

GEOCRES #31L-73



MERLEX ENGINEERING LTD.

CONSULTING GEOTECHNICAL ENGINEERS

FOUNDATION INVESTIGATION AND DESIGN REPORT

W.P. 167-90-00

Highway 63,
From 1.0 km N of Jct. of Hwy 533, N'ly to Quebec Border, 23.5 km

M.T.O. District 54, Sudbury

Merlex Reference No. 00/04/00036-F

January 2001

Submitted to

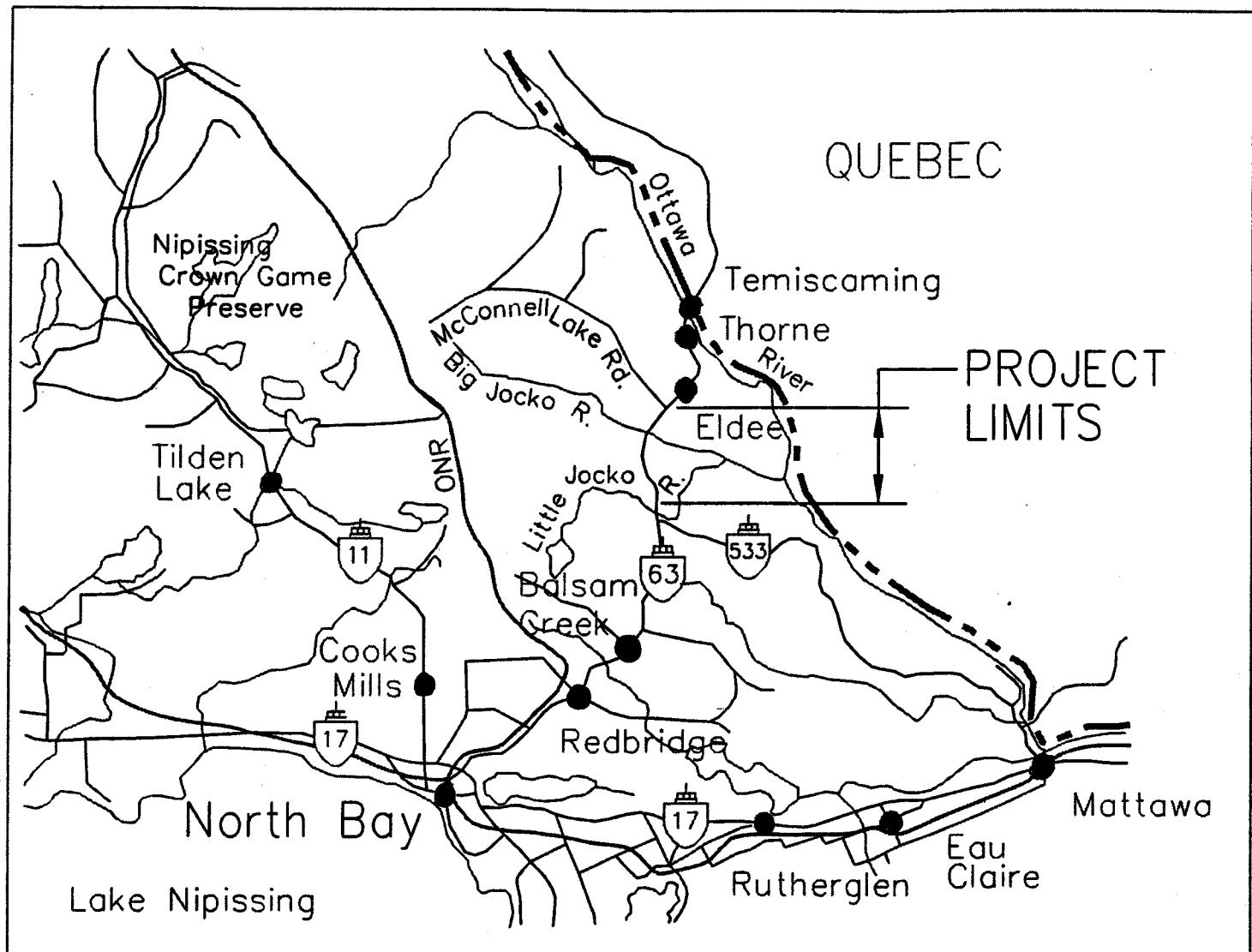
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Figure 1



Highway 63

From 1.0 km N of Jct. of Hwy 533, N'ly to
Quebec Border, 23.5 km
M.T.O. District 54, Sudbury

W.P. 167-90-00



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1.0 INTRODUCTION

Merlex Engineering Ltd. has been retained by Earth Tech (Canada) Inc., on behalf of the Ministry of Transportation to carry out a foundation investigation at the site of the proposed horizontal realignment of Highway 63, in the area of the Jocko/Clarkson Township line. The new alignment eliminates a 250 radius curve with a tangent section between Station 20+875 Jocko and Station 10+350 Clarkson (new chainage).

The purpose of this investigation was to delineate the subsurface conditions along the new horizontal alignment with sampled boreholes. During the geotechnical investigation, relatively deep deposits of peat were encountered at two additional locations, Station 13+250 to 13+825 and Station 20+300 to 20+450 Township of Jocko, where platform widening is to be carried out on the right side. A foundation investigation was subsequently requested for these areas.

The terms of reference for this scope of work are outlined in our proposal P-00-12 dated March 16, 2000 and subsequent proposal, for the additional areas, dated July 24, 2000. The work was carried out in accordance with the "Guidelines for Professional Engineers Providing Geotechnical Engineering Services" (1993) and the provisions in the RFP Terms of Reference.

2.0 SITE DESCRIPTION

The initial area of investigation is located to the west of the existing Highway 63 at the Jocko/Clarkson Township line approximately 2 km north of the Big Jocko River and has been designated as Area 3 in this report. The two additional foundation investigation sites, Station 13+250 to 13+825 and Station 20+300 to 20+450, Township of Jocko, have been designated Areas 1 and 2 respectively. Area 1 is located 5 km south of the Big Jocko River, whereas Area 2 is 1.5 km to the north. These sites are located within the MTO District 54 approximately 45 km north of the City of North Bay.

The proposed construction consists of widening the existing platform 3.3 m and 2.25 m to the right in Areas 1 and 2, respectively and constructing a new road platform in Area 3. Plans and profiles, of the areas, are shown on the enclosed Figures 2 to 8 inclusive. Throughout Areas 1, 2 and 3 the ground surface is generally flat and varies between about elevation 305, 302 and 289 m respectively.

3.0 INVESTIGATION PROCEDURES

The field work for this investigation was carried out during the period of July 27 and August 31, 2000 and consisted of a total of 45 boreholes along with 42 dynamic cone penetration tests at the boring locations.

The borings were advanced with a bombardier mounted CME 45B diesel powered drill rig, equipped with 160 mm outside diameter (O.D.) continuous flight hollow stem augers. Soil samples were obtained at regular intervals of depth using a 50 mm O.D. split spoon sampler in accordance with the Standard Penetration Test (SPT) procedure. The boreholes were advanced to a 10 m depth or practical auger refusal, which ever occurred first, whereas the

dynamic cone penetration tests were advanced to refusal or below the deeper boreholes into a dense stratum. The in-situ shear strength of the peat deposits was measured in the boreholes using an "N" size MTO vane and calibrated torque-meter. The groundwater conditions in the open boreholes were observed during the drilling operation and are described on the Record of Borehole sheets that follow the text.

The field work was under the supervision of a senior member of our field engineering staff, who was responsible for locating the boreholes and dynamic cone penetration test locations, supervising the drilling, sampling and testing operations, logging the boreholes along with examining and preparing the samples for shipment to our North Bay Laboratory for further examination and select testing. Laboratory testing included: natural moisture content and grain size analysis. The results of the laboratory testing are given on the Record of Borehole Sheets.

Investigation locations, Boreholes 1 to 11 inclusive, were marked in the field and surveyed by the firm of Simpson and Osburn Surveying Inc., whereas the locations of Boreholes 13 to 45 inclusive were established relative to new chainage and center line offset as surveyed in the field.

4.0 SUBSURFACE CONDITIONS

The subsurface conditions encountered at the borehole locations, along with the laboratory test results, are presented on the Record of Borehole sheets. The stratigraphic boundaries indicated on the Records of Borehole are inferred from non-continuous sampling, observations taken during drilling, the results of Standard Penetration Tests (SPT's), and Dynamic Cone Penetration Resistance test values. The boundaries between various strata shown on the Record of Borehole generally represent transition from one soil type to another and should not

be regarded as exact planes of geological change. Furthermore, subsurface conditions will vary between and beyond the borehole locations.

In general, the native subsurface conditions consist of peat (varying in thickness from 300 mm to 4.2 m) underlain by non-cohesive deposits of varying composition (fine sands with varying silt content to silt with varying fine sand content). At boreholes put down through the existing platform shoulder granular fills were present overlying the peat deposit. Refusal to further advance of the augers or advance of the dynamic cone penetration test was generally met at depths of 5 to 10 m below grade.

Laboratory test results for the predominant soil types are shown on the Record of Borehole Sheets. The laboratory testing was carried out in accordance with the MTO LS Manual and ASTM Standards.

A summary of the general subsurface conditions at each of the areas is as follows:

4.1 Area 1: Township of Jocko Station 13+250 to 13+825

A plan and profile showing the borehole locations and stratigraphies for Area 1 is shown on Figures 2, 3A, 3B, 4A and 4B. Boreholes 34 to 45 inclusive, were advanced through the existing right shoulder, where the ground surface elevation at the boreholes varied between 308.9 to 304.0 m. Boreholes 13 to 25 inclusive, were put down at a location off-set from the right toe of slope, where the ground surface elevation at the boreholes varied between 307.8 to 303.5 m. The boreholes were advanced to depths ranging from 1.4 to 10.9 m (average depth 7.2 m).

At the toe of slope, a peat deposit was encountered at the borehole locations and extended to depths ranging between 1.9 to 4.2 m, with an average depth of 3.1 m. The peat was described as a black fine fibrous peat with occasional coarse fibers and occasional organic silt seams. The average in-situ vane shear strength was measured at 32.7 kPa (range 15 to 58 kPa) (see Figure 9). The variation in natural moisture content of this deposit, ranged from 89 to 831% (average 366%) as shown on Figure 11.

Boreholes put down through the right shoulder encountered a thin crushed gravel layer underlain by a sand (platform) fill which extended to depths ranging between 1.1 to 2.0 m (average 1.4 m). The platform fill was underlain by the black fine fibrous peat, average thickness 2.4 m, with an average in-situ vane shear strength measured at 55.3 kPa (range 30 to 90 kPa) as shown on Figure 10. The variation in natural moisture content of this deposit ranged from 88 to 653% (average 309%) as shown on Figure 11.

Underlying the peat deposits a cohesionless deposit of varying composition (silty sand with varying fine sand and silt content, and frequently containing gravel and occasional cobbles at depth) was encountered at the boreholes. Based on the Standard Penetration Test (N) values and Dynamic Cone Penetration Test (DCPT) values, the relative density of the cohesionless soils varied from loose to very dense, generally compact. Grain size data is shown on the individual borehole records. These cohesionless deposits were encountered to the depths at which refusal to further auger penetration was met or termination of the borehole (average depth 7.2 m).

4.2 Area 2: Township of Jocko Station 20+300 to 20+450

A plan and profile showing borehole locations and stratigraphies of Area 2 is shown on Figures 5a and 5b. Boreholes 30 to 33 inclusive, were advanced through the right shoulder of the

existing road platform, where the ground surface elevation at the borehole locations, varied between 302.8 to 303.6 m. Boreholes 26 to 29 inclusive, were put down at locations offset from the right toe of slope, where the ground surface elevation at the boreholes varied between elevation 301.6 to 302.1 m. The boreholes were advanced to depths ranging between 4.4 to 8.5 m (average 6.1 m) below existing grade.

At the toe of slope, a peat deposit was penetrated at the borehole locations and extended to depths ranging between 1.7 to 3.3 m, with an average depth of 2.4 m. The peat was described as black fine fibrous peat with occasional coarse fibers and occasional organic silt seam. The average in-situ vane shear strength, was measured at 24.9 kPa (range 12 to 32 kPa) (see Figure 9). The variation in natural moisture content of this deposit ranged between 131% to 694% (average 483%) as shown on Figure 12.

Boreholes put down through the road platform, right shoulder, (Boreholes 30 to 33 inclusive) encountered a thin crushed gravel layer underlain by a sand (platform) fill, which extended to depths ranging between 1.5 to 2.0 m. Based on (N) values, this stratum of platform fill was in very loose to compact (generally loose) state of relative density. Directly underlying the platform granular fill, a black fine fibrous peat was encountered with a thickness ranging from 0.6 to 1.8 m (average 1.1m) The average in-situ shear strength was measured at 48.0 kPa (range 37 to 75 kPa) (see Figure 10). The variation of natural moisture content of this deposit ranged from 222% to 376% (average 273%) as shown on Figure 12.

Underlying the peat stratum, a cohesionless deposit of varying composition (silty sand with varying fine sand and silt content and frequently containing gravel and occasional cobbles at depth) was penetrated at the borehole locations. Based on the Standard Penetration Tests (N) values and Dynamic Cone Penetration Tests values, the relative density of the cohesionless soils varied from loose to very dense, generally compact. Grain size data is shown on the

individual borehole records. Refusal to further penetration of the augers or advanced of the Dynamic Cone Penetration Test, was met at depths ranging between 4.4 to 8.5 m (average 6.1 m).

4.3 Area 3: Township of Jocko Station 20+150 to Township of Clarkson Station 10+350

A plan and profile showing the borehole locations and stratigraphies for Area 3 is shown on Figures 6 to 8 inclusive. Boreholes 1 to 11 inclusive were advanced along the approved new centreline. The existing grade at the borehole locations was at elevation 289.0 m ±, except at Borehole 11 where the grade rose to 292.4 m. The boreholes were advanced to an average depth of 9.6 m below existing grade (range 1.4 to 12.2 m). At Boreholes 1 through 10 inclusive, a black fine fibrous peat deposit was penetrated from the ground surface. This stratum ranged in thickness from 1.8 to 2.4 m (average 2.1 m) and the average in-situ vane shear strength was measured at 29.3 kPa (range 18 to 44 kPa) (see Figure 9). The variation in natural moisture content of this deposit ranged between 87% to 921% (average 604%) as shown on Figure 13. Underlying the peat deposit a cohesionless stratum of varying composition (sands to silty sands with varying fine sand and silt content frequently contained gravel and cobbles at depth) was encountered at the borehole locations. Based on the Standard Penetration Tests (N) values and the Dynamic Cone Penetration Tests the relative density of this cohesionless soil varied from loose to very dense, generally compact. Grain size data for individual samples is shown on the enclosed Borehole Logs 1 through 11 inclusive.

MERLEX ENGINEERING LTD.



M. A. Merleau, P. Eng.
Principal



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5.0 DESIGN COMMENTS AND RECOMMENDATIONS

5.1 General

Throughout Areas 1 and 2, the shift in the horizontal alignment to the right had been established prior to this investigation. The vertical alignment will essentially remain constant, or increase slightly (order of 300 mm±), throughout these areas to accommodate the lateral shift in the new platform. Typical cross-section schematics through the central area of the widening in Area 1 are shown on Figure 14 (Station 13+450 and 13+700).

In Area 3, a new horizontal and vertical alignment was established to correct a substandard horizontal curve.

5.2 Design Options

In Areas 1 and 2, a shift of 3.3 and 2.25 m to the right respectively has been approved. Throughout these two areas, the existing road platform, which varies in average thickness from 1.4 to 1.8 m (Areas 1 and 2 respectively), is underlain by a fine fibrous peat of average thickness 2.4 and 1.1 m respectively. At the toe of slope, to the right of the existing platform (area of embankment widening) the average peat depth, from existing grade, is 3.1 to 2.4 m respectively. For construction of the embankment widening to one side in these two areas, the following three options have been considered and are summarized on Table 1:

- Excavation of peat, to underlying sands, as per OPSD 203.020 in area of widening.
- Full width excavation of all peat from under platform.
- Place embankment widening fill directly on existing peat grade.

In Area 3, the proposed new alignment traverses an area of shallow peat cover (average thickness 2.1 m) underlain by competent, generally compact cohesionless soils (sands, silty sands and sandy silt). The embankment height reduces from approximately 8 and 5.5 m, at the

south and north ends respectively to some 1.5 m throughout the sag. Considering the relatively shallow depth of peat, as identified at Boreholes 1 to 11 inclusive, the only option considered is to excavate out the peat to mineral soil and construct the embankment as per OPSD 203.010, for the full platform width, since "floating" the road platform over the shallow peat deposit is not considered appropriate for a road of this standard.

Although final quantities for the project have not been calculated at the time of preparation of this report, it is likely that large quantities of rock fill will not be available for backfilling. Therefore, we assume swamp backfill will consist of a select subgrade material.

5.3 FOUNDATION

5.3.1 Area 1: Township of Jocko Station 13+250 to 13+825

Throughout this area the shift in the horizontal alignment is 3.3 m to the right. Between Stations 13+250 and 13+825, Boreholes 13 to 25 were put down at the right toe of slope and Boreholes 34 to 45 inclusive were put down through the right shoulder of the existing platform. The latter series of borings indicate that the existing platform was constructed of sand fills (average 1.4 m thick), overlying the native fine fibrous peat stratum, which, on average, was 2.4 m thick. Boreholes put down beyond the right toe of slope encountered the fine fibrous peat deposit at existing grade and indicated an average thickness of 3.1 m. The peat stratum was underlain by competent cohesionless deposits of sands and silty sands with varying silt content frequently containing cobbles/gravel at depths generally greater than 6 m. The mineral soil, underlying the peat, can safely support the proposed granular fill widening material. The following three options have been considered for construction of the widening:

Option A-1

- Excavate out the existing peat on the right, under area of widening, as per OPSD 203.020, down to mineral soil and backfill with granular fill.

This option has the following disadvantages. Firstly, by the depth of peat underlying the existing platform, at the boring locations, varies from 0.7 to 3.2 m (average of 2.4 m). The measured in-situ shear strength ranged from 30 to 90 kPa. A total stress slope stability analysis was carried out for a section at Station 13+700 modelling the excavation stage. The analysis was performed using the commercially available program SLOPE/W (version 4.0). The program has the capability of either using a constant undrained shear strength value or a linear shear strength pattern within a given soil layer. The program uses the general equilibrium method of analysis to calculate the factor of safety of numerous potential trial failure surfaces and minimum factor of safety, which is defined as the ratio of the forces tending to resist failure to the driving forces tending to cause failure. Using a shear strength, reduced for anisotropy, the factor of safety is just shy of unity (ie 0.98), indicating the peat will fail if left unsupported for even a short period of time. A method of carrying out this excavation, and minimizing the risk of local embankment instability, would be to excavate in windows perpendicular to the slope, maximum open face 3 m, and backfill immediately. Traffic, passing the area of excavation, must be kept back outside the zone of influence. This zone can be defined by an imaginary line drawn up into the platform, on a 45° to the horizontal, from the bottom of the excavation face, plus 1 m. A typical example of this zone of influence is shown on Cross-Sectional Schematic Figure 14.

Secondly, differential movement will occur, continuously, between the portion of the existing road platform founded on the peat and the portion of the widening founded on mineral soil. In addition, differential settlement will develop, below the triangular section of new platform fill, due to compressions of the peat remaining under the existing platform. As can be seen from the typical section at Station 13+700, Figure 14, the thickness of new fill above the inside vertical face of embankment widening excavation is

some 500 mm, and on average 300 mm thick at the new centre line. Compression of the peat, remaining below the existing platform, has been estimated to be up to 50% of the thickness of new fill. This settlement will be greatest in the area of the right lane. Differential movement and settlements of this magnitude are considered unacceptable for a highway of this standard, considering the stated desire of the Ministry to reduce the amount of future settlement to the minimum achievable.

Option A-2

This section is a modification of Option A-1 and consists of partial excavation of the peat in order to improve the stability of the excavation face during construction. Stability analysis at Typical Section 13+700 (see Figure 15) indicates the factor of safety increases by some 22% to 1.26 if only half the peat deposit (1.5 m depth) is excavated. However, settlement of the widening will now develop due to compression of the remaining peat associated with new load resulting from the 3 m ± of widening fill.

Option B

- Full width excavation of all peat from under the existing platform and widening.

With the full width excavation of the peat subgrade, the underlying competent cohesionless granular soils will adequately support the platform. Future distortions/distress of the paved surface and possible future liability associated with differential settlement resulting from compression of the peat subgrade, will be eliminated. Maintenance cost will also be reduced and the Ministry's desire to reduce the amount of future settlement to the minimum achievable will be satisfied.

Removal of the peat can be carried out in two different ways:

1. Continuously excavate the existing right slope (one end, progressing to other end) as per OPSD 203.020, construct the widening and extend the widening further to the right to accommodate a detour; or

2. Float a temporary detour road, offset adequately from existing platform to eliminate risk of instability resulting from the excavation and commence excavation of the existing platform as per OPSD 203.010. The detour road must be constructed beyond the zone of influence. This is achievable since the right of way on this project is 60.96 m.

There are several major advantages of constructing a temporary detour road offset from the existing alignment:

- a) The impact on traffic of local slope instability occurring during embankment excavation is eliminated.
- b) Additional widening to the right, to accommodate a detour, will require peat excavation and backfilling approaching the volume required to excavate the existing platform to the left of the widening, resulting in a much higher cost for detour construction.
- c) Mass excavation of the existing platform, as per OPSD 203.010, will be much quicker, therefore more cost effective.

The temporary detour should consist of a 1 m thick platform of granular fill placed over a separating layer of Class I geotextile, reinforced with a geogrid (similar to Tensar BX1100).

In addition to the high compressibility of this peat deposit, the shear strengths are somewhat low and detour filling operations must be carried out such that embankment failures do not occur. If the peat is overloaded in the filling operations, an embankment failure is likely to occur and create a "mud wave" in front of the advancing fill displacing the majority of the peat and subsequently, increasing the volumes of fill required to construct the detour. As such, we recommend the following guidelines be adhered to during the construction of the detour:

1. Utilize a geogrid, similar to Tensar BX1100, directly overtop of the existing "undisturbed" peat surface. This geogrid should be overlapped a minimum of 2.0 m on the ends. A Class I geotextile should be placed over the grid to control loss of sand fill into the peat.

- It is imperative to ensure the natural higher shear strength of the peat surface is not deteriorated during construction.
2. Commence end dumping the lift of free draining granular fill, similar to coarse Granular
 - B. The thickness of this lift should be maintained at 1.0 m, over the entire length to prevent embankment failure.
 3. Filling operations should commence at one end such that a free draining boundary is maintained in three directions to reduce the build up of excess pore water pressure.

Option C

- Place embankment widening fill directly on existing peat grade.

Fill for widening will be placed directly over the existing ditch on the right. Calculations based on the in-situ vane testing, adjusted downward for the anisotropic characteristics of peat, indicate local bearing failure during relatively rapid placement of widening fill will occur. Therefore, a geogrid has been considered to improve stability.

