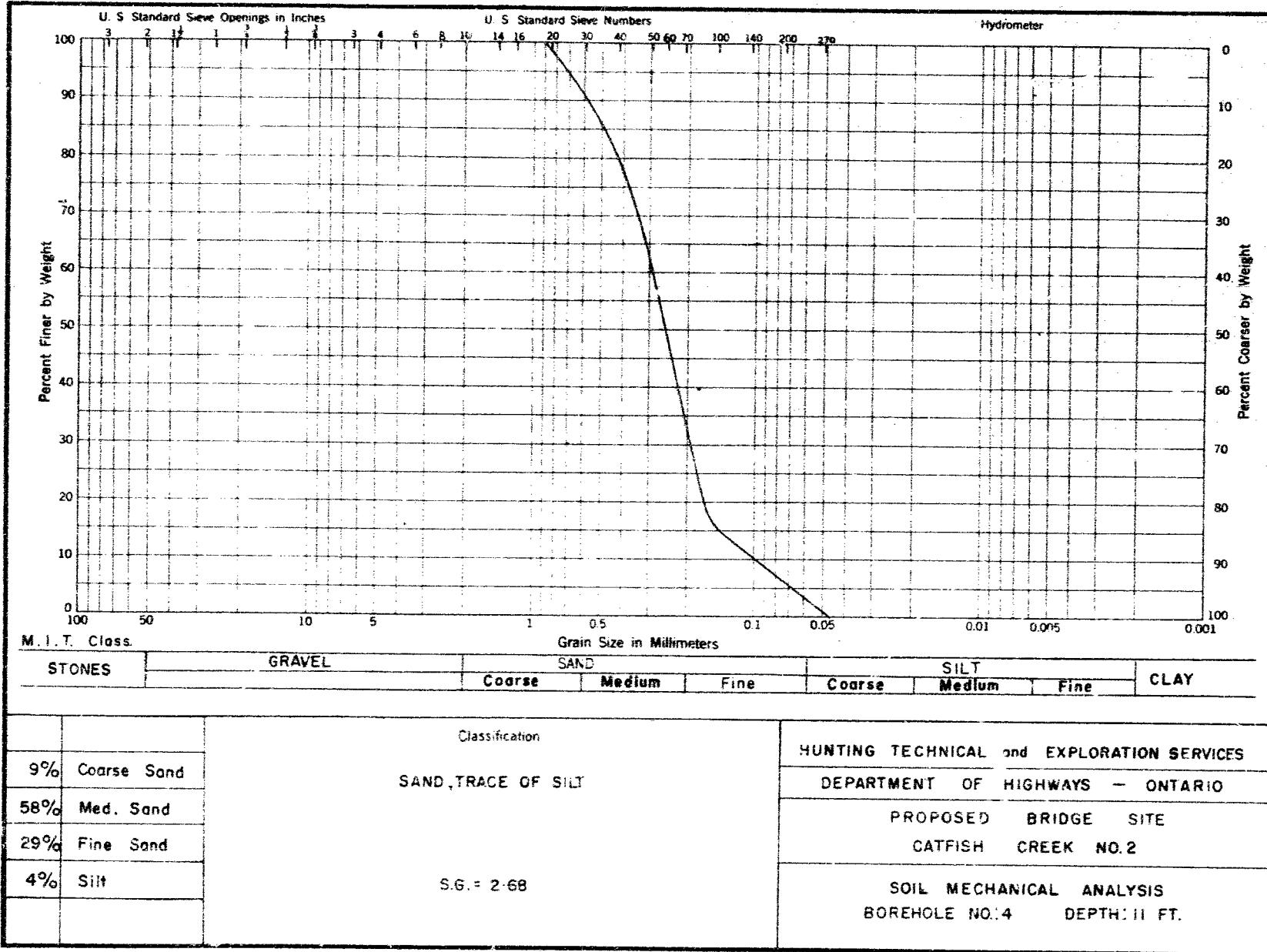


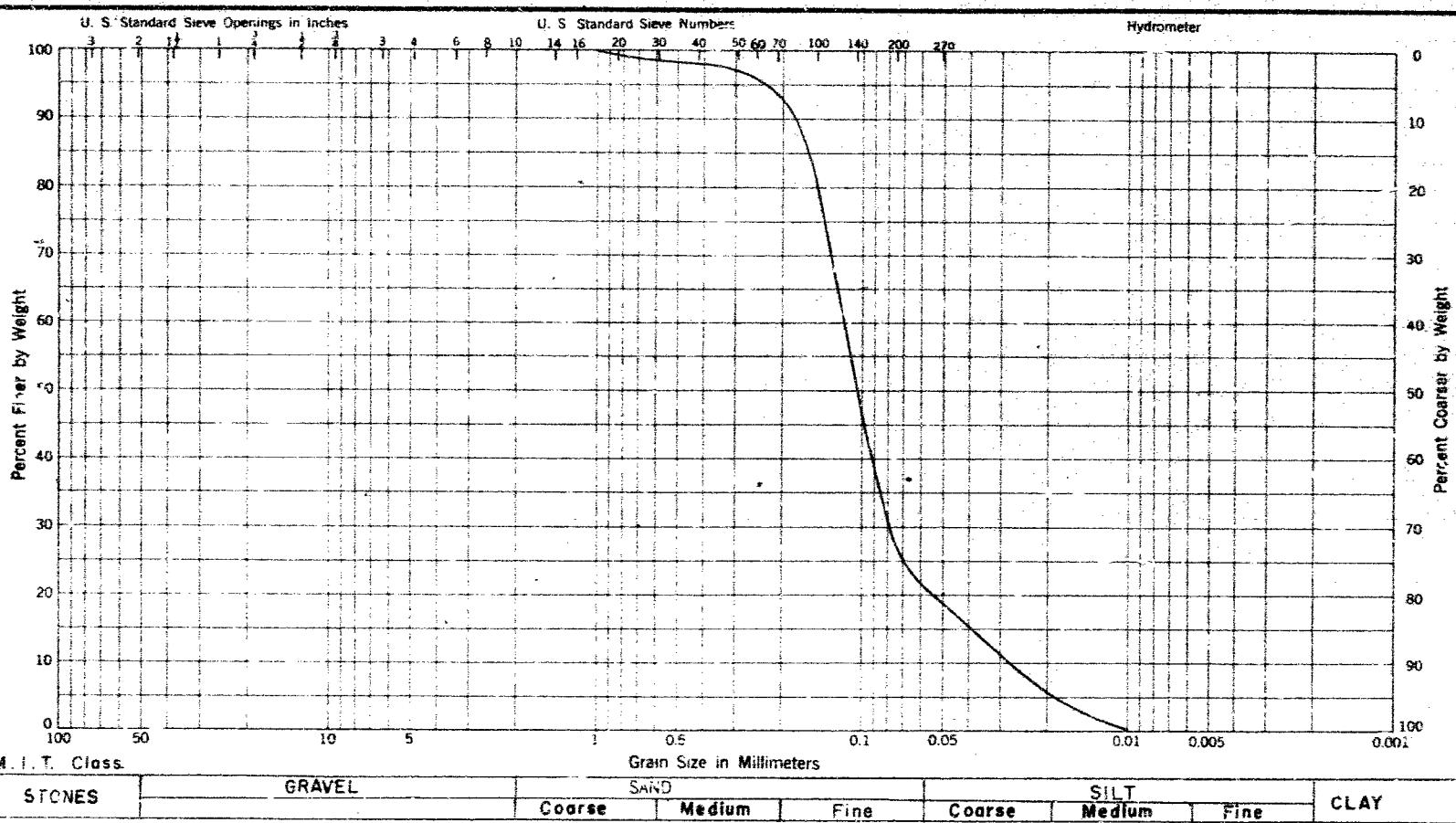




