

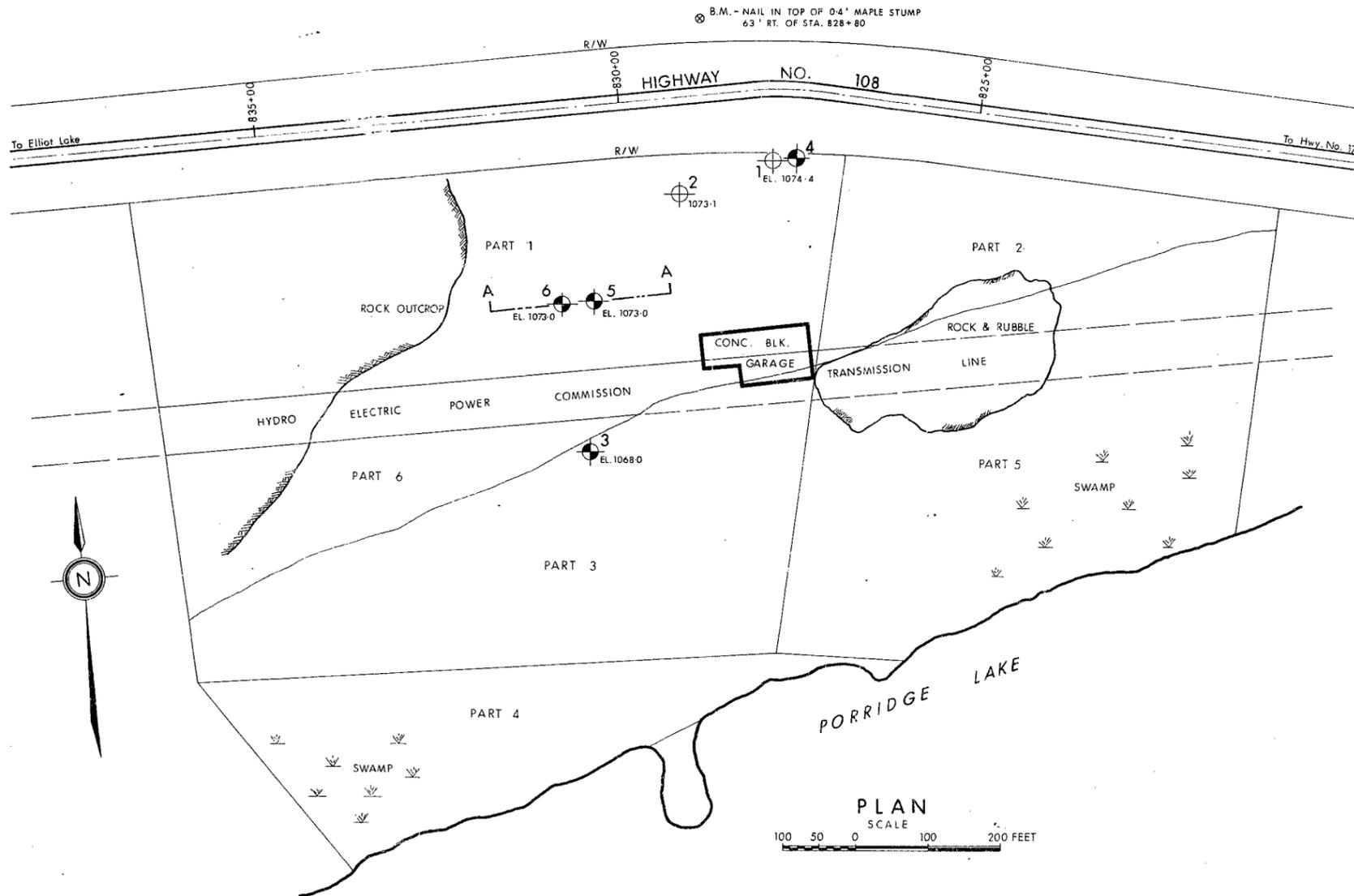
#65-F(R)-52

HWY. #108

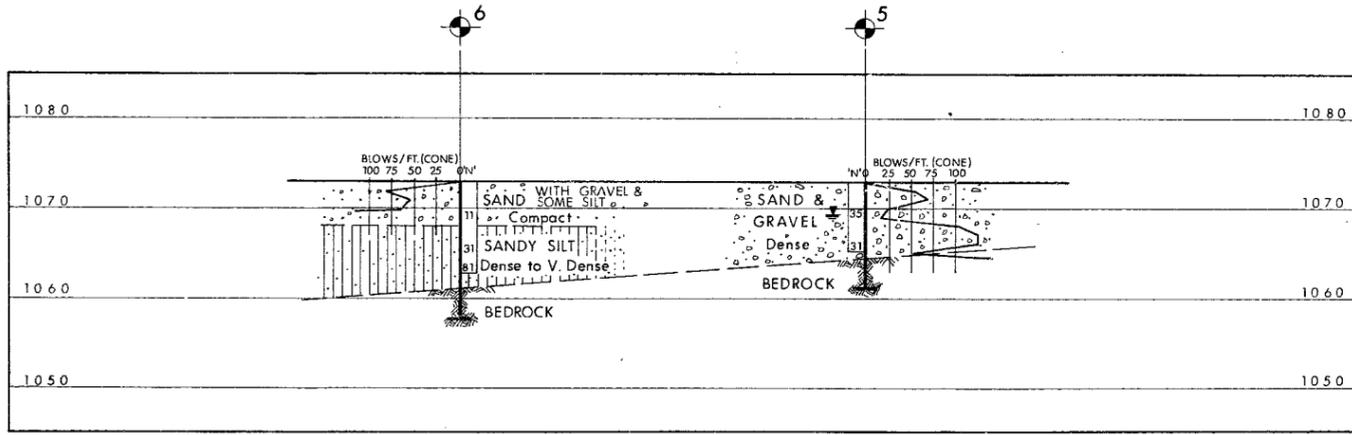
D.H.O. PATROL

YARD

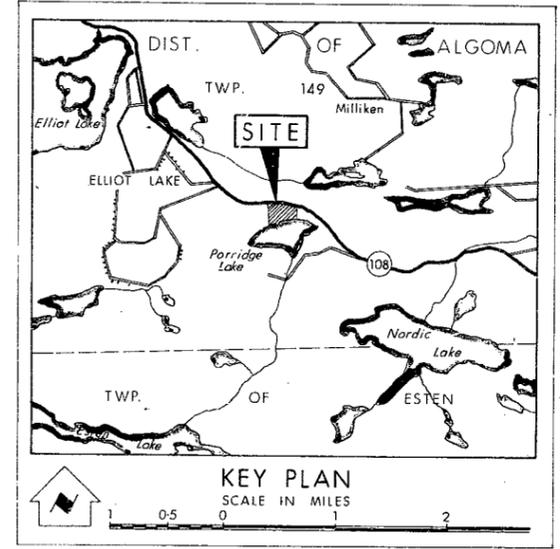
ELLIOT LAKE



PLAN  
SCALE  
100 50 0 100 200 FEET



SECTION A-A  
SCALE  
10 5 0 10 20 FEET



LEGEND

- ⊕ Cone Penetration Hole
- ⊙ Bore & Cone Penetration Hole
- ⬇ Water Level (22 May 1965)

- NOTE -  
THE BOUNDARIES BETWEEN SOIL STRATA HAVE BEEN ESTABLISHED ONLY AT BORE HOLE LOCATIONS. BETWEEN BORE HOLES THE BOUNDARIES ARE ASSUMED FROM GEOLOGICAL EVIDENCE AND MAY BE SUBJECT TO CONSIDERABLE ERROR.

