

#58-F-13

W.P. #34-58

HWY #401 &

GRAVEL RD. REVISION

2 MI. W. OF

CAMPBELLVILLE

NASSAGAWEYA

FOUNDATION REPORT

ON

**NEW BRIDGE AT HIGHWAY 401 AND
GRAVEL ROAD REVISION CROSSING, 2
MILES WEST OF CAMPBELLVILLE (CON.IAII)
TOWNSHIP OF NASDAQAWA**

Plan No. F-3523413

Station No:288/30

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Mr. D. C. Ramsay Design Engineer	(1)
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Foundation Section	(1)
File	(1)

W.P. 5-58

W.L. F-3523

INTRODUCTION:

A subsoil investigation was carried out to determine the bearing values of the subsoil layers for supporting the foundations of the proposed structure.

The site is located at about 2 miles west of Campbellville where the new highway no. 401 underpasses the proposed gravel road Revision between con. I & II in the Township of Massaraweys. (station 288/30, profile No. F-3523-12).

The job started on April 25, 1958 and was completed on May 2, 1958.

DESCRIPTION OF SITE AND FIELD WORK:

The site is located in the area referred to as "Flamborough Plain". It is basically limestone plain with bouldery glacial till or sand and gravel as overburden. The surface topography is characterized by scattered drumlins, wooded swamps, and spots of limestone outcrop. (One such outcrop exists some 200 ft. west of the investigation site).

The subsoil investigation was carried out by means of a skid mounted coredrill machine. In the course of investigations four boreholes were made. The boreholes were advanced by alternately driving and washing the PI casing. During this operation samples were extracted and standard penetration resistance was registered. By driving 2" diameter cone from ground surface down to refusal the dynamic cone penetration profiles were established. The boreholes were stopped after bedrock was encountered at depths shown on log sheets.

The locations of the boreholes is shown on drawing no. F-58-13A and their elevations on log sheets under Appendix I.

FIELD AND LABORATORY FINDINGS:

The investigations carried out at this site revealed the following subsoil stratigraphy:

Under the topsoil down to bedrock it is one layer of gravel and sandy loam spotted with various sizes of boulders. Underlying this layer is bedrock which was encountered in all four boreholes. The bedrock was drilled by means of AIT diamond bit and core samples were extracted. From laboratory analysis the bedrock was identified as pitted Dolomite.

The samples tested at the laboratory gave the textural composition of the subsoil encountered in the boreholes as tabulated below:

	<u>Binder</u>	<u>Fine AGG.</u>	<u>Coarse AGG.</u>
B. H. No. 1	20%	39%	31%
2	19%	23%	58%
3	30%	30%	40%
4	20%	33%	47%

The natural moisture of the layer was measured to be 8%. The nature of the soil prevented the performing of any other reliable tests in the laboratory. The soil in the layer is considered to be nonplastic and inorganic.

SUPPORT OF THE ABUTMENTS:

The new highway no. 401 is underpassing the proposed

gravel road in vision at this crossing. According to the new grade line the surface elevation of the new highway will be lowered to elevation 964 ft. It is presumed that the new structure will be supported on 7 ft. wide continuous footings and that these footings will be placed at about elevation 958 ft. (allowing some 6 ft. for ditching and frost). The soil in the layer is considered to be nonplastic, granular and bearing values were derived from standard penetration tests. According to the bulb pressure distribution, the stressed layer is in between the elevation where the footing will be placed (958 ft.) and the elevation at a depth of twice the width of the footing (944 ft.). The average bearing value in this depth interval, derived from standard penetration test results, is more than 3 T.s.f. for one inch maximum settlement. It will be seen that the proposed elevation for placing the footings is some 2 to 6 ft. above the encountered bedrock. If desired the footings could be placed on bedrock where ample bearing values will be available.

CONCLUSIONS AND RECOMMENDATIONS:

From the above discussion it will follow that:

1. The subsoil at this site is one layer of gravel and sandy loam, spotted with various sizes of boulders.
2. The layer is considered to be made up of nonplastic, granular material. The bearing values were derived from standard penetration test results.

