

#64-F-217C

W.P.# 27-62

Hwy # 53

C.N.R. SUBWAY

EASTWOOD

## DEPARTMENT OF HIGHWAYS ONTARIO

## MEMORANDUM

To: Mr. A. M. Toye,  
Bridge Engineer,  
Bridge Division.

FROM: Foundation Section,  
Materials & Testing Div.,  
Room 107, Lab. Bldg.

Attn: Mr. F. I. Hewson,  
Consultant Liaison Engr.

DATE: July 23, 1964

OUR FILE REF.

IN REPLY TO

SUBJECT:

FOUNDATION INVESTIGATION REPORT BY:  
Warnock Hersey Soil Investigations Ltd.  
For Canadian National Railways, Toronto.  
Reconstruction of Hwy. No. 11 Subway  
near Eastwood, Ontario, Mile +.9, Dundas  
Sub-Division. (D.H.C. District No. 2)

The report of the foundation investigation at the above site, submitted by Warnock Hersey Soil Investigations Ltd. has been reviewed.

The Consultant has suggested using piles for the foundation of the structure. However, the approach used by the Consultant to arrive at this recommendation is rather unconventional and conservative. It is our opinion that spread footings may be used with a design load of 3 T.S.F. at the proposed elevation of 945.0.

We believe that the foregoing comments will provide the information required. Should there be any queries in connection with this project, please feel free to contact our office.

KYL/MdeF

cc: Foundations Office  
Gen. Files

*J.W.A. G. Stermac,*  
PRINCIPAL FOUNDATION ENGINEER



BA 1884

## WARNOCK HERSEY SOIL INVESTIGATIONS LTD.

250 MADISON AVENUE, TORONTO 7, ONT. WA. 4-9691

S-64-45

February 28, 1964.

Canadian National Railways,  
151 Front Street West,  
Toronto 1, Ontario.

Attn: Mr. E. J. Napier  
Bridge Engineer.

Dear Sirs:

Enclosed is our report on the soil investigation recently conducted for the proposed reconstruction of the Highway No. 53 Subway near Eastwood, Ontario, Mile 44.9, Dundas Sub-Division. (Your File No. 1640-206).

We believe this report to be complete but should you have any queries regarding its content or interpretation, please contact the undersigned.

Yours truly,

WARNOCK HERSEY SOIL INVESTIGATIONS LTD



P. E. Lawrence, P. Eng.,  
Manager.

PBL/eb

COMPLETE FOUNDATION AND SUBGRADE INVESTIGATIONS

SOIL BORINGS AND SAMPLING • LABORATORY AND FIELD TESTING • LOAD BEARING TESTS • PILE LOADING TESTS • ROCK AND CONCRETE CORING • SEISMIC INVESTIGATIONS



INTRODUCTION

We were authorized by your letter dated February 11, 1964 to carry out a number of test borings at the proposed reconstruction of Highway No. 53 Subway near Eastwood, Ontario, Mile 44.9 Dundas Sub-Division.

This work consisted of drilling four (4) test holes to about 60 foot depth with soil sampling and penetration resistance tests carried out at regular intervals.

The purpose of this investigation was to determine -

1. Sub-soil strength and bearing values for foundation design.
2. Ground water conditions.
3. Any unusual sub-soil conditions which would require special attention in foundation design.

PROCEDURE

The field work was carried out during the period from February 13th to February 21st, 1964.

The test holes were located in accordance with your drawing by Mr. W. J. Wannemaker, Area Engineer at London and our drilling crew. Surface elevations of these test holes were supplied to us by Mr. Wannemaker. These elevations were taken with reference to the base of rail as shown on the enclosed sketch.

Continued...

S-64-45



PROCEDURE  
(Cont.)

These test holes were advanced by the wash boring procedure and standard split spoon samples were taken ahead of the BX size pipe used to case the holes. For each split spoon sample, the penetration blows to drive the sampler one foot were recorded. The energy of each blow was 4200 inch-pound obtained by a 140 pound hammer falling a distance of 30 inches. These penetration blows ( N value ) in sand and finer grained soils provide an empirical means of determining the strength, density and bearing value of the soil. All samples were returned to our laboratory for examination and classification. Water levels were measured at the completion of the drilling and at intervals of time thereafter. The final static water levels were determined by bailing the test hole dry and recording the depth to water when the equilibrium was reached. These depths and elevations are indicated on the enclosed bore-logs for Test Holes No. 1, 2, and 4A.