DEPARTMENT OF HIGHWAYS - ONTARIO MATERIALS & RESEARCH SECTION		
PROPOSED ELLIOT LAKE PATROL YARD		
SHOWING POSITIONS & ELEVATIONS OF HOLES		
HWY. 108	DISTRICT 17	COUNTY ALGOMA
TOWNSHIP 149	LOT	CON.
LOCATION 0.5 MILES SOUTH OF ELLIOT LAKE		
DRAWN BY: S. O.	CHECKED BY:	W.P.
DATE 17 AUG. 1965	APPROVED BY: <i>[Signature]</i>	DRAWING NO. 65-F(R)-52A
SCALE AS SHOWN		

DEPARTMENT OF HIGHWAYS ONTARIO

MEMORANDUM

*Dist. 38-17.*

Mr. C. S. Moase,  
Manager,  
Special Services Section,  
Admin. Bldg.

FROM: Foundation Section,  
Materials & Testing Div.,  
Room 107, Lab. Bldg.

DATE: July 15, 1965

OUR FILE REF.

IN REPLY TO

SUBJECT:

FOUNDATION INVESTIGATION REPORT

For

D.H.O. Patrol Yard at Elliot Lake,  
Hwy. #108, Township #149, District  
of Algoma, District #17 (Sudbury).

W.J. 65-F(R)-52 - W.P. (N11)

Attached, we are forwarding to you, our detailed foundation investigation report on the subsoil conditions existing at the above structure site.

We believe that you will find the factual data and recommendations contained therein, adequate for your design requirements. Should you require additional information, please feel free to contact our Office.

KYL/MdeF  
Attach.

cc: Messrs. C. S. Moase (4)  
E. J. Orr  
D. W. Farren  
T. A. Sharpe  
E. R. Saint  
A. Watt

*K. Y. Lo*  
K. Y. Lo,  
SUPERVISING FOUNDATION ENGINEER

Foundations Office  
Gen. Files /

FOUNDATION INVESTIGATION REPORT

For

D.H.O. Patrol Yard at Elliot Lake,  
Hwy. #108, Township #149, District  
of Algoma, District #17 (Sudbury).

W.J. 65-F(R)-52 - W.P. (Nil)

A request, dated March 24, 1965, for a foundation investigation at the site of a proposed Patrol Yard in Elliot Lake, was received by this Section from the Special Services Section.

The site itself, appears to be a disused building contractor's yard. It is roughly trapezoidal in shape, covering a total area of 23.42 acres and has mean dimensions of approximately 1,500' x 700'.

Roughly in the centre of this area is a large, 150' x 80', concrete block garage and adjacent to this and to the East is a large mound of soil, rock and concrete. This mound is about 30' high with a ground coverage of nearly 300' x 200'.

The extreme South-East and South-West corners of this site are swamp areas. Porridge Lake adjoins the site all along the Southern edge.

Bedrock outcrops occur in the North-West corner and at other random places throughout the site.

The area with which this investigation is concerned has dimensions of about 500' x 300' and occurs to the North and West of the existing garage.

cont'd. /2 ...

The topography in the vicinity of the site is undulating to hilly and consists mainly of bush with many lakes and outcrops of rock. Mining and forestry appear to be the main means of subsistence in this area.

Six dynamic cone penetration holes and four sampled boreholes were carried out during the course of the investigation. These are shown in detail in the Appendix to this report.

The subsoil at this site consists of silt to sand and gravel with some silt. The mean constituent makeup of this material is as follows: 9% gravel, 51% sand, and 40% silt and clay. The silt and clay fractions were grouped together for convenience, but in the writer's estimation, the mean clay fraction is no greater than 2%.

This material was yellowy-brown to brownish-grey in colour, and has an extremely dense surface layer in the area in which the building is proposed. This upper surface layer is fill which extends to a maximum depth of 5' below ground level.

Bedrock occurs at 8' to 12.5' below ground level under the proposed building. Ground level in this area is between El. 1,073.1 and El. 1,074.4 and ground water exists at a minimum depth of 4' below ground level.

