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DIST. 1 REGION \_\_\_\_\_

W.P. No. 122-65-01

CONT. No. 75-027

W. O. No. \_\_\_\_\_

STR. SITE No. \_\_\_\_\_

HWY. No. 402

LOCATION Mode Land Road,  
Interchange

No. of PAGES - —

                 =                 

Oversize Drawings to be included with this report. \_\_\_\_\_

REMARKS: \_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

40 J 16-8 WP Z9-62 (F)

-27 WP 122-65-01 (F)

-36 WP 122-65-01 FILE

-40 WP 122-65-03 & 04  
CONT 75-27

## MEMORANDUM

40 J 101

GOCRES No.

To: Mr. E. R. Davis,  
Bridge Engineer,  
Bridge Office,  
Admin. Bldg.  
  
ATTENTION: Mr. S. McCombie  
  
OUR FILE REF.

FROM: Foundation Section,  
Materials & Testing Office,  
Room 107, Lab. Bldg

DATE: April 21, 1970

IN REPLY TO

MAY 4 1970

40J/6-36

GOCRES No.

SUBJECT:

Sheets

FOUNDATION INVESTIGATION REPORT  
For

The Proposed Approaches  
In the Vicinity of Modeland Road  
Interchange --- C.A.H. #402  
Twp. of Sarnia, Co. of Lambton  
District No. 1 (Chatham, Ont.)  
W.J. 69-F-119 --- W.P. 122-65-01

20,21,27,29,30

Attached, we are forwarding to you our detailed foundation investigation report on the subsoil conditions existing at the above structure site.

We believe that the factual data and recommendations contained therein, will prove adequate for your design requirements. Should additional information be required, please feel free to contact our Office.

AGS/MdeF  
Attach.

*A. G. Stermac*  
A. G. Stermac  
PRINCIPAL FOUNDATION ENGINEER

cc: Messrs. B. R. Davis  
H. A. Tregaskes  
D. W. Farren  
W. Zonnenberg  
F. C. Brown  
A. P. Watt (2)  
J. Roy  
B. A. Singh

Foundations Files ✓  
Gen. Files

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FOUNDATION INVESTIGATION REPORT  
For

The Proposed Approaches  
In the Vicinity of Modeland Road  
Interchange -- C.A.H. #402  
Twp. of Sarnia, Co. of Lambton  
District No. 1 (Chatham, Ont.)  
W.J. 69-F-119 -- W.P. 122-65-01

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1. INTRODUCTION:

During the routine soils investigation in the vicinity of the proposed Modeland Road and C.A.H. #402 Interchange, deep deposits of organic material were discovered at locations where embankments were to be constructed. Following this discovery, a discussion was held between the Foundation Section and the Regional Materials Engineer, and it was decided that additional deep borings were needed to determine accurately the lateral and vertical extent of the organic deposit, and also the soil properties.

The additional borings were carried out jointly by the Foundation Section and the Regional Soil Section. Presented in this report, are the results of the field investigation, together with recommendations pertaining to the design of the proposed approach embankments.

2. DESCRIPTION OF THE SITE:

The site of the proposed approach embankments is situated in the Eastern outskirts of the City of Sarnia, approx. 0.4 miles North of the existing Hwy. #402.

The area investigated is flat and cultivated farmland.

Physiographically, the site is located in the region referred to as the Huron Fringe.

### 3. FIELD AND LABORATORY INVESTIGATION PROCEDURES:

A total of 21 sampled boreholes and 18 dynamic cone penetration tests were carried out by the Foundation Section during the course of the field work. Boring was achieved by means of continuous flight auger machines adapted for soil sampling purposes.

During the field work, 'disturbed' samples were obtained by means of a standard split-spoon sampler; the energy used in driving it, conformed to the requirements of the Standard Penetration Test.

'Undisturbed' samples were recovered using 2-inch I.D. Shelby tubes, which were pushed into the soil hydraulically, or by hand. Where possible, field vane tests were carried out at elevations 12 inches below sample depths.

Dynamic cone penetration tests were carried out adjacent to some boreholes and, also, at six other locations. Driving energy to advance the cone was 350 ft.-lbs. per blow. The boreholes were surveyed in the field by personnel from London Region Engineering Surveys Section. The locations and elevations of the borings (including those carried out by the Soils Section, where depth of organics exceeded 5 ft.), are shown on Drawing No. 69-F-119A, which accompanies this report.

All samples were visually examined and classified at the site as well as in the laboratory. Following this inspection, laboratory tests were carried out on selected samples to determine the following physical properties:

- Atterberg Limits (oven and air-dried)
- Moisture Content
- Grain-size Distribution
- Organic Content
- Undrained Shear Strength
- Bulk Density

The test results are summarized on the Record of Borehole sheets contained in the Appendix of this report.

4. SOIL TYPES AND SOIL CONDITIONS:

4.1) General:

An extensive deposit of organic soil was found to overlie the terrain traversed by the proposed Hwy. #402 between approximate Sta. 60+00 and Sta. 85+00. A similar deposit was found to extend between Sta. 411+00 and Sta. 437+00 on Modeland Road.

The depth of organics varies greatly from a minimum of 5 ft. to a maximum of about 30 ft. At some locations the organic soil is overlain by up to 10 ft. of sand, and at other locations, sand layers of varying thickness are contained within the organic deposits.

Reference should be made to Drawing No. 69-F-119A, where the horizontal and vertical extent of the organic deposit is plotted. Borelogs for the 21 holes carried out by the Foundation Section are included in the Report Appendix.

4.2) Silty Sand to Sand:

This stratum was encountered in the following boreholes immediately below the topsoil: #100, #102, #105, #108, #110, #111 and #208. The depth was found to vary between 4 and 23 ft. The material in the deposit consists mainly of sand and silt with traces of clay. The natural moisture content ranges from 12% to 30%. Based on the Standard Penetration Test, the relative density may be described as very loose to compact.

4.3) Organic Silt and Clay:

This material was found to cover a large area in the vicinity of proposed Modeland Road Interchange. The lateral and vertical extent of the deposit is shown on the above mentioned drawing. In general, the thickness was found to vary between 5 and 30 ft.

The overall deposit is made up of layers of organic silt, organic clay, silty fine sand with decayed and undecayed

4. SOIL TYPES AND SOIL CONDITIONS: (cont'd.) ...

4.3) Organic Silt and Clay: (cont'd.) ...

organic substances and occasionally black-coloured, very soft peat. The thickness of the individual layers ranged from a few inches to 30 ft.

Although the consistency of the organic silts and clays is in general soft, a fairly wide scatter of results of undrained shear strength measurements was obtained, ranging from a low of about 200 p.s.f. to a high of about 900 p.s.f. For design purposes, however, it may be assumed that the upper 18 ft. of the deposit has an average shear strength of 400 p.s.f., whilst below this level, the average is about 700 p.s.f.

The natural moisture content is in general, in excess of 60%.

The physical properties of the overall deposit are plotted on the Record of Borehole sheets contained in the Appendix. It is pointed out, however, that the major portion of the organic material exhibits very low shear strength upon remoulding.

4.4) Groundwater Conditions:

The groundwater level was found to be at or slightly below the ground surface, during the field investigation.

5. DISCUSSION AND RECOMMENDATIONS:

It is proposed to construct approach embankments at the intersection of the proposed new Hwy. #402 and Modeland Road. The maximum height of the fill will be in the order of 26 ft. above the existing ground level.

The subsoil at the site was found to consist of irregular deposits of organic material and sand, up to 30 ft. in thickness. Groundwater level was at or slightly below the ground surface.

5. DISCUSSION AND RECOMMENDATIONS: (cont'd.) ...

There are two main problems to be overcome on this project due to the presence of the organic soil. The first is stability of the embankments, and the second is the settlement which will occur under the embankments. The problem of embankment stability can be solved by excavating all or part of the organic soil and replacing this material with suitable granular fill. The problem of settlements can be minimized, if not completely solved, by surcharging those portions of the fill where the organic soil has not been completely excavated. Following, therefore, are our recommendations relating to the construction of the proposed Hwy. #402 and Modeland Rd.

(1) Excavate all organic soil and replace with suitable granular up to about 3 ft. above water level, and suitable earth fill above that level. If this treatment is carried out, there should be no stability or settlement problems.

(2) Excavate all organic soil where it occurs down to a depth of about 13 ft. and replace with fill material as in (1). At those areas where organic soil still remains in place, the fill should be surcharged with a minimum of 3 ft. of soil, and a maximum of about 6 ft. over the deepest remaining deposits. It will be necessary to observe, by means of settlement plates, the performance of the fill so that the appropriate duration of time of surcharging can be determined. It is believed that a period of time not less than 1 year will be required. If the foregoing treatment is carried out, it is believed that stability problems will be solved, and that settlement problems will be reduced to an acceptable level.