3. It would possibly be desirable to place the footings at elevation 958 ft. in which case the bearing value of 3 T.s.f. for one inch settlement could be used. However, in view of the proximity of the bedrock, it would appear more appropriate to place the footings on the bedrock where ample bearing value will be available.
4. The approach fills to the new structure do not present any stability problem.


Y. Korlu,
Foundation Engineer.

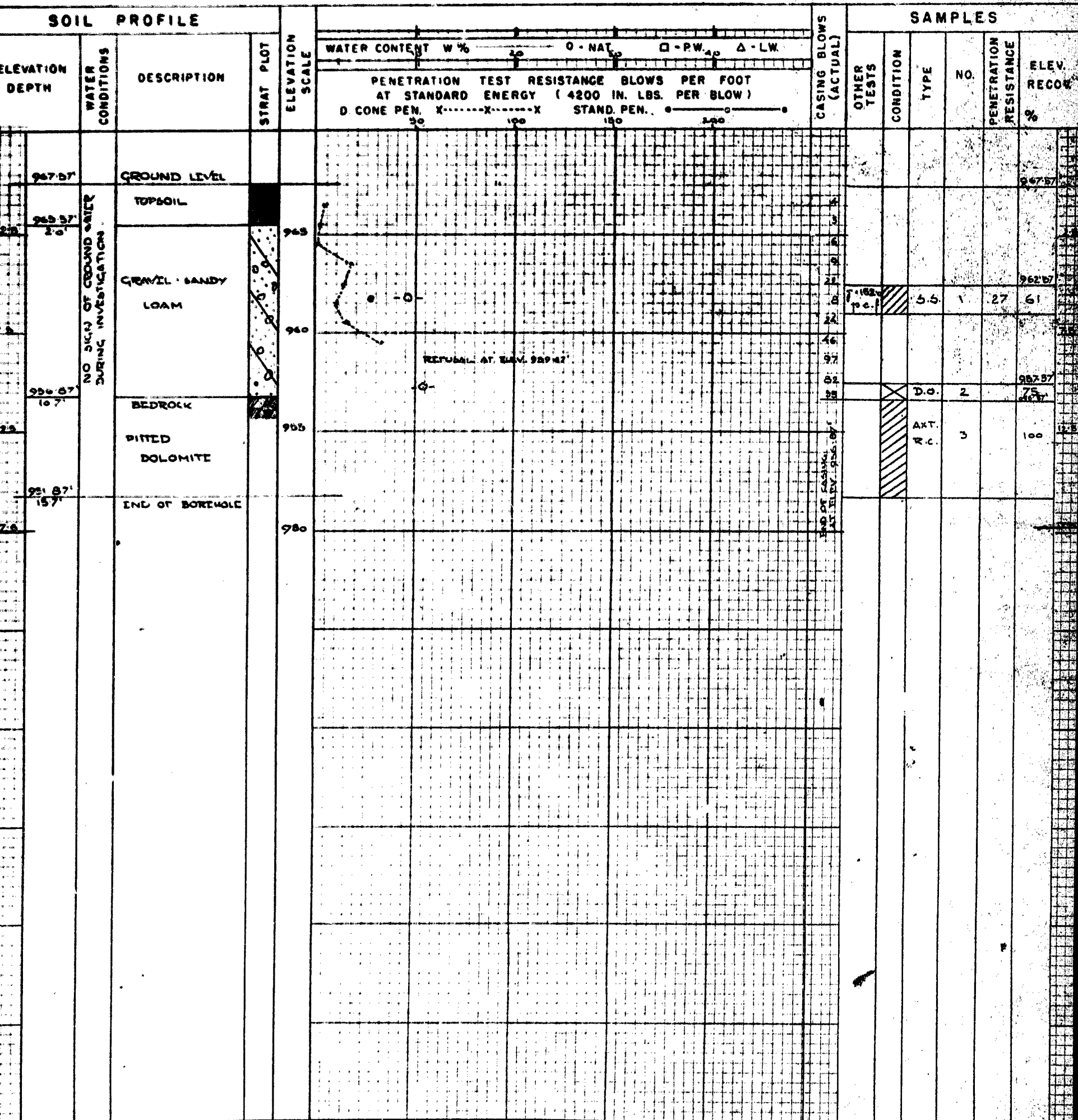
APPENDIX I.