Recommended foundations for this site are spread footings founded on bedrock with a design bearing load of 10 tons/square foot.

A dewatering scheme may be necessary as foundations will be below ground water level.

It was observed that a 33' x 22' area of flat bedrock outcropped level with the surface about 100 ft. to the North-East

of the proposed building and it is suggested that a 50-ft. change in position of the proposed building would result in foundations on bedrock about 5 ft. below ground level as opposed to the existing 8' to 12.5' below ground level, or with a 100-ft. move, the building could be built on surface bedrock.

These measures are obviously more economical with respect to the foundations and would have to be considered in relationship to the necessity of having the building in the exact location originally proposed.

The field work was carried out during May 18 to May 22, 1965, under the supervision of Mr. P.M.A. McGlone, Project Foundation Engineer, who also wrote this report. This project was under the general supervision of Mr. K. G. Selby, Senior Foundation Engineer, who also reviewed this report.

July 1965

APPENDIX I.







DEPARTMENT OF HIGHWAYS - ONTARIO

## RECORD OF BOREHOLE NO. 5

FOUNDATION SECTION

MATERIALS &amp; TESTING DIVISION

JOB 65-F-52LOCATION As shown on Drawing.

ORIGINATED BY \_\_\_\_\_

W.P. \_\_\_\_\_

BORING DATE May 22, 1965.

COMPILED BY \_\_\_\_\_

DATUM GeodeticBOREHOLE TYPE BX Casing - Washboring.CHECKED BY dlr

SOIL PROFILE			SAMPLES			ELEV. SCALE	DYNAMIC PENETRATION RESISTANCE					LIQUID LIMIT — WL		BULK DENSITY	REMARKS
ELEV. DEPTH	DESCRIPTION	STRAT. PLOT	NUMBER	TYPE	BLOWS / FOOT		BLOWS / FOOT	20	40	60	80	100	PLASTIC LIMIT — WP		
1073.0															
	Sand and gravel with some silt.	•••••				1070									
	Dense.		1	SS	35										
	Grey.														
			2	SS	31										
1064.4															
8.6	Bedrock														
12.0	End of borehole.					1060									