Design of the fill widening reinforcement has been carried out by Tensar Corporation. Their recommendation is enclosed in Appendix D.

This will provide stability for the fill widening, however, settlement of the widening will occur. Settlement with the geogrid reinforcement will probably be of similar magnitude as that of an equivalent thickness of fill placed directly on the peat surface.

Settlement

Settlement of embankments will occur when new load (fill) is placed. The magnitude of settlement varies between different peat deposits and is generally estimated as a percentage of the thickness of new fill. In Area 1 the average thickness of peat under

the existing platform is 0.7 m less than the average thickness of peat at the toe of slope, where no fill is present. The average platform thickness throughout this area is 1.4 m. This represents a peat compression equal to 50% of the fill thickness.

Therefore, on this project, it is reasonable to estimate platform settlement as 50% of the thickness of new fill. Of this total settlement, the immediate compression of the peat will likely be in the order of 40 to 50% of the total settlement and will occur rapidly with the addition of the fill. The balance of settlement will likely occur slowly, due to secondary compression of the peat and will likely occur over a period of a decade with the majority occurring within a period of 2 to 3 years. This settlement will be further aggravated since new fill will have to be added to maintain cross-fall grade.

5.3.2 Area 2: Township of Jocko Station 20+300 to 20+450

Throughout this area the shift in horizontal alignment will be 2.25 m to the right. Boreholes 30 to 33 inclusive, put down through the existing right shoulder and Boreholes 26 to 29 inclusive, put down offset from the toe of slope, revealed similar subsurface conditions as those in Area 1. The platform fill averaged 1.8 m thick overlying an average peat thickness of 1.1 m (range 0.6 to 1.8 m). The peat thickness at the toe of slope (no surcharge) averaged 2.4 m thick (range 1.7 to 3.3 m). The soils, underlying the peat, were cohesionless deposits of silty sands with varying silt and fine sand content, which can safely support the proposed platform widening.

Typical cross-sections of Area 2 are shown in Appendix C Figure C-2. The profile grade will be retained or lowered, as is the case at Station 20+450, therefore, maintaining or decreasing the load over the existing platform area. As such, if the peat under the area of widening is excavated, as per OPS 203.020, differential settlement of the platform should be negligible and therefore, Option A-1 would be applicable.

However, lowering the platform, in the area of Station 20+450, may reduce the thickness of platform supporting the pavement structure on the existing peat subgrade. This platform thickness should not be less than 1 m. If insufficient platform remains then Option B "Full Width Excavation" will have to be undertaken in this area.

5.3.3 Area 3: Township of Jocko Station 20+750 to Township of Clarkson 10+350

Boreholes 1 to 11 inclusive were put down along the new alignment and indicate a somewhat uniform peat deposit (on average 2.1 m thick range 1.8 to 2.4 m) underlain by competent, generally compact, cohesionless soils, except at Borehole 11, where the peat was absent and shallow auger refusal was met, probably on bedrock.

Through this section, the fill height will generally be less than 3 m high, except at the two ends. All peat must be excavated as per OPSD 203.010. Where the embankment height exceeds 3 m the side slopes should be constructed at a 2:1 and the fill should be placed full platform width, from the centreline out to the sides, in lifts not exceeding a 2 m height.

Backfill with either SSM (Select Subgrade Material, as per OPSS1010) or rock fill. If SSM is used, ensure it is compacted as per OPSS Series 500.

6.0 CLOSURE

Information provided in this report is valid only at the locations drilled. Any assumptions of continuity of soil stratigraphy between boreholes, as shown on the enclosed cross-sections, is intended as an aid for design purposes only and does not constitute a statement of existing conditions for contractual or construction purposes.

Details of the investigation, the material analysis and recommendation in this report are considered to be complete. However, should any questions arise, please do not hesitate to contact the undersigned.

MERLEX ENGINEERING LTD.

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Principal



J. R. Berghamer, P. Eng.



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RECORD OF BOREHOLES

Area 1:

**Boreholes 13 to 25
and
Boreholes 34 to 45**

METRIC**RECORD OF BOREHOLE No. 13**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 13+250 8.7m RT D -1.3m; N'ly 5158453.068 E'ly 330900.929 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 17/8/00 - 17/8/00 TIME 11:10:00 AM CHECKED BY MAM

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT w_p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w_L	WATER CONTENT (%)	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			20	40	60	80	100	SHEAR STRENGTH kPa					
307.79	Ground Surface												5.6					
0.0	PEAT	1/1																
0.30	(Very Loose) SILTY SAND	1/1	1	AS											○			
	Grey fine sandy silt to yellow silt trace fine sand to grey silt trace of fine sand. Trace of gravel/cobble with depth. (Loose to Compact)	1/1	2	SS	10										○			
		1/1	3	SS	6										○			
		1/1	4	SS	13										○			
		1/1	5	SS	55										○			
304.29																		
3.50	Auger refusal (Boulder/Bedrock) End of Borehole																	
COMMENTS						+ ³ , X ³	Numbers refer to Sensitivity					WATER LEVEL RECORDS						
						O 3%	STRAIN AT FAILURE					Date (dd/mm/yy)/Time	Water Depth (m)	Cave In Level (m)				
												17/8/00; 11:15:00 AM	0.3	1.42				

METRIC

RECORD OF BOREHOLE No. 14

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic

LOCATION Sta 13+300 8.7m RT D -1.1m; N'ly 5158500.578 E'ly 330885.347 ORIGINATED BY ELS

PROJECT Highway No. 63 W.P. 167-90-00

BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test

COMPILED BY MR

CLIENT EarthTech

DATE (Started/Completed) 17/8/00 - 17/8/00

TIME 1:10:00 P

CHECKED BY MAM

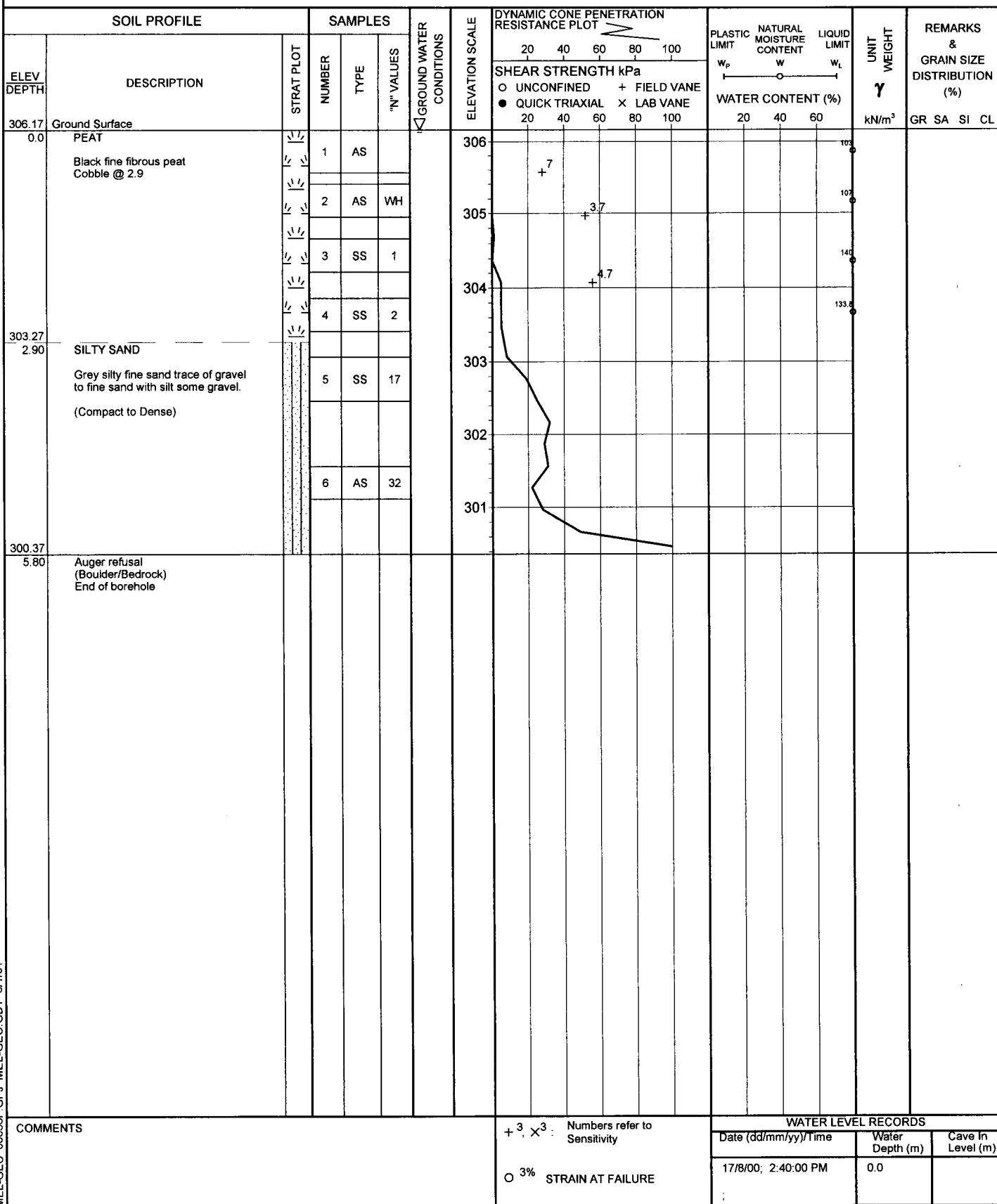
SOIL PROFILE			SAMPLES			GND. WATER COND.	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _P	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	WATER CONTENT (%)	UNIT WEIGHT kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%)	
ELEV	DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE		"N" VALUES	20	40	60	80							100
								O UNCONFINED	+ FIELD VANE	● QUICK TRIAXIAL	X LAB VANE							
306.57	Ground Surface																	
0.0	PEAT	Black fine fibrous peat 150mm black/gray organic silt seam at 1.2m (Very Loose)	1	AS			1.6									306.57		
304.27	SAND	Fine to medium sand some silt some gravel. (Wet) (Compact)	2	SS	WH			+ 3								176.6		
2.30			3	SS	WH			+ 3.7								149.8		
300.37			4	AS	11													
			5	SS	16											12 73 (15)		
			6	SS	10											13 72 (15)		
6.20		Auger refusal (Boulder/Bedrock) End of borehole																
COMMENTS												+ ³ , X ³	Numbers refer to Sensitivity	WATER LEVEL RECORDS				
												O 3%	STRAIN AT FAILURE	Date (dd/mm/yy)/Time	Water Depth (m)	Cave In Level (m)		
												17/6/00; 1:16:00 PM	0.28	2.29				

METRIC**RECORD OF BOREHOLE No. 15**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 13+350 8.7m RT D -1.4m; N'ly 5158548.088 E'ly 330869.764 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 17/8/00 - 17/8/00 TIME 2:38:00 PM CHECKED BY MAM



ENCLOSURE NO.:

METRIC**RECORD OF BOREHOLE No. 16**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 13+400 8.7m RT D -1.0m; N'ly 5158595.598 E'ly 330854.182 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 17/8/00 - 17/8/00 TIME 4:37:00 PM CHECKED BY MAM

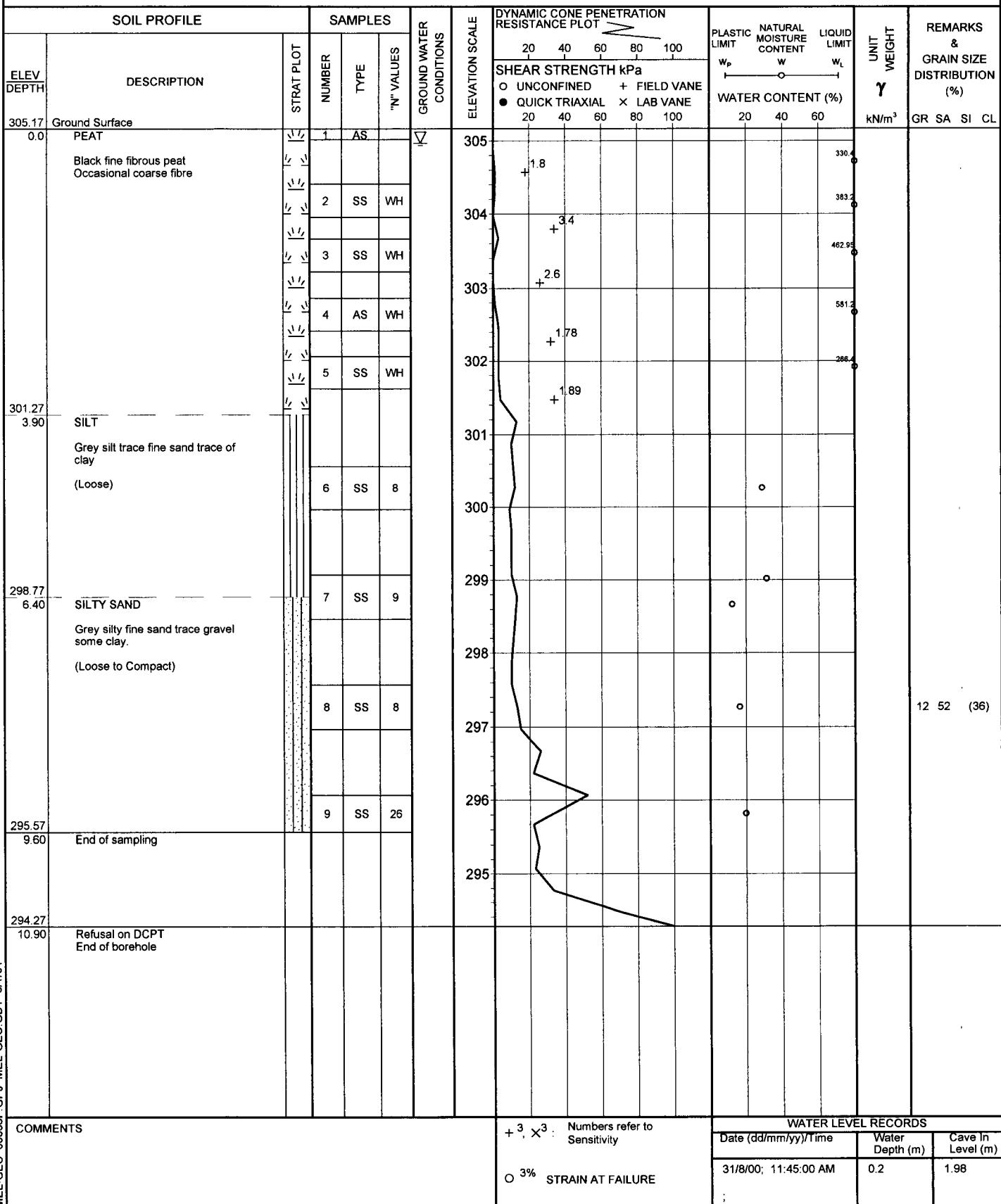
SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT w _p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w _L	WATER CONTENT (%)	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)	
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			20	40	60	80	100	SHEAR STRENGTH kPa	○ UNCONFINED	+ FIELD VANE	● QUICK TRIAXIAL	X LAB VANE		
305.44	Ground Surface																		
0.0	PEAT		1	AS									305		2.83			117.5	
	Black fine fibrous peat Grey silt seam @ 2.6m (12mm thick) (Very Loose)		2	SS	WH								304		4			121.5	
			3	AS	2								303		2.3			247.7	
			4	SS	WH								302		2.6			140.8	
			5	SS	WH								301		2.2			89.3	
301.24	SILTY SAND		6	SS	27								300						
4.20	Grey fine to medium sand trace gravel trace silt to silty fine sand trace gravel. Occasional cobble (Compact to Dense)		7	AS	31								299						
298.04													298						
297.99	Auger refusal (Boulder) End of sampling Refusal on DCPT End of Borehole																		
7.67																			
COMMENTS								+ ³	X ³	Numbers refer to Sensitivity			WATER LEVEL RECORDS						
								O	3%	STRAIN AT FAILURE			Date (dd/mm/yy)/Time	Water Depth (m)	Cave In Level (m)				

METRIC**RECORD OF BOREHOLE No. 17**

1 OF 1



REFERENCE 00/04/0036 DATUM Geodetic LOCATION Sta 13+450 8.7m RT; N'y 5158643.108 E'y 330838.600 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 21/8/00 - 21/8/00 TIME 11:20:00 AM CHECKED BY MAM

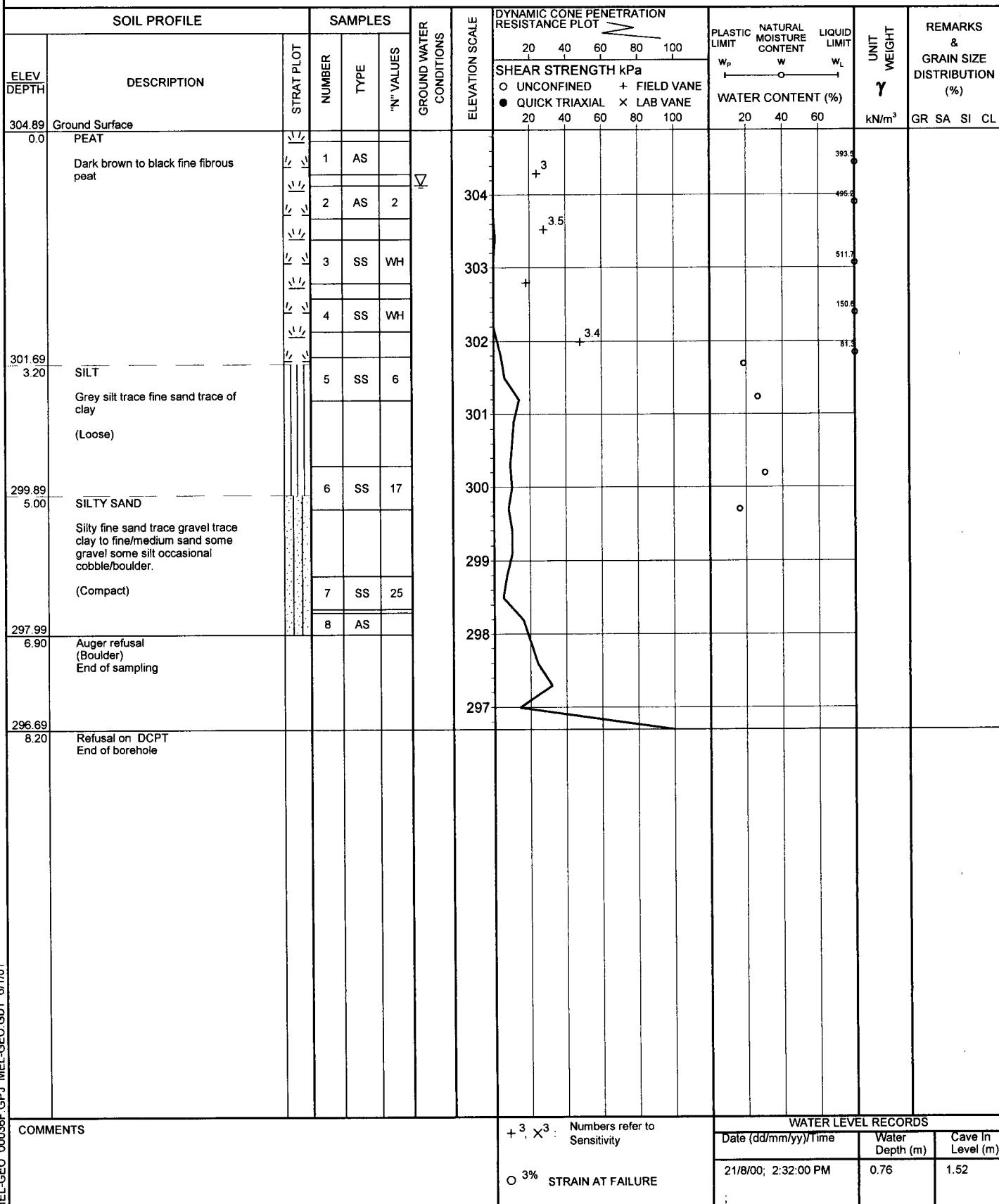


METRIC**RECORD OF BOREHOLE No. 18**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 13+500 8.7m RT D -850, N'ly 5158690.618 E'ly 330823.018 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 21/8/00 - 21/8/00 TIME 2:23:00 PM CHECKED BY MAM



METRIC**RECORD OF BOREHOLE No. 19**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 13+550 8.7m RT D -700; N'ly 5158738.128 E'ly 330807.435 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 21/8/00 - 21/8/00 TIME 4:00:00 PM CHECKED BY MAM

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _P	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	WATER CONTENT (%)	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)	
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			20	40	60	80	100	SHEAR STRENGTH kPa	20	40	60	80	100	
304.52	Ground Surface																		
0.0	PEAT		1	AS															
	Black fine fibrous peat		2	AS	WH														
			3	SS	WH														
			4	SS	1														
301.17	SAND		5	SS	6														
3.35	Grey fine to medium sand some silt (Loose)		6	SS	25														
299.92	SILTY SAND		7	SS	37														
4.60	Silty fine sand trace gravel trace clay occasional cobble/boulder (Till structure evident) (Compact to Dense)																		
297.52																			
297.00	Auger refusal (Boulder)																		
7.20	End of sampling Refusal on DCPT End of borehole																		
COMMENTS								+ ³	X ³	Numbers refer to Sensitivity					WATER LEVEL RECORDS				
								O	3%	STRAIN AT FAILURE					Date (dd/mm/yy)/Time	Water Depth (m)	Cave In Level (m)		
															21/8/00; 4:05:00 PM	0.86	1.83		
															31/8/00; 11:35:00 AM	0.3	1.32		

ENCLOSURE NO.:

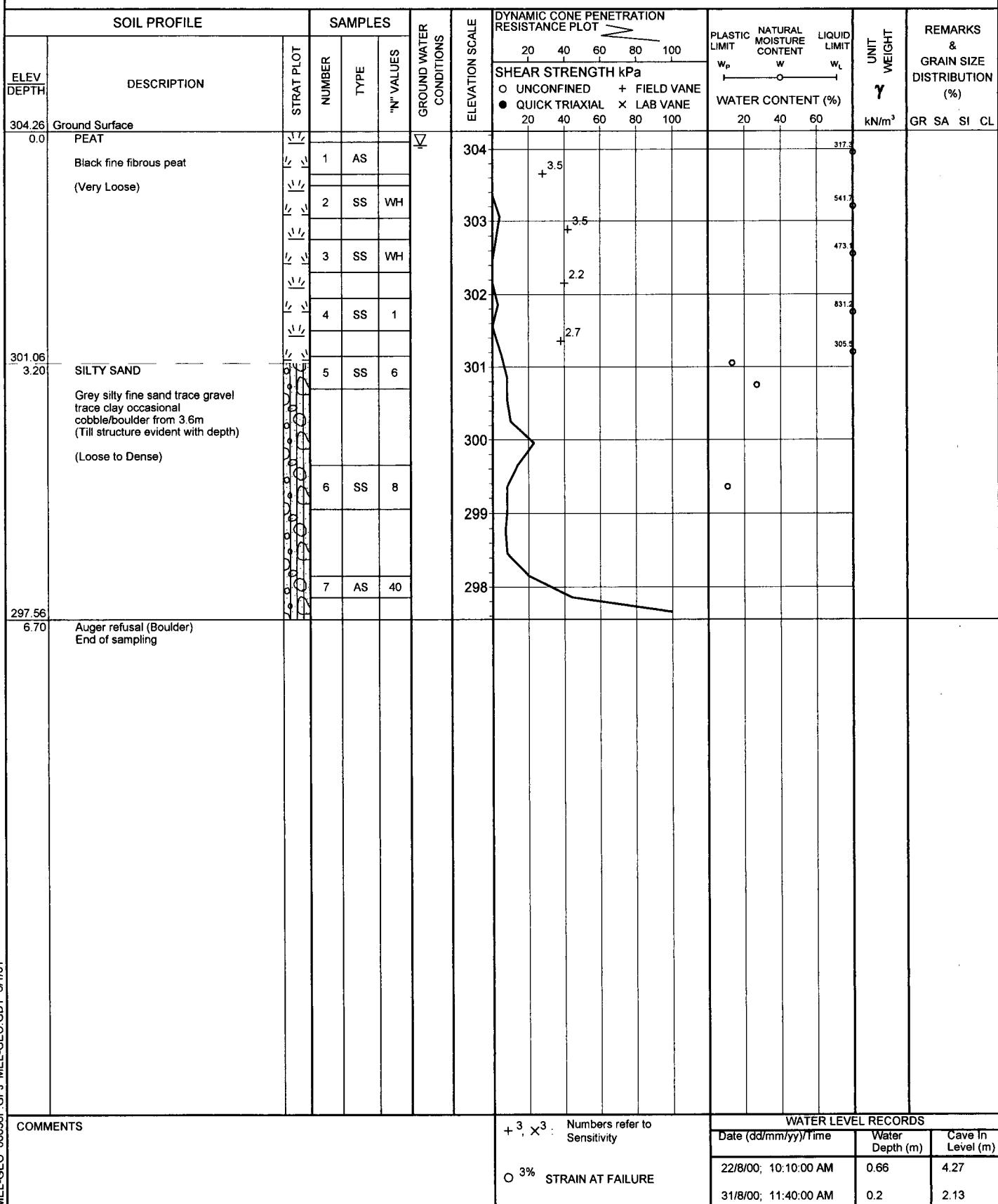
METRIC

RECORD OF BOREHOLE No. 20

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 13+600 8.7m RT; N'ly 5158785.637 E'ly 330791.853 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 21/8/00 - 22/8/00 TIME 10:05:00 AM CHECKED BY MAM



MEL-GEO 00036F.GPJ MEL-GEO.GDT 6/1/01

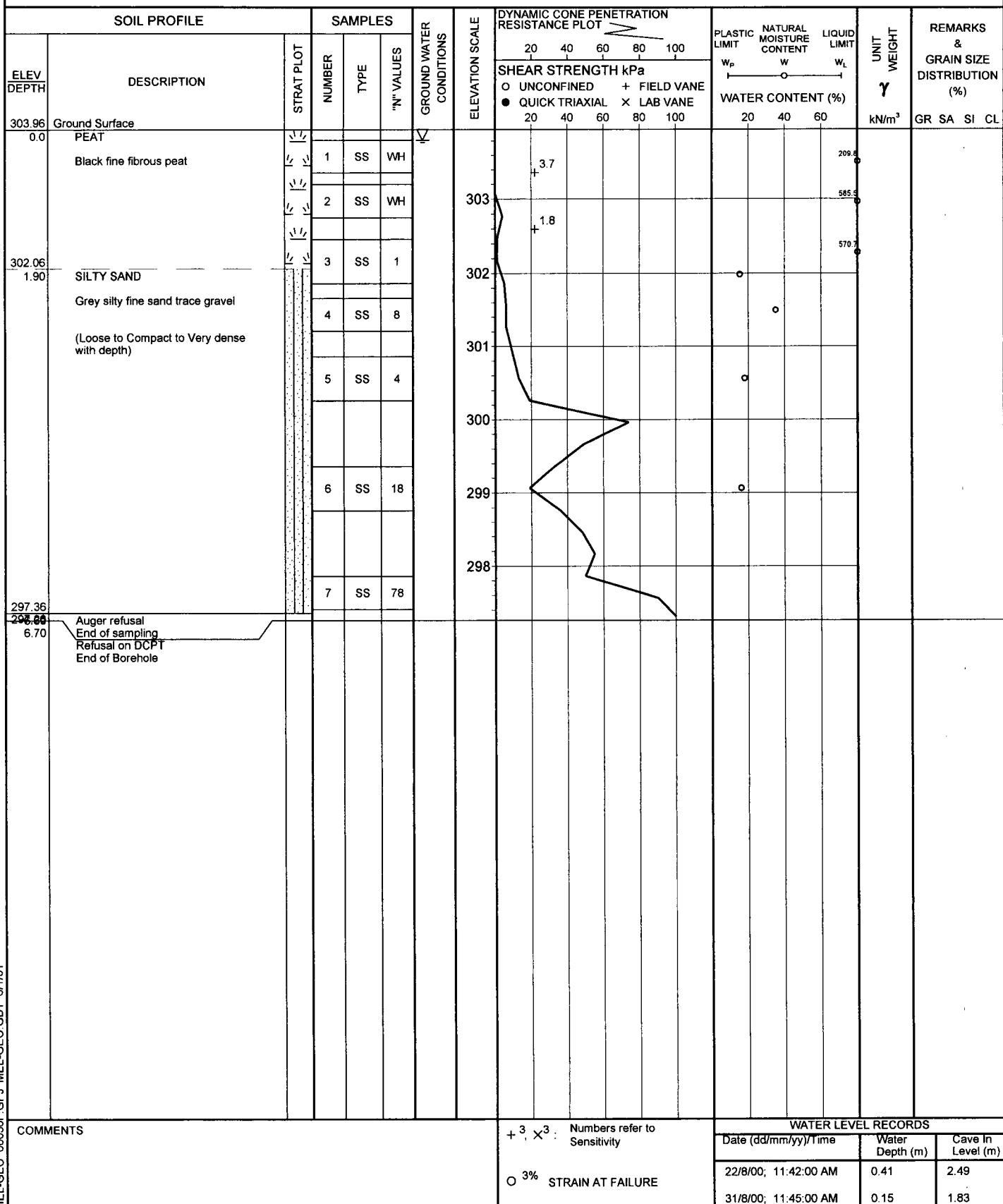
METRIC

RECORD OF BOREHOLE No. 21

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 13+650 8.7m RT D-700; N'y 5158833.147 E'y 330776.271 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 22/8/00 - 22/8/00 TIME 11:40:00 AM CHECKED BY MAM

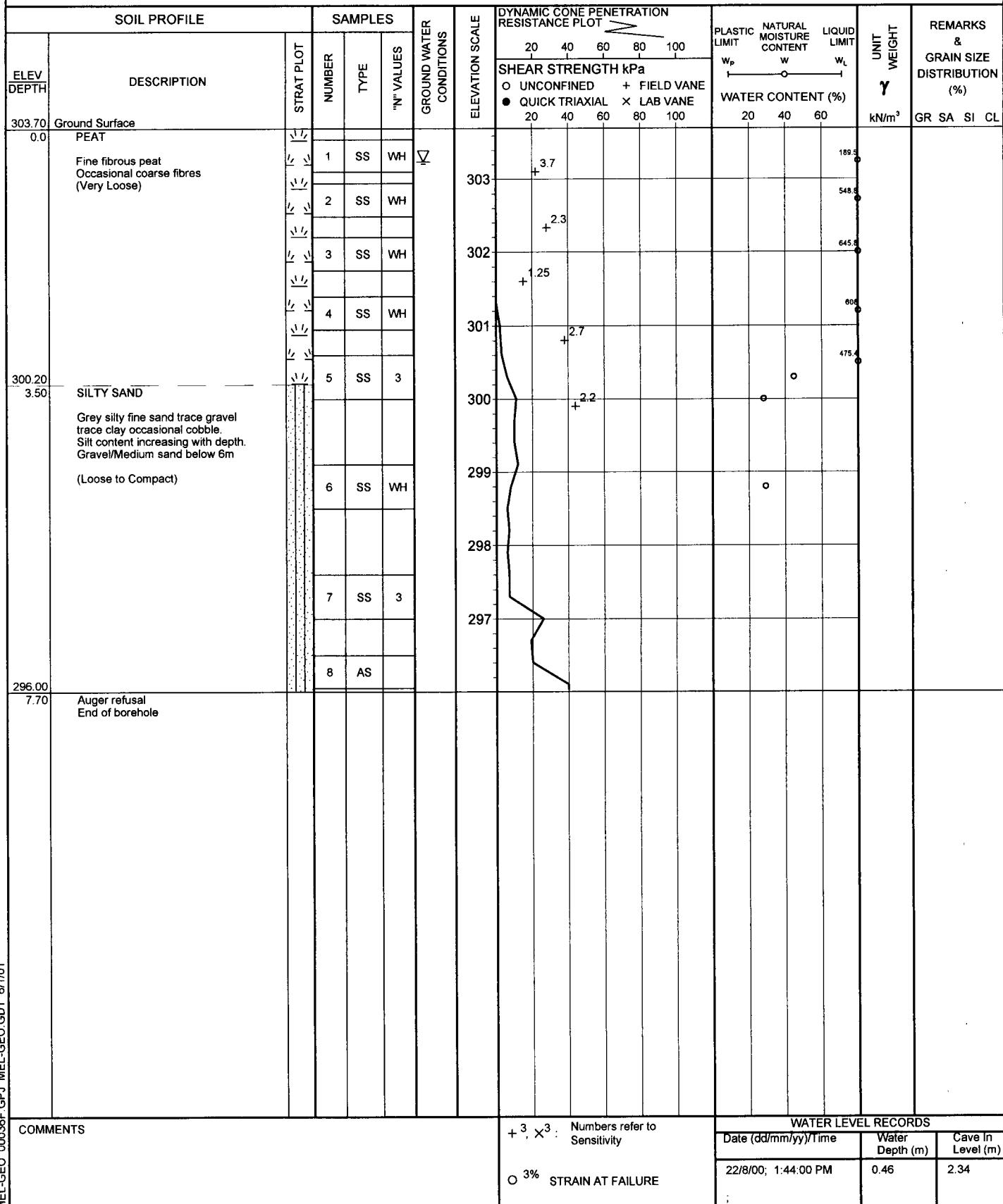


RECORD OF BOREHOLE No. 22

1 OF 1

**METRIC**

REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 13+700 8.7m RT D -650; N'ly 5158880.657 E'ly 330760.688 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 22/8/00 - 22/8/00 TIME 1:37:00 PM CHECKED BY MAM



ENCLOSURE NO.:

METRIC**RECORD OF BOREHOLE No. 23**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 13+750 8.7m RT D -500, N'ly 5158928.167 E'ly 330745.106 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 22/8/00 - 22/8/00 TIME 2:45:00 PM CHECKED BY MAM

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT w_p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w_L	WATER CONTENT (%)	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)	
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			20	40	60	80	100	SHEAR STRENGTH kPa	○ UNCONFINED	+ FIELD VANE	● QUICK TRIAXIAL	X LAB VANE		
303.54	Ground Surface																		
0.0	PEAT																		
	Black fine fibrous peat		1	SS	WH								303	3.0				290.0	
			2	SS	WH								302	2.4				754.6	
			3	SS	WH								301	2				625.8	
			4	SS	9								300					○	
			5	SS	7								299						
301.14	SILTY SAND																		
2.40	Fine to medium sand some silt to silty fine sand Occasional cobble/gravel with increasing depth (Loose to Compact)																		
299.24																			
4.30	Auger refusal End of sampling																		
298.34																			
5.20	Refusal on DCPT (30blows/0mm) End of Borehole																		
COMMENTS												+ 3, X 3	Numbers refer to Sensitivity	WATER LEVEL RECORDS					
												O 3%	STRAIN AT FAILURE	Date (dd/mm/yy)/Time	Water Depth (m)	Cave In Level (m)			
														22/8/00; 2:48:00 PM	0.91	2.59			

ENCLOSURE NO.:

METRIC**RECORD OF BOREHOLE No. 24**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 13+800 8.7m RT D -700; N'ly 5158976.667 E'ly 330729.524 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 22/8/00 - 22/8/00 TIME 3:30:00 PM CHECKED BY MAM

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT w_p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w_L	WATER CONTENT (%)	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			20	40	60	80	100	SHEAR STRENGTH kPa	○ UNCONFINED + FIELD VANE	● QUICK TRIAXIAL X LAB VANE	20	40	60
304.27	Ground Surface																	
304.00 0.15	TOPSOIL SILT		1	SS	4		304											
303.36	Yellow silt trace fine sand																	
300.97 1.10	(Loose) SAND		2	SS	9													
	Fine to medium sand some silt trace gravel (Loose) End of borehole																	
	AP#24 13+792 8.7m RT D -1.0 0 - 305 Silty organics 305 - 1.37 Silty fine sand Wet @ 0.46m																	
COMMENTS								+ ³ , X ³	Numbers refer to Sensitivity			WATER LEVEL RECORDS						
								O ^{3%}	STRAIN AT FAILURE			Date (dd/mm/yy)/Time	Water Depth (m)	Cave In Level (m)				

MEL-GEO 00036F.GPJ MEL-GEO.GDT 6/1/01

ENCLOSURE NO.:

METRIC**RECORD OF BOREHOLE No. 25**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 13+825 8.7m RT; N'ly 5158999.432 E'ly 330721.733 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 22/8/00 - 22/8/00 TIME CHECKED BY MAM

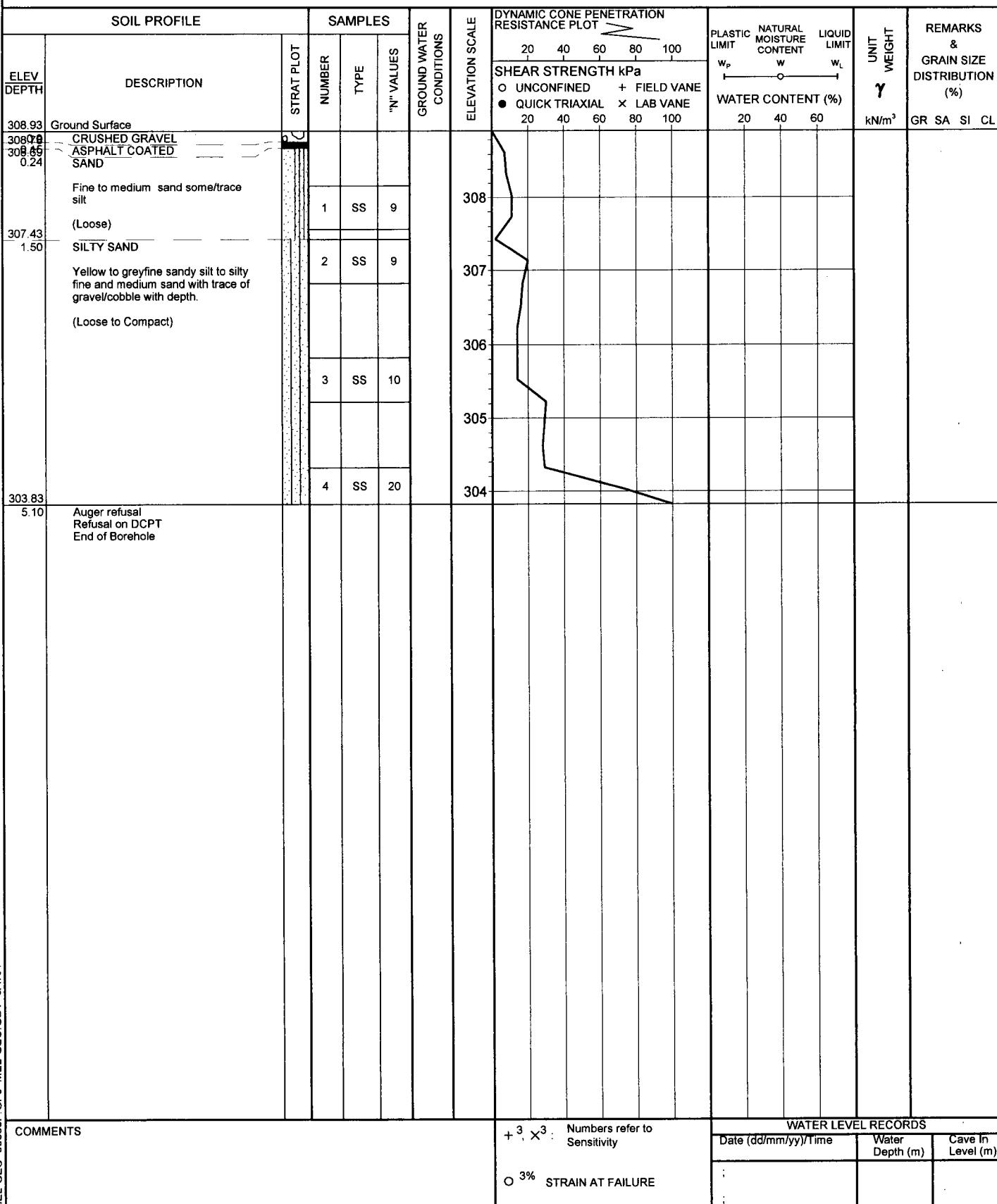
SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT w_p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w_L	WATER CONTENT (%)	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			20 40 60 80 100	20 40 60 80 100	SHEAR STRENGTH kPa	○ UNCONFINED + FIELD VANE	● QUICK TRIAXIAL X LAB VANE	20 40 60 80 100	20 40 60	kN/m³	GR SA SI CL		
307.00	Ground Surface																	
306.88 0.15	TOPSOIL SILTY SAND	X /	1	SS	6													
305.80 1.20	Silty fine sand trace gravel to fine/medium sand trace gravel trace silt Occasional cobble (Loose) Auger refusal End of borehole	X /	2	AS			306											
COMMENTS						+ 3 X 3 : Numbers refer to Sensitivity						O 3% STRAIN AT FAILURE	WATER LEVEL RECORDS					
													Date (dd/mm/yy)/Time	Water Depth (m)	Cave In Level (m)			

METRIC**RECORD OF BOREHOLE No. 34**

1 OF 1



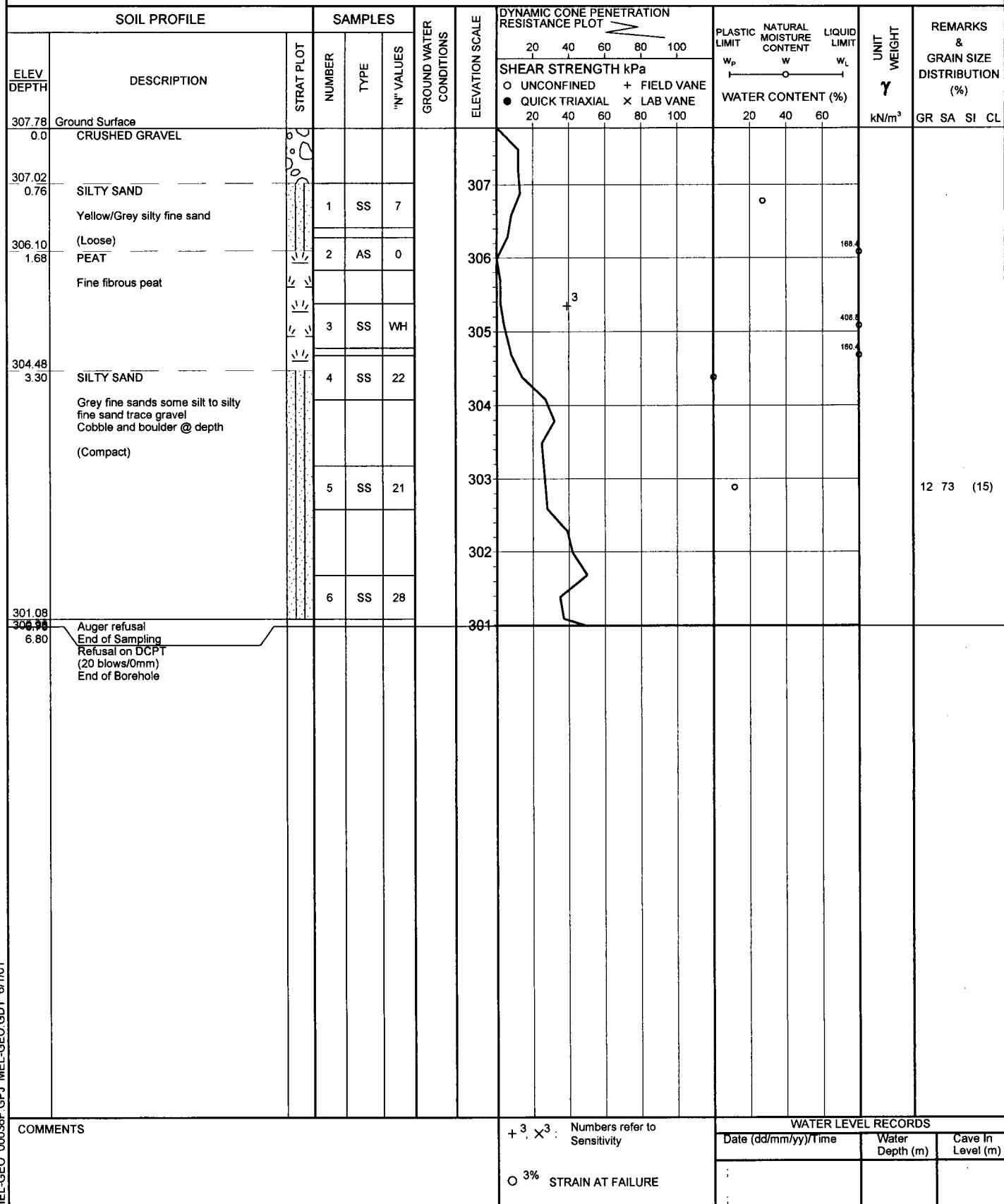
REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 13+250 0.9m RT; N'ly 5158450.637 E'ly 330893.517 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 28/8/00 - 28/8/00 TIME 1:00:00 PM CHECKED BY MAM



ENCLOSURE NO.:

METRIC**RECORD OF BOREHOLE No. 35**

1 OF 1

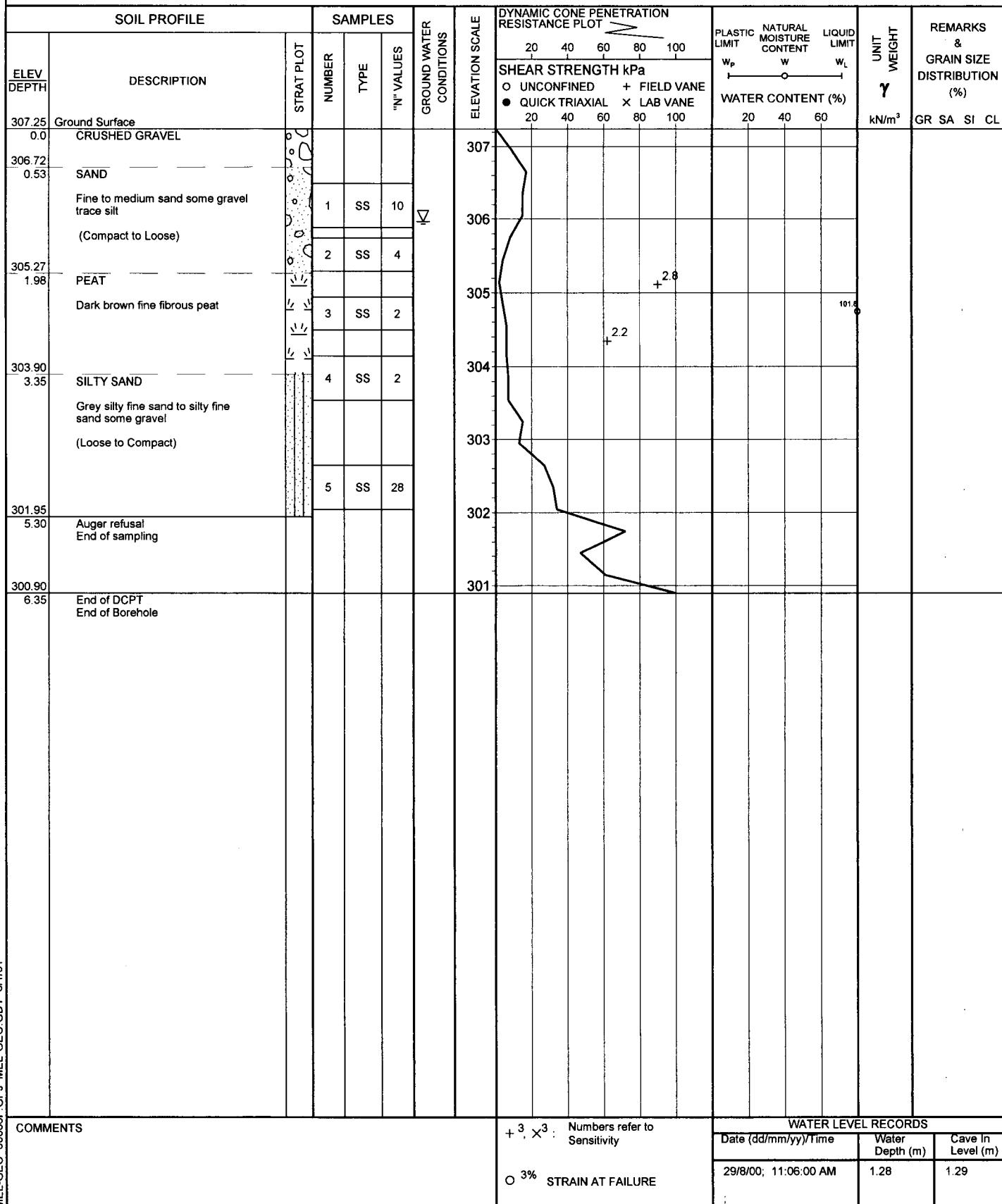
PEREFERENCE 00/04/0036 DATUM GeodeticLOCATION Sta 13+300 0.9m RT; N'ly 5158498.147 E'ly 330877.935ORIGINATED BY ELSPROJECT Highway No. 63 W.P. 167-90-00BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration TestCOMPILED BY MRCLIENT EarthTechDATE (Started/Completed) 28/8/00 - 28/8/00TIME 3:45:00 PMCHECKED BY MAM

METRIC**RECORD OF BOREHOLE No. 36**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 13+350 0.9m RT; N'ly 5158545.657 E'ly 330862.353 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 29/8/00 - 29/8/00 TIME 11:00:00 AM CHECKED BY MAM



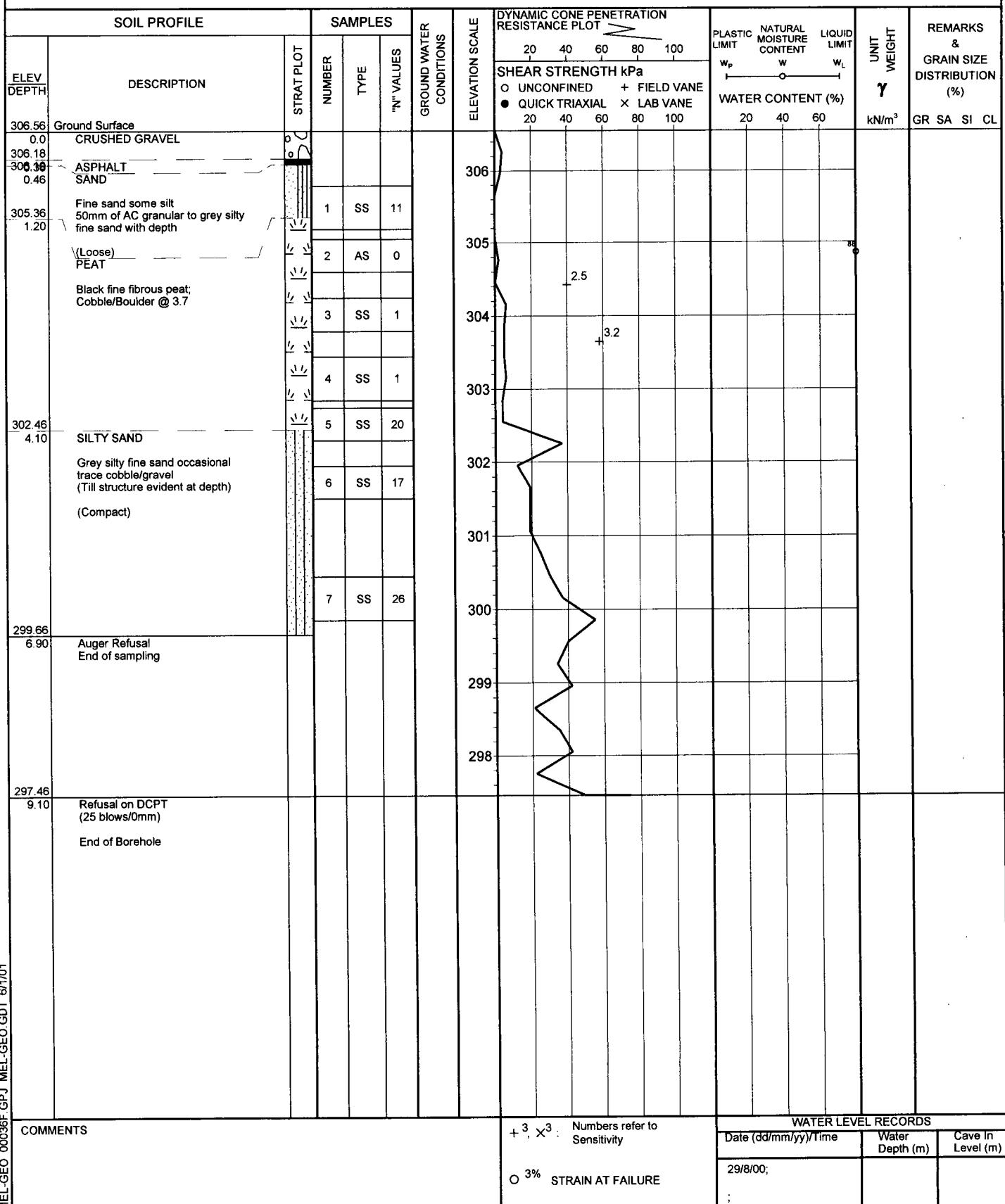
ENCLOSURE NO.:

METRIC**RECORD OF BOREHOLE No. 37**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 13+400 0.9m RT; N'ly 5158593.167 E'ly 330846.771 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 29/8/00 - 29/8/00 TIME 2:00:00 PM CHECKED BY MAM

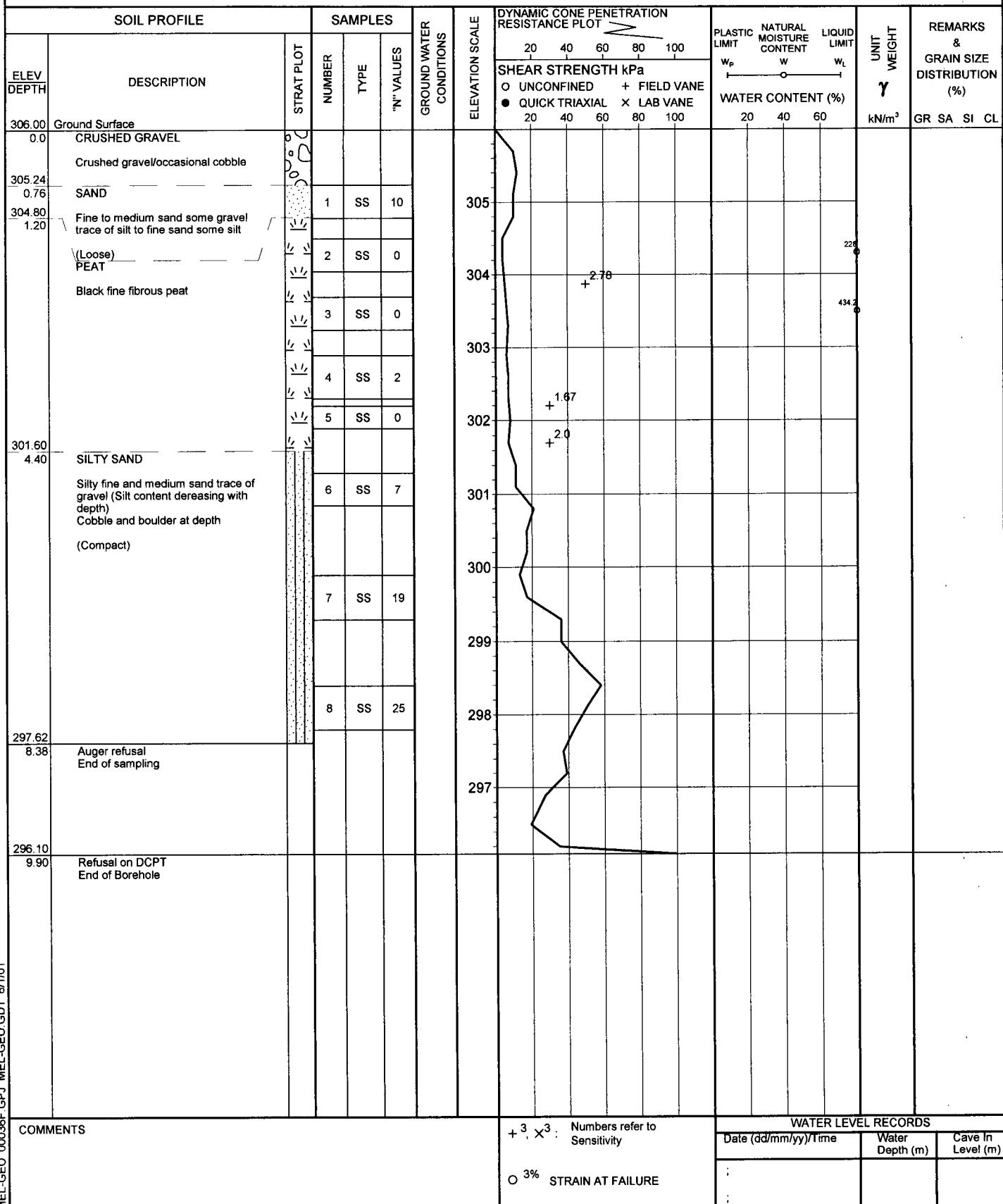


METRIC**RECORD OF BOREHOLE No. 38**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 13+450 0.9m RT; N'ly 5158640.677 E'ly 330831.188 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 29/8/00 - 29/8/00 TIME 4:40:00 PM CHECKED BY MAM



ENCLOSURE NO.:

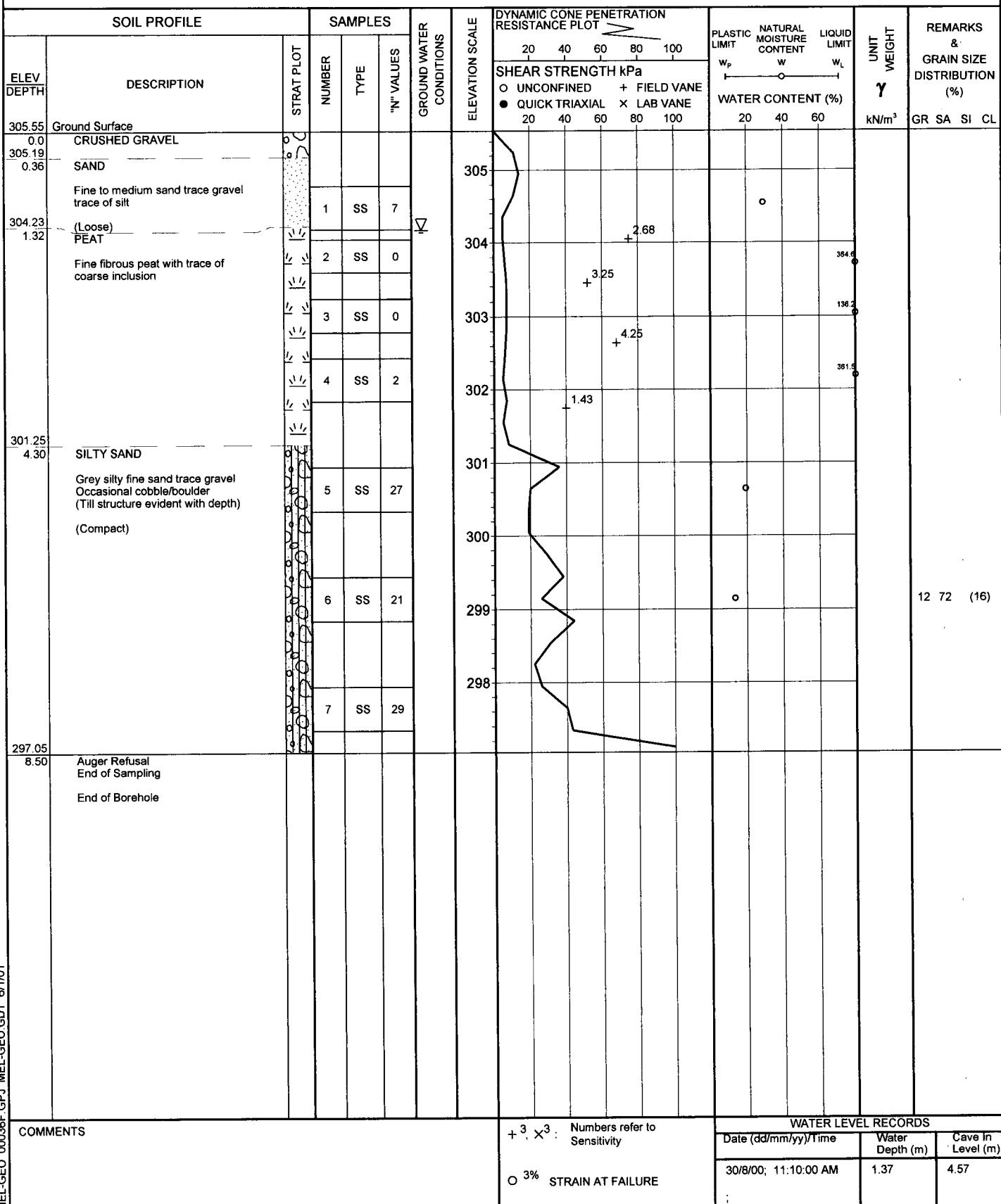
RECORD OF BOREHOLE No. 39

1 OF 1



METRIC

REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 13+500 0.9m RT; N'ly 5158688.187 E'ly 330815.606 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 30/8/00 - 30/8/00 TIME 11:16:00 AM CHECKED BY MAM



ENCLOSURE NO.:

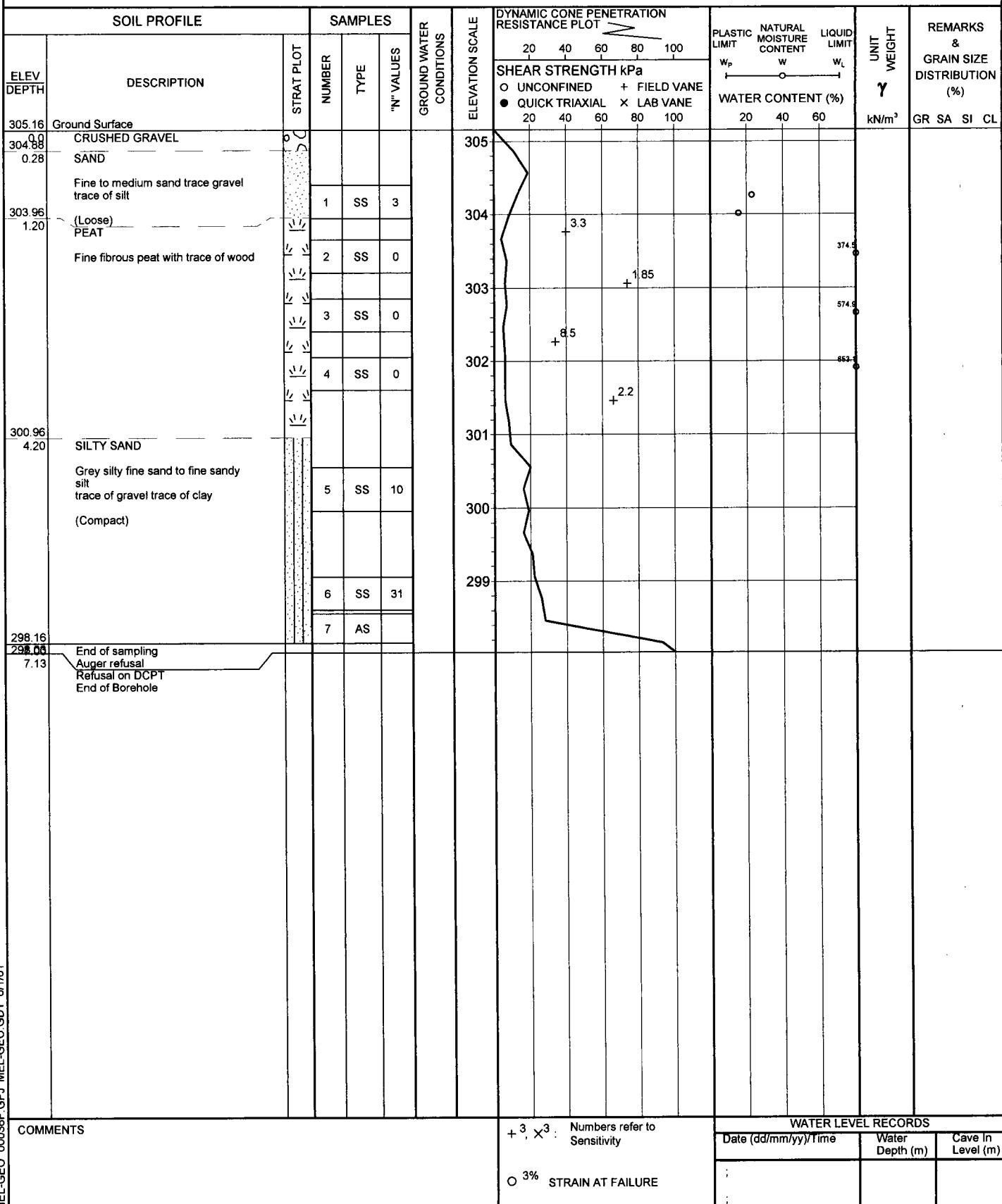
RECORD OF BOREHOLE No. 40

1 OF 1



METRIC

REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 13+550 0.9m RT; N'ly 5158735.697 E'ly 330800.024 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 30/8/00 - 30/8/00 TIME 1:20:00 PM CHECKED BY MAM



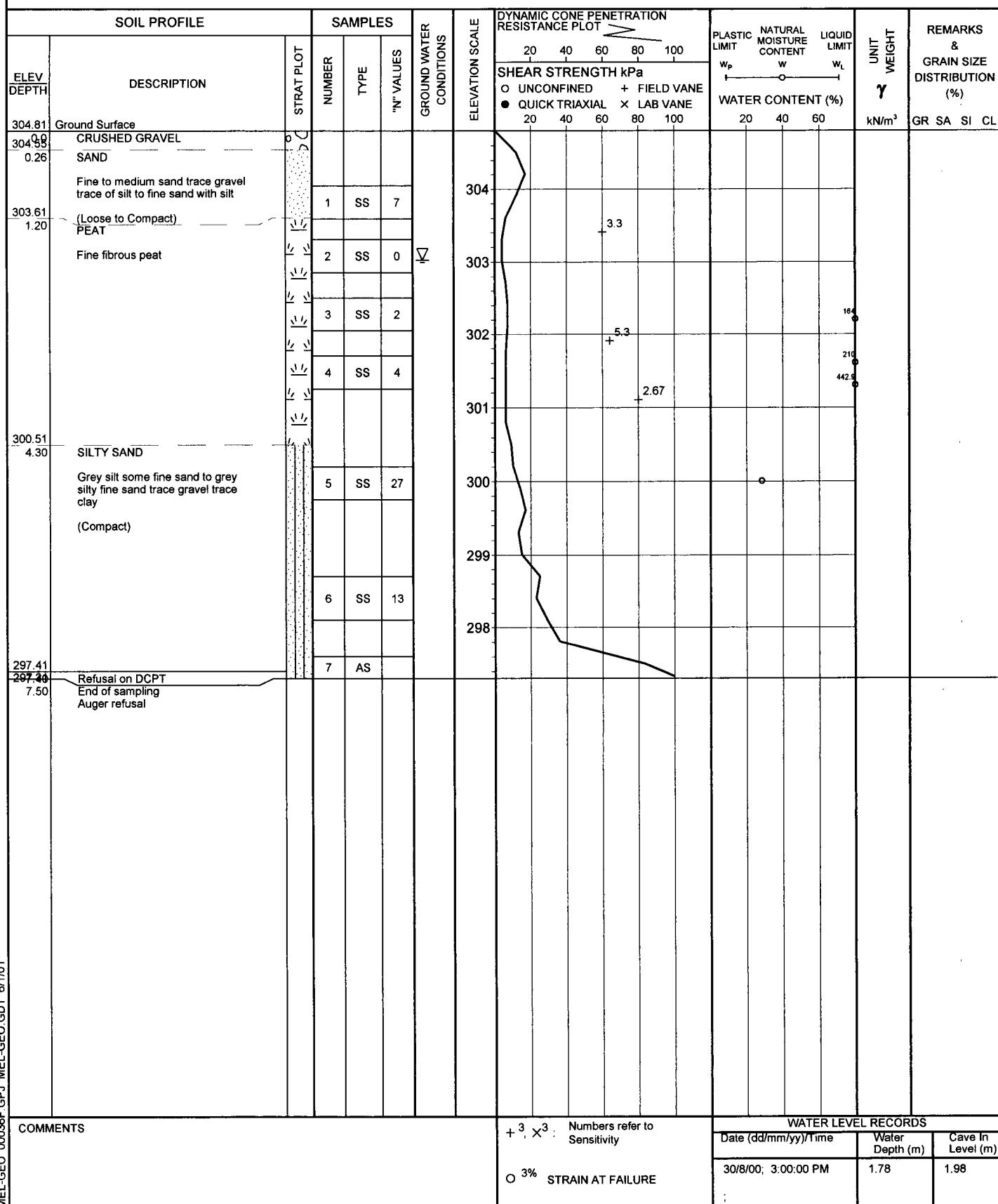
ENCLOSURE NO.:

METRIC**RECORD OF BOREHOLE No. 41**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 13+600 0.9m RT; N'ly 5158783.207 E'ly 330784.441 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 30/8/00 - 30/8/00 TIME 2:50:00 PM CHECKED BY MAM



ENCLOSURE NO.:

METRIC**RECORD OF BOREHOLE No. 42**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 13+650 0.9m RT; N'ly 5158830.717 E'ly 330768.859 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 30/8/00 - 30/8/00 TIME 5:00:00 PM CHECKED BY MAM

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT w_p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w_l	WATER CONTENT (%)	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			20	40	60	80	100						
304.60	Ground Surface																	
304.38	CRUSHED GRAVEL	0																
0.25	SAND	0																
	Fine to medium sand trace gravel trace of silt to fine sand with silt																	
303.40	(Loose) PEAT	1/1																
1.20	Fine fibrous peat	1/1																
302.50	SILTY SAND	1/1																
2.10	Grey silty fine sand trace gravel, occasional cobble/boulder trace of clay (Till structure evident with depth) (Compact to Very Dense)	1/1																
298.80																		
5.80	End of sampling Auger refusal (Boulder)																	
298.20																		
6.40	Refusal on DCPT End of Borehole																	
COMMENTS						+ ³	X ³	Numbers refer to Sensitivity					WATER LEVEL RECORDS					
						O	3%	STRAIN AT FAILURE					Date (dd/mm/yy)/Time	Water Depth (m)	Cave In Level (m)			
													30/8/00; 5:10:00 PM	1.27	1.32			

MEL-GEO 00036F GPJ MEL-GEO GDT 6/1/01

METRIC

RECORD OF BOREHOLE No. 43

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic

LOCATION Sta 13+700 0.9m RT; N'ly 5158878.226 E'ly 330753.277

— ORIGINATED BY ELS

PROJECT Highway No. 63 W.P. 167-90-00

BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test

COMPILED BY

CLIENT EarthTech

DATE (Started/Completed) 31/8/00 - 31/8/00

TIME 11:30:00 AM

CHECKED BY MAM

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT w_p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w_L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL						
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES		ELEVATION SCALE	20	40	60	80						100	SHEAR STRENGTH KPa	○ UNCONFINED ● QUICK TRIAXIAL	+ FIELD VANE X LAB VANE	WATER CONTENT (%)	20
304.21	Ground Surface					304																
303.91	0.0 CRUSHED GRAVEL	○				303																
0.30	SAND	○				302																
303.11	Fine to medium sand trace gravel trace of silt to fine sand with silt (Loose to Compact)	○	1	SS	6	301																
1.10	PEAT	○	2	SS	0	300																
	Fine fibrous peat	○	3	SS	3	299																
		○	4	SS	0	298																
300.41	3.80 SILTY SAND	○	5	SS	4	297																
	Fine to medium sand trace of gravel Grey fine sandy silt to silt with fine sand to fine sandy silt Sand content increasing with depth as well as cobble and gravel (Loose to Compact/Dense)	○	6	SS	2	296																
		○	7	SS	10																	
295.71	8.50 End of sampling 295.31 Auger refusal																					
8.90	Refusal on DCPT (25 blows/0mm) End of Borehole																					
COMMENTS												$+^3 \times^3$	Numbers refer to Sensitivity	WATER LEVEL RECORDS								
												$\circ 3\%$	STRAIN AT FAILURE	Date (dd/mm/yy)/Time	Water Depth (m)	Cave In Level (m)						
													31/8/00; 11:40:00 AM	1.68								

METRIC**RECORD OF BOREHOLE No. 44**

1 OF 1



REFERENCE 00/04/00036

DATUM Geodetic

LOCATION Sta 13+750 0.9m RT; Nly 5158925.736 Ely 330737.695

ORIGINATED BY ELS

PROJECT Highway No. 63 W.P. 167-90-00

BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test

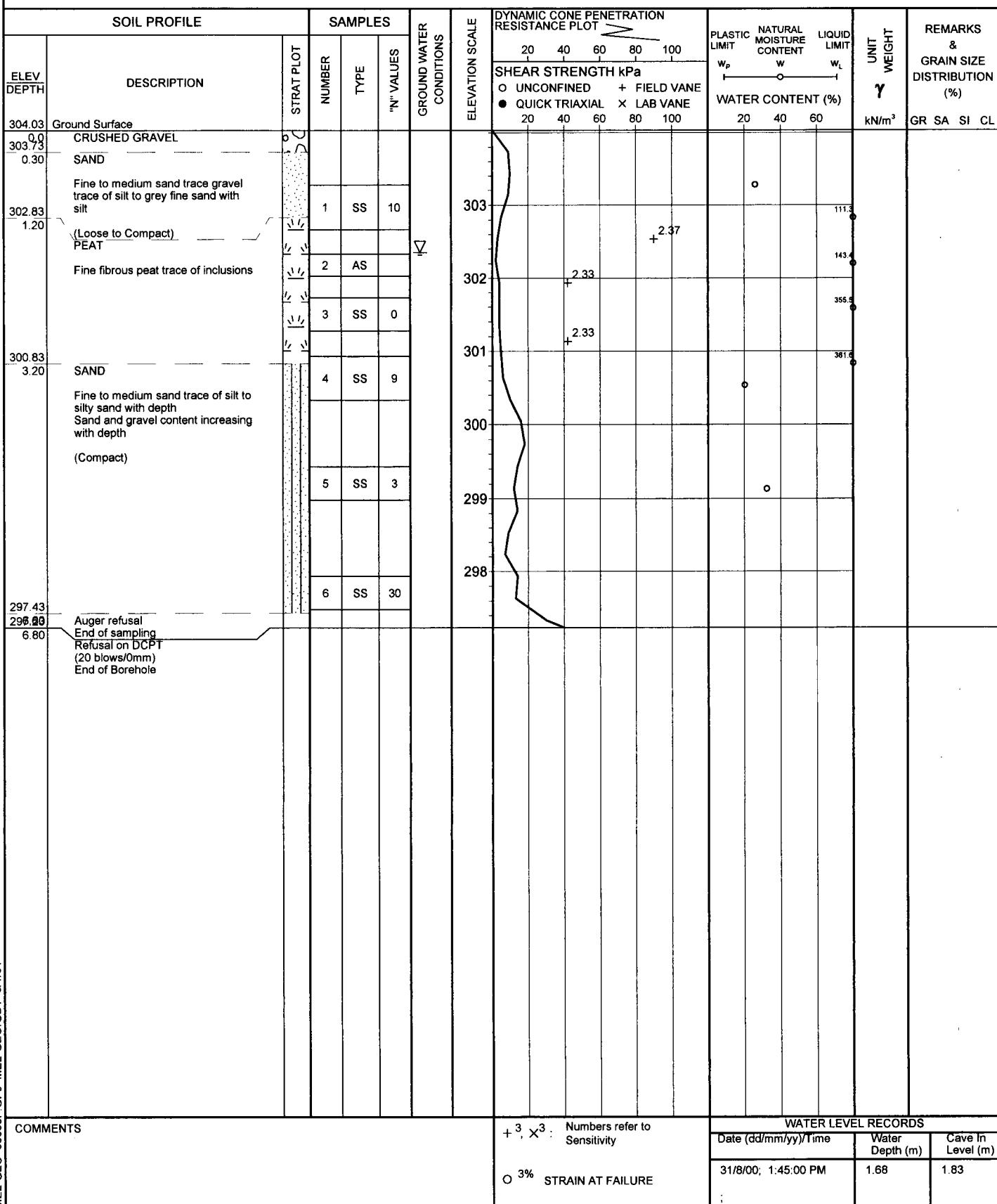
COMPILED BY MR

CLIENT EarthTech

DATE (Started/Completed) 31/8/00 - 31/8/00

TIME 1:40:00 PM

CHECKED BY MAM



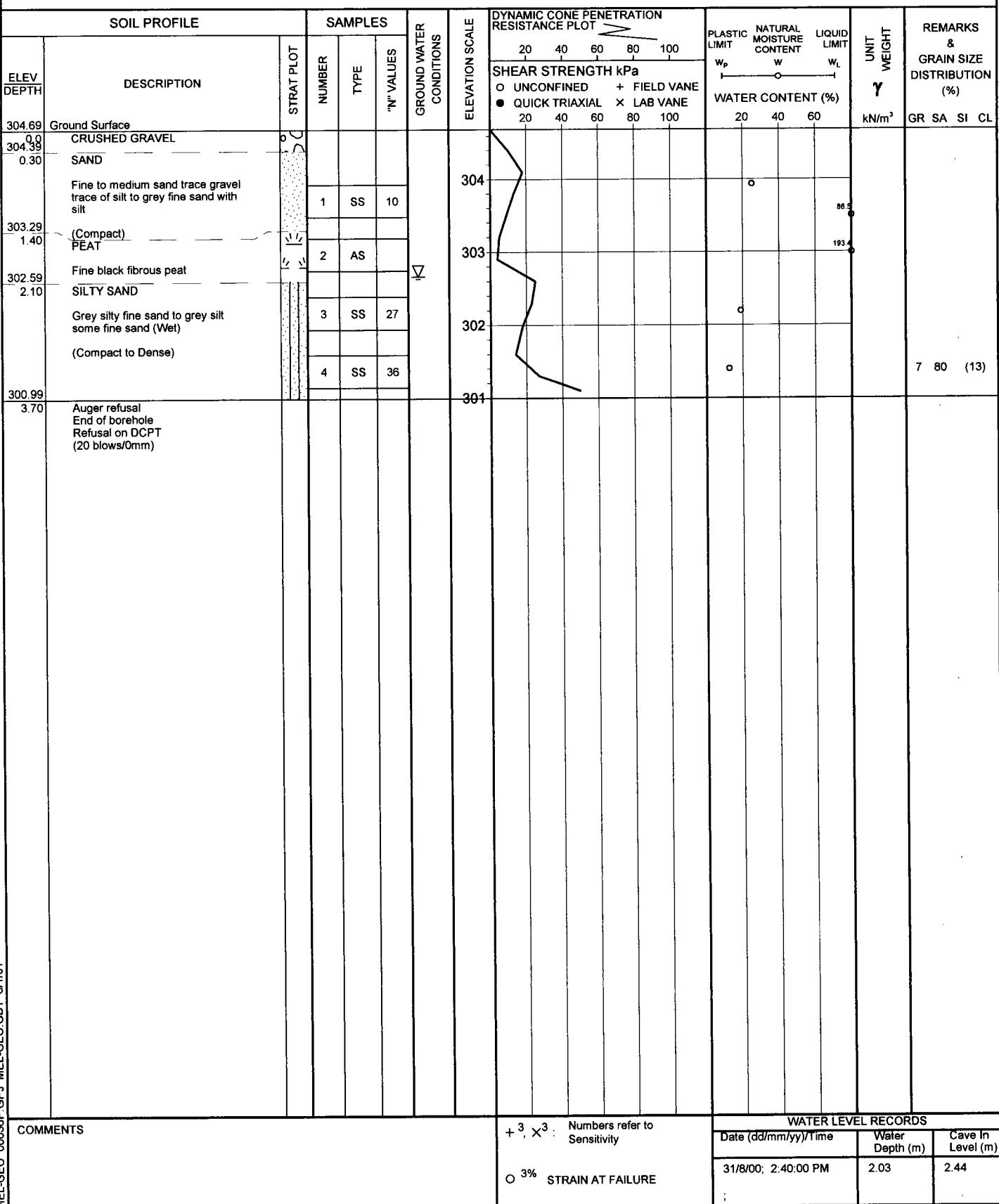
ENCLOSURE NO.:

METRIC**RECORD OF BOREHOLE No. 45**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 13+800 0.9m RT; N'ly 5158973.246 E'ly 330722.112 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 31/8/00 - 31/8/00 TIME 2:40:00 PM CHECKED BY MAM



RECORD OF BOREHOLES

Area 2:

Boreholes 26 to 33

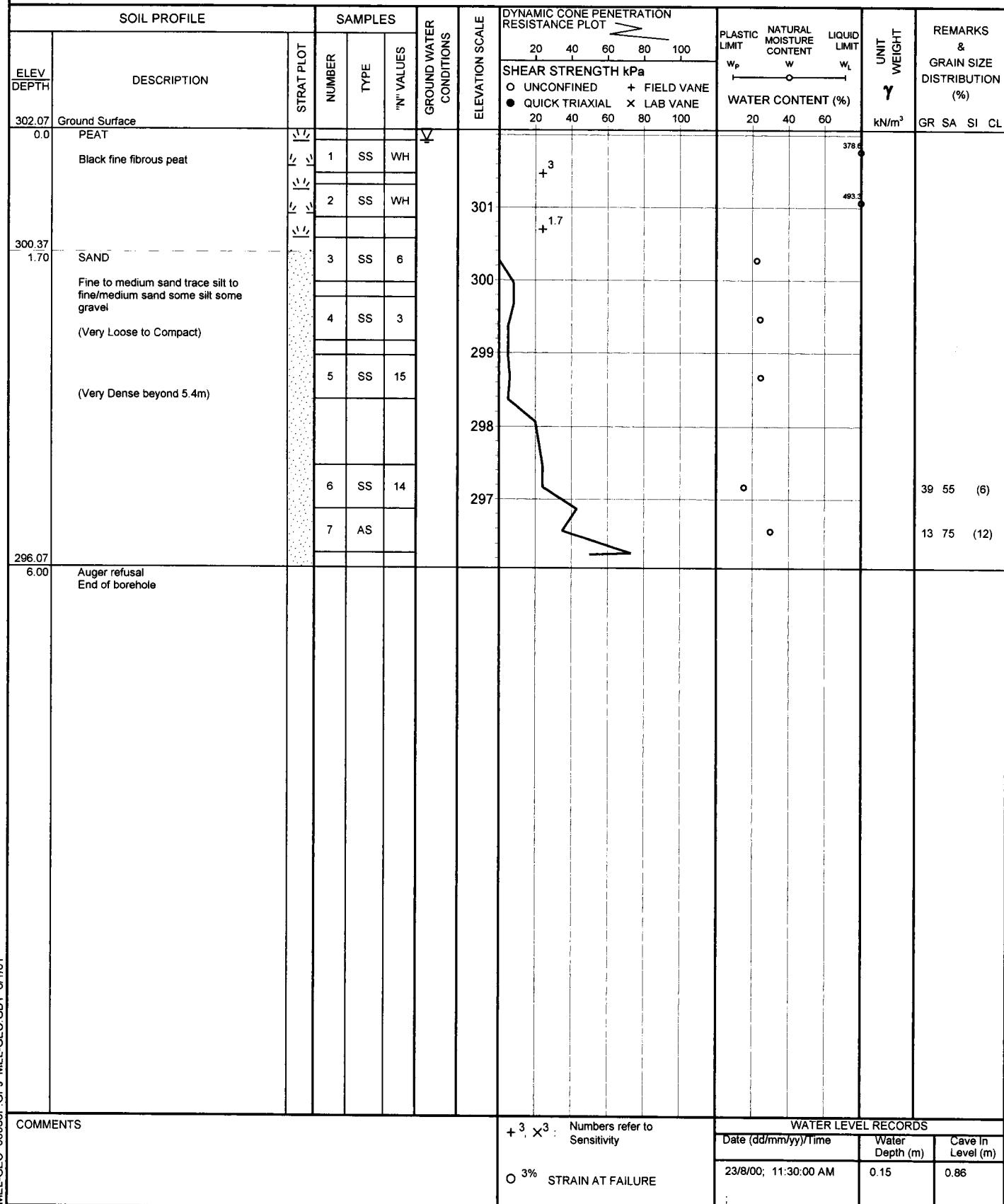
METRIC

RECORD OF BOREHOLE No. 26

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 20+400 8.8m RT D -1.2; Nly 5164750.121 Ely 331231.671 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 22/8/00 - 23/8/00 TIME 11:26:00 AM CHECKED BY MAM



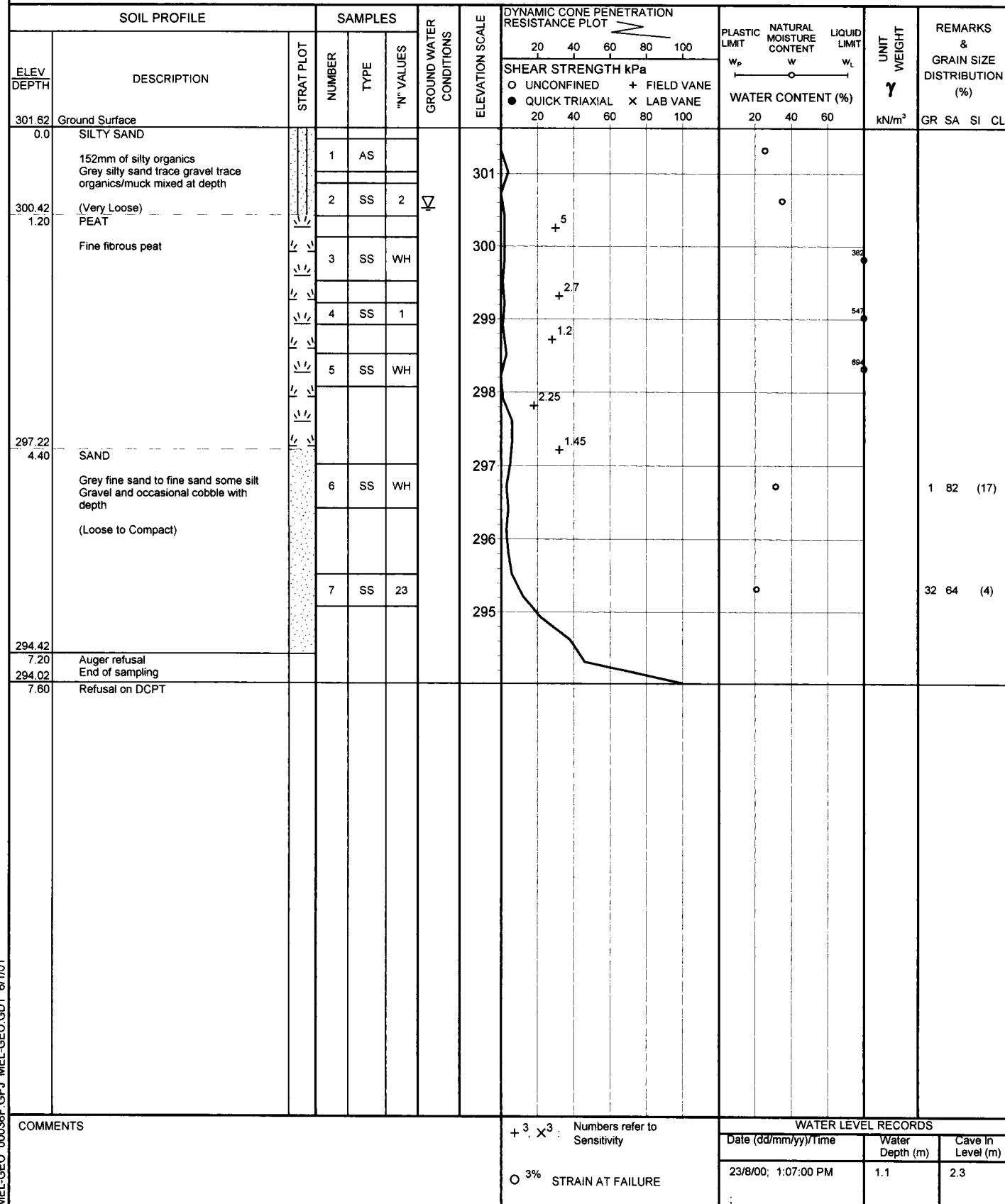
ENCLOSURE NO.:

METRIC**RECORD OF BOREHOLE No. 27**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 20+350 8.8m RT D -1.3, Nly 5164721.345 Ely 331190.782 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 23/8/00 - 23/8/00 TIME 1:03:00 PM CHECKED BY MAM

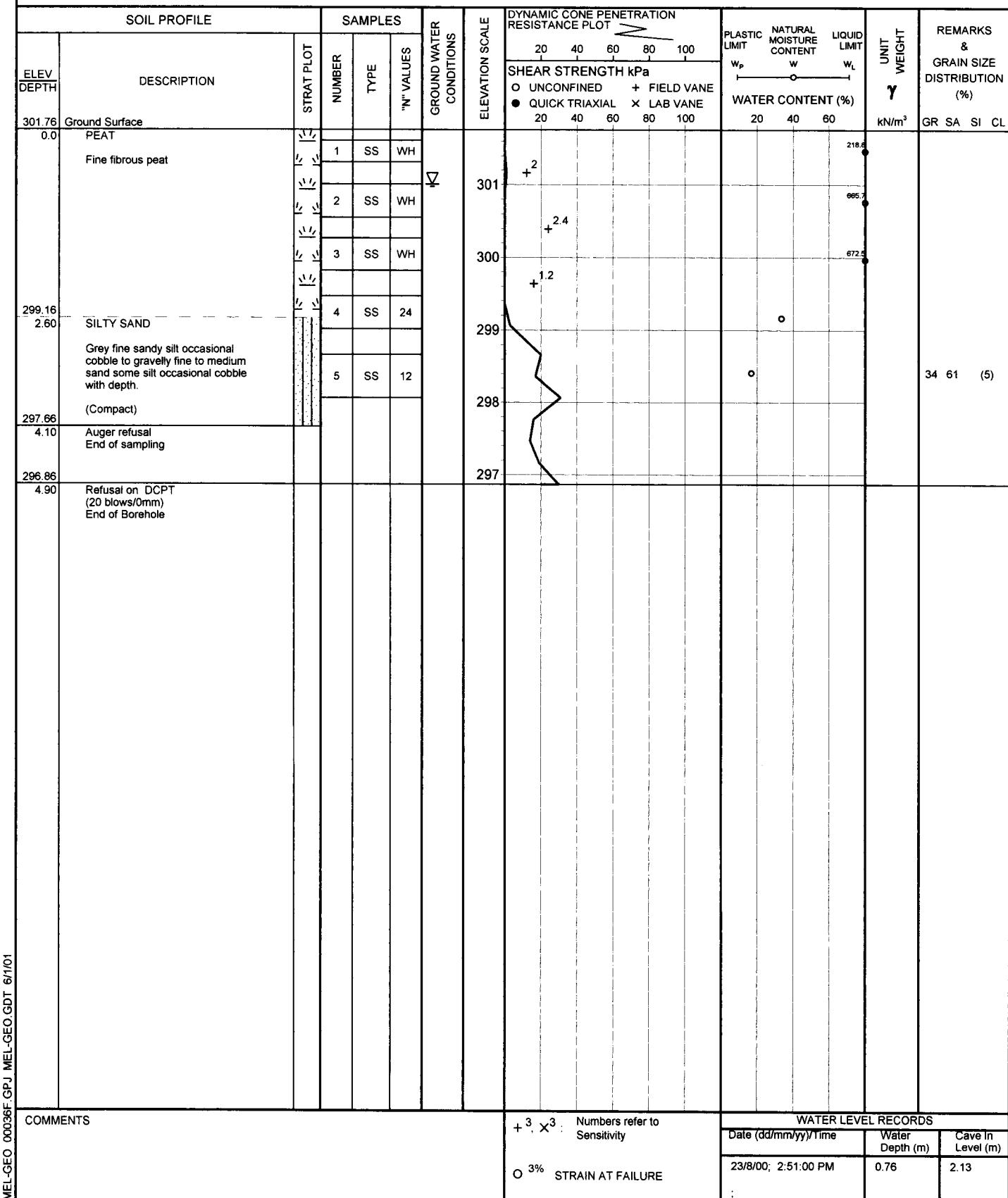


METRIC**RECORD OF BOREHOLE No. 28**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 20+300 8.8m RT D -1.3; N'ly 5164692.568 E'ly 331149.893 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 23/8/00 - 23/8/00 TIME 2:50:00 PM CHECKED BY MAM