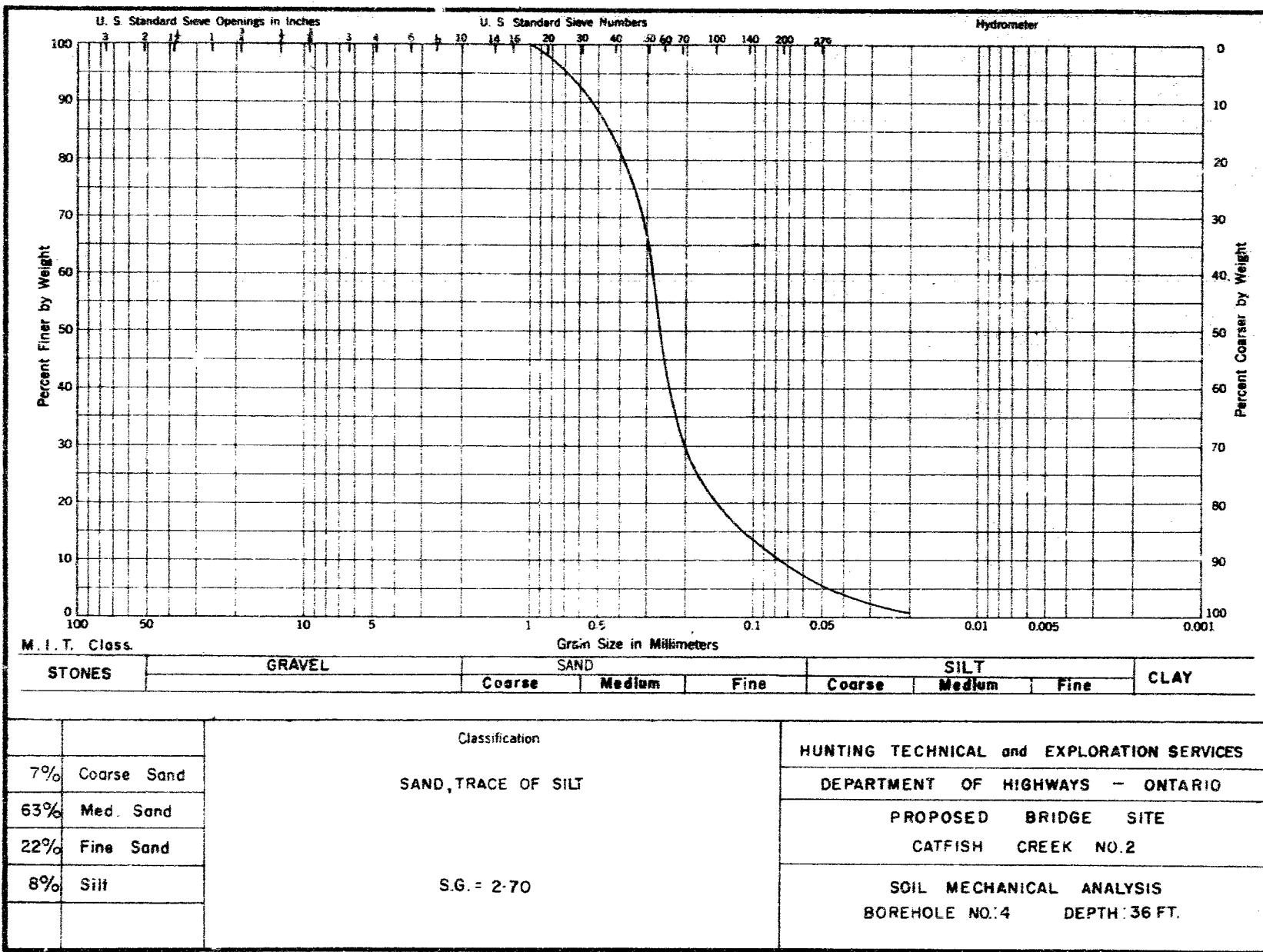


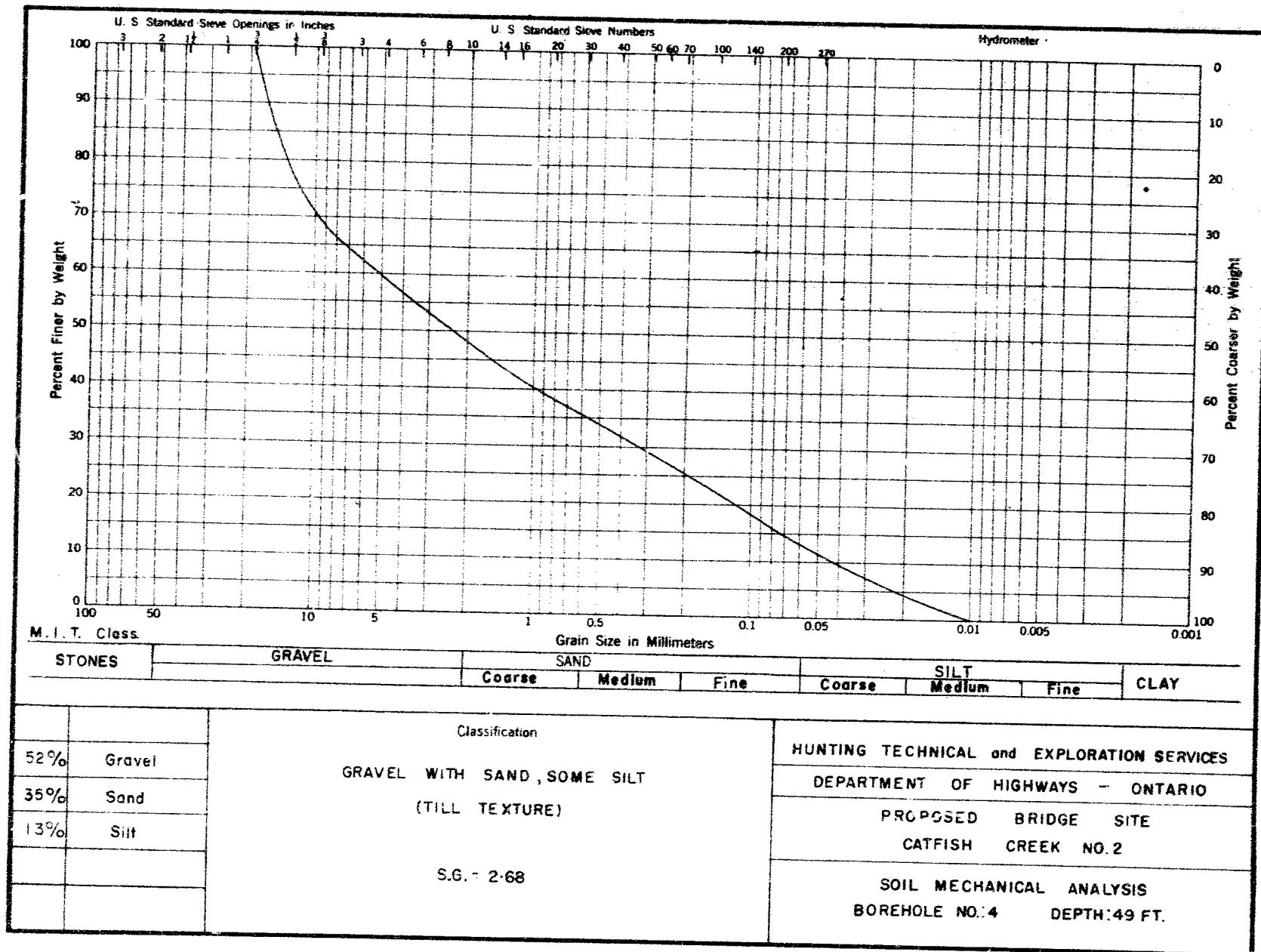