SOIL PROFILES

All four (4) test holes showed a surface layer of mixed organic fill ranging in thickness from 1 to 3 feet. Below this is a medium to dense glacial till, which again changes to a less dense very wet sand. This fine sand layer was encountered at the following elevations: -

Bore Hole No. 1	Elevation 952.6
Bore Hole No. 2	Elevation 935.1
Bore Hole No. 3A	Elevation 936.4
Bore Hole No. 4A	Elevation 946.5

Continued...

S-64-45



SOIL PROFILES  
(Cont.)

Below this sand stratum, which ranged in depth from 7 to 27 feet, the soil changed back to a medium dense glacial till with several thick sand layers.

A detailed description of all of the soil types encountered with the elevation of strata changes are shown on the enclosed borelogs at the end of this report.

WATER CONDITIONS

All samples below the 12 to 15 foot depth were very moist to wet. In particular, the stratum of sand encountered showed a very high water content.

The static water levels were recorded at the following depths below ground surface and elevations: -

<u>Bore Hole</u>	<u>Depth Below Ground Surface</u>	<u>Elevation</u>
1	15' - 0"	950.1
2	14' - 0"	949.1
4B	12' - 0"	948.5

These water levels are shown on the borelogs enclosed at the end of this report.

CONCLUSIONS

&

RECOMMENDATIONS

1. The following table gives the theoretical allowable bearing values for spread footings at various depths below the ground surface at the boreholes: -

Continued...

## ALLOWABLE BEARING VALUES

Tons/square Foot

Bore Hole No. -

123A4A

Elevation -

965.1

963.1

961.9

960.5

Footing Width -

	<u>Top Loss</u>	<u>5-10<sup>1</sup></u>	<u>5-10<sup>2</sup></u>	<u>5-10<sup>3</sup></u>	<u>Top Loss</u>	<u>5-10<sup>1</sup></u>	<u>5-10<sup>2</sup></u>	<u>5-10<sup>3</sup></u>
--	-----------------	-------------------------	-------------------------	-------------------------	-----------------	-------------------------	-------------------------	-------------------------

Depth

3'	1.67	1.67	-	-	4.80	4.80	-	-
5'	3.00	3.00	3.36	3.36	4.80	4.80	1.54	1.54
7'	2.76	2.76	3.12	3.12	4.80	4.80	1.92	1.92
10'	3.60	3.60	3.36	3.36	2.16	2.16	3.12	3.12
12'	3.37	2.39	3.60	3.60	2.40	2.40	3.24	3.24
15'	3.99	1.68	4.00	4.00	2.36*	2.16*	2.49*	2.12*
20'	1.50*	1.24*	3.60*	3.60*	4.40	4.40	2.49	2.12
25'	1.25	1.02	2.76	2.76	1.75	1.46	1.99	1.68
30'	2.29	2.55	3.75	3.22	1.75	1.46	3.50	3.00
35'	3.12	2.57	1.99	1.68	4.20	4.20	2.76	2.76
40'	4.50	3.68	3.48	3.48	4.00	4.00	3.24	3.24
45'	4.00	3.14	3.20	3.20	3.24	3.24	4.00	4.00
50'	4.50	3.88	4.75	4.10	4.80	4.50	4.00	4.00
55'	4.75	4.10	4.75	4.10	4.80	4.80	4.60	4.60
60'	4.75	4.10	4.75	4.10	4.75	4.10	4.80	4.80



\* Approximate Elevation 945.0 \*

S-64-45



CONCLUSIONS  
&  
RECOMMENDATIONS  
(Cont.)

These tabulated values are based on the relationship of standard penetration blows and bearing values of the soil.

They include a factor of safety with regard to strength of 3.0 and a maximum settlement of one (1) inch.

Note: When using the above bearing values for design purposes, the smallest value must be chosen from the table for a distance of 1 1/2 times the footing width below the base of the footing. Since we understand the desired footing elevation for this reconstruction is approximately 945.0 feet, the following example has been worked out to illustrate the above note -

Example:

- Bore Hole No. 1(worst condition).
- Footing Width - 10 feet, - Footing depth-Elevation 945.0
- Allowable bearing value is only 1.02 tons per square foot at 15 feet below the footing.

2. To get the preferred allowable bearing value of 3.0 tons per square foot, it would be necessary to found normal spread footing at or below 40 foot depth.
3. If footing base is to be founded about Elevation 945.0, it will be necessary to use a pile foundation. A displacement type pile such as reinforced concrete would probably not penetrate more than 15 to 20 feet below Elevation 945.0.