Gr 46% Ss 47%  
Sl & Cl 7%

DEPARTMENT OF HIGHWAYS - ONTARIO

MATERIALS & TESTING DIVISION

RECORD OF BOREHOLE NO. 6

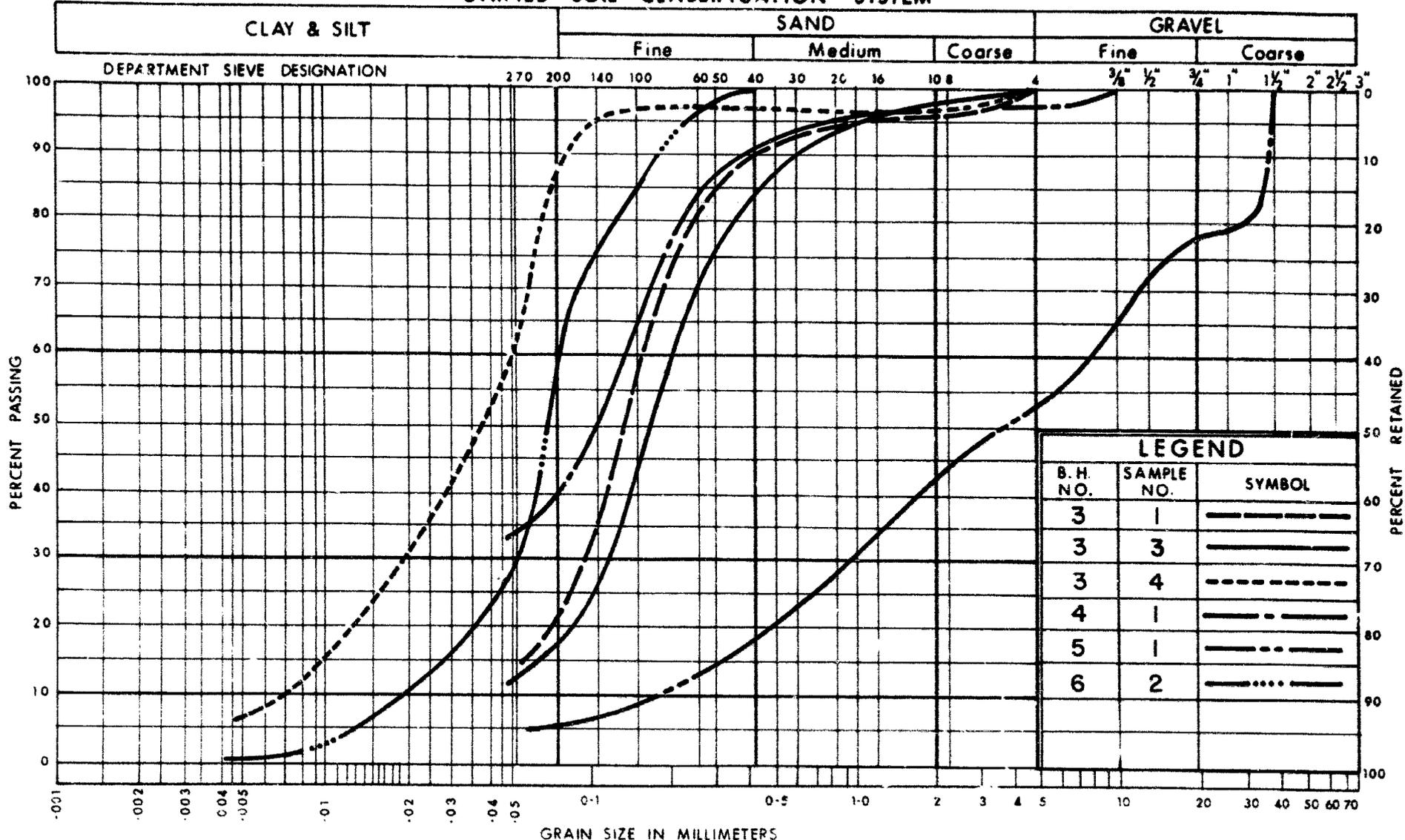
FOUNDATION SECTION

JOB 65-F-52 LOCATION As shown on Drawing. ORIGINATED BY P. McG  
 W.P. \_\_\_\_\_ BORING DATE May 22, 1965. COMPILED BY \_\_\_\_\_  
 DATUM Geodetic BOREHOLE TYPE BX Casing - Washboring. CHECKED BY HR

SOIL PROFILE			SAMPLES			ELEV. SCALE	DYNAMIC PENETRATION RESISTANCE					LIQUID LIMIT — WL PLASTIC LIMIT — WP WATER CONTENT — W WP — W — WL WATER CONTENT %	BULK DENSITY P.C.F.	REMARKS	
ELEV. DEPTH	DESCRIPTION	STRAT. PLOT	NUMBER	TYPE	BLOWS / FOOT		BLOWS / FOOT 20 40 60 80 100								SHEAR STRENGTH P.S.F.
1073.0															
	Sand with gravel and some silt. Compact Brown (Fill)		1	SS	11	1070									
1068.0															
5.0	Sandy-silt Dense to very dense. Brown-Grey		2	SS	31										
			3	SS	81										
1061.0															
12.0	Bedrock					1060									
1056.5															
16.5	End of Hole.					1050									

Sa 39% Si 60%  
Cl 1%

### UNIFIED SOIL CLASSIFICATION SYSTEM



DEPARTMENT OF HIGHWAYS  
MATERIALS and  
TESTING  
DIVISION

## GRAIN SIZE DISTRIBUTION

W.P. No.