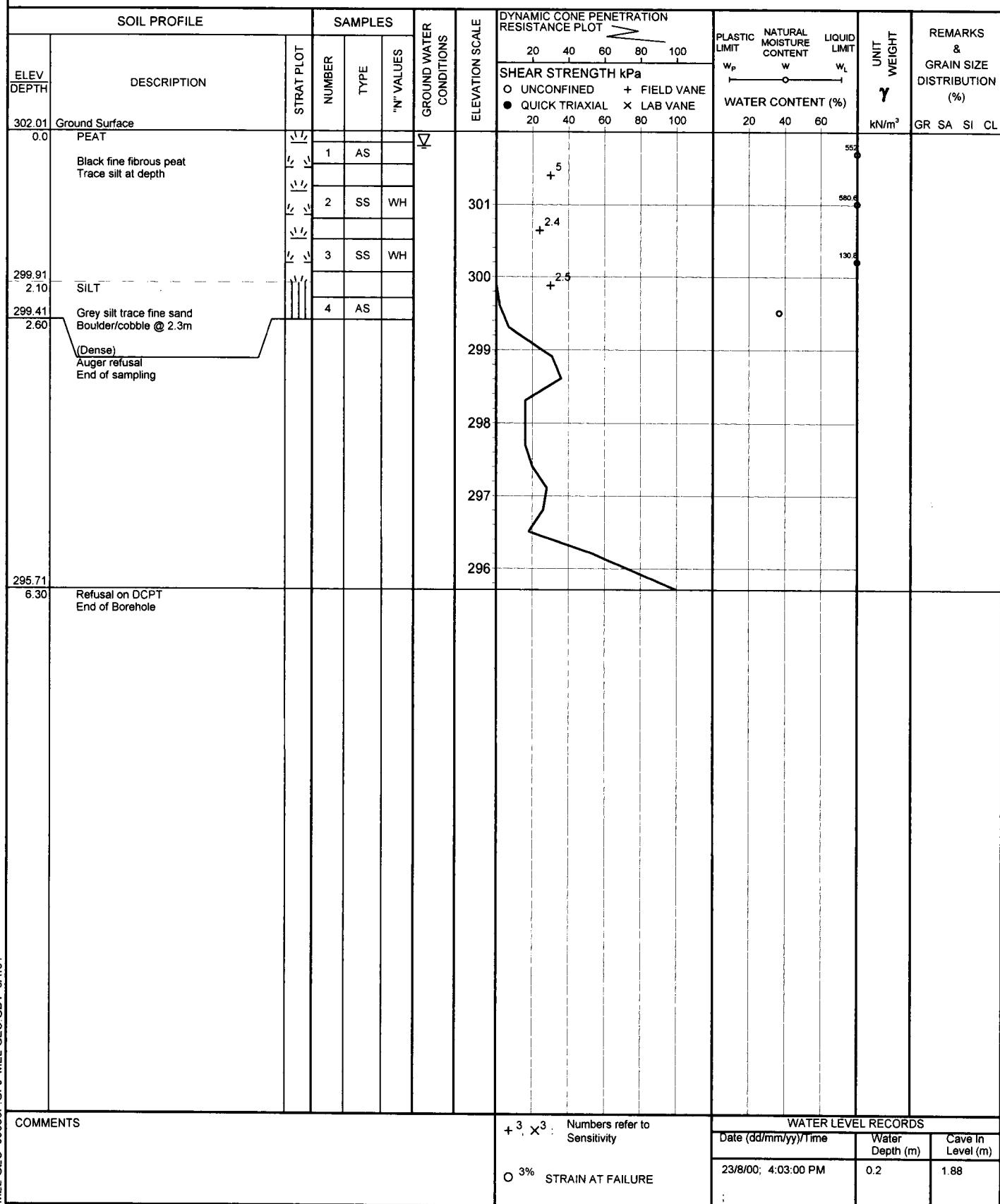


METRIC**RECORD OF BOREHOLE No. 29**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 20+450 8.8m RT D -1.7; N'ly 5164778.898 E'ly 331272.560 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 23/8/00 - 23/8/00 TIME 4:00:00 PM CHECKED BY MAM



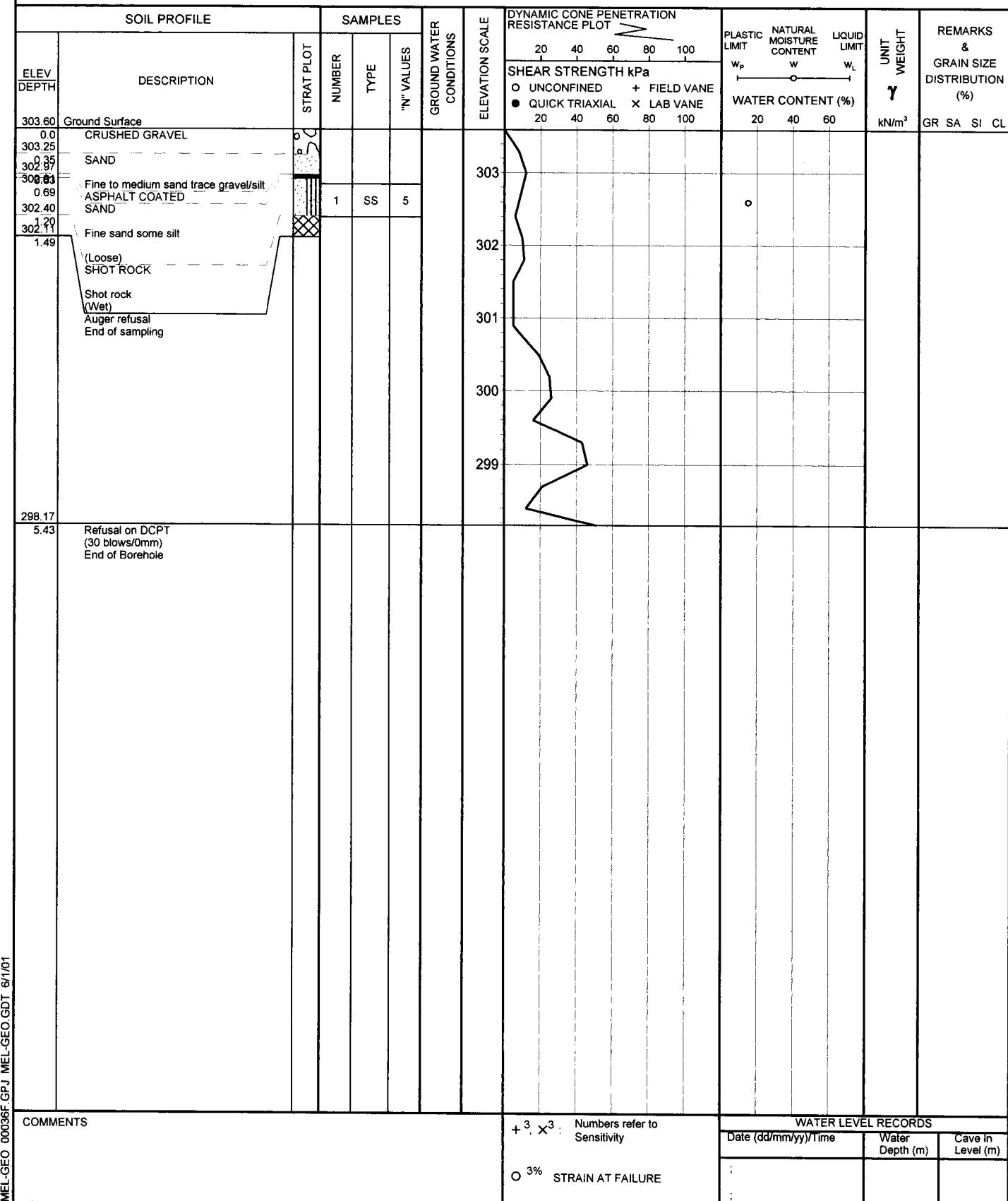
METRIC

RECORD OF BOREHOLE No. 30

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 20+450 2.0m RT; N'y 5164784.459 E'y 331268.646 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 24/8/00 - 24/8/00 TIME 11:10:00 AM CHECKED BY MAM



METRIC**RECORD OF BOREHOLE No. 30A**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 20+450 2.0m RT; N'ly 5164785.035 E'ly 331269.464 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 28/8/00 - 28/8/00 TIME 11:13:00 AM CHECKED BY MAM

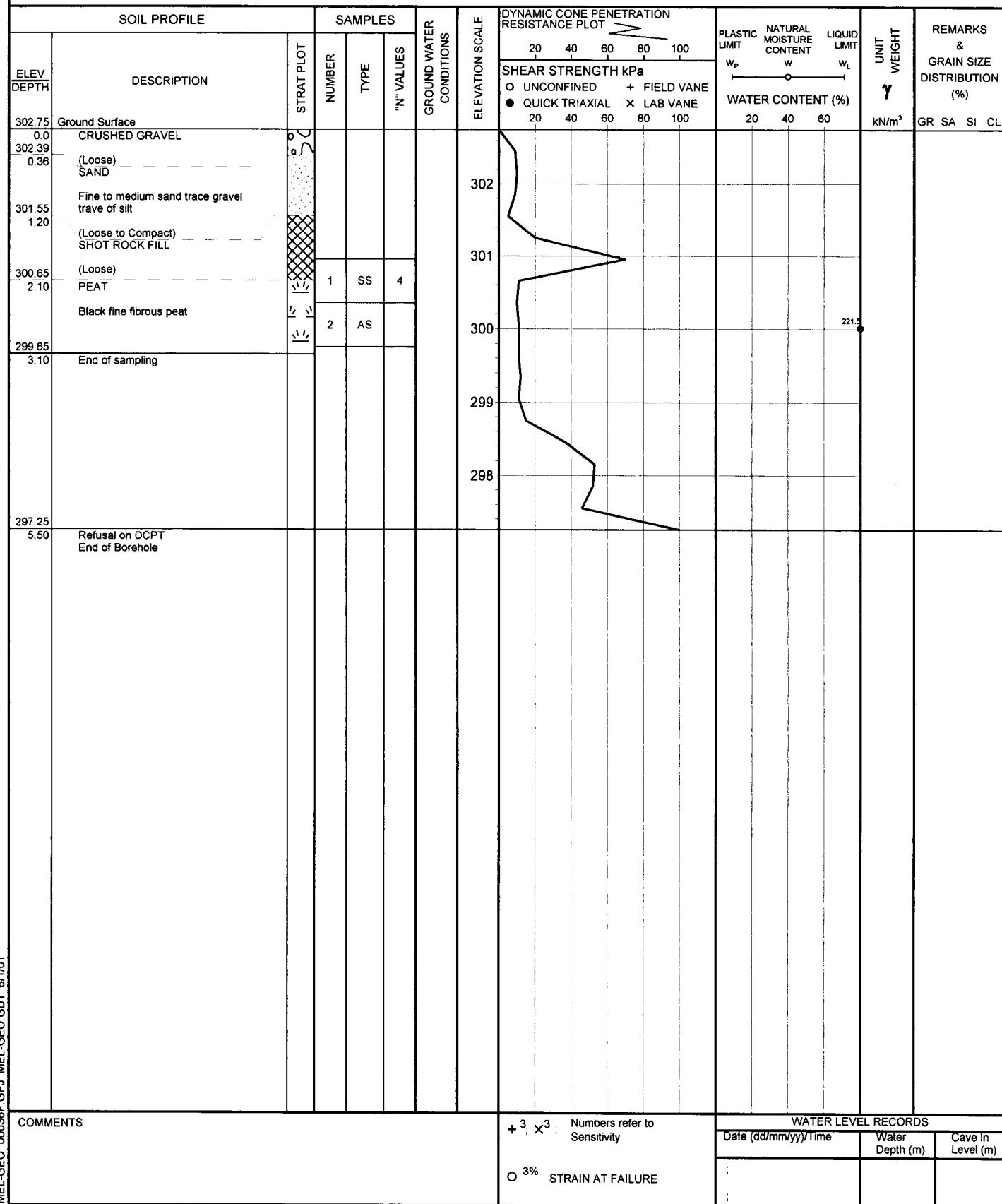
SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT w_p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w_L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)	
ELEV. DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			20	40	60	80	100	SHEAR STRENGTH kPa	○ UNCONFINED + FIELD VANE	● QUICK TRIAXIAL X LAB VANE	20	40	60
303.61	Ground Surface																	
0.0	CRUSHED GRAVEL																	
303.26	SAND																	
0.35	Fine to medium sand trace gravel/silt Layer of Asphalt Coated layer @ .64m to .69m																	
302.24	SHOT ROCK																	
1.37																		
301.63	Shot rock/ sand and peat at depth		1	SS	8													
1.98	(Loose) PEAT																	
301.02	Black/brown fine fibrous peat		2	SS	3													
2.59	SILTY SAND																	
300.01	Grey silt some fine sand to sand with silt to gravelly sand some silt with depth. Cobble @ 3.2m		3	SS	21													
3.60	(Compact) Auger refusal End of borehole																	
COMMENTS						+ ³	³ X ³	Numbers refer to Sensitivity					WATER LEVEL RECORDS					
						O	3%	STRAIN AT FAILURE					Date (dd/mm/yy)/Time	Water Depth (m)	Cave In Level (m)			
													3/8/00, 11:15:00 AM		1.2			

METRIC**RECORD OF BOREHOLE No. 31**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 20+300 2.0m RT; N'ly 5164698.129 E'ly 331145.979 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 24/8/00 - 24/8/00 TIME CHECKED BY MAM



ENCLOSURE NO.:

METRIC**RECORD OF BOREHOLE No. 31A**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 20+299 2.0m RT; N'ly 5164697.553 E'ly 331145.162 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 24/8/00 - 24/8/00 TIME 2:15:00 PM CHECKED BY MAM

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT w_p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w_L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)	
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	'N' VALUES			20	40	60	80	100	SHEAR STRENGTH kPa	○ UNCONFINED	+ FIELD VANE	● QUICK TRIAXIAL	X LAB VANE	
302.77	Ground Surface																	
0.0	CRUSHED GRAVEL																	
302.41	(Loose) SAND																	
0.36	Fine to medium sand trace gravel traces of silt																	
301.57	(Loose to Compact) SHOT ROCK FILL																	
1.20	(Loose) PEAT																	
300.77	Black fine fibrous peat																	
2.00			1	SS	2													
			2	SS	WH													
298.97	SILTY SAND		3	AS														
3.80	Grey silty fine sand trace gravel occasional cobble																	
298.37																		
4.40	Auger Refusal End of borehole																	
COMMENTS						+ 3, X 3 : ○ 3% STRAIN AT FAILURE	Numbers refer to Sensitivity					WATER LEVEL RECORDS						
												Date (dd/mm/yy)/Time	Water Depth (m)	Cave In Level (m)				

ENCLOSURE NO.:

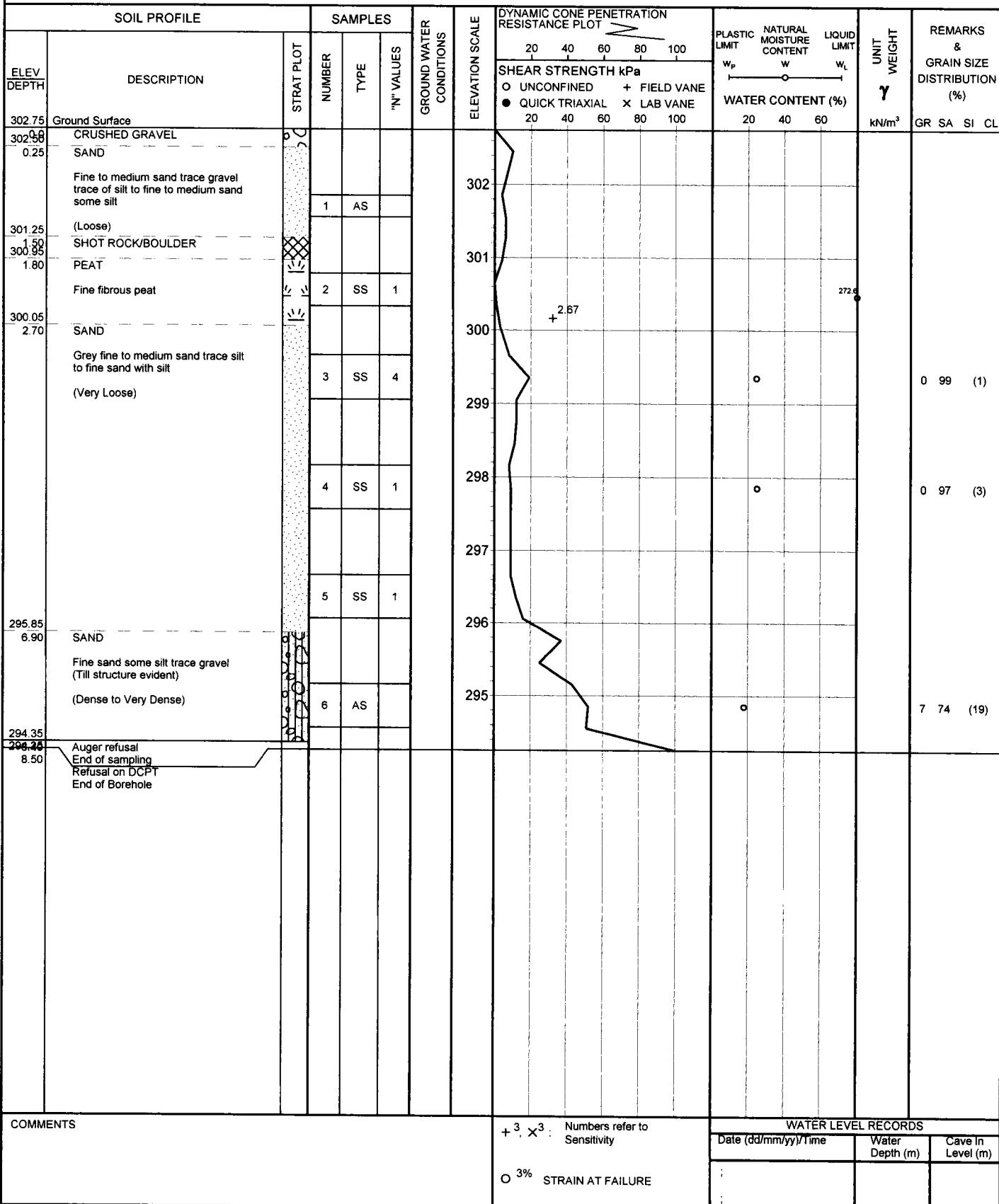
METRIC

RECORD OF BOREHOLE No. 32

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 20+350 2.0m RT; N'ly 5164726.906 E'ly 331186.868 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 24/8/00 - 24/8/00 TIME 5:00:00 PM CHECKED BY MAM



METRIC

RECORD OF BOREHOLE No. 33

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 20+400 2.0m RT; N'ly 5164755.682 E'ly 331227.757 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 24/8/00 - 25/8/00 TIME 11:00:00 AM CHECKED BY MAM

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT w_p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w_L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)	
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			20 40 60 80 100	SHEAR STRENGTH kPa	○ UNCONFINED	+ FIELD VANE	● QUICK TRIAXIAL	X LAB VANE	20 40 60 80 100	20 40 60	kN/m³	GR SA SI CL	
303.01	Ground Surface																	
0.0	CRUSHED GRAVEL																	
302.68																		
0.33	SAND																	
301.91	Fine to medium sand trace gravel trace of silt to fine to medium sand some silt																	
1.10	SHOT ROCK																	
301.51																		
1.50	PEAT																	
	Fine fibrous peat																	
300.41																		
2.60	SILT																	
299.81																		
3.20	Organic silt (Wet) (Very Loose) SAND																	
	Fine and medium sand trace silt some gravel.																	
	(Compact) (Wet)																	
297.41																		
5.60	Auger refusal End of sampling Refusal on DCPT End of Borehole																	
COMMENTS						+ 3 , \times^3 : Numbers refer to Sensitivity				○ 3% STRAIN AT FAILURE				WATER LEVEL RECORDS				
														Date (dd/mm/yy)/Time	Water Depth (m)	Cave In Level (m)		
														:	:	:		

RECORD OF BOREHOLES

Area 3:

Boreholes 1 to 11

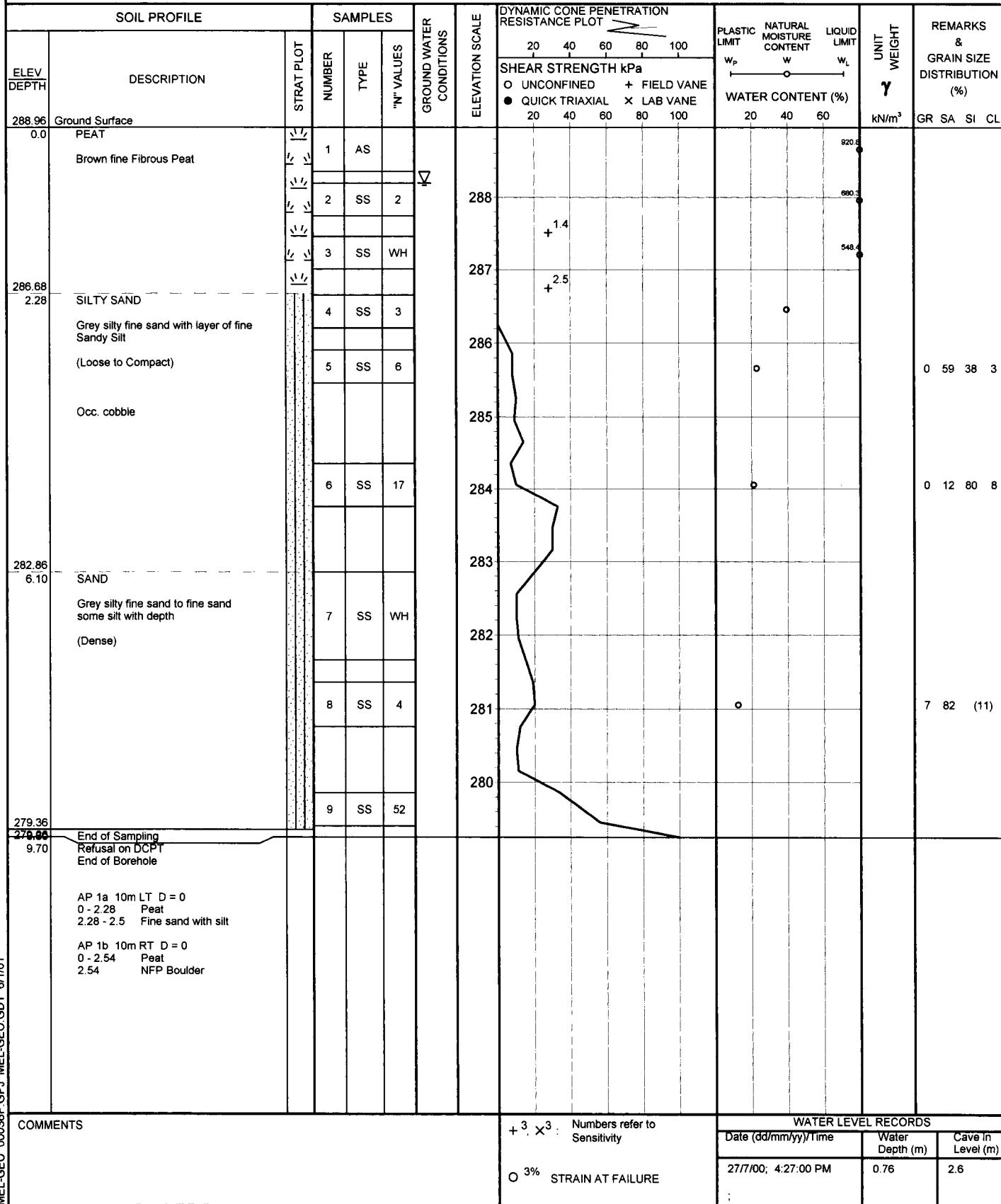
ENCLOSURE NO.:

METRIC**RECORD OF BOREHOLE No. 1**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 10+000 On Centerline, Nly 5165060.985 Ely 331658.175 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 27/7/00 - 27/7/00 TIME 4:07:00 PM CHECKED BY MAM

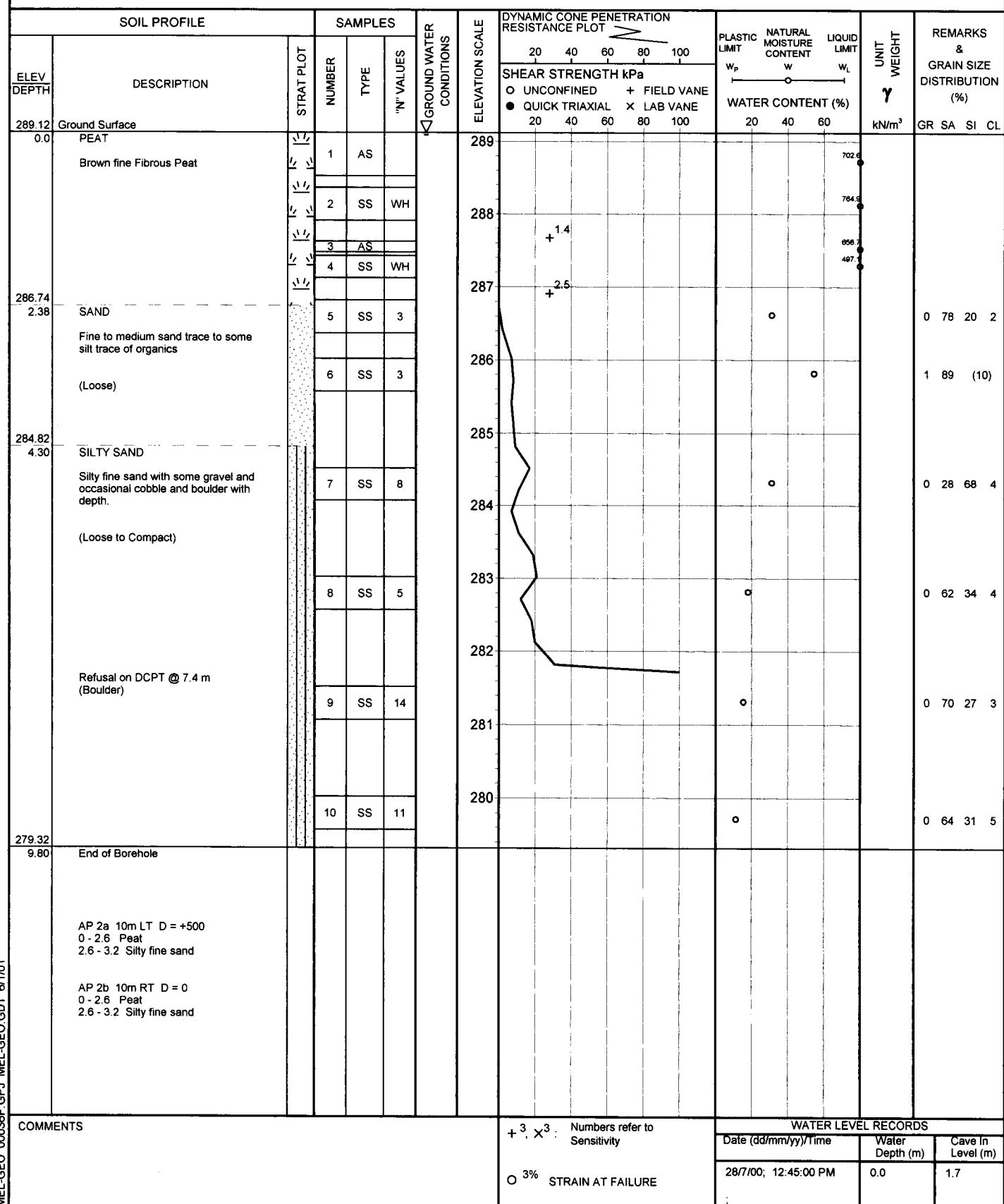


METRIC**RECORD OF BOREHOLE No. 2**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 20+875 On Centerline; N'y 5165033.781 E'y 331619.521 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 28/7/00 - 28/7/00 TIME 12:45:00 PM CHECKED BY MAM



ENCLOSURE NO.:

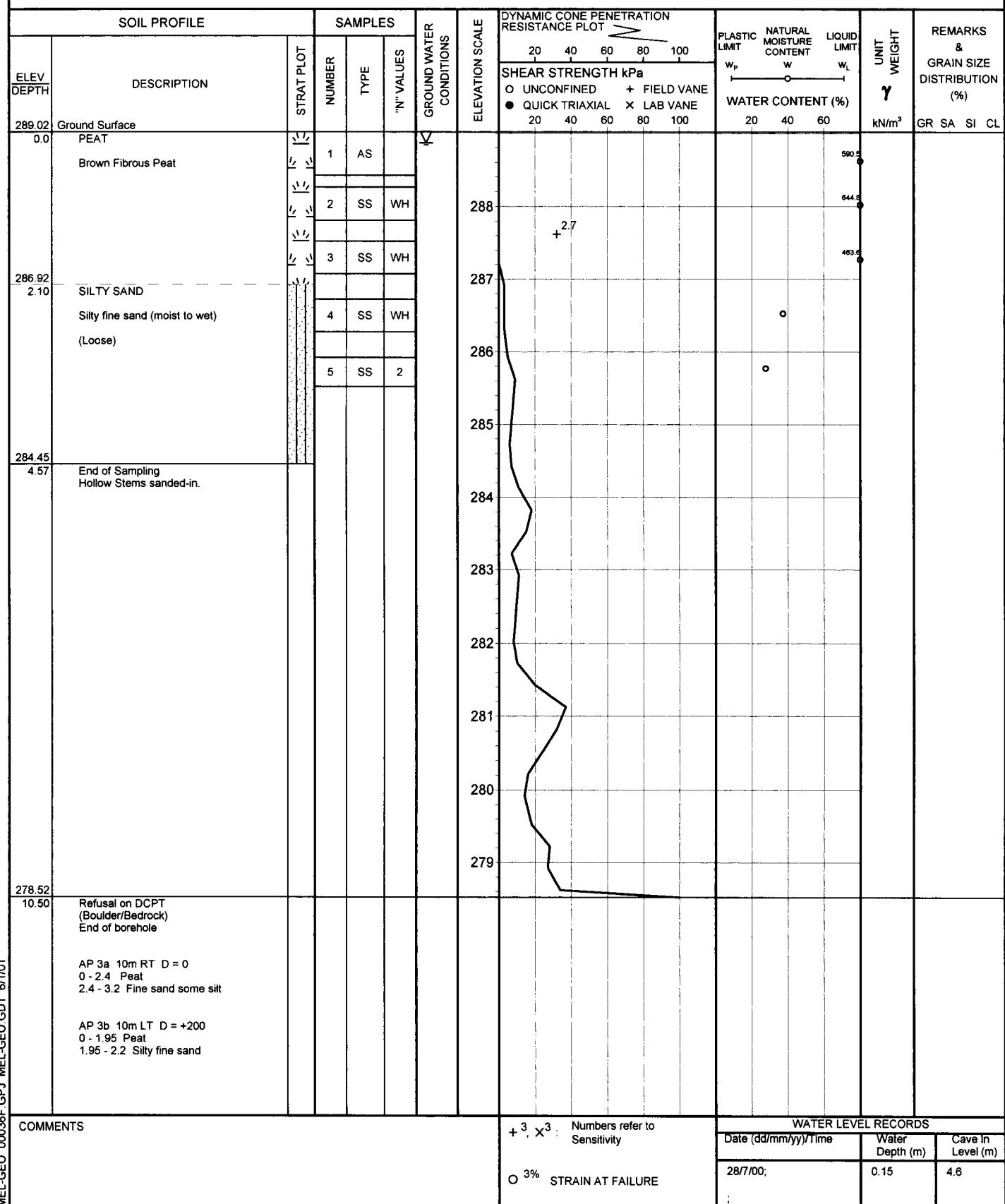
METRIC

RECORD OF BOREHOLE No. 3

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 20+800 On Centerline; N'ly 5164990.616 E'ly 331558.187 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 28/7/00 - 28/7/00 TIME 3:50:00 PM CHECKED BY MAM



MEL-GEO 00036F GPJ MEL-GEO GDT 6/1/01

ENCLOSURE NO.:

METRIC**RECORD OF BOREHOLE No. 4**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 20+750 On Centerline; N'ly 5164961.839 E'ly 331517.298 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 1/8/00 - 1/8/00 TIME CHECKED BY MAM

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT w_p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w_L	WATER CONTENT (%)	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)	
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			20	40	60	80	100	SHEAR STRENGTH kPa	○ UNCONFINED	+ FIELD VANE	● QUICK TRIAXIAL	X LAB VANE		
288.96	Ground Surface																		
0.0	PEAT																		
	Brown Fibrous Peat		1	AS									3	+				715.5	
			2	SS	WH													506.6	
287.16	SAND		3	SS	2													332.7	
1.80	Fine to medium sand trace/some silt. Colour change from grey to yellow with depth. Trace of gravel and cobble @ 4.9m (Loose to compact with depth)		4	SS	4														6 90 (4)
			5	SS	6														
			6	SS	19														21 66 (13)
283.42																			
5.54	Auger Refusal BLD End of Sampling																		
279.46																			
9.50	Refusal on DCPT (Boulder/Bedrock) End of borehole																		
	AP 4 10m LT 0 - 2.29 Peat 2.29 - 3.05 Grey fine sand with/some silt																		
COMMENTS								+ 3	X 3	Numbers refer to Sensitivity					WATER LEVEL RECORDS				
								O 3%	X 3%						Date (dd/mm/yy)/Time	Water Depth (m)	Cave In Level (m)		
															1/8/00; 4:10:00 PM	0.36	2.4		

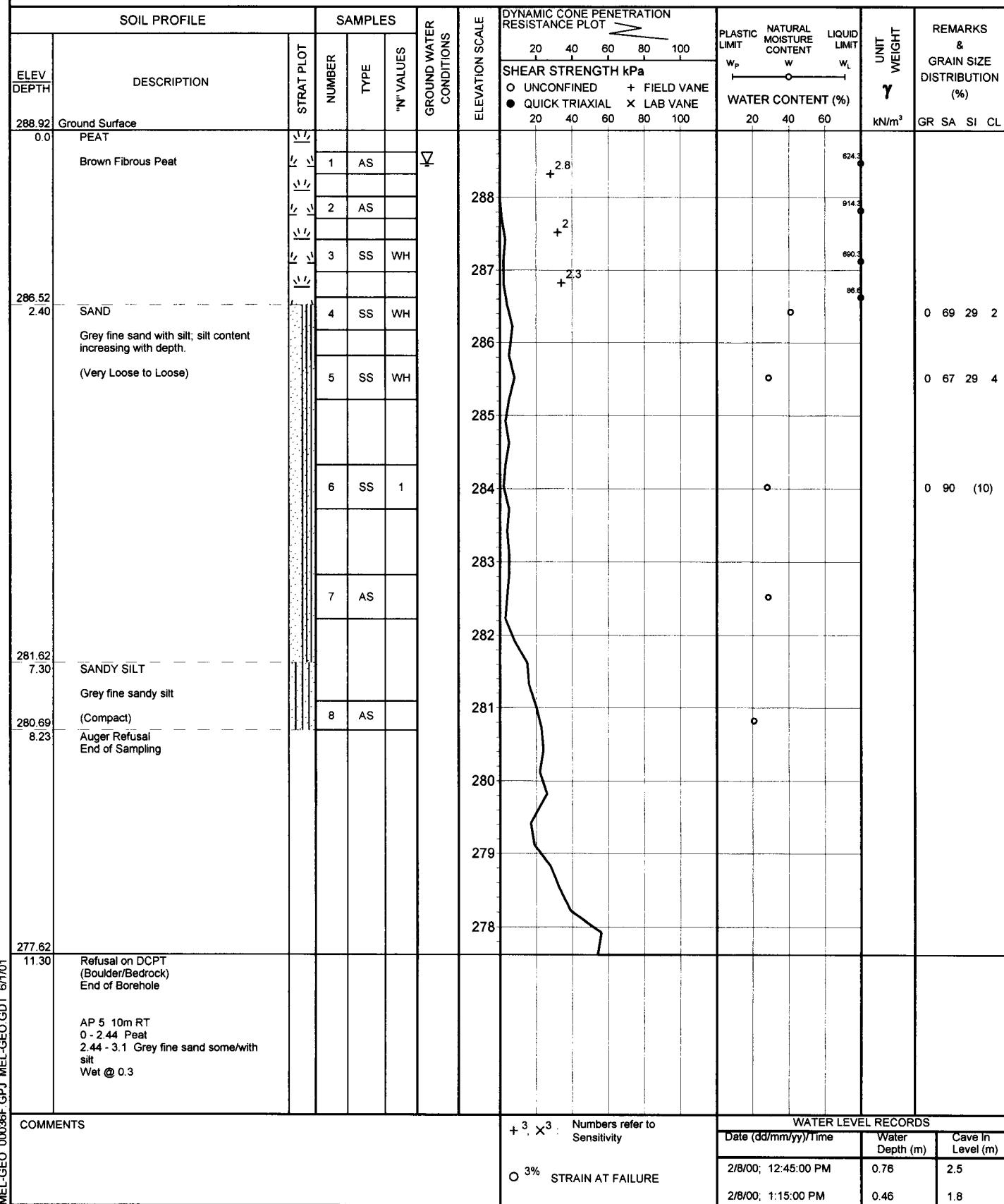
ENCLOSURE NO.:

METRIC**RECORD OF BOREHOLE No. 5**

1 OF 1



REFERENCE 00/04/0036 DATUM Geodetic LOCATION Sta 10+050 On Centerline; Nly 5165089.761 E'y 331699.063 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 2/8/00 - 2/8/00 TIME 12:38:00 PM CHECKED BY MAM



MEL-GEO 00026F.GPJ MEL-GEO.GDT 6/1/01

MERLEX ENGINEERING LTD.

Consulting Geotechnical Engineers

ENCLOSURE NO.:

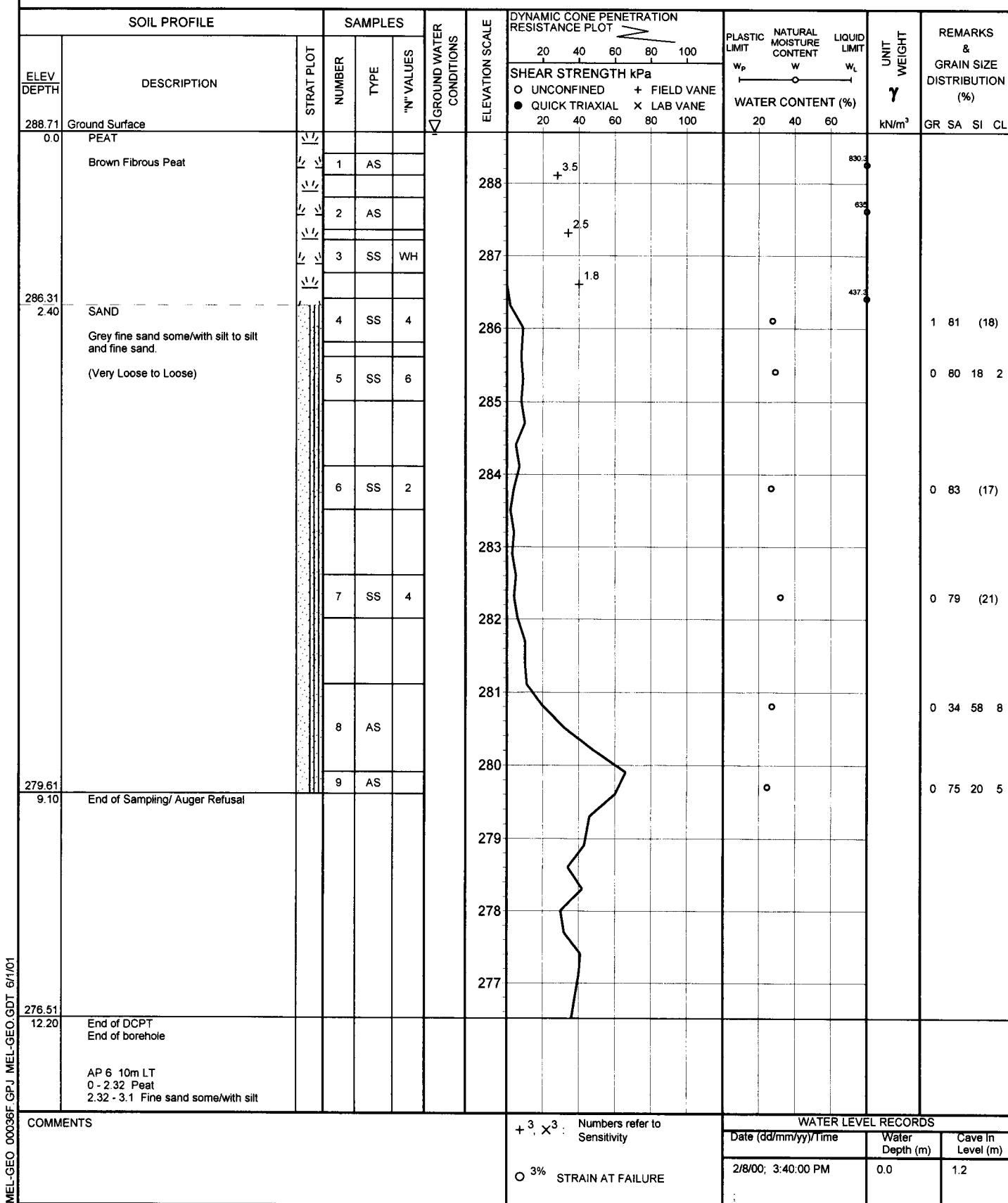
METRIC

RECORD OF BOREHOLE No. 6

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 10+100 On Centerline, Nly 5165118.538 Ely 331739.952 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 2/8/00 - 2/8/00 TIME 3:37:00 PM CHECKED BY MAM



MEL-GEO 00036F GPJ MELGEO.GDT 6/1/01

ENCLOSURE NO.:

METRIC

RECORD OF BOREHOLE No. 7

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 10+150 On Centerline; Nly 5165147.315 Ely 331780.841 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 3/8/00 - 3/8/00 TIME 10:20:00 AM CHECKED BY MAM

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT w _p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			20 40 60 80 100	SHEAR STRENGTH kPa	20 40 60 80 100	20 40 60	WATER CONTENT (%)					
288.76	Ground Surface																
0.0	PEAT	1	SS	WH													
	Brown Fibrous Peat (Very Loose)	2	SS	WH													
286.76	SILTY SAND to SANDY SILT	3	SS	WH													
2.00	Grey silty fine sand to fine sandy silt (Loose to Very Loose to Compact at depth)	4	SS	5													0 68 29 3
		5	SS	4													0 25 68 7
		6	SS	WH													0 65 30 5
		7	SS	2													0 58 40 2
		8	SS	30													0 65 29 6
279.66	9.10 End of sampling	9	SS														0 31 61 8
276.56	12.20 End of DCPT End of borehole																
COMMENTS									+ 3 X 3 : Numbers refer to Sensitivity					WATER LEVEL RECORDS			
									O 3% STRAIN AT FAILURE					Date (dd/mm/yy)/Time	Water Depth (m)	Cave In Level (m)	
														3/8/00; 10:28:00 AM	0.3	4	

MELGEO 00036F GPJ MELGEO.GDT 6/101

ENCLOSURE NO.:

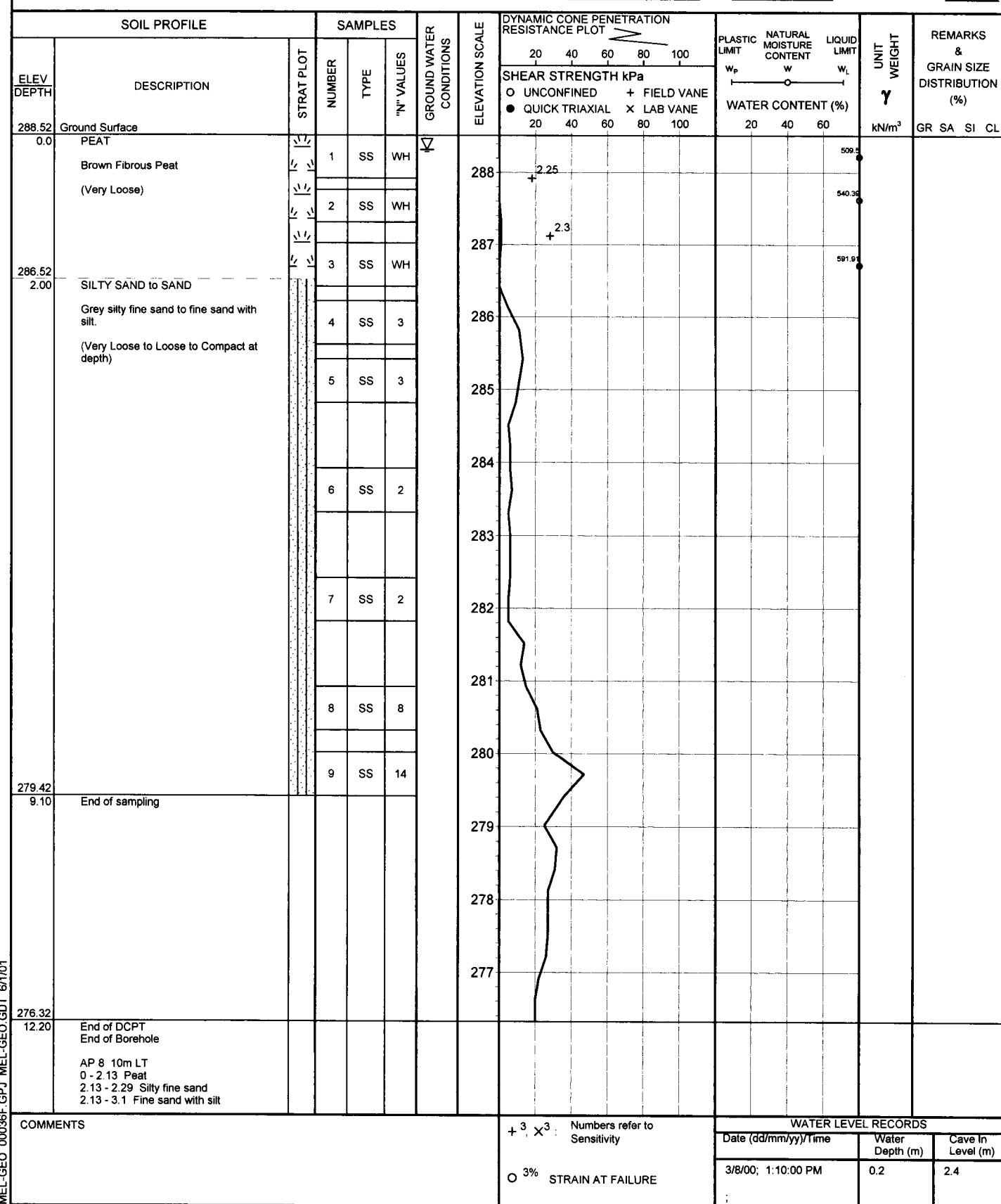
METRIC

RECORD OF BOREHOLE No. 8

1 OF 1



REFERENCE 00/04/0036 DATUM Geodetic LOCATION Sta 10+200 On Centerline; Nly 5165176.097 Ely 331821.726 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 3/8/00 - 3/8/00 TIME 1:04:00 PM CHECKED BY MAM



MEL-GEO 00036F.GPJ MEL-GEO.GDT 6/1/01

ENCLOSURE NO.:

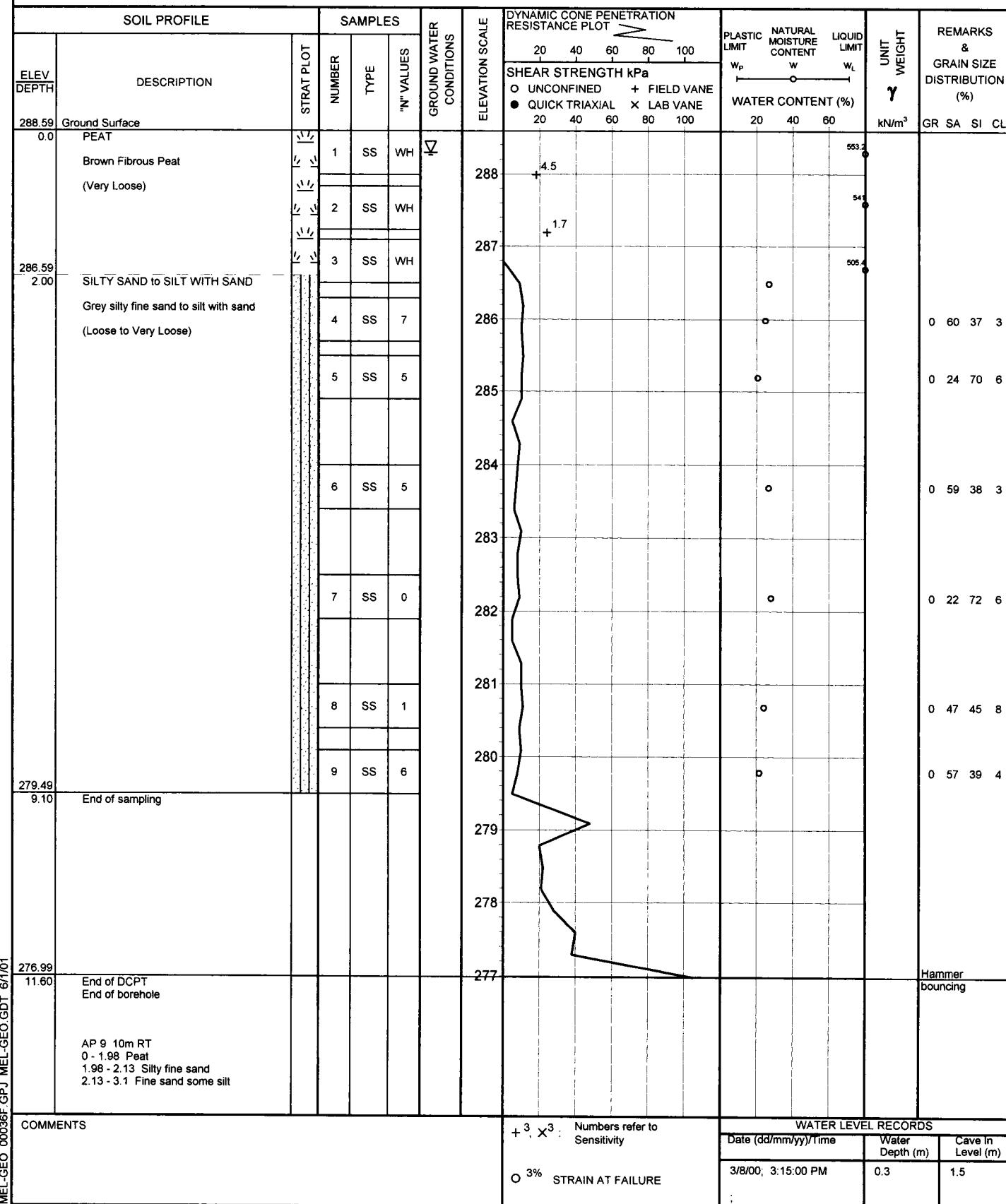
METRIC

RECORD OF BOREHOLE No. 9

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 10+250 On Centerline; N'y 5165205.479 E'y 331862.180 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 3/8/00 - 3/8/00 TIME 3:10:00 PM CHECKED BY MAM



MEL-GEO 00036F GPJ MEL-GEO GDT 6/1/01

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ENCLOSURE NO.:

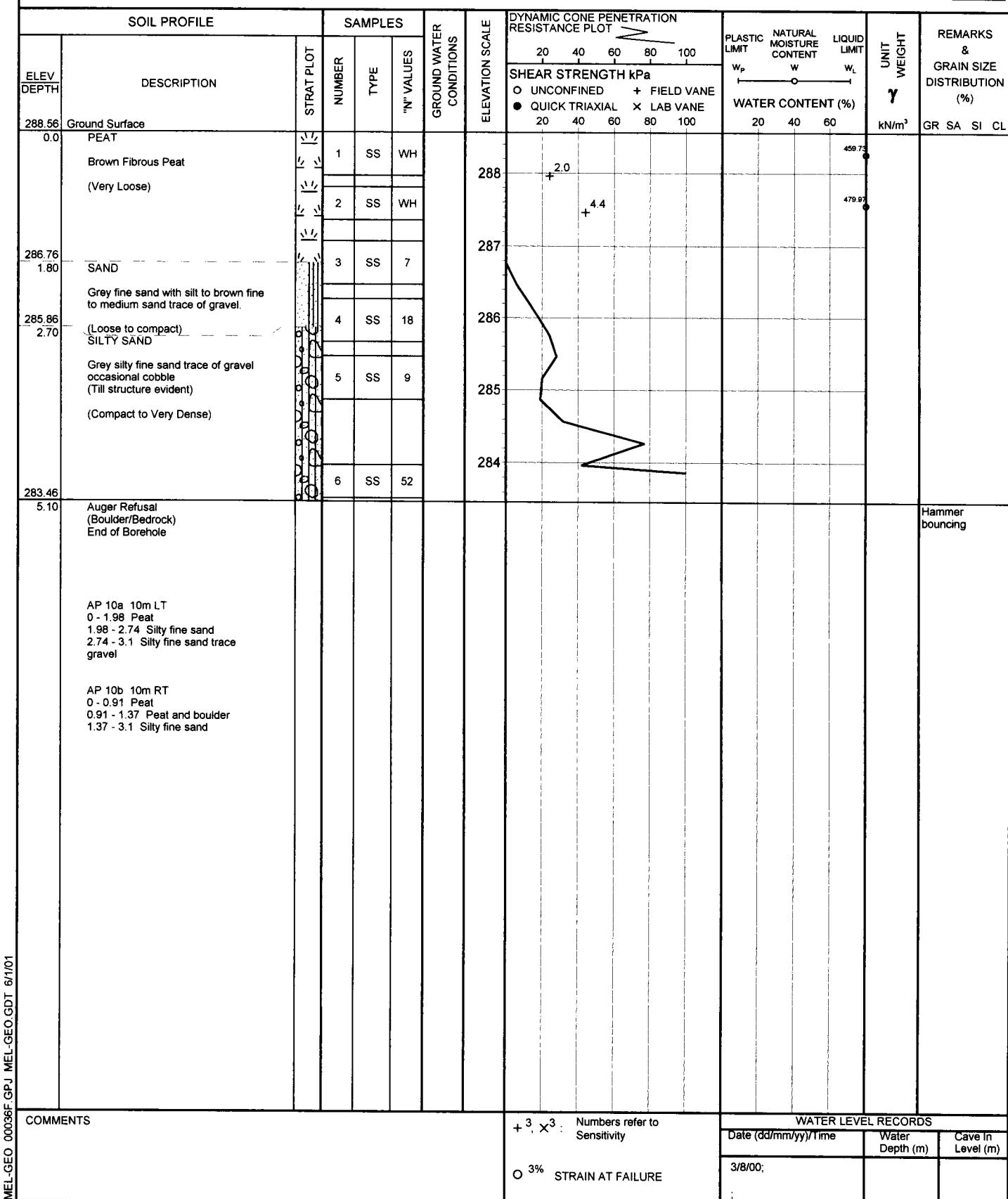
METRIC

RECORD OF BOREHOLE No. 10

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 10+300 On Centerline; Nly 5165236.664 E'ly 331901.255 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers, Dynamic Cone Penetration Test COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 3/8/00 - 3/8/00 TIME 4:57:00 PM CHECKED BY MAM



METRIC**RECORD OF BOREHOLE No. 11**

1 OF 1



REFERENCE 00/04/00036 DATUM Geodetic LOCATION Sta 10+350 On Centerline; Nly 5165269.764 Ely 331938.724 ORIGINATED BY ELS
 PROJECT Highway No. 63 W.P. 167-90-00 BOREHOLE TYPE Hollow Stem Augers COMPILED BY MR
 CLIENT EarthTech DATE (Started/Completed) 4/8/00 - 4/8/00 TIME CHECKED BY MAM

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT w_p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w_L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)	
ELEV. DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			20	40	60	80	100	SHEAR STRENGTH kPa	○ UNCONFINED + FIELD VANE	● QUICK TRIAXIAL X LAB VANE	20	40	60
292.42	Ground Surface																	
292.00	PEAT																	
0.10	Brown Fibrous Peat (Very Loose) SAND																	
291.02	Yellow fine sand trace of gravel some silt		1	SS	20		292											
1.40	(Wet) (Compact) Auger Refusal (Boulder/Bedrock) End of Borehole																	
	AP 11a 10m RT 0 - 100 Organics 100 - 400 Fine to med. sand some silt trace gravel 400 - 2.7 Silty fine sand trace of gravel 2.7 NFP BR																	
	AP 11b 10m LT 0 - 100 Organics 100 - 500 Fine to med. sand some silt trace gravel 500 - 1.3 Silty fine sand trace gravel 1.3 NFP BLD/BR																	
	AP 11c 10+320 CL 0 - 100 Silty organics 100 - 1.5 Silty fine sand trace gravel (wet) 1.5 NFP BLD/BR																	
	AP 11d 10+400 CL 0 - 50 Silty organics 50 - 2.3 Silty fine sand trace gravel occasional boulder and cobble 2.3 NFP																	
COMMENTS						+ ³ , \times^3 : ○ 3% STRAIN AT FAILURE	Numbers refer to Sensitivity					WATER LEVEL RECORDS						
												Date (dd/mm/yy)/Time	Water Depth (m)	Cave In Level (m)				

TABLE 1

Option Comparison Area 1 & 2

TABLE 1
OPTION COMPARISONS AREA 1 & 2

OPTIONS	ADVANTAGE	DISADVANTAGE	ESTIMATED POSSIBLE TOTAL SETTLEMENTS AT TYPICAL SECTION 13+700 AREA 1 *	
			EXISTING PLATFORM (MM)	WIDENING (MM)
A-1) Full depth excavation of peat from under widening (OPSD 203.020)	<ul style="list-style-type: none"> - Eliminates distress under widening - Approximately 70% less costly than Option B 	<ul style="list-style-type: none"> - Movement will occur due to differential subgrade conditions - Differential settlement of existing platform will occur 	0 – 150	0
A-2) Partial depth excavation of peat (1/2 depth) from under widening.	<ul style="list-style-type: none"> - Improves stability during partial excavation (approximately 22%) - Approximately 80% less costly than Option B 	<ul style="list-style-type: none"> - Does not effectively reduce settlement associated with peat compression 	0 – 150	< 750
B) Full width excavation of all peat.	<ul style="list-style-type: none"> - No post construction distress / distortion - No maintenance costs associated with compression of peat subgrade. - No post construction liability, due to differential settlement in driving lane 	- Highest cost	0	0
C) Place fill widening directly on peat.	- Least cost	- Long term differential settlement under widening & existing platform	0 – 150	750 **

* Estimates of settlement based on loadings of 300 mm new fill being placed over new center line and 1.5 m new fill over existing right ditch line (see Figure 14).

Compressions of peat estimate based on 50% of new fill thickness up to ½ the thickness of the peat layer.

** It is estimated 50% of peat compression will occur during construction with the remaining compression occurring at a decreasing rate, over a period of a decade with or without geogrid reinforcement.

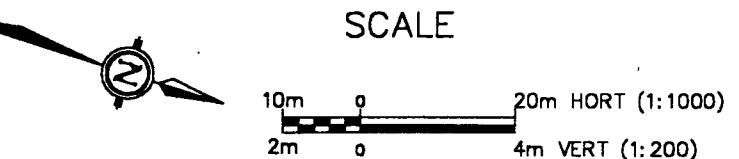
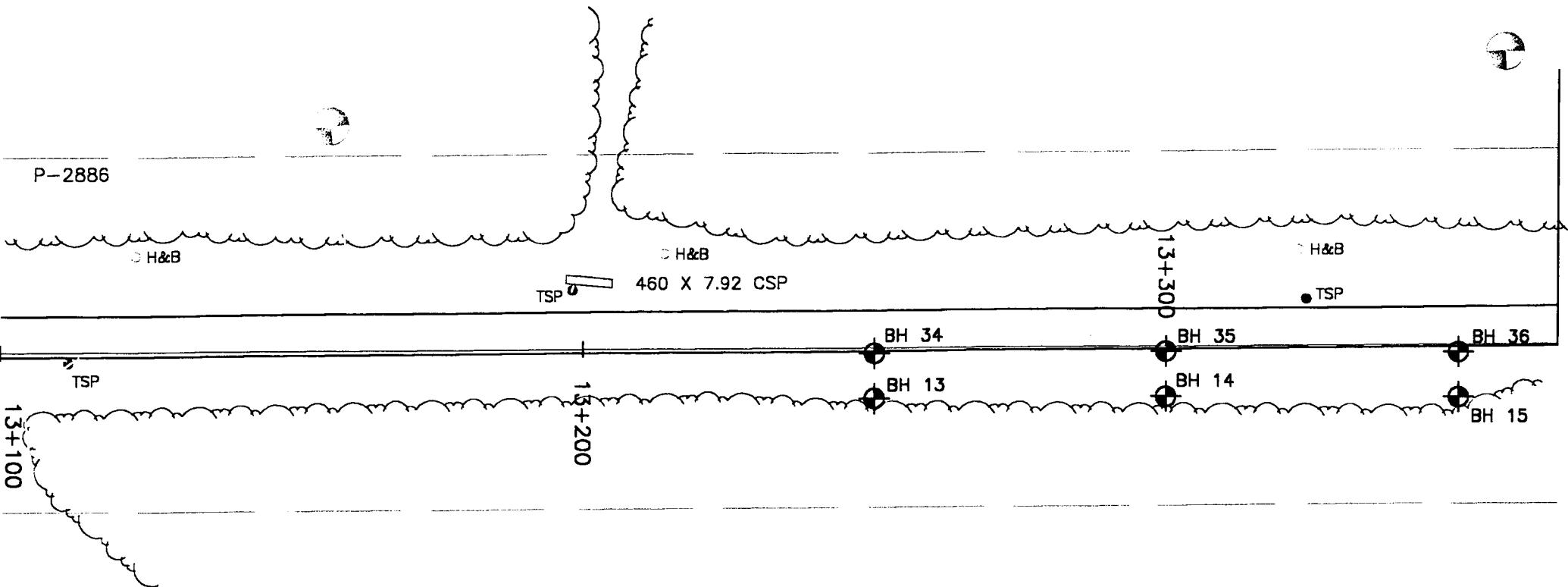
FIGURES 2 TO 8

Borehole Location and Soil Strata (3 Areas)

CONT NO.
W.P. NO. 167 - 90 - 00

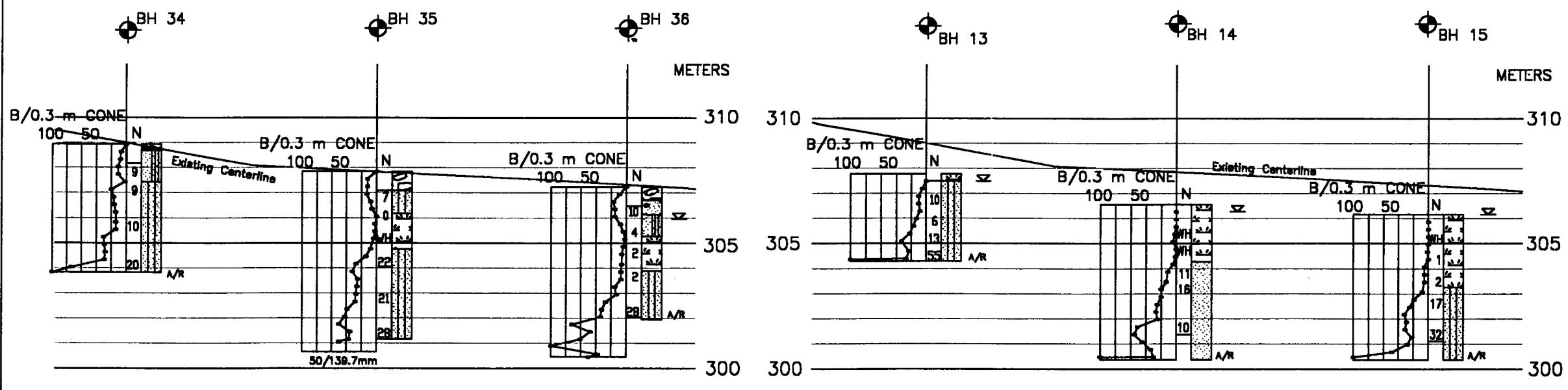
HWY 63
FOUNDATION INVESTIGATION - AREA 1
BOREHOLE LOCATIONS AND SOIL STRATA

FIGURE
2



STRATIGRAPHY LEGEND

TOPSOIL	SAND	SILTY SAND/ SANDY SILT
PEAT	SAND & GRAVEL	SILT
VARVED/ INTERLAYERED CLAYS & SILTS	CLAY	SILTY CLAY
FILL	TILL	CRUSHED GRAVEL
ASPHALT COATED		



LEGEND		
Borehole and Dynamic Cone Penetration Test		
Borehole		
N Blows/0.3 m		
sz Water Level at Time of Investigation		
A/R Auger Refusal at Elevation		
Borehole No.	Co-ordinates North East	Elevation
BOREHOLE No. 00-34	5158450.837	330883.517
BOREHOLE No. 00-35	5158498.147	330877.935
BOREHOLE No. 00-36	5158545.857	330882.353
BOREHOLE No. 00-13	5158453.068	330900.929
BOREHOLE No. 00-14	5158500.578	330885.347
BOREHOLE No. 00-15	5158548.088	330869.784

NOTE 1:
The boundaries between soil strata have been established at the borehole locations only. The boundaries between boreholes are assumed based on borehole data.



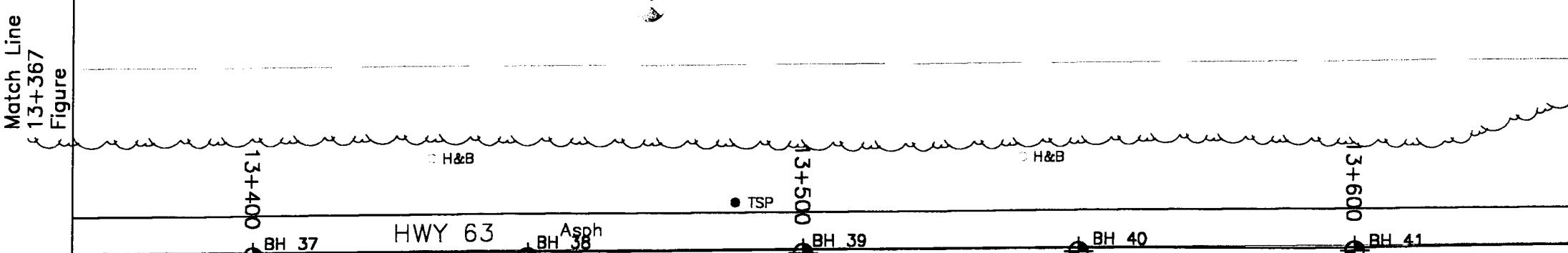
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Consulting Geotechnical Engineers

PROJECT: HWY. 63, Foundation Investigation	REFERENCE NO.: 00036F	DATE: August 28, 2000
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W.P. NO. 167 - 90 - 00

HWY 63
FOUNDATION INVESTIGATION - AREA 1
BOREHOLE LOCATIONS AND SOIL STRATA

FIGURE
3A



Match Line
13+642 &
Figures

SCALE

10m 0 20m HORT (1:1000)
2m 0 4m VERT (1:200)