Continued...

S-64-45



CONCLUSIONS

&

RECOMMENDATIONS  
(Cont.)

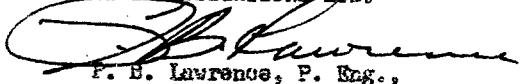
This would also densify considerably the looser sand stratum.

A steel "H" pile designed for skin friction plus end bearing would probably not penetrate more than 20 to 25 feet below Elevation 945.0.

4. Some water seepage is to be expected through the sand stratum when the excavation is carried below the water table at 12 to 14 foot depth.
  5. Excavations through the cohesive till material will stand with vertical sides for 10 feet or more, but all excavations through the wet sand stratum will require adequate shoring and bracing.
- SUMMARY
- The sub-soil at this site just below the preferred footing level, Elevation 945.0, consists of a fine sand which is inadequate for supporting the required bridge loadings on normal spread footings. We feel that it is necessary to use a pile type foundation consisting of quite short steel or concrete piles to support the structure.

Respectfully submitted,

WARNOCK HERSEY SOIL INVESTIGATIONS LTD.

  
P. B. Lawrence, P. Eng.,  
Manager.

Report by -  
R. S. Fleming.

PBL/eb



W.W.M.L TRACK

E.W.M.L TRACK

WEST TO TORONTO

B.H. #2 (ELV. 363.07)

REFERENCE S/S  
ELV. 374.08

EAST TO HAMILTON

B.H. #3A (ELV. 361.86)



DEFECTS IN NEGATIVE DUE TO  
CONDITION OF ORIGINAL DOCUMENT

WARNICK HERSEY SOIL INVESTIGATIONS LTD.

LOCATION OF BOREHOLES

No. 53 SUBWAY

EAST WOOD

CANADIAN NATIONAL RAILWAYS

TORONTO

JOB NO. 0-24235  
DATE FEB. 20, 1954

N.Y. 100-1000  
N.Y. 100-1000

# Warnock Hersey Soil Investigations Ltd

Casing BX Diameter 2 3/8" Elevn. 965.08  
 Casing Hammer 350 lbs. Wt. 24" Drop  
 Sample Hammer 140 lbs. Wt. 30" Drop



# Office Report Of Soil Exploration

Client Canadian National Order Number S-64-45  
 Railways Highway #53 Subway near Eastwood Borehole Number 1  
 Ontario, Mile 44.9 Dundas S/D. Date Feb. 16 & 17, 1964.