JOB No. 65-F(R)-52

## ABBREVIATIONS USED IN THIS REPORT

### PENETRATION RESISTANCE

STANDARD PENETRATION RESISTANCE 'N' -- THE NUMBER OF BLOWS REQUIRED TO ADVANCE A STANDARD SPLIT SPOON SAMPLER 12 INCHES INTO THE SUBSOIL, DRIVEN BY MEANS OF A 140 POUND HAMMER FALLING FREELY A DISTANCE OF 30 INCHES.

DYNAMIC PENETRATION RESISTANCE -- THE NUMBER OF BLOWS REQUIRED TO ADVANCE A 2 INCH, 60 DEGREE CONE, FITTED TO THE END OF DRILL RODS, 12 INCHES INTO THE SUBSOIL, THE DRIVING ENERGY BEING 350 FOOT POUNDS PER BLOW.

### DESCRIPTION OF SOIL

THE CONSISTENCY OF COHESIVE SOILS AND THE RELATIVE DENSITY OR DENSENESS OF COHESIONLESS SOILS ARE DESCRIBED IN THE FOLLOWING TERMS :-

<u>CONSISTENCY</u>	<u>'N' BLOWS / FT.</u>	<u>c LB. / SQ FT.</u>	<u>DENSENESS</u>	<u>'N' BLOWS / FT.</u>
VERY SOFT	0 - 2	0 - 250	VERY LOOSE	0 - 4
SOFT	2 - 4	250 - 500	LOOSE	4 - 10
FIRM	4 - 8	500 - 1000	COMPACT	10 - 30
STIFF	8 - 15	1000 - 2000	DENSE	30 - 50
VERY STIFF	15 - 30	2000 - 4000	VERY DENSE	> 50
HARD	> 30	> 4000		

### TYPE OF SAMPLE

S.S	SPLIT SPOON	T W	THINWALL OPEN
W S	WASHED SAMPLE	T P	THINWALL PISTON
S.B	SCRAPER BUCKET SAMPLE	O S	OESTERBERG SAMPLE
A S	AUGER SAMPLE	F S	FOIL SAMPLE
C S	CHUNK SAMPLE	R C	ROCK CORE
S T	SLOTTED TUBE SAMPLE		
	P H		SAMPLE ADVANCED HYDRAULICALLY
	M		SAMPLE ADVANCED MANUALLY

### SOIL TESTS

Q <sub>u</sub>	UNCONFINED COMPRESSION	L.V	LABORATORY VANE
Q	UNDRAINED TRIAXIAL	F.V	FIELD VANE
Q <sub>cu</sub>	CONSOLIDATED UNDRAINED TRIAXIAL	C	CONSOLIDATION
Q <sub>d</sub>	DRAINED TRIAXIAL	S	SENSITIVITY