DEPARTMENT OF HIGHWAYS - ONTARIO
MATERIALS & RESEARCH BRANCH - FOUNDATIONS SECTION - DOWNSVIEW
OFFICE REPORT ON SOIL EXPLORATION

DRILL RIG B-1-B OPERATION BORE & PENET JOB T-58-13 WP 34-58 BORING 1 STA. 288+16 (32 FT)
CASING Bx (standard samplers to fit unless noted) DATUM GEODETIC DATE REPORT MAY 1958
SAMPLER HAMMER WT 250 LBS. DROP 18 INCHES COMPILED BY H.S. CHECKED BY A.L. DATE BORING 25 APRIL 1958

ABBREVIATIONS
V - INSITU VANE SHEAR TEST Q - TRIAXIAL QUICK K - PERMIABILITY CS - CHUNK
M - MECHANICAL ANALYSIS S - TRIAXIAL SLOW C - CONSOLIDATION DO - DRIVE OPEN
U - UNCONFINED COMPRESSION WL - WATER LEVEL IN CASING CA - CASING DF - DRIVE FOOT VALVE
Qc - TRIAXIAL CONSOLIDATED QUICK WT - WATER TABLE IN SOIL γ - UNIT WEIGHT TO - THIN WALLED OPEN
RS - SLEEVE SAMPLE
PS - PISTON SAMPLE
WS - WASHED SAMPLE
RC - ROCK CORE

SAMPLE CONDITION
 - DISTURBED
- FAIR
- GOOD
- LOST



DEPARTMENT OF HIGHWAYS - ONTARIO

MATERIALS & RESEARCH BRANCH - FOUNDATIONS SECTION - DOWNSVIEW

OFFICE REPORT ON SOIL EXPLORATION

DRILL RIG 54-5 OPERATION BORE & PENET'N JOB F-58-13 WP 34-58 BORING 2 STA. 243+92 (32' T)

CASING BX (standard samplers to fit unless noted) DATUM GEODETIC DATE REPORT MAY 1958