## SAMPLE CONDITION & TYPE



Disturbed  
Good  
Lost

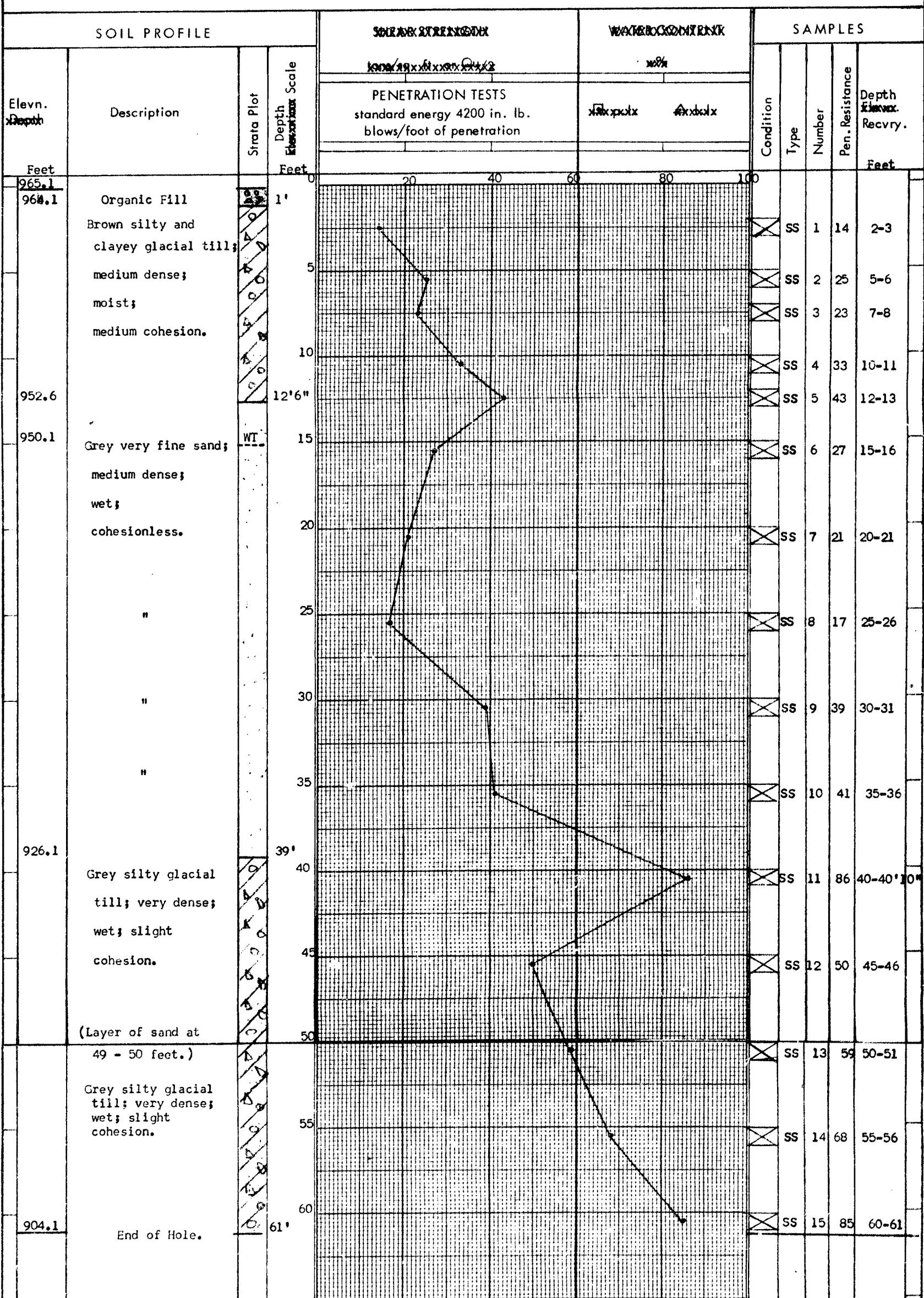
SS - Split Spoon  
CS - Chunk  
DO - Drive Open  
DF - Drive Footvalve  
TO - Thinwalled Open  
WS - Washed Sample  
RC - Rock Core

V - Insitu Vane Shear Test  
M - Mechanical Analysis  
U - Unconfined Compression  
Qc - Triaxial Consolidated Quick  
Q - Triaxial Quick  
S - Triaxial Slow

## ABBREVIATIONS

- Unit Weight  
K - Permeability  
C - Consolidation  
CA - Casing  
WL - Water Level in Casing  
WT - Water Table in Soil

## SOIL PROFILE



# Warnock Hersey Soil Investigations Ltd

# Office Report Of Soil Exploration

Casing BX Diameter 2 3/8" Elev. 963.07  
 Casing Hammer 350 lbs. Wt. 24" Drop  
 Sample Hammer 140 lbs. Wt. 30" Drop



Client Canadian National Order Number S-64-45

Railways Borehole Number 2

Highway #53 Subway near Eastwood

Ontario. Mile 44.9 Dundas S/D. Date Feb. 13, 14 & 15, 1964.

