

BA 745

Plans.

S6673

REPORT

TO

DEPARTMENT OF HIGHWAYS, ONTARIO

ON

SOIL CONDITIONS AND FOUNDATIONS

PROPOSED MONTREAL RIVER BRIDGE

HIGHWAY 11

LATCHFORD

ONTARIO

58-F-310C

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Rexdale, Ontario,
June 2nd, 1958.

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Toronto 2, Ontario.

58-F-310 C

Attention: Mr. A. M. Teye, P. Eng.,
Bridge Engineer.

Re: Site Investigation,
Proposed Montreal River Bridge,
Highway 11,
Latchford, Ontario.

Dear Sirs:

This letter reports the results of the above investigation carried out in accordance with our proposal dated May 2nd, 1958 and accepted on May 5th, 1958. The object of this investigation was to determine and interpret the subsoil conditions at the above site, as they affect the design of foundations for the proposed bridge.

The site of the proposed bridge on the Montreal River is located south of Latchford, Ontario and between the existing conservation dam and Ontario Northland Railway bridge. The ground level at the site varies from a minimum elevation of about 895 at the river bed to a maximum elevation of about 930 on the south bank of the river. The width of the river at the site is approximately 205 feet. From available geological information, it is known that, at the site, sands, gravels and boulders in the river channel and boulder till elsewhere overlie bedrock. Bedrock is Precambrian siliceous shale of the Cabot series.

The field work was commenced on May 8th and completed on May 15th, 1958. Four exploratory boreholes were put down to depths between 23 feet and 32 feet. A shallow test pit was put down on the north bank of the river



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to check the soil conditions. The locations of the borings and the test pit together with the inferred soil stratigraphy are shown on Drawing S6673-1 attached at the rear of this report. Detailed logs of each borehole are given on the Office Reports on Soil Exploration in Appendix I.

The soil and rock samples obtained will be stored until December 1st, 1958 and will then be destroyed unless further instructions are received.

The locations of the borings were obtained from a site plan No. 1714-T-1 supplied by the Foundation of Canada Engineering Corporation Limited. Elevations are Geodetic and were obtained by reference to water level readings at the conservation dam.

SOIL CONDITIONS

The principal subsoil strata encountered by the borings are as follows:

Peat

A layer of dark brown peat, about 1 foot in thickness, was generally found to cover the area around test pit 5.

Fill

A layer of sand, gravel and boulder fill, about 3 feet in thickness, was encountered at ground surface in borehole 4, put down on the south bank of the river and adjacent to the existing band stand. The relative density of the fill layer is estimated from the resistance to core drilling and core recovery to be compact to dense.

Boulders

The river bed consists of boulders, the upper surface of which is irregular and varies from about 3 feet below water level, to about water

SOIL CONDITIONS (continued)

Boulders (continued)

level. The thickness of the boulder stratum as encountered in boreholes 1, 2 and 3, varies from about 4 to 12 feet. The boulders range in size to a maximum of about 6 feet and are of assorted geological origin. In borehole 2, located in the relatively calm portion of the river channel, some sand and gravel sizes were encountered among the boulders.

From observation of the gaps between boulders and from the core recovery, it is estimated that the upper portion of the boulder stratum is of loose relative density. The relative density of the remainder of the stratum is estimated to be compact.

Boulder Clay Till

Beneath the peat in test pit 5, the fill in borehole 4 and the boulders in borehole 3, a stratum of boulders in a matrix of grey-brown clay till was encountered. Due to the presence of the numerous boulders, it was very difficult to estimate the relative density of the clay till, but based on the core recovery, it is estimated to be dense.

Bedrock

Underlying the boulder till in boreholes 3 and 4 and the boulders in boreholes 1 and 2, bedrock was encountered. Bedrock is a sound dark grey siliceous shale of the Cobalt series separated by occasional thin bands of arkose. The shale is laminated by thin alternating bands of dark grey and dull red. The upper 1 to 5 feet of the shale has been subjected to weathering resulting in a somewhat fragmental and broken structure, occasionally resulting in poor rock core recovery. Bedrock was proved by diamond drilling for up to 25 feet in borehole 1.

WATER CONDITIONS

During the time of the investigation, the river water level varied between elevation 900.3 and 900.8.

DISCUSSION

It is understood that the proposed bridge is to be either a two-span through truss steel structure with a pier located in the middle of the river or a single span steel structure. The proposed location of the bridge is as shown on Drawing S6673-1. The exact details of the bridge structure are at present not known, but the boreholes were located by the Foundation of Canada Engineering Corporation Limited so that a multi-span structure may be studied.