SAMPLER HAMMER WT. 250 LBS. DROP 18 INCHES COMPILED BY 4.6 CHECKED BY A.L. DATE BORING 29 APR. 1958


ABBREVIATIONS

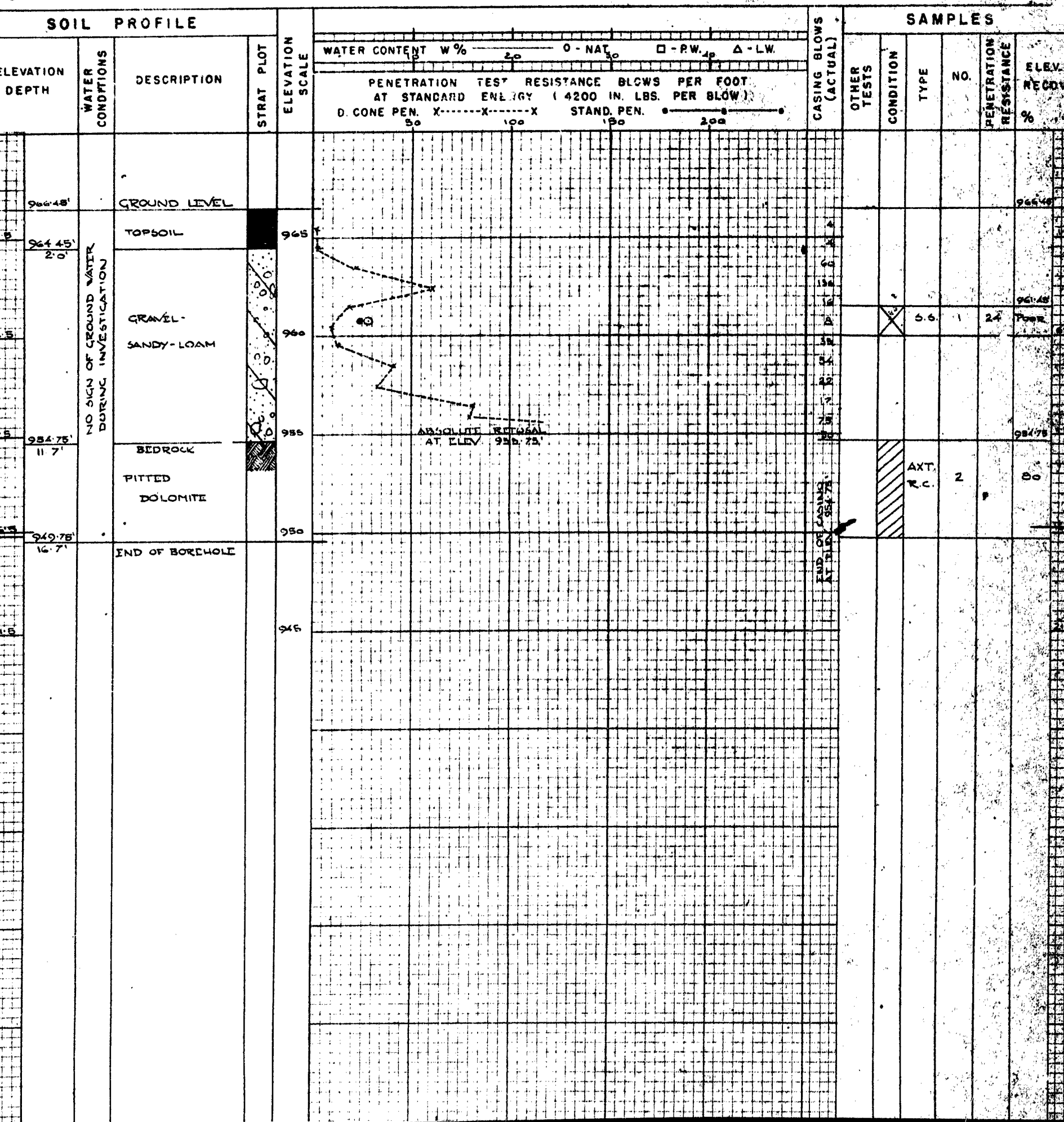
V - INSITU VANE SHEAR TEST Q - TRIAXIAL QUICK K - PERMIABILITY C.S. - CHUNK S.S. - SLEEVE SAMPLE

M - MECHANICAL ANALYSIS S - TRIAXIAL SLOW C - CONSOLIDATION D.O. - DRIVE OPEN P.S. - PISTON SAMPLE

U - UNCONFINED COMPRESSION WL - WATER LEVEL IN CASING CA - CASING D.F. - DRIVE FOOT VALVE W.S. - WASHED SAMPLE

Qc - TRIAXIAL CONSOLIDATED QUICK WT - WATER TABLE IN SOIL γ - UNIT WEIGHT T.O. - THIN WALLED OPEN R.C. - ROCK CORE

 - DISTURBED
- FAIR
- GOOD
- LOST



DEPARTMENT OF HIGHWAYS - ONTARIO
MATERIALS & RESEARCH BRANCH - FOUNDATIONS SECTION - DOWNSVIEW
OFFICE REPORT ON SOIL EXPLORATION

DRILL RIG 34-5 OPERATION BORE & PENET'N JOB T-58-13 WP 34-58 BORING 3 STA. 288+48 (441)
CASING 3X (standard samplers to fit unless noted) DATUM GEODETIC DATE REPORT MAY 1958
SAMPLER HAMMER WT. 250 LBS. DROP 18 INCHES COMPILED BY H.S. CHECKED BY A.L. DATE BORING 30 APR. 1958

ABBREVIATIONS

V - INSITU VANE SHEAR TEST Q - TRIAXIAL QUICK K - PERMIABILITY
M - MECHANICAL ANALYSIS S - TRIAXIAL SLOW C - CONSOLIDATION
U - UNCONFINED COMPRESSION WL - WATER LEVEL IN CASING CA - CASING
Qc - TRIAXIAL CONSOLIDATED QUICK WT - WATER TABLE IN SOIL γ - UNIT WEIGHT

SAMPLE TYPES

C.S. - CHUNK S.S. - SLEEVE SAMPLE
D.O. - DRIVE OPEN P.S. - PISTON SAMPLE
D.F. - DRIVE FOOT VALVE W.S. - WASHED SAMPLE
T.O. - THIN WALLED OPEN R.C. - ROCK CORE