## SAMPLE CONDITION & TYPE

SS - Split Spoon

CS - Chunk

DO - Drive Open

DF - Drive Footvalve

TO - Thinwalled Open

WS - Washed Sample

RC - Rock Core

## ABBREVIATIONS

- Unit Weight

K - Permeability

C - Consolidation

CA - Casing

WL - Water Level in Casing

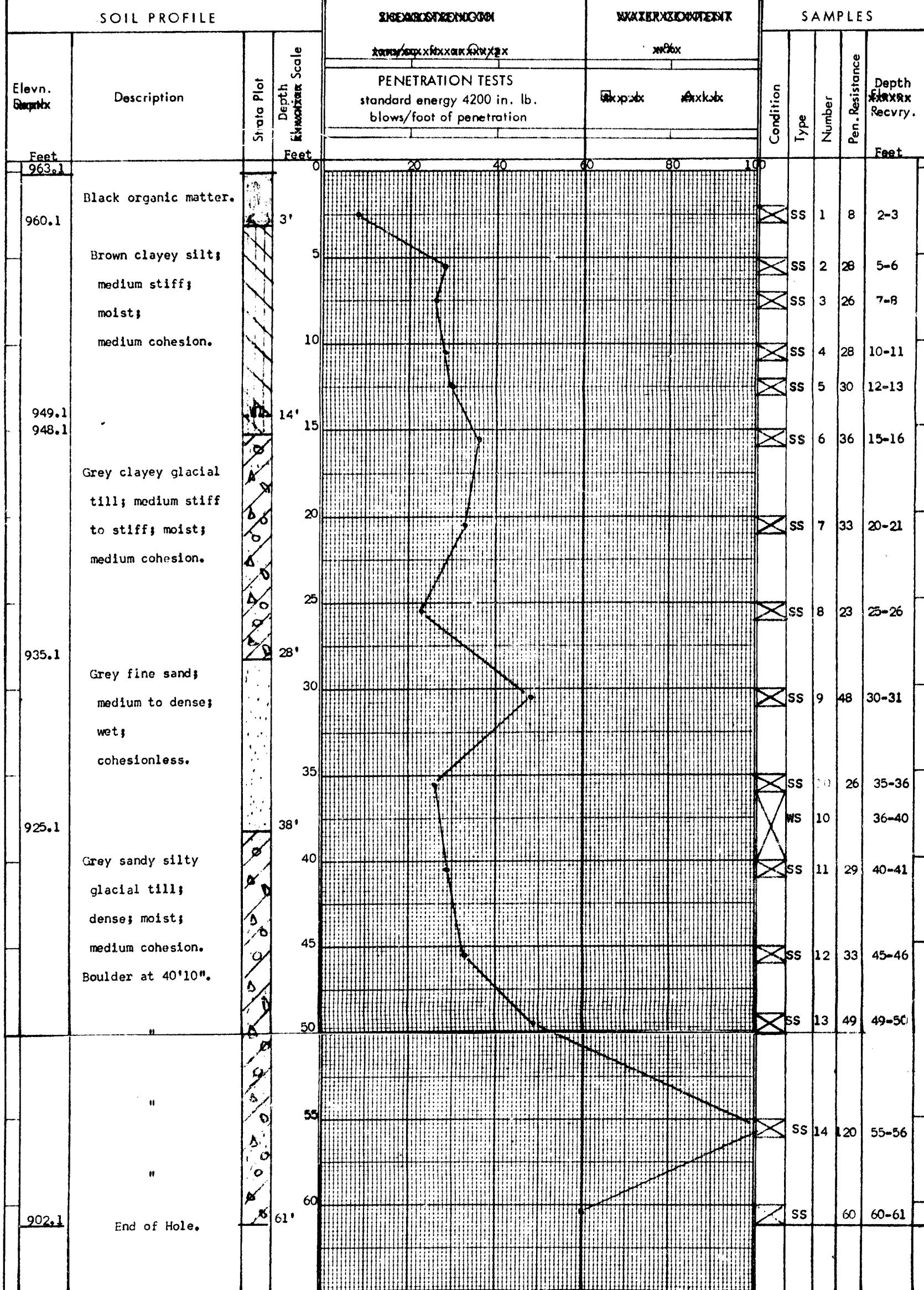
WT - Water Table in Soil

## SOIL PROFILE

## TESTS & INVESTIGATIONS

## WATER CONTENT

## SAMPLES



# Warnock Hersey Soil Investigations Ltd

Casing BX Diameter 2 3/8" Elevn. 961.86  
 Casing Hammer 350 lbs. Wt. 24" Drop  
 Sample Hammer 140 lbs. Wt. 30" Drop



# Office Report Of Soil Exploration

Client Canadian National Order Number S-64-45  
 Railways.  
 Highway #53 Subway near Eastwood  
 Ontario. Mile 44.9 Dundas S/D Date Feb. 18 & 19, 1964.