For the pier and abutment foundations, it is considered that the boulder stratum is not a suitable bearing stratum due to its erratic and loose relative density. It is therefore recommended that the pier and abutment foundations be carried to the sound portion of the bedrock, ranging from about elevation 892 to 883 as shown on Drawing S6673-1, and that the weathered and fragmental upper portion of the bedrock be removed. It is further recommended that an inspection of the bedrock be made following excavation to ensure that it is in a sound condition. An allowable bearing pressure of 20 tons per square foot may be used for design of foundations resting on the sound portion of the bedrock.

Prior to the construction of approach embankments, it is recommended that all peat and topsoil be removed. The boulder till is suitable for the construction of embankments and based on the soil conditions encountered in this investigation, it is considered that for embankment design an angle of internal friction of 40 degrees and a wet unit weight of 130 pounds per cubic foot may be used. For example, an embankment about 20 feet in height with side slopes of 1 vertical to $1\frac{1}{2}$ horizontal would have an adequate factor of safety for overall stability. It is further recommended that the face of the embankment be protected by rip rap to prevent scour in the river.

Department of Highways, Ontario,
June 2nd, 1958,
Page 5.

We believe that this letter report gives all the information necessary to enable you to proceed with the design of the proposed bridge. If however, we can be of any further assistance, please do not hesitate to contact us.

Yours very truly,

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VA/dw
S6673

V. Milligan per J. L. S.
V. Milligan, P. Eng.,
District Engineer.

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APPENDIX I

OFFICE REPORTS ON SOIL EXPLORATION

EXPLANATION OF THE FORM "OFFICE REPORT ON SOIL EXPLORATION"

The object of this form is to enable a comprehensive study of the soil to be made by combining on one sheet all of the information obtained from the boring. An explanation of the various columns of the report follows.

ELEVATION AND DEPTH

This column gives the elevation and depth of boundaries between the various soil strata. The elevation is referred to the datum shown in the general heading.

WATER CONDITIONS

In this column the water level in the casing at the time of boring or the water table in the ground, determined by a series of observations in a piezometer or standpipe, is indicated to scale by a horizontal line with the symbol W.L. or W.T. above the line. A notation of any complicated groundwater conditions will be made in this column.

DESCRIPTION

A description of the soil, using standard terminology, is contained in this column. The consistency of cohesive soils and the relative density of non-cohesive soils are described by the following terms:

Consistency	U-Strength Tons/sq. ft.	Relative Density	Standard Penetration Resistance, Blows/ft.
Very soft	0.03 to 0.25	Very loose	0 to 4
Soft	0.25 to 0.5	Loose	4 to 10
Firm	0.5 to 1.0	Compact	10 to 30
Stiff	1.0 to 2.0	Dense	30 to 50
Very stiff	2.0 to 4.0	Very dense	over 50
Hard	over 4.0		

STRATIGRAPHIC PLOT

The stratigraphic plot follows the standard symbols of the National Research Council, Canada.

ELEVATION SCALE

The information in all columns is plotted to a true elevation scale which is shown in this column.

GRAPHS

The main body of the report forms a graph which is used to plot to correct elevation the important soil properties which are obtained through field and laboratory tests. The scales and symbols for the plotting are shown at the head of the column.

OTHER TESTS

In this column are shown, by symbol, the other field or laboratory tests which have been performed on the soil and for which the results have not been plotted on the above graph.

SAMPLES

The first three columns describe the condition, type and number of each sample obtained from the boring. The location and extent of each sample is plotted to scale.

In the last column is shown the penetration resistance in blows of 4200 inch-pounds required to drive one foot of the sampler into the ground. When a 2 inch Drive Sampler is used the result obtained is termed the "Standard Penetration Resistance".

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OFFICE REPORT ON SOIL EXPLORATION

CONTRACT 52473 BORING # APP-1 DATUM GEODETIC CASING EX-1 ANT
 BORING DATE MAY 10, 1953 REPORT DATE MAY 21, 1953 COMPILED BY MNV CHECKED BY NLS
 SAMPLER HAMMER WT. 175 LBS. DROP 27 INCHES (PENETRATION RESISTANCES CONVERTED TO BLOWS OF 4200 IN. LBS. ENERGY)

SAMPLE CONDITION



AS - AUGER SAMPLE
 ST - SLOTTED TUBE
 WS - WASHED SAMPLE
 GO - DRIVE-OPEN
 DF - DRIVE-FOOT VALVE
 CS - CHUNK SAMPLE

SAMPLE TYPES

FS - FOIL SAMPLE
 SO - SLEEVE-OPEN
 SF - SLEEVE-FOOT VALVE
 TO - THIN WALLED OPEN
 RC - ROCK CORE

ABBREVIATIONS

V - IN SITU VANE TEST
 M - MECHANICAL ANALYSIS
 U - UNCONFINED COMPRESSION
 GC - TRIAXIAL CONSOLIDATED QUICK
 Q - TRIAXIAL QUICK
 S - TRIAXIAL SLOW
 W - WET UNIT WEIGHT
 K - PERMEABILITY
 C - CONSOLIDATION
 WL - WATER LEVEL IN CASING
 WT - WATER TABLE IN SOIL