Figure No. 1, on the following page, shows the details of excavation and backfilling for Cases (1) and (2).

5. DISCUSSION AND RECOMMENDATIONS: (cont'd.) ...

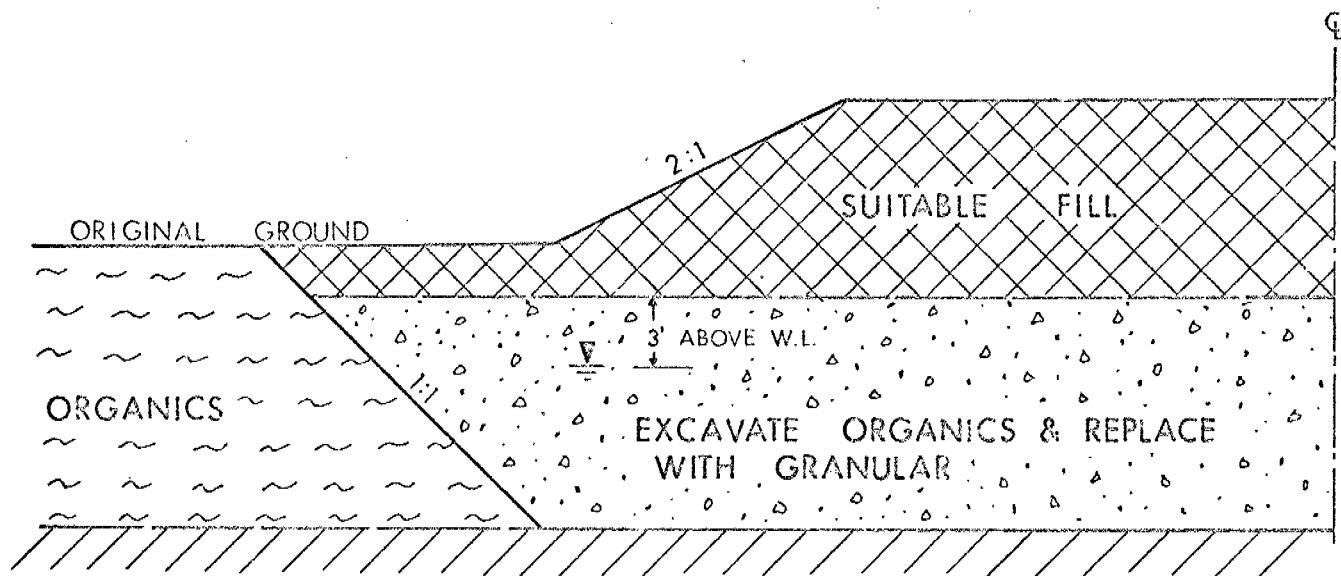


Fig. No. 1

Stability analyses carried out in terms of total stresses, indicate that the proposed highway embankments will be stable if the above described recommendations are carried out.

It may be advantageous to adjust the present line of Hwy. #402 to avoid the deeper organic deposits on the North side.

6. MISCELLANEOUS:

The field investigation was carried out during the period December 11 - 19, 1969, under the supervision of Messrs. P. Payer and A. Prakash, Project Foundation Engineers.

Equipment was owned and operated by Dominion Soil Investigation Limited, and G. Wimpey (Canada) Limited.

This report was written by Mr. P. Payer, and reviewed by Mr. K. G. Selby, Supervising Foundation Engineer.

April, 1970

APPENDIX I

---

DEPARTMENT OF HIGHWAYS - ONTARIO  
MATERIALS & TESTING OFFICE

RECORD OF BOREHOLE No. 100

## FOUNDATION SECTION

JOB 69-F-119

LOCATION Sta. 66 + 00 150' Lt. Hwy. 402

ORIGINATED BY AP

W.P. 122-65-01

BORING DATE December 11, 1969

COMPILED BY PP

DATUM Geodetic

## BOREHOLE TYPE Cont. Flight Auber

CHECKED BY

**DEPARTMENT OF HIGHWAYS- ONTARIO**  
**MATERIALS & TESTING OFFICE**

RECORD OF BOREHOLE No. 101

## FOUNDATION SECTION

JOB 69-F-119  
W.P. 122-65-01  
DATUM Geodetic

LOCATION Sta. 67 + 00 & Hwy. 402  
BORING DATE December 12, 1969  
BOREHOLE TYPE Cont. Flight Auger

ORIGINATED BY AP  
COMPILED BY PP  
CHECKED BY

SOIL PROFILE			SAMPLES			ELEV. SCALE	DYNAMIC PENETRATION RESISTANCE BLOWS / FOOT			LIQUID LIMIT — WL			BULK DENSITY $\gamma$	REMARKS
ELEV.	DEPTH	DESCRIPTION	NUMBER	TYPE	BLOWS / FOOT		SHEAR STRENGTH P.S.F.	○ UNCONFINED ● QUICK TRIAXIAL	+ FIELD VANE x LAB VANE	W <sub>P</sub>	W	W <sub>L</sub>		
588.6	Ground Level	Ground Level	1	SS	5	580	1000	●	+ 2.1	25	50	75	16	0 82 16 2
0.0	Topsoil	Silty sand, traces of clay & organics	2	SS	4	580	2000	●	+ 2.1	0	0	0		
580.6	Loose	Loose	3	SS	3	570	1000	●	+ 1.9	0	0	0		
8.0	Organic silt, clay	Organic silt, clay	4	TW	PM	570	2000	●	+ 1.9	0	0	0		
	Layers of sand	Layers of sand	5	SS	4	560	1000	●	+ 1.8	0	0	0		
	Soft to stiff	Soft to stiff	6	TW	PM	560	2000	●	+ 1.8	0	0	0		
560.1	28.5	Clayey silt	7	SS	7	560	1000	●	+ 1.8	0	0	0		
557.1	Stiff	Stiff	8	SS	12	560	2000	●	+ 1.8	0	0	0	93	

**DEPARTMENT OF HIGHWAYS - ONTARIO**  
**MATERIALS & TESTING OFFICE**

RECORD OF BOREHOLE No. 102

## FOUNDATION SECTION

JOB 69-F-119

LOCATION Sta. 68 + 00 & Hwy. 402

ORIGINATED BY PP

W 8 122-65-01

BORING DATE December 15, 1969

COMPILED BY PP

**DATUM**      **Geodetic**

## **BOREHOLE TYPE** Cont. Flight Auger

CHECKED BY *[Signature]*

**DEPARTMENT OF HIGHWAYS - ONTARIO**  
**MATERIALS & TESTING OFFICE**

RECORD OF BOREHOLE No. 10.

## FOUNDATION SECTION

JOB 69-F-119

LOCATION Sta. 68 + 00 150' Lt. Hwy. 40

ORIGINATED BY AP

W.P. 122-65-01

BORING DATE December 12, 1969

COMPILED BY PP

DATUM Geodetic

**BOREHOLE TYPE** Cont. Flight Auger

CHECKED BY

**DEPARTMENT OF HIGHWAYS- ONTARIO**  
**MATERIALS & TESTING OFFICE**

RECORD OF BOREHOLE No. 10

## FOUNDATION SECTION

JOB 69-F-119  
W.P. 122-65-01  
DATUM Geodetic

LOCATION Sta. 69 + 00 150' Lt. Hwy. 402  
BORING DATE December 15, 1969  
BOREHOLE TYPE Cont. Flight Auger

ORIGINATED BY PP  
COMPILED BY PP  
CHECKED BY

**DEPARTMENT OF HIGHWAYS - ONTARIO**  
**MATERIALS & TESTING OFFICE**

RECORD OF BOREHOLE No. 105

## FOUNDATION SECTION

108 69-F-119

LOCATION Sta. 70 + 00 150' Lt. Hwy. 402

ORIGINATED BY PP

W P 122-65-01

BORING DATE December 15, 1969

COMPILED BY F

DATUM Geodetic

**BOREHOLE TYPE** Cont. Flight Auger

CHECKED 8

DEPARTMENT OF HIGHWAYS - ONTARIO  
MATERIALS & TESTING OFFICE

RECORD OF BOREHOLE No. 107

## FOUNDATION SECTION

JOB 69-F-119  
W.P. 122-65-01  
DATUM Geodetic

LOCATION Sta. 81+00 100' Lt. Hwy. 402  
BORING DATE December 16, 1969  
BOREHOLE TYPE Cont. Flight Auger