## SAMPLE CONDITION & TYPE

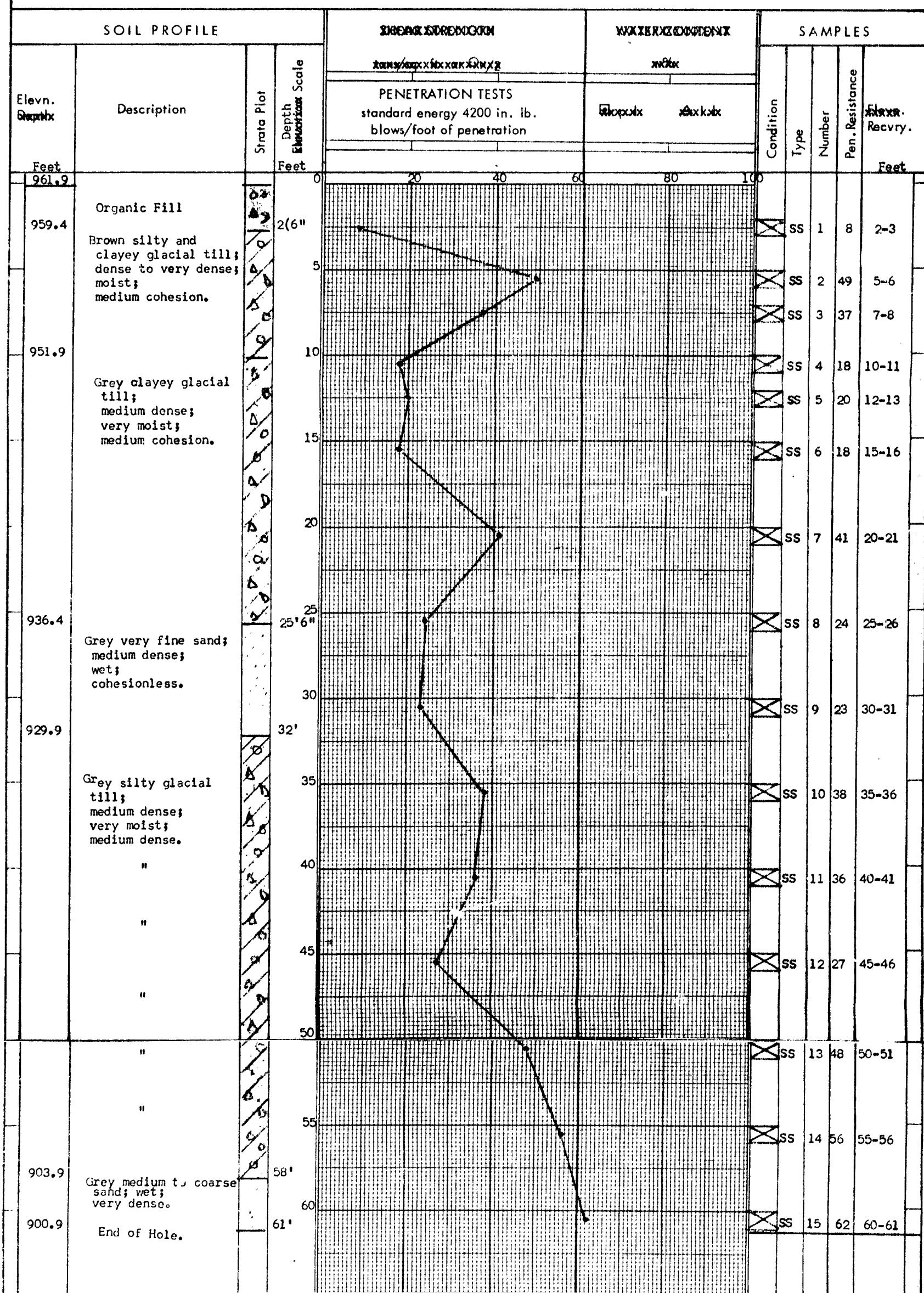
SS - Split Spoon  
 CS - Chunk  
 DO - Drive Open  
 DF - Drive Footvalve  
 TO - Thinwalled Open  
 WS - Washed Sample  
 RC - Rock Core

Disturbed  
 Good  
 Lost

V - Insitu Vane Shear Test  
 M - Mechanical Analysis  
 U - Unconfined Compression  
 Qc - Triaxial Consolidated Quick  
 Q - Triaxial Quick  
 S - Triaxial Slow

- Unit Weight  
 K - Permeability  
 C - Consolidation  
 CA - Casing  
 WL - Water Level in Casing  
 WT - Water Table in Soil!

## SOIL PROFILE



Casing BX Diameter 2 3/8" Elevn. 960.53  
 Casing Hammer 350 lbs. Wt. 24" Drop  
 Sample Hammer 140 lbs. Wt. 30" Drop



Client Canadian National Order Number S-64-45  
 Railways.  
 Highway #53 Subway near Eastwood Borehole Number 4A.  
 Ontario. Mile 44.9 Dundas S/D. Date Feb. 20, 1964