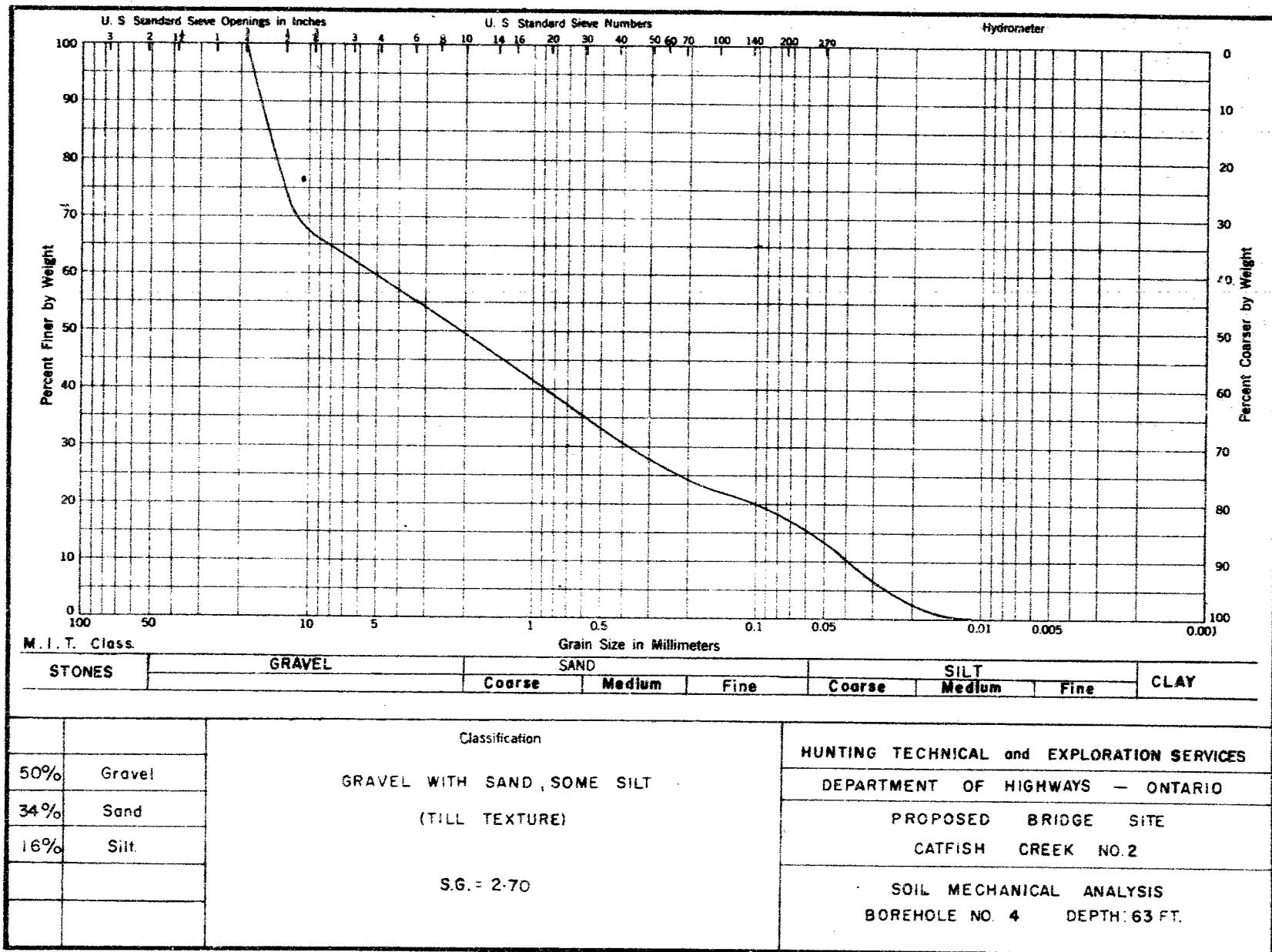




HUNTING TECHNICAL and EXPLORATION SERVICES  
 DEPARTMENT OF HIGHWAYS - ONTARIO  
 PROPOSED BRIDGE SITE  
 CATFISH CREEK NO. 2  
 SOIL MECHANICAL ANALYSIS  
 BOREHOLE NO. 4 DEPTH 21 FT.