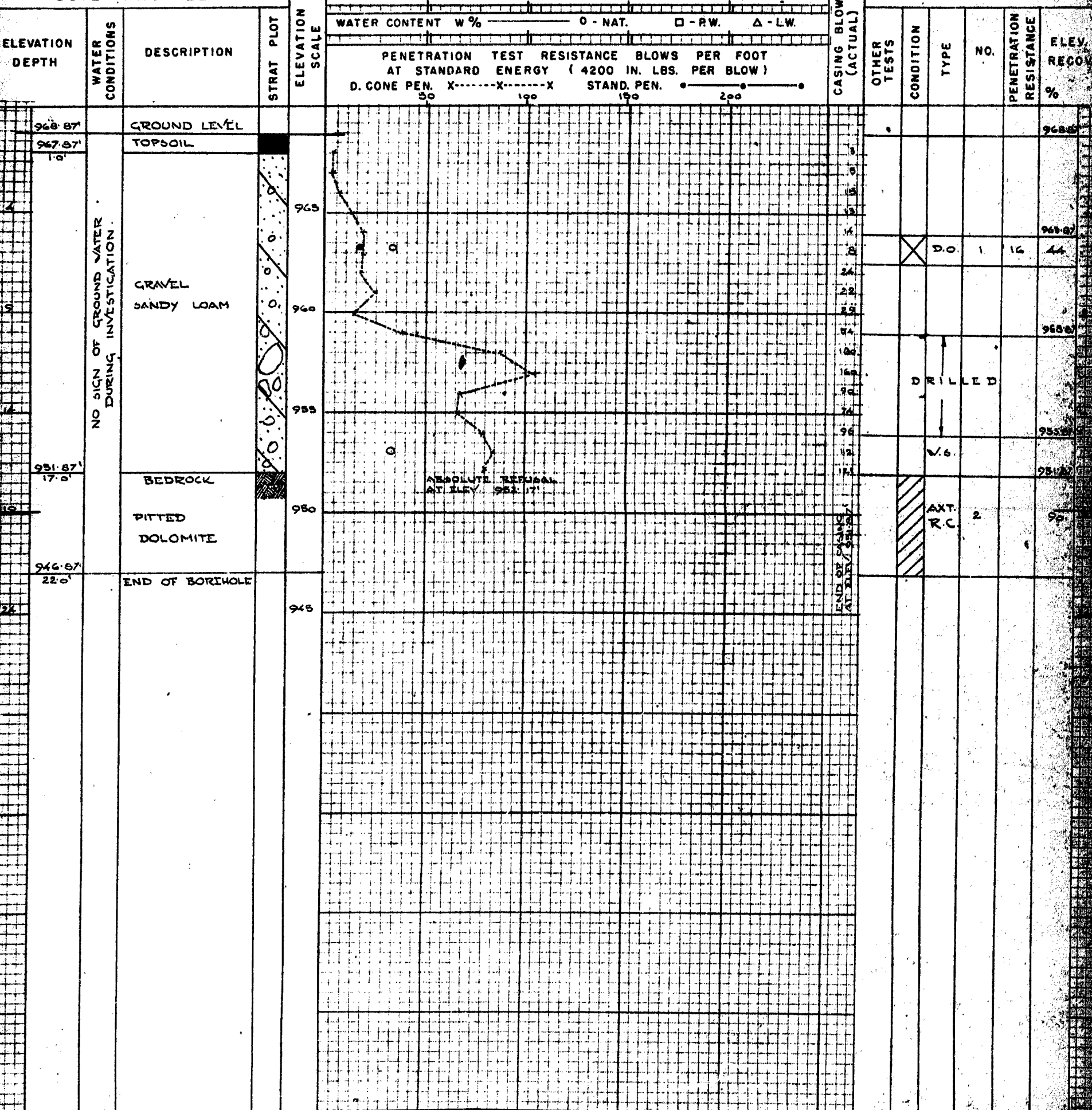
SAMPLE CONDITION



- DISTURBED
- FAIR
- GOOD
- LOST

SOIL PROFILE

SAMPLES



DEPARTMENT OF HIGHWAYS - ONTARIO
MATERIALS & RESEARCH BRANCH - FOUNDATIONS SECTION - DOWNSVIEW
OFFICE REPORT ON SOIL EXPLORATION