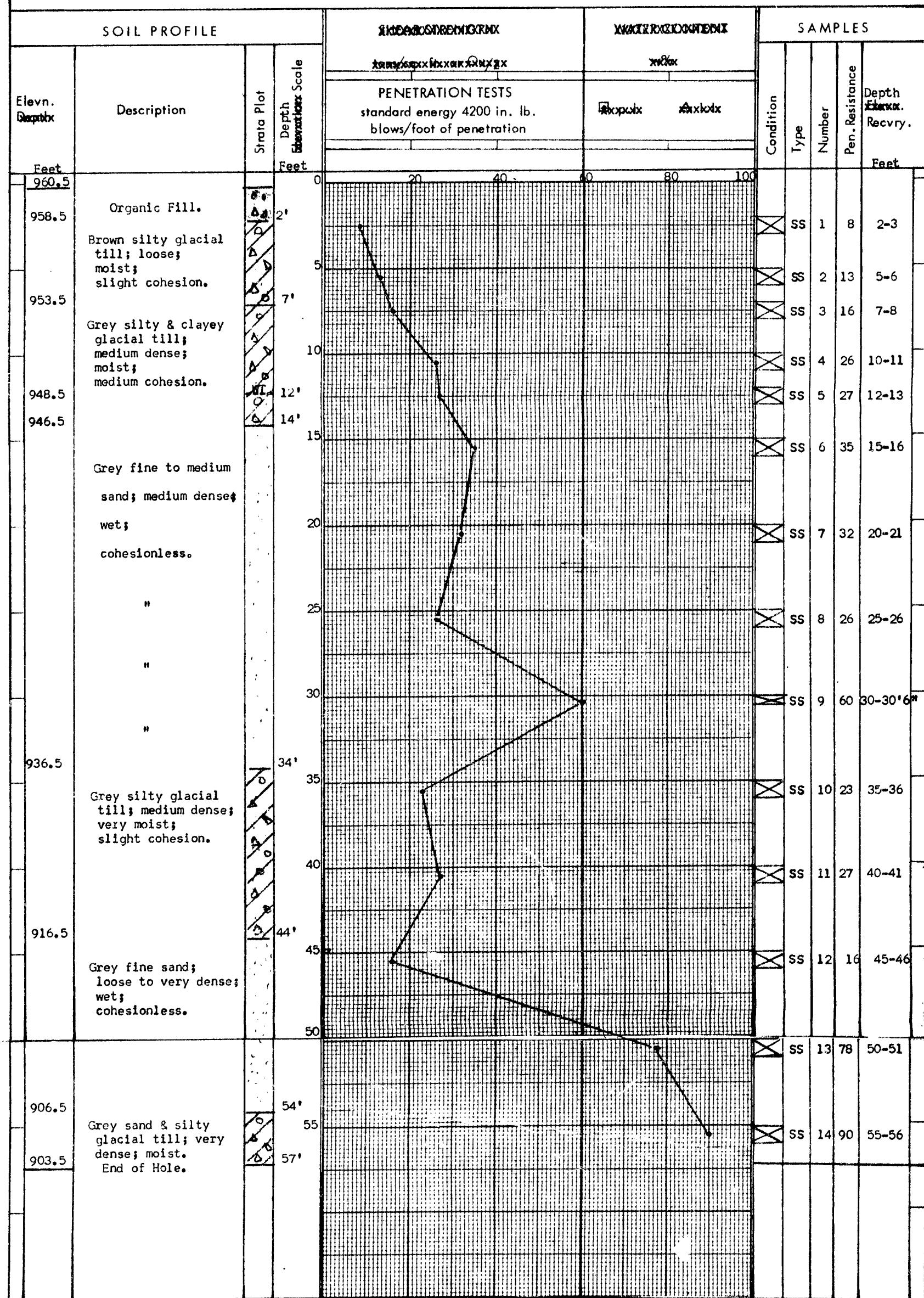
## SAMPLE CONDITION &amp; TYPE

SS - Split Spoon  
 CS - Chunk  
 DO - Drive Open  
 DF - Drive Footvalve  
 TO - Thinwalled Open  
 WS - Washed Sample  
 RC - Rock Core

## ABBREVIATIONS

V - Insitu Vane Shear Test  
 M - Mechanical Analysis  
 U - Unconfined Compression  
 Qc - Triaxial Consolidated Quick  
 Q - Triaxial Quick  
 S - Triaxial Slow  
 - Unit Weight  
 K - Permeability  
 C - Consolidation  
 CA - Casing  
 WL - Water Level in Casing  
 WT - Water Table in Soil

## SOIL PROFILE



B.H. # 2

Elev

945.0

N = 35

W.L. Elev

949.0

(Material - glacial till)

Clay, silt etc)

B.H. # 1

945.0

N = 20

(fine sand)

W.L.