SOIL PROFILE

ELEV. DEPTH	WATER CONDITIONS	DESCRIPTION	STRAT. PLOT	ELEVATION SCALE
300.5		WATER LEVEL		
1.0		RIVER BOTTOM		
		BOULDERS		
291.5		WEATHERED SILICEOUS SHALE BEDROCK		
286.5		ROUND DARK GREY SILICEOUS SHALE BEDROCK		
274.5		END OF HOLE		

WATER CONTENT W₁ NAT. LW PW

DYNAMIC PENETRATION TEST BLOWS PER FOOT

OTHER TESTS

SAMPLES

CONDITION	TYPE	NUMBER	PENETRATION RESISTANCE BLOWS/FT
RECOVERY 15%	RC BX		
RECOVERY 47%	RC AX		
RECOVERY 75%	RC AX		
RECOVERY 100%	RC AX		
RECOVERY 100%	RC AX		

APPENDIX I

SAMPLE CONDITION

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SAMPLE TYPES

AS	AUGER SAMPLE	FS	FOIL SAMPLE
ST	SLOTTED TUBE	SO	SLEEVE OPEN
WS	WASHED SAMPLE	SV	SLEEVE FOOT VALVE
DO	DRIVE OPEN	TO	THIN WALLED OPEN
DF	DRIVE FOOT VALVE	RC	ROCK CORE
CS	CRUSH SAMPLE		

ABBREVIATIONS

- * - IN-SITU VANE TEST
- M - MECHANICAL ANALYSIS
- C - UNCONFINED COMPRESSION
- QC - TRIAXIAL CONSOLIDATED QUICK
- Q - TRIAXIAL QUICK
- CU - TRIAXIAL SLOW

- 1. WET UNIT WEIGHT
- 2. PERMEABILITY
- 3. CONSOLIDATION

WL - WATER LEVEL IN CASING
WT - WATER TABLE IN SOIL

SOIL PROFILE

[illegible]

WATER CONTENT W

DYNAMIC PENETRATION TEST BLOWS PER FOOT

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SAMPLES

THE
STANDARD
OF
THE
NATIONAL
BANK
OF
THE
UNITED
STATES
OF
AMERICA
INCORPORATED
IN
THE
STATE
OF
NEW
YORK
CAPITAL
PAID
UP
\$1,000,000
RESERVE
FUND
\$500,000
TOTAL
ASSETS
\$1,500,000
LIABILITIES
\$1,500,000
NEW
YORK
1890

APR 1951

SAMPLE CONDITION

SAMPLE TYPES

F.S. FOIL SAMPLE
S.O. SLEEVE OPEN
S.F. SLEEVE FOOT VALVE
T.O. THIN WALLED OPEN
R.C. ROCK CORE

- V - IN-SITU VANE TEST
- M - MECHANICAL ANALYSIS
- U - UNCONFINED COMPRESSION
- QC - TRIAXIAL CONSOLIDATED QUICK
- Q - TRIAXIAL QUICK
- S - TRIAXIAL SLOW

ABBREVIATIONS

- 2. WET UNIT WEIGHT
- X. PERMEABILITY
- C. CONSOLIDATION

WL - WATER LEVEL IN CASIN
WT - WATER TABLE IN SOIL



DISTURBED
FAIR
GOOD
LOST

AS - AUGER SAMPLE
ST - SLOTTED TUBE
WS - WASHED SAMPLE
DO - DRIVE OPEN
DF - DRIVE FOOT VALVE
CS - CHUNK SAMPLE

SOIL PROFILE

ELEV. DEPTH	WATER CONDITIONS	DESCRIPTION	STRAT. PILOT ELEVATION SCALE	WATER CONTENT W%				OTHER TESTS	CONDITION	TYPE	NUMBER	PENETRATION RESISTANCE BLOWS FT.
				NAT	LW	LP						
				DYNAMIC PENETRATION TEST BLOWS PER FOOT								
895.0 8.0 805.0 3.0		GROUND LEVEL SAND GRAVEL AND BOULDER FILL	910					RECOVER 80%	RC BXT			
		BOULDERS IN MATRIX OF CLAY TILL	900					RECOVER 19%	RC BXT		3	
893.0		WEATHERED SILICEOUS SHALE BEDROCK						RECOVER 7%	RC BXT		4	
16.0		SOUND DARK GREY SILICEOUS SHALE BEDROCK	891.1					RECOVER 50%	RC BXT		5	
884.7 23.3		END OF HOLE	890.0					RECOVER 45%	RC BXT		6	
								RECOVER 75%	RC BXT			
805.0 50.0 1.0 2.0		GROUND LEVEL PEAT	705									
		END OF TEST PIT										
		BOULDERS IN MATRIX OF CLAY TILL	800									

58F-310C

Hwy # 11

MONTREAL RIVER