DRILL RIG 54-5 OPERATION BORE & PENET'N JOB F-58-13 WP 34-58 BORING # STA. 208+47 (33' RT.)
CASING BX (standard samplers to fit unless noted) DATUM GEODETIC DATE REPORT MAY 1958
SAMPLER HAMMER WT. 250 LBS. DROP 18 INCHES COMPILED BY H.S. CHECKED BY A.L. DATE BORING 1 MAY 1958

ABBREVIATIONS

V - INSITU VANE SHEAR TEST Q - TRIAXIAL QUICK K - PERMIABILITY
M - MECHANICAL ANALYSIS S - TRIAXIAL SLOW C - CONSOLIDATION
U - UNCONFINED COMPRESSION WL - WATER LEVEL IN CASING CA - CASING
QC - TRIAXIAL CONSOLIDATED QUICK WT - WATER TABLE IN SOIL γ - UNIT WEIGHT

SAMPLE TYPES

CS - CHUNK SS - SLEEVE SAMPLE
DO - DRIVE OPEN PS - PISTON SAMPLE
DF - DRIVE FOOT VALVE WS - WASHED SAMPLE
TO - THIN WALLED OPEN RC - ROCK CORE

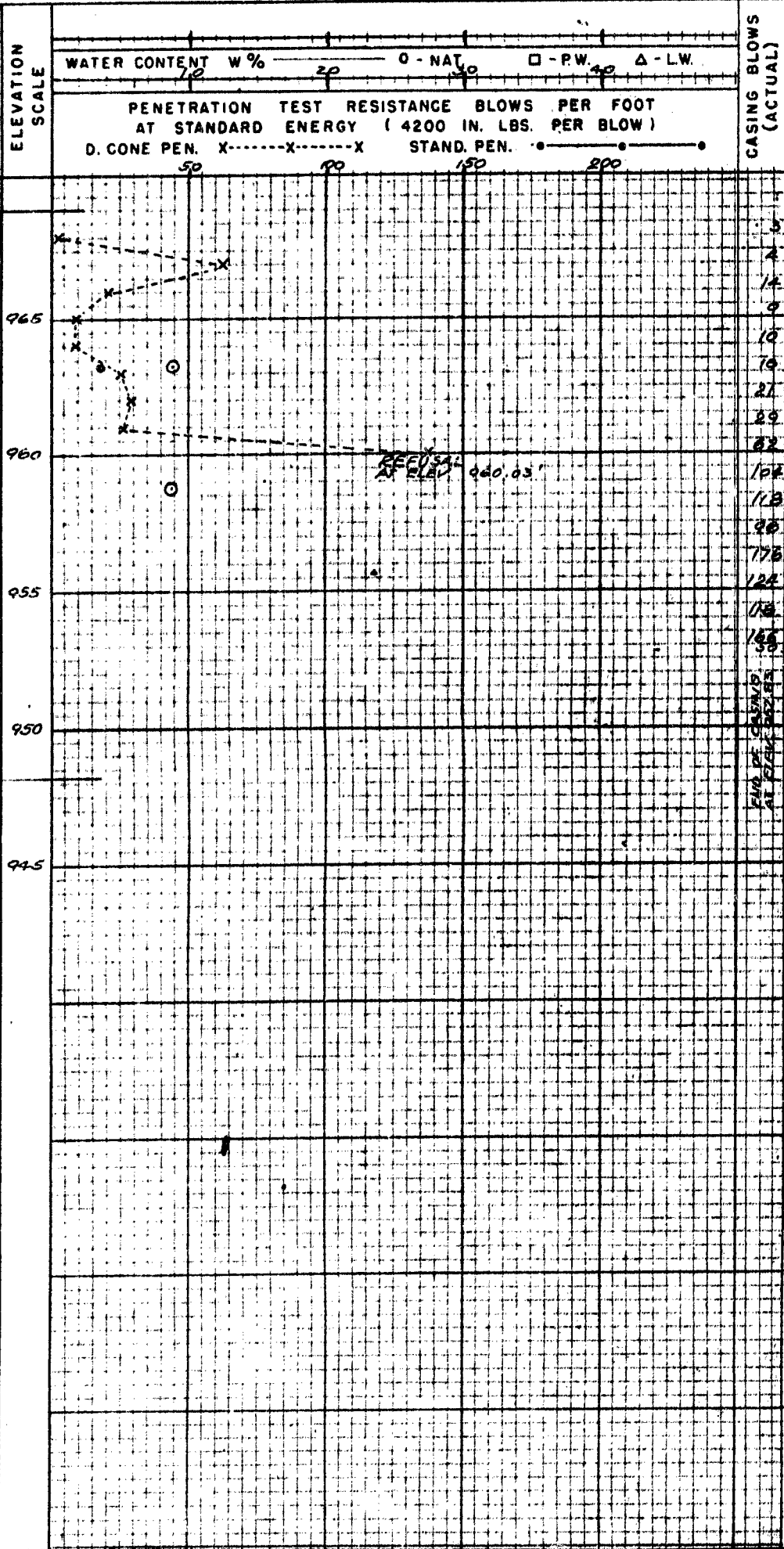
SAMPLE CONDITION



- DISTURBED
- FAIR
- GOOD
- LOST

SOIL PROFILE

ELEVATION DEPTH	WATER CONDITIONS	DESCRIPTION	STRAT. PLOT
969.13'		GROUND LEVEL	
967.63' 1.5'		TOP SOIL	
		GRAVEL - SANDY LOAM	
952.83' 16.3'	NO SIGN OF GROUND WATER DURING INVESTIGATION	BEDROCK	
		PITTED DOLOMITE	
948.33' 20.8'		END OF BOREHOLE	



SAMPLES

OTHER TESTS	CONDITION	TYPE	NO.	PENETRATION RESISTANCE %	ELEV. RECOV.
					969.13
					967.63
					964.13
		DO.	1	18	67
					959.13
		DO.	2		63
					954.13
					949.13
					944.13
					939.13
					934.13
					929.13
					924.13
					919.13
					914.13
					909.13
					904.13
					899.13
					894.13
					889.13
					884.13
					879.13
					874.13
					869.13
					864.13
					859.13
					854.13
					849.13
					844.13
					839.13
					834.13
					829.13
					824.13
					819.13
					814.13
					809.13
					804.13
					799.13
					794.13
					789.13
					784.13
					779.13
					774.13
					769.13
					764.13
					759.13
					754.13
					749.13
					744.13