950.0

B.H. # 3A

N = 25

(clayey silt till)

W.L.

not recorded

B.H. # 4 A

N = 35

(fine to Med sand)

W.L.

948.5

$$Q = \frac{1}{2} B \gamma N_r + \gamma D_f n_q$$

$$= \frac{1}{2} \times 10 \times 65 \times 20 + 65 \times 5 \times 20$$

$$= 5 \times 65 \times 20 + 65 \times 20 \times 5$$

$$= 65 \times 20 (5+5) = \frac{200}{6000}$$

Say, 2 + s.f.

However N values in B.H. # 1 in sand may be corrected according to Gibbs & Holtz — 3 + s.f. may be safe. Elsewhere 3 + s.f. can be used — Even in the vicinity of B.H. # 1 the footings may be placed slightly lower — Pillar nonsense.

Department of Highways Ontario

Copy for the information of

Mr. A. G. Stermac,

Principal Foundation Engineer,  
Room 107, Lab. Bldg.

file  
ayp

Bridge Division,  
Downsview, Ontario.  
August 14, 1964.

Canadian National Railways,  
151 Front Street West,  
Toronto 1, Ontario.

Att.: Mr. J. Geronimus

RE: Your File 1640-206,  
Our W.P. 27-62,  
CNR Subway Near Eastwood,  
Hwy. #53 Dist. #2.

Dear Sir:

Attached is a copy of the comments of our  
Foundation Engineer on Warnock Hersey's report on  
the soil investigation they conducted at this site.

Mr. Stermac would be happy to discuss this  
further if you so desire.

Yours truly,

FIH:go  
c.c. A. G. Stermac

F. I. Hewson,  
Consultant Liaison Engineer.

Mr. A. M. Toye,  
Bridge Engineer,  
Bridge Division.

Foundation Section,  
Materials & Testing Div.,  
Room 107, Lab. Bldg.

Attn: Mr. F. I. Hewson,  
Consultant Liaison Engr.

July 23, 1964

FOUNDATION INVESTIGATION REPORT BY:  
Warnock Hersey Soil Investigations Ltd.  
For Canadian National Railways, Toronto.  
Reconstruction of Hwy. No. 53 Subway  
near Eastwood, Ontario, Mile 44.9, Dundas  
Sub-Division. (D.H.O. District No. 2)

The report of the foundation investigation at the above site, submitted by Warnock Hersey Soil Investigations Ltd. has been reviewed.

The Consultant has suggested using piles for the foundation of the structure. However, the approach used by the Consultant to arrive at this recommendation is rather unconventional and conservative. It is our opinion that spread footings may be used with a design load of 3 T.S.F. at the proposed elevation of 945.0.

We believe that the foregoing comments will provide the information required. Should there be any queries in connection with this project, please feel free to contact our office.



A. G. Stermac,  
PRINCIPAL FOUNDATION ENGINEER

FYL/Mdef  
cc: Foundations Office  
Gen. Files

Department of Highways Ontario

Copy for the information of

Mr. A. Stermac,  
Principal Foundation Eng.  
Room 107, Lab. Bldg.

To be filed  
with Corrision  
report  
Ward 1 Jersey  
964

Bridge Division,  
Downsview, Ontario,  
February 3, 1964.

Mr. W. E. Griffiths,  
Regional Chief Engineer,  
Canadian National Railways,  
151 Front Street, Room 868,  
TORONTO, Ontario.

RE: Bridge Site #24-175 W.P. 27-62  
C.N.R. Subway at Eastwood  
Hwy. 53 District #2

Dear Sir:

The location of the above structure has been approved as on Line "A" shown on the attached Preliminary Print of the Bridge Site Plan.

The clearances we will require for the Highway are vertical 15'-3" and horizontal 38' (28' roadway) as measured normal to the highway.

We understand from your Mr. Workman that before establishing the depth of deck, and hence the drainage and highway profiles, it would be desirable to make a foundation soils investigation for this site.

Please consider this your authority to arrange, as soon as practicable, for the Foundation Soils Investigation for the above bridge.

We will be pleased to know, at your earliest convenience, the depth of deck (base of rail to soffit) you propose to use for the design also as to whether the present rail elevation must be maintained.

Yours truly,

G.Scott,, P. Eng.  
Bridge Location Engineer.

GS/es  
cc. J. Walter  
cc. S. McCombie  
cc. A. Stermac  
cc. W. Kinnear  
cc. C. Hansen  
cc. R. Fitzgibbon