ORIGINATED BY \_\_\_\_\_ PP  
COMPILED BY \_\_\_\_\_ PP  
CHECKED BY \_\_\_\_\_

DEPARTMENT OF HIGHWAYS- ONTARIO  
MATERIALS & TESTING OFFICE

## RECORD OF BOREHOLE No. 108

FOUNDATION SECTION

JOB 69-F-119

LOCATION Sta. 81 + 00 100' Rt. Hwy. 402

ORIGINATED BY PP

W.P. 122-65-01

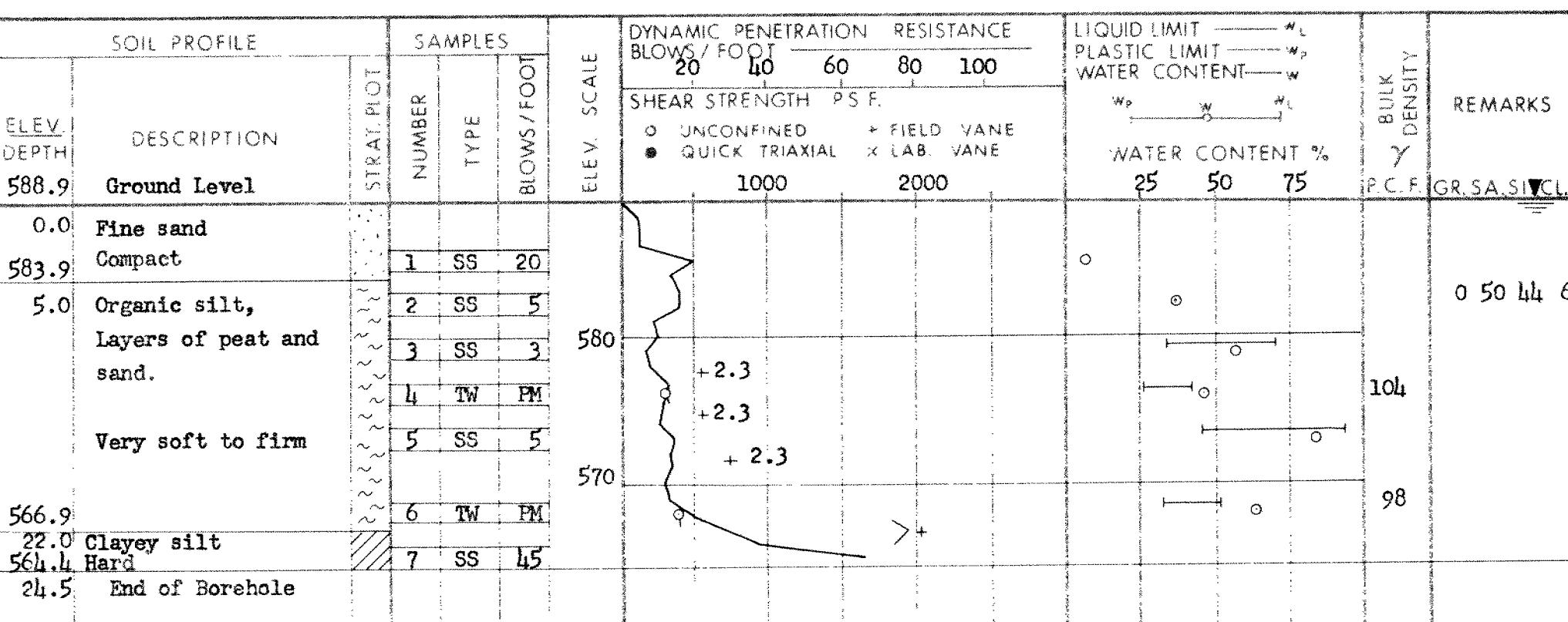
BORING DATE December 16, 1969

COMPILED BY PP

DATUM Geodetic

BOREHOLE TYPE Cont. Flight Auger

CHECKED BY



DEPARTMENT OF HIGHWAYS - ONTARIO  
MATERIALS & TESTING OFFICE

RECORD OF BOREHOLE No. 109

## FOUNDATION SECTION

JOB 69-F-119  
W.P. 122-65-01  
DATUM Geodetic

LOCATION Sta. 82 + 00 100' Lt. Hwy. 402  
BORING DATE December 16, 1969  
BOREHOLE TYPE Cont. Flight Auger

ORIGINATED BY PP  
COMPILED BY PP  
CHECKED BY PP

DEPARTMENT OF HIGHWAYS - ONTARIO  
MATERIALS & TESTING OFFICE

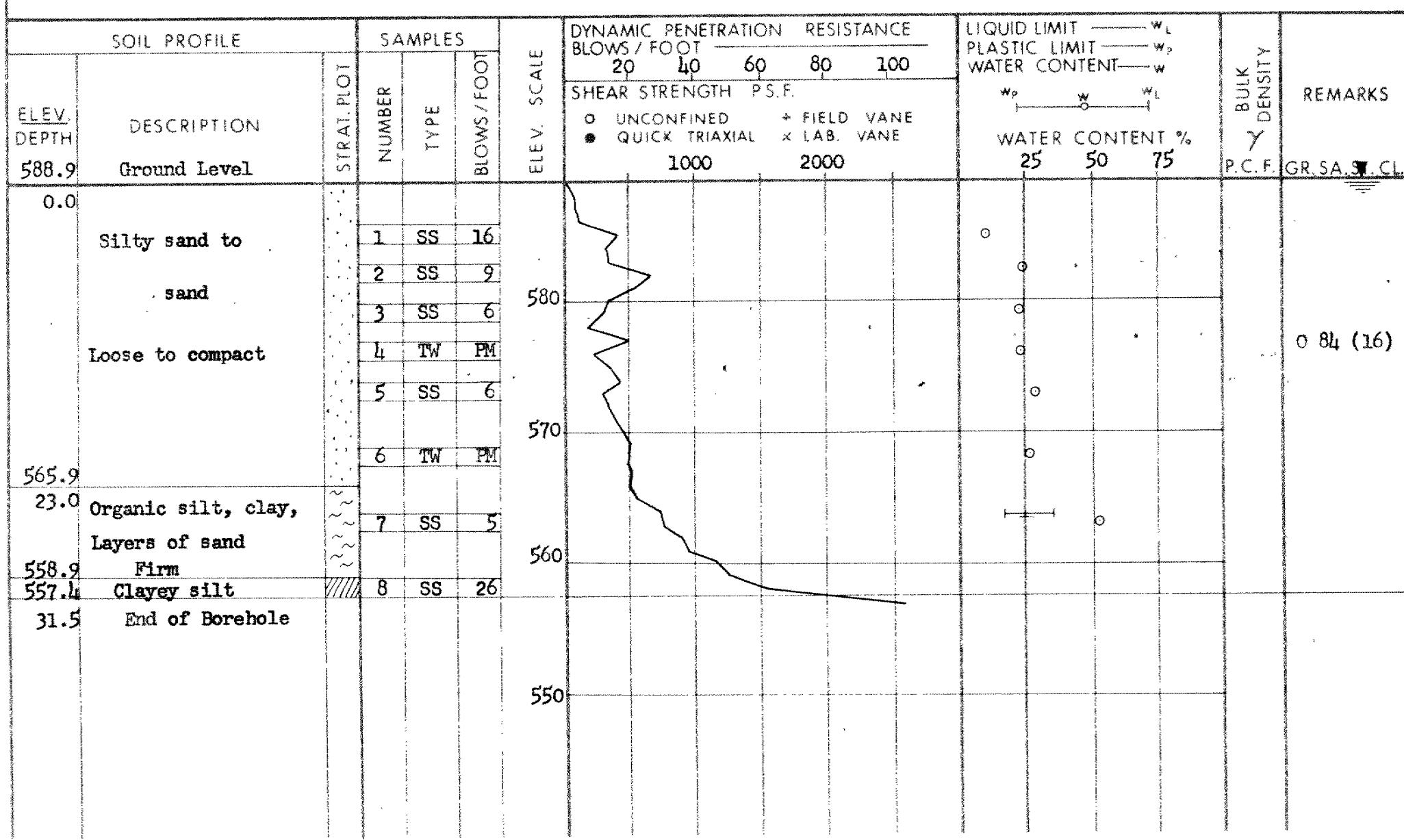
## RECORD OF BOREHOLE No. 110

FOUNDATION SECTION

JOB 69-F-119 LOCATION Sta. 82 + 00 100' Rt. Hwy. 402 ORIGINATED BY PP

W.P. 122-65-01 BORING DATE December 16, 1969 COMPILED BY PP

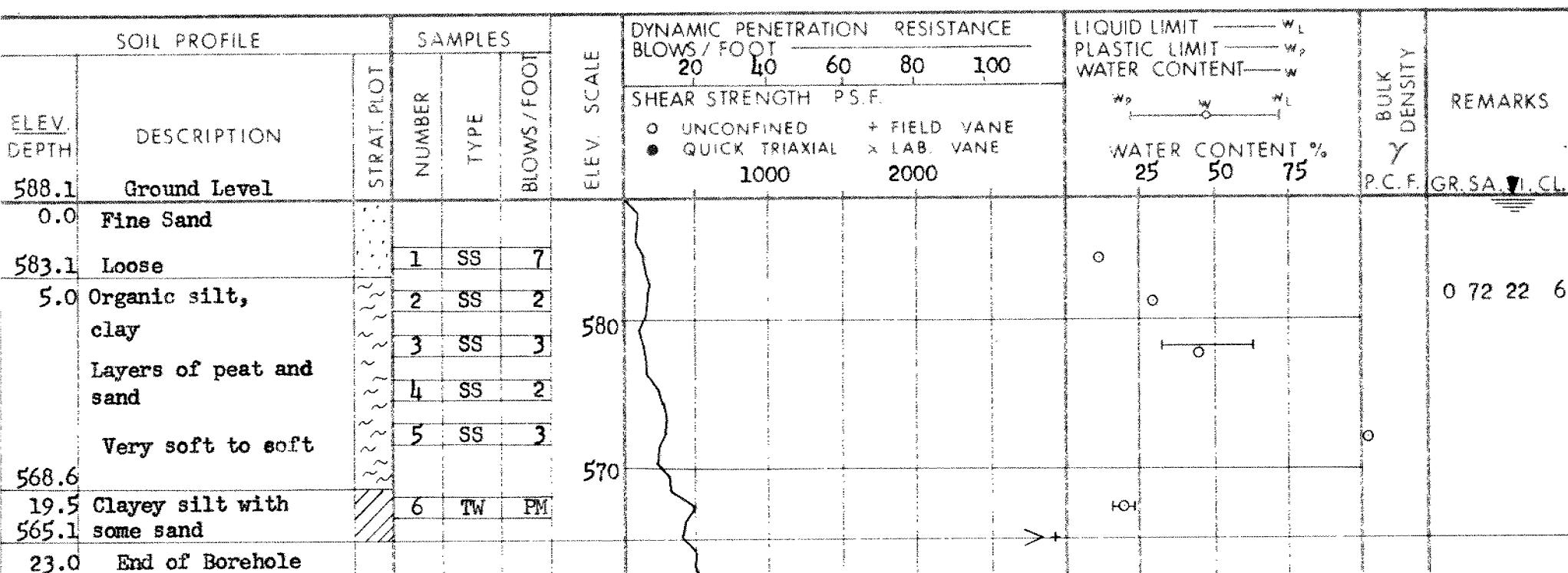
DATUM Geodetic BOREHOLE TYPE Cont. Flight Auger CHECKED BY [Signature]



DEPARTMENT OF HIGHWAYS- ONTARIO  
MATERIALS & TESTING OFFICE

## RECORD OF BOREHOLE No. 111

FOUNDATION SECTION

JOB 69-F-119  
W.P. 122-65-01  
DATUM GeodeticLOCATION Sta. 83 + 00 100' Lt. Hwy. 402  
BORING DATE December 16, 1969  
BOREHOLE TYPE Cont. Flight AugerORIGINATED BY PP  
COMPILED BY PP  
CHECKED BY J.A.

DEPARTMENT OF HIGHWAYS - ONTARIO  
MATERIALS & TESTING OFFICE

RECORD OF BOREHOLE No. 113

## FOUNDATION SECTION

JOB 69-F-119

Sta. 84 + 00 100' Rt. Hwy. 402

ORIGINATED BY PP

W P 122-65-01

LOCATION Sta. 84 + 00 100' Rt. Hwy. 4

COMPILED BY F

DATUM **Ge**

**BOREHOLE TYPE** Cont. Flight Auger

CHECKED BY

DEPARTMENT OF HIGHWAYS - ONTARIO  
MATERIALS & TESTING OFFICE

RECORD OF BOREHOLE No. 114

## FOUNDATION SECTION

108 69-F-119

LOCATION Sta. 67 + 00 160' Lt. Hwy. 402

ORIGINATED BY AP

W.E. 122-65-01

BORING DATE December 11, 1969

COMPILED BY P

**DATUM** Geodeti

### **BOREHOLE TYPE Cont. Flight Auger**

CHECKED BY

DEPARTMENT OF HIGHWAYS- ONTARIO  
MATERIALS & TESTING OFFICE

## RECORD OF BOREHOLE No. 115

FOUNDATION SECTION

JOB 69-F-119

LOCATION Sta. 79 + 00 &amp; Hwy. 402

ORIGINATED BY PP

W.P. 122-65-01

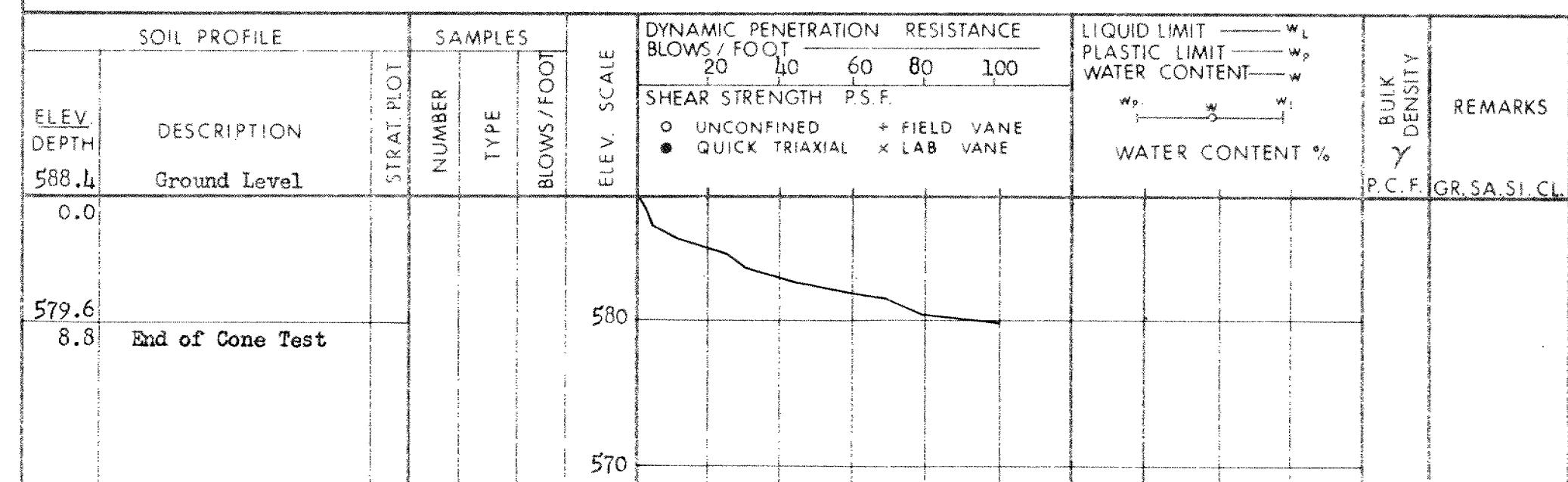
BORING DATE December 17, 1969

COMPILED BY PP

DATUM Geodetic

BOREHOLE TYPE Cone Test Only

CHECKED BY



DEPARTMENT OF HIGHWAYS- ONTARIO  
MATERIALS & TESTING OFFICE

## RECORD OF BOREHOLE No. 116

FOUNDATION SECTION

JOB 69-F-119

LOCATION Sta. 77 + 00 # Hwy. 402

ORIGINATED BY PP

W.P. 122-65-01

BORING DATE December 17, 1969

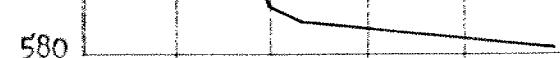
COMPILED BY PP

DATUM Geodetic

BOREHOLE TYPE Cone Test Only

CHECKED BY JES

SOIL PROFILE		SAMPLES		ELEV. SCALE	DYNAMIC PENETRATION RESISTANCE					LIQUID LIMIT — WL	PLASTIC LIMIT — WP	WATER CONTENT — W	BULK DENSITY Y	REMARKS	
ELEV. DEPTH	DESCRIPTION	STRAT. PLOT	NUMBER	Type	BLOWS / FOOT	20	40	60	80	100	SHEAR STRENGTH P.S.F.				
588.4	Ground Level			O	UNCONFINED	+ FIELD VANE									
0.0				●	QUICK TRIAXIAL	X LAB. VANE									
500.2															
8.2	End of Cone Test														



DEPARTMENT OF HIGHWAYS - ONTARIO  
MATERIALS & TESTING OFFICE

RECORD OF BOREHOLE No. 200

## FOUNDATION SECTION

JOB 69-F-119

### LOCATION

Sta. 416 + 60 125<sup>1</sup> Lt. Modeland Rd.

ORIGINATED BY PP

W P 122-65-01

**BORING DATE**

December 17, 1969

COMPILED BY

DATUM Geodetic

### **BOREHOLE TYPE**

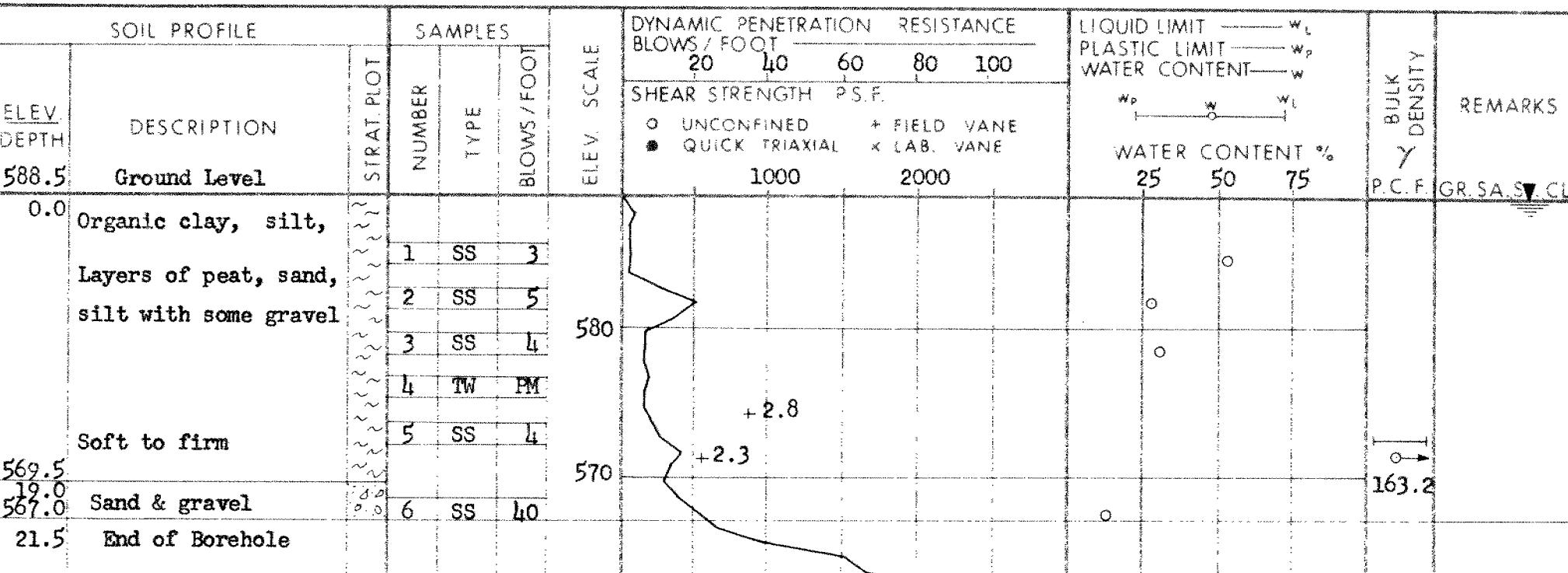
### Cont. Flight Auger

CHECKED BY

DEPARTMENT OF HIGHWAYS- ONTARIO  
MATERIALS & TESTING OFFICE

## RECORD OF BOREHOLE No. 201

FOUNDATION SECTION

JOB 69-F-119  
W.P. 122-65-01  
DATUM GeodeticLOCATION Sta. 418 + 55 125' Lt. Modeland Rd.  
BORING DATE December 17, 1969  
BOREHOLE TYPE Cont. Flight AugerORIGINATED BY PP  
COMPILED BY PP  
CHECKED BY

DEPARTMENT OF HIGHWAYS - ONTARIO  
MATERIALS & TESTING OFFICE

## RECORD OF BOREHOLE No. 202

FOUNDATION SECTION

JOB 69-F-119

LOCATION Sta. 59 + 00 200' Lt. Hwy. 402

ORIGINATED BY PP

W.P. 122-65-C1

BORING DATE Dec. 18, 1969

COMPILED BY PP

DATUM Geodetic

BOREHOLE TYPE Cont. Flight Auger

CHECKED BY

ELEV. DEPTH	DESCRIPTION	SOIL PROFILE			SAMPLES	DYNAMIC PENETRATION BLOWS / FOOT	RESISTANCE	LIQUID LIMIT — WL	PLASTIC LIMIT — WP	WATER CONTENT — W	BULK DENSITY	REMARKS
		STRAT. PLOT	NUMBER	TYPE								
583.5	Ground Level											
0.0	Layers of organic material and sand	~										
583.5		~	1	SS	7							
5.0	Clayey silt with some sand & traces of gravel	~	2	SS	29							
		~	3	TW	PH							
		~	4	SS	16							
572.0	Stiff to very stiff	~	5	SS	18							
16.5	End of Borehole											

ELEV. SCALE  
 DYNAMIC PENETRATION  
 BLOWS / FOOT  
 20 40 60 80 100

SHEAR STRENGTH PSF

○ UNCONFINED  
 ● QUICK TRIAXIAL

FIELD VANE

LAB VANE

1000

2000

WATER CONTENT %

WL

WP

W

25

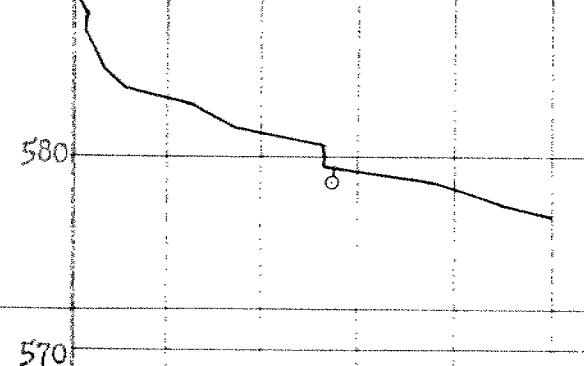
50

75

Y  
P.C.F.

GR. SA. SI. CL

129



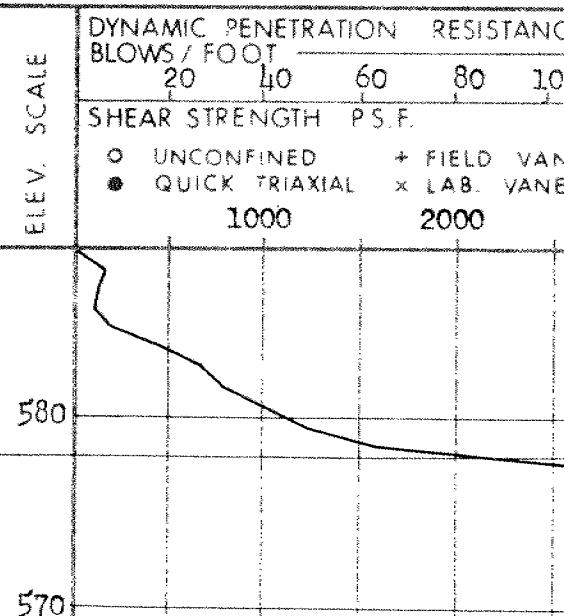
DEPARTMENT OF HIGHWAYS - ONTARIO  
MATERIALS & TESTING OFFICE

## RECORD OF BOREHOLE No. 203

FOUNDATION SECTION

JOB 69-E-119  
W.P. 122-65-01  
DATUM GeodeticLOCATION Sta. 418 + 55 310' Lt. Modeland Rd.  
BORING DATE December 18, 1969  
BOREHOLE TYPE Cont. Flight AugerORIGINATED BY PP  
COMPILED BY PP  
CHECKED BY J.L.

SOIL PROFILE		SAMPLES			ELEV. SCALE	DYNAMIC PENETRATION RESISTANCE	LIQUID LIMIT — WL	PLASTIC LIMIT — WP	WATER CONTENT — W	BULK DENSITY Y	REMARKS
ELEV. DEPTH	DESCRIPTION	STRAT. PLOT	NUMBER	TYPE	BLOWS / FOOT	BLOWS / FOOT 20 40 60 80 100	SHEAR STRENGTH P.S.F. ○ UNCONFINED + FIELD VANE ● QUICK TRIAXIAL X LAB. VANE 1000 2000	WP	W	WL	
588.5	Ground Level										
0.0	Layers of organics &										
584.5	sand										
4.0	Clayey silt with some sand & traces of gravel.		1	SS	9						
			2	SS	30						
578.0	Hard		3	SS	31						
10.5	End of Borehole										



DEPARTMENT OF HIGHWAYS- ONTARIO  
MATERIALS & TESTING OFFICE

## RECORD OF BOREHOLE No.204

FOUNDATION SECTION

JOB 69-F-119

LOCATION Sta. 57 + 00 200' Lt. Hwy. 402

ORIGINATED BY PP

W.P. 122-65-01

BORING DATE December 18, 1969

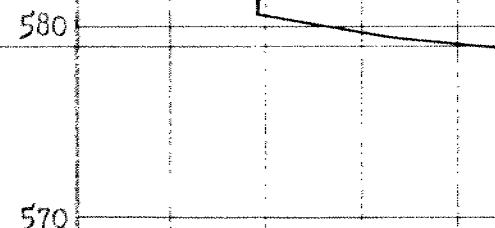
COMPILED BY PP

DATUM Geodetic

BOREHOLE TYPE Cont. Flight Auger

CHECKED BY

SOIL PROFILE		SAMPLES			ELEV. SCALE	DYNAMIC PENETRATION RESISTANCE BLOWS / FOOT					LIQUID LIMIT $w_L$	PLASTIC LIMIT $w_P$	WATER CONTENT $w$	BULK DENSITY $\gamma$	REMARKS	
ELEV.	DEPTH	STRAT. PLOT	NUMBER	TYPE		20	40	60	80	100		○ UNCONFINED	+ FIELD VANE	× LAB VANE		
588.5	Ground Level															
0.0	Probably organics															
584.5																
4.0	Probably clayey silt															
579.0																
9.5	End of Borehole	1	SS	35	580											



570

DEPARTMENT OF HIGHWAYS- ONTARIO  
MATERIALS & TESTING OFFICE

## RECORD OF BOREHOLE No. 205

FOUNDATION SECTION

JOB 69-F-119

LOCATION Sta. 418 + 55 520' Lt. Modeland Rd.

ORIGINATED BY PP

W.P. 122-65-01

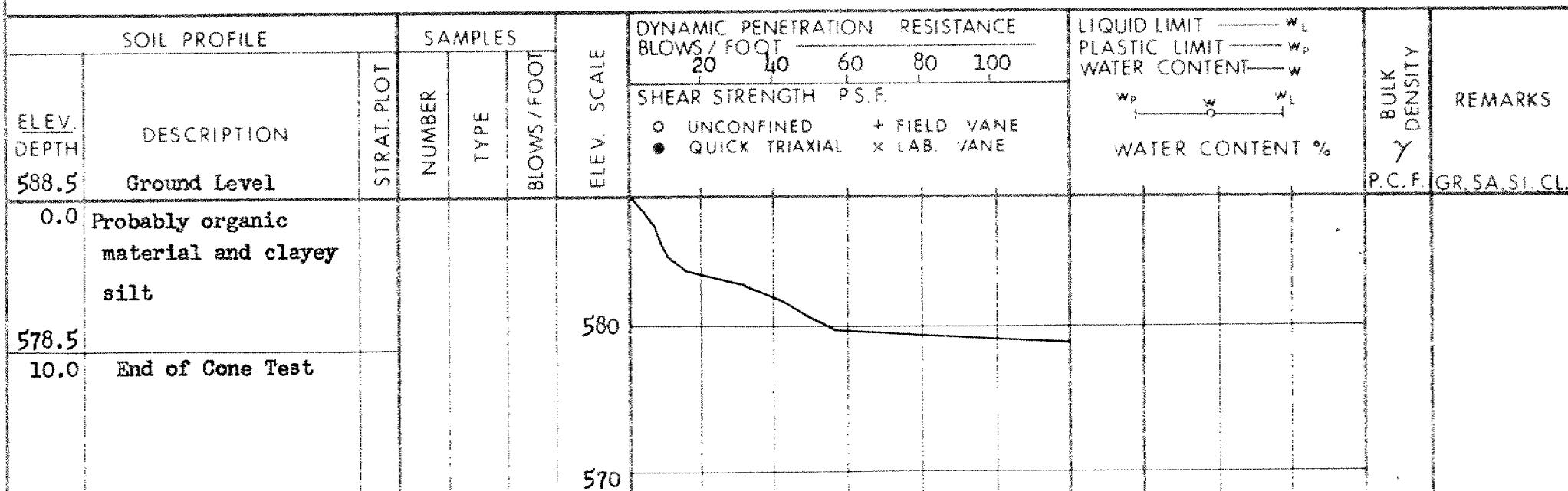
BORING DATE December 18, 1969

COMPILED BY PP

DATUM Geodetic

BOREHOLE TYPE Cone Test Only

CHECKED BY L.



DEPARTMENT OF HIGHWAYS - ONTARIO  
MATERIALS & TESTING OFFICE

**RECORD OF BOREHOLE No. 206**

## FOUNDATION SECTION

JOB 69-F-119

LOCATION Sta. 423 + 00 115' Lt. Modeland Rd.

ORIGINATED BY pp

W.P. 122-65-01

BORING DATE December 18, 1969

COMPILED BY P

### DATUM Geodetic

## BOREHOLE TYPE Cont. Flight Auger

CHECKED BY

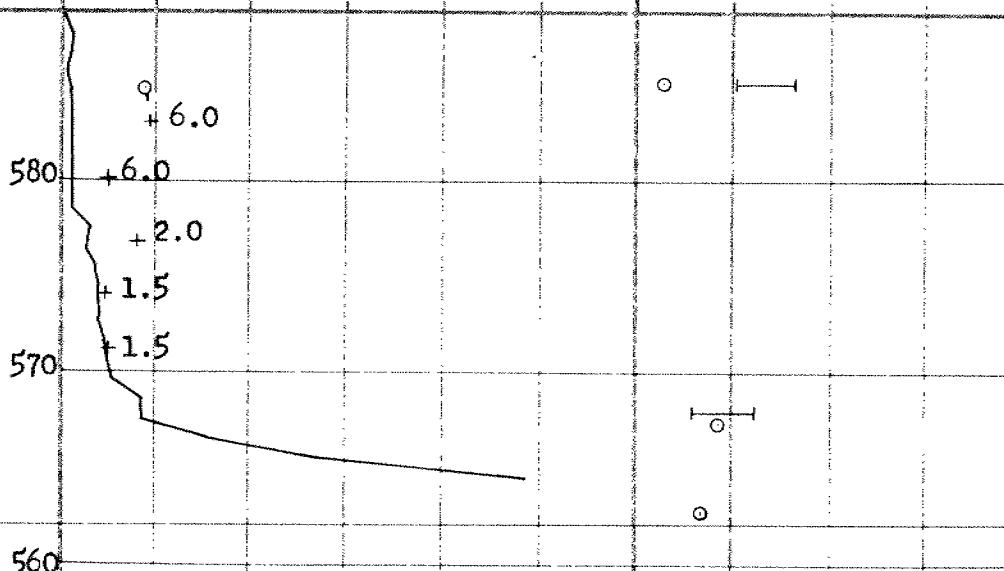
DEPARTMENT OF HIGHWAYS - ONTARIO  
MATERIALS & TESTING OFFICE

## RECORD OF BOREHOLE No. 207

FOUNDATION SECTION

JOB 69-F-119	LOCATION Sta. 425 + 80 75' Lt. Modeland Rd.	ORIGINATED BY PP
W.P. 122-65-01	BORING DATE December 18, 1969	COMPILED BY PP
DATUM Geodetic	BOREHOLE TYPE Cont. Flight Auger	CHECKED BY J.L.

SOIL PROFILE		SAMPLES		ELEV. SCALE	DYNAMIC PENETRATION RESISTANCE BLOWS / FOOT	LIQUID LIMIT — WL PLASTIC LIMIT — WP WATER CONTENT — W	BULK DENSITY Y	REMARKS
ELEV. DEPTH	DESCRIPTION	STRAT. PLOT	NUMBER	Type	BLOWS / FOOT	WP	WL	
588.5	Ground Level							GR. S.A. S.V.C.L.
0.0	Organic clay, silt, Layers of peat and sand		1	TW	PM			108
			2	SS	2			
			3	TW	PM			
			4	TW	PM			
			5	SS	2			
	Very soft to firm		6	SS	24			
567.5	Clayey silt with some sand and traces of gravel		7	SS	39			
562.0								
26.5	End of Borehole							



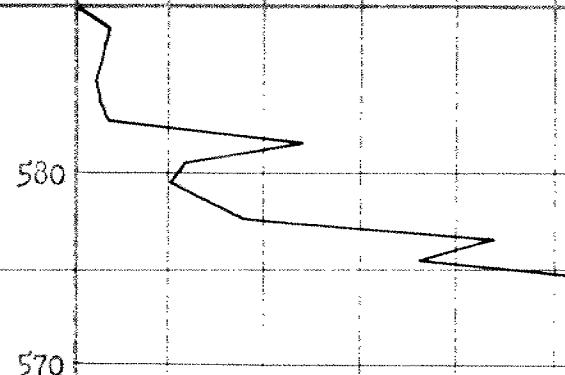
DEPARTMENT OF HIGHWAYS- ONTARIO  
MATERIALS & TESTING OFFICE

## RECORD OF BOREHOLE No. 208

FOUNDATION SECTION

JOB	69-F-119	LOCATION	Sta. 427 + 80 75' Lt. Modeland Rd.	ORIGINATED BY	PP
W.P.	122-65-01	BORING DATE	December 13, 1969	COMPILED BY	PP
DATUM	Geodetic	BOREHOLE TYPE	Cont. Flight Auger	CHECKED BY	12

SOIL PROFILE		SAMPLES		ELEV. SCALE	DYNAMIC PENETRATION RESISTANCE					SHEAR STRENGTH P.S.F.	UNCONFINED 1000	FIELD VANE 2000	LAB VANE	LIQUID LIMIT — $w_L$	PLASTIC LIMIT — $w_p$	WATER CONTENT — $w$	BULK DENSITY $\gamma$	REMARKS
ELEV.	DEPTH	STRAT. PLOT	NUMBER	Type	BLOWS / FOOT	20	40	60	80	100								
588.5	Ground Level																	
0.0	Sandy silt traces of clay Very loose		1	SS	4													
582.0			2	SS	30													
6.5	Clayey silt with some sand and traces of gravel		3	SS	28													
575.0			4	SS	49													
13.5	End of Borehole																	



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DEPARTMENT OF HIGHWAYS- ONTARIO  
MATERIALS & TESTING OFFICE

## RECORD OF BOREHOLE No. 209

FOUNDATION SECTION

JOB 69-F-119

LOCATION Sta. 425 + 80 175' Lt. Modeland Rd.

ORIGINATED BY PP

W.P. 122-65-01

BORING DATE December 18, 1969

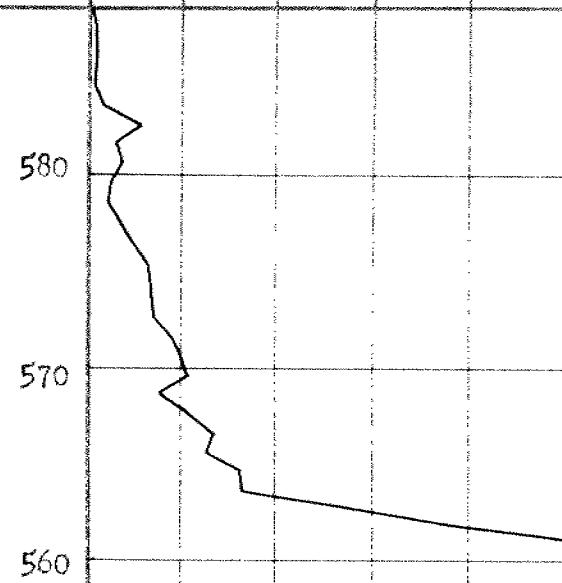
COMPILED BY PP

DATUM Geodetic

BOREHOLE TYPE Cone Test Only

CHECKED BY *[Signature]*

SOIL PROFILE		SAMPLES			ELEV. SCALE	DYNAMIC PENETRATION RESISTANCE BLOWS / FOOT					LIQUID LIMIT $w_L$ PLASTIC LIMIT $w_p$ WATER CONTENT $w$			BULK DENSITY $\gamma$	REMARKS	
ELEV. DEPTH	DESCRIPTION	STRAT. PLOT	NUMBER	TYPE		BLOWS / FOOT	20	40	60	80	100	SHEAR STRENGTH PSF.	$w_p$	$w$	$w_L$	
588.5	Ground Level															
0.0	Probably organic material and layers of silt & silty clay															
560.8	End of Cone Test															



DEPARTMENT OF HIGHWAYS - ONTARIO  
MATERIALS & TESTING OFFICE

## RECORD OF BOREHOLE No. 210

FOUNDATION SECTION

JOB 69-F-119

LOCATION Sta. 427 + 80 175' Lt. Modeland Rd.

ORIGINATED BY PP

W.P. 122-55-01

BORING DATE December 19, 1969

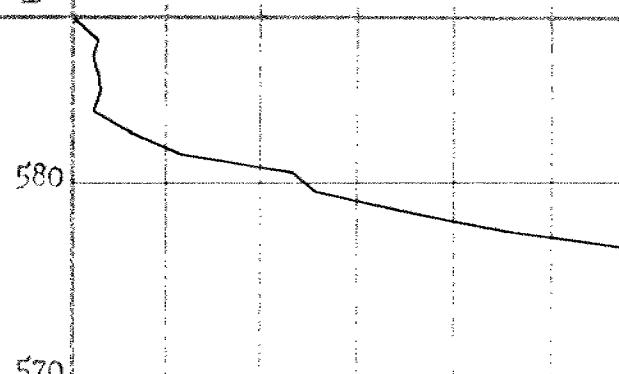
COMPILED BY PP

DATUM Geodetic

BOREHOLE TYPE Cone Test only

CHECKED BY

SOIL PROFILE		SAMPLES		ELEV. SCALE	DYNAMIC PENETRATION RESISTANCE					LIQUID LIMIT $w_L$			BULK DENSITY $\gamma$	REMARKS		
ELEV. DEPTH	DESCRIPTION	STRAT. PLOT	SAMPLE NUMBER		BLOWS / FOOT	20	40	60	80	100	FIELD VANE	LAB VANE	W <sub>0</sub>	W <sub>L</sub>	W <sub>C</sub>	
588.5	Ground Level															
0.0	Probably organic material layers of sand and clayey silt															
576.5	End of Cone Test															
12.0																



DEPARTMENT OF HIGHWAYS - ONTARIO  
MATERIALS & TESTING OFFICE

## RECORD OF BOREHOLE No. 211

FOUNDATION SECTION

JOB 69-F-119 LOCATION Sta. 423 + 00 175' Lt. Modeland Rd. ORIGINATED BY PP

W.P. 122-65-01 BORING DATE December 19, 1969 COMPILED BY PP

DATUM Geodetic BOREHOLE TYPE Cont. Flight Auger CHECKED BY

SOIL PROFILE		SAMPLES			ELEV. SCALE	DYNAMIC PENETRATION RESISTANCE					LIQUID LIMIT — WL	PLASTIC LIMIT — WP	WATER CONTENT — W	BULK DENSITY $\gamma$	REMARKS		
ELEV.	DEPTH	STRAT. PLOT	NUMBER	TYPE		20	40	60	80	100	SHEAR STRENGTH P.S.F	O UNCONFINED + FIELD VANE	● QUICK TRIAXIAL X LAB VANE	WP	W	WL	
588.5	Ground Level																
0.0	Clayey silt with organics and sand.		1	SS	5												
576.5	Firm to stiff		2	SS	10												
12.0	Clayey silt with some sand & traces of grav.		3	SS	33												
572.0																	
16.5	End of Borehole																

The graph plots Dynamic Penetration Resistance (Blows / Foot) against Depth (Elevation). The vertical axis ranges from 570 to 580 feet, and the horizontal axis ranges from 0.0 to 100 blows/foot. A single data series is plotted, showing a sharp initial increase from 0.0 to 5.0 blows/foot at the surface, followed by a gradual decrease to approximately 1.0 blow/foot at 16.5 meters depth.

## ABBREVIATIONS USED IN THIS REPORT

### PENETRATION RESISTANCE

STANDARD PENETRATION RESISTANCE 'N' :- THE NUMBER OF BLOWS REQUIRED TO ADVANCE A STANDARD SPLIT SPOON SAMPLER 12 INCHES INTO THE SUBSOIL, DRIVEN BY MEANS OF A 140 POUND HAMMER FALLING FREELY A DISTANCE OF 30 INCHES.

DYNAMIC PENETRATION RESISTANCE :- THE NUMBER OF BLOWS REQUIRED TO ADVANCE A 2 INCH, 60 DEGREE CONE, FITTED TO THE END OF DRILL RODS, 12 INCHES INTO THE SUBSOIL, THE DRIVING ENERGY BEING 350 FOOT POUNDS PER BLOW.

### DESCRIPTION OF SOIL

THE CONSISTENCY OF COHESIVE SOILS AND THE RELATIVE DENSITY OR DENSENESS OF COHESIONLESS SOILS ARE DESCRIBED IN THE FOLLOWING TERMS :-

CONSISTENCY	'N' BLOWS / FT.	c LB. / SQ. FT.	DENSENESS	'N' BLOWS / FT.
VERY SOFT	0 - 2	0 - 250	VERY LOOSE	0 - 4
SOFT	2 - 4	250 - 500	LOOSE	4 - 10
FIRM	4 - 8	500 - 1000	COMPACT	10 - 30
STIFF	8 - 15	1000 - 2000	DENSE	30 - 50
VERY STIFF	15 - 30	2000 - 4000	VERY DENSE	> 50
HARD	> 30	> 4000		

### TYPE OF SAMPLE

S.S.	SPLIT SPOON	T.W.	THINWALL OPEN
W.S.	WASHED SAMPLE	T.P.	THINWALL PISTON
S.B.	SCRAPER BUCKET SAMPLE	O.S.	OESTERBERG SAMPLE
A.S.	AUGER SAMPLE	F.S.	FOIL SAMPLE
C.S.	CHUNK SAMPLE	R.C.	ROCK CORE
S.T.	SLOTTED TUBE SAMPLE		
P.H.	SAMPLE ADVANCED HYDRAULICALLY		
P.M.	SAMPLE ADVANCED MANUALLY		

### SOIL TESTS

Qu	UNCONFINED COMPRESSION	L.V.	LABORATORY VANE
Q	UNDRAINED TRIAXIAL	F.V.	FIELD VANE
Qcu	CONSOLIDATED UNDRAINED TRIAXIAL	C	CONSOLIDATION
Qd	DRAINED TRIAXIAL	S	SENSITIVITY

## ABBREVIATIONS USED IN THIS REPORT

### SOIL PROPERTIES

$\gamma$	UNIT WEIGHT OF SOIL (BULK DENSITY)
$\gamma_s$	UNIT WEIGHT OF SOLID PARTICLES
$\gamma_w$	UNIT WEIGHT OF WATER
$\gamma_d$	UNIT DRY WEIGHT OF SOIL (DRY DENSITY)
$\gamma'$	UNIT WEIGHT OF SUBMERGED SOIL
G	SPECIFIC GRAVITY OF SOLID PARTICLES $G = \frac{\gamma_s}{\gamma_w}$
e	VOID RATIO
n	POROSITY
w	WATER CONTENT
$S_r$	DEGREE OF SATURATION
$w_L$	LIQUID LIMIT
$w_P$	PLASTIC LIMIT
$I_p$	PLASTICITY INDEX
s	SHRINKAGE LIMIT
$I_L$	LIQUIDITY INDEX = $\frac{w - w_p}{I_p}$
$I_c$	CONSISTENCY INDEX = $\frac{w_L - w}{I_p}$
$e_{max}$	VOID RATIO IN LOOSEST STATE
$e_{min}$	VOID RATIO IN DENSEST STATE
$I_d$	DENSITY INDEX = $\frac{e_{max} - e}{e_{max} - e_{min}}$
	RELATIVE DENSITY $D_r$ IS ALSO USED
h	HYDRAULIC HEAD OR POTENTIAL
q	RATE OF DISCHARGE
v	VELOCITY OF FLOW
i	HYDRAULIC GRADIENT
k	COEFFICIENT OF PERMEABILITY
j	SEEPAGE FORCE PER UNIT VOLUME
$m_v$	COEFFICIENT OF VOLUME CHANGE = $\frac{-\Delta e}{(1+e)\Delta \sigma}$
$c_v$	COEFFICIENT OF CONSOLIDATION
$C_c$	COMPRESSION INDEX = $\frac{\Delta e}{\Delta \log_{10} \sigma'}$
$T_v$	TIME FACTOR = $\frac{c_v t}{d}$ (d, DRAINAGE PATH)
U	DEGREE OF CONSOLIDATION
$T_f$	SHEAR STRENGTH
$c'$	EFFECTIVE COHESION INTERCEPT
$\phi'$	EFFECTIVE ANGLE OF SHEARING RESISTANCE, OR FRICTION
$c_u$	APPARENT COHESION
$\phi_u$	APPARENT ANGLE OF SHEARING RESISTANCE, OR FRICTION
$\mu$	COEFFICIENT OF FRICTION
$S_t$	SENSITIVITY

### GENERAL

$\pi$	= 3.1416
e	BASE OF NATURAL LOGARITHMS 2.7183
$\log_e \sigma$ OR $\ln \sigma$	NATURAL LOGARITHM OF $\sigma$
$\log_{10} \sigma$ OR $\log \sigma$	LOGARITHM OF $\sigma$ TO BASE 10
t	TIME
g	ACCELERATION DUE TO GRAVITY
V	VOLUME
W	WEIGHT
M	MOMENT
F	FACTOR OF SAFETY

### STRESS AND STRAIN

u	PORE PRESSURE
$\sigma$	NORMAL STRESS
$\sigma'$	NORMAL EFFECTIVE STRESS ( $\sigma'$ IS ALSO USED)
$\tau$	SHEAR STRESS
$\epsilon$	LINEAR STRAIN
$\gamma$	SHEAR STRAIN
$\nu$	POISSON'S RATIO ( $\mu$ IS ALSO USED)
E	MODULUS OF LINEAR DEFORMATION (YOUNG'S MODULUS)
G	MODULUS OF SHEAR DEFORMATION
K	MODULUS OF COMPRESSIBILITY
$\eta$	COEFFICIENT OF VISCOSITY

### EARTH PRESSURE

d	DISTANCE FROM TOP OF WALL TO POINT OF APPLICATION OF PRESSURE
$\delta$	ANGLE OF WALL FRICTION
K	DIMENSIONLESS COEFFICIENT TO BE USED WITH VARIOUS SUFFIXES IN EXPRESSIONS REFERRING TO NORMAL STRESS ON WALLS
$K_o$	COEFFICIENT OF EARTH PRESSURE AT REST

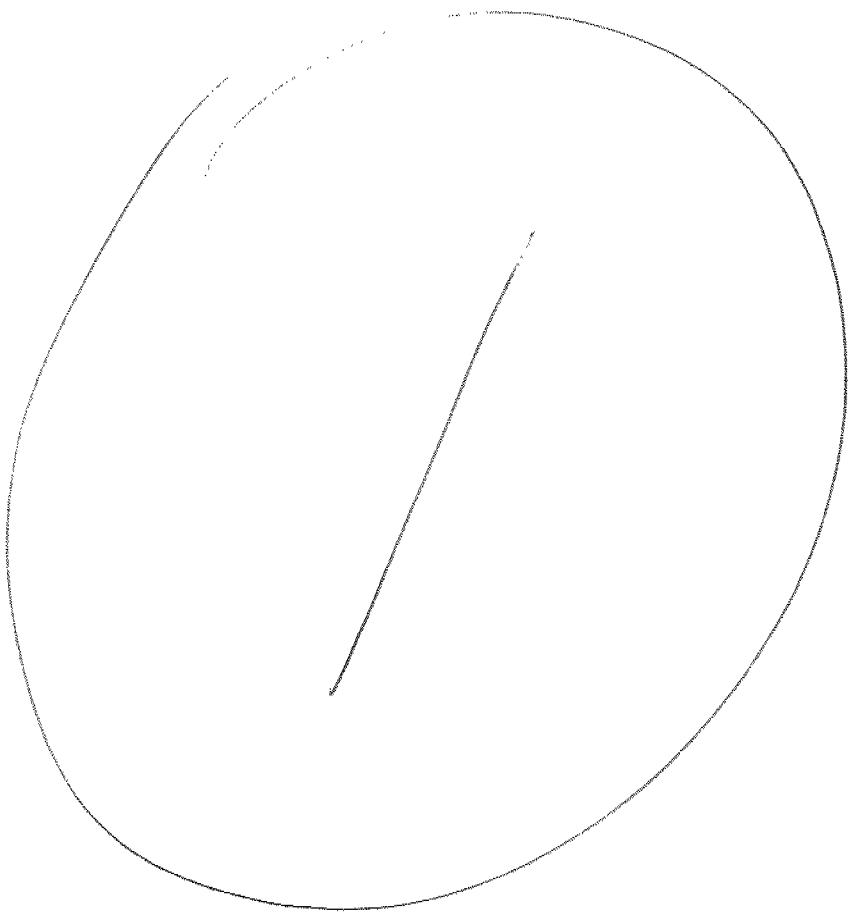
### FOUNDATIONS

B	BREADTH OF FOUNDATION
L	LENGTH OF FOUNDATION
D	DEPTH OF FOUNDATION BENEATH GROUND
N	DIMENSIONLESS COEFFICIENT USED WITH A SUFFIX APPLYING TO SPECIFIC GRAVITY, DEPTH AND COHESION ETC. IN THE FORMULA FOR BEARING CAPACITY
$K_s$	MODULUS OF SUBGRADE REACTION

### SLOPES

H	VERTICAL HEIGHT OF SLOPE
D	DEPTH BELOW TOE OF SLOPE TO HARD STRATUM
$\beta$	ANGLE OF SLOPE TO HORIZONTAL

# 35MM DRAWING



# 35MM DRAWING