					739.13
					734.13
					729.13
					724.13
					719.13
					714.13
					709.13
					704.13
					699.13
					694.13
					689.13
					684.13
					679.13
					674.13
					669.13
					664.13
					659.13
					654.13
					649.13
					644.13
					639.13
					634.13
					629.13
					624.13
					619.13
					614.13
					609.13
					604.13
					599.13
					594.13
					589.13
					584.13
					579.13
					574.13
					569.13
					564.13
					559.13
					554.13
					549.13
					544.13
					539.13
					534.13
					529.13
					524.13
					519.13
					514.13
					509.13
					504.13
					499.13
					494.13
					489.13
					484.13
					479.13
					474.13
					469.13
					464.13
					459.13
					454.13
					449.13
					444.13
					439.13
					434.13
					429.13
					424.13
					419.13
					414.13
					409.13
					404.13
					399.13
					394.13
					389.13
					384.13
					379.13
					374.13
					369.13
					364.13
					359.13
					354.13
					349.13
					344.13
					339.13
					334.13
					329.13
					324.13
					319.13
					314.13
					309.13
					304.13
					299.13
					294.13
					289.13
					284.13
					279.13
					274.13
					269.13
					264.13
					259.13
					254.13
					249.13
					244.13
					239.13
					234.13
					229.13
					224.13
					219.13
					214.13
					209.13
					204.13
					199.13
					194.13
					189.13
					184.13
					179.13
					174.13
					169.13
					164.13
					159.13
					154.13
					149.13
					144.13
					139.13
					134.13
					129.13
					124.13
					119.13
					114.13
					109.13
					104.13
					99.13
					94.13
					89.13
					84.13
					79.13
					74.13
					69.13
					64.13
					59.13
					54.13
					49.13
					44.13
					39.13
					34.13
					29.13
					24.13
					19.13
					14.13
					9.13
					4.13