# ABBREVIATIONS USED IN THIS REPORT

## SOIL PROPERTIES

$\gamma$	UNIT WEIGHT OF SOIL (BULK DENSITY)
$\gamma_s$	UNIT WEIGHT OF SOLID PARTICLES
$\gamma_w$	UNIT WEIGHT OF WATER
$\gamma_d$	UNIT DRY WEIGHT OF SOIL (DRY DENSITY)
$\gamma'$	UNIT WEIGHT OF SUBMERGED SOIL
G	SPECIFIC GRAVITY OF SOLID PARTICLES $G = \frac{\gamma_s}{\gamma_w}$
e	VOID RATIO
n	POROSITY
w	WATER CONTENT
$S_r$	DEGREE OF SATURATION
$w_L$	LIQUID LIMIT
$w_p$	PLASTIC LIMIT
$I_p$	PLASTICITY INDEX
s	SHRINKAGE LIMIT
$I_L$	LIQUIDITY INDEX = $\frac{w - w_p}{I_p}$
$I_C$	CONSISTENCY INDEX = $\frac{w_L - w}{I_p}$
$e_{max}$	VOID RATIO IN LOOSEST STATE
$e_{min}$	VOID RATIO IN DENSEST STATE
$I_D$	DENSITY INDEX = $\frac{e_{max} - e}{e_{max} - e_{min}}$
	RELATIVE DENSITY $D_r$ IS ALSO USED
h	HYDRAULIC HEAD OR POTENTIAL
q	RATE OF DISCHARGE
v	VELOCITY OF FLOW
i	HYDRAULIC GRADIENT
k	COEFFICIENT OF PERMEABILITY
j	SEEPAGE FORCE PER UNIT VOLUME
$m_v$	COEFFICIENT OF VOLUME CHANGE = $\frac{-\Delta e}{(1+e)\Delta\sigma}$
$c_v$	COEFFICIENT OF CONSOLIDATION
$C_c$	COMPRESSION INDEX = $\frac{\Delta e}{\Delta \log_{10} \sigma}$
$T_v$	TIME FACTOR = $\frac{C_v t}{d^2}$ (d, DRAINAGE PATH)
U	DEGREE OF CONSOLIDATION
$\tau_f$	SHEAR STRENGTH
$c'$	EFFECTIVE COHESION INTERCEPT
$\phi'$	EFFECTIVE ANGLE OF SHEARING RESISTANCE, OR FRICTION
$c_u$	APPARENT COHESION
$\phi_u$	APPARENT ANGLE OF SHEARING RESISTANCE, OR FRICTION
$\mu$	COEFFICIENT OF FRICTION
$S_t$	SENSITIVITY

## GENERAL

$\pi$	= 3.1416
e	BASE OF NATURAL LOGARITHMS 2.7183
$\log_e a$ OR $\ln a$	NATURAL LOGARITHM OF a
$\log_{10} a$ OR $\lg a$	LOGARITHM OF a TO BASE 10
t	TIME
g	ACCELERATION DUE TO GRAVITY
V	VOLUME
W	WEIGHT
M	MOMENT
F	FACTOR OF SAFETY

## STRESS AND STRAIN

u	PORE PRESSURE
$\sigma$	NORMAL STRESS
$\sigma'$	NORMAL EFFECTIVE STRESS ( $\bar{\sigma}$ IS ALSO USED)
$\tau$	SHEAR STRESS
$\epsilon$	LINEAR STRAIN
$\gamma$	SHEAR STRAIN
$\nu$	POISSON'S RATIO ( $\mu$ IS ALSO USED)
E	MODULUS OF LINEAR DEFORMATION (YOUNG'S MODULUS)
G	MODULUS OF SHEAR DEFORMATION
K	MODULUS OF COMPRESSIBILITY
$\eta$	COEFFICIENT OF VISCOSITY

## EARTH PRESSURE

d	DISTANCE FROM TOP OF WALL TO POINT OF APPLICATION OF PRESSURE
$\delta$	ANGLE OF WALL FRICTION
K	DIMENSIONLESS COEFFICIENT TO BE USED WITH VARIOUS SUFFIXES IN EXPRESSIONS REFERRING TO NORMAL STRESS ON WALLS
$K_0$	COEFFICIENT OF EARTH PRESSURE AT REST

## FOUNDATIONS

B	BREADTH OF FOUNDATION
L	LENGTH OF FOUNDATION
D	DEPTH OF FOUNDATION BENEATH GROUND
N	DIMENSIONLESS COEFFICIENT USED WITH A SUFFIX APPLYING TO SPECIFIC GRAVITY, DEPTH AND COHESION ETC. IN THE FORMULA FOR BEARING CAPACITY
$k_s$	MODULUS OF SUBGRADE REACTION

## SLOPES

H	VERTICAL HEIGHT OF SLOPE
D	DEPTH BELOW TOE OF SLOPE TO HARD STRATUM
$\beta$	ANGLE OF SLOPE TO HORIZONTAL