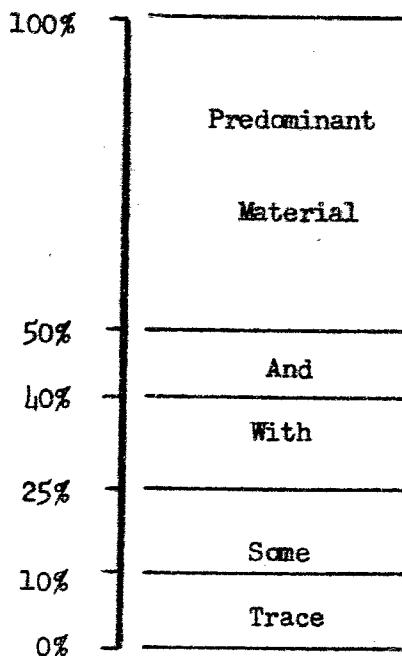


HUNTING TECHNICAL & EXPLORATION SERVICES

1450 O'Connor Drive      Toronto, Ontario

SOIL TYPES

The following system was used in classifying the various soils by name:



Example:

Medium dense      grey      silt      with      fine      sand  
(Penet. resist.) (colour) (pred. type) (25%-40%) (other type)  
or relative density

Unless believed to have a significant effect on the soil characteristics the minor soil types (i.e. traces) present are disregarded in the name used on the boring log and cross-sections. The complete classification is given with the gradation analysis.

In all cases the strength characteristics (e.g. penetration resistance) is quoted first, followed by the colour and finally the descriptive name based on the mechanical analysis.

HUNTING TECHNICAL & EXPLORATION SERVICES  
1450 O'Connor Drive      Toronto, Ontario

CLASSIFICATION OF SOILS FOR ENGINEERING PURPOSES

Soils encountered in sub surface exploration for engineering purposes are composed of organic or inorganic materials, water, air and dissolved salts. The water and air are generally considered to be uniform so that identification is primarily in the nature of organic or inorganic (mineral grains) and dissolved salts.

In the field a soil is generally identified in terms of grain size characteristics, color and mineral content — properties of the mineral grains. Occasionally, the origin of a soil is included in the identification.

The systems used to describe soils in terms of engineering properties are called classification systems. In the system described below, the soils are first identified and then classified in terms of strength characteristics which are of prime importance in utilizing the soil boring data in designing a safe and economical foundation.

Penetration measured by dropping 140 lb. hammer 30" on 2" O.D. split spoon sampler.

Identification (Soil Type)	Classification	Classification Criteria	
		Unconfined Compressive Strength	
Clay	Soft	Less than 0.50 Tons/Sq. Ft.	
	Medium	0.50 to 1.00 Tons/Sq. Ft.	
	Stiff	1.00 to 2.00 Tons/Sq. Ft.	
	Very Stiff	2.00 to 4.00 Tons/Sq. Ft.	
	Hard	Greater than 4.00 Tons/Sq. Ft.	
Silt	Density		
	Loose	Less than 80 lbs./Cu. Ft.	
	Medium Dense	80 to 95 lbs./Cu. Ft.	
	Dense	Greater than 95 lbs./Cu. Ft.	
Sand	Relative Density		Penetration Resist.
	Loose	0 - 30%	0 - 10 Blows/Ft.
	Medium Dense	30 - 60%	10 - 30 Blows/Ft.
	Dense	60 - 90%	30 - 50 Blows/Ft.
	Very Dense	90 - 100%	Over 50 Blows/Ft.
Gravel	Penetration Resist.		
	Loose	Less than 30 Blows	
Hardpan	Dense	Over 30 Blows/Ft.	
		Cemented on partially cemented sandy gravels, sands, gravels with or without some clay and silt and having unconfined compression strength greater than 5 tons/Sq. Ft.	
Fill	Organic	Very Loose	0 - 4 Blows/Ft.
		Loose	4 - 10 Blows/Ft.
		Medium	10 - 30 Blows/Ft.
	Inorganic	Dense	30 - 50 Blows/Ft.
		Very Dense	Over 50 Blows/Ft.
Peat	Unconfined Compressive Strength		
	Very Soft	Less than 0.30 Tons/Sq. Ft.	
	Soft	0.30 to 0.60 Tons/Sq. Ft.	
	Stiff	Greater than 0.60 Tons/Sq. Ft.	
Organic Silt (Muck)	Density		
	Loose	Less than 30 lbs./Cu. Ft.	
	Medium Dense	Greater than 30 lbs./Cu. Ft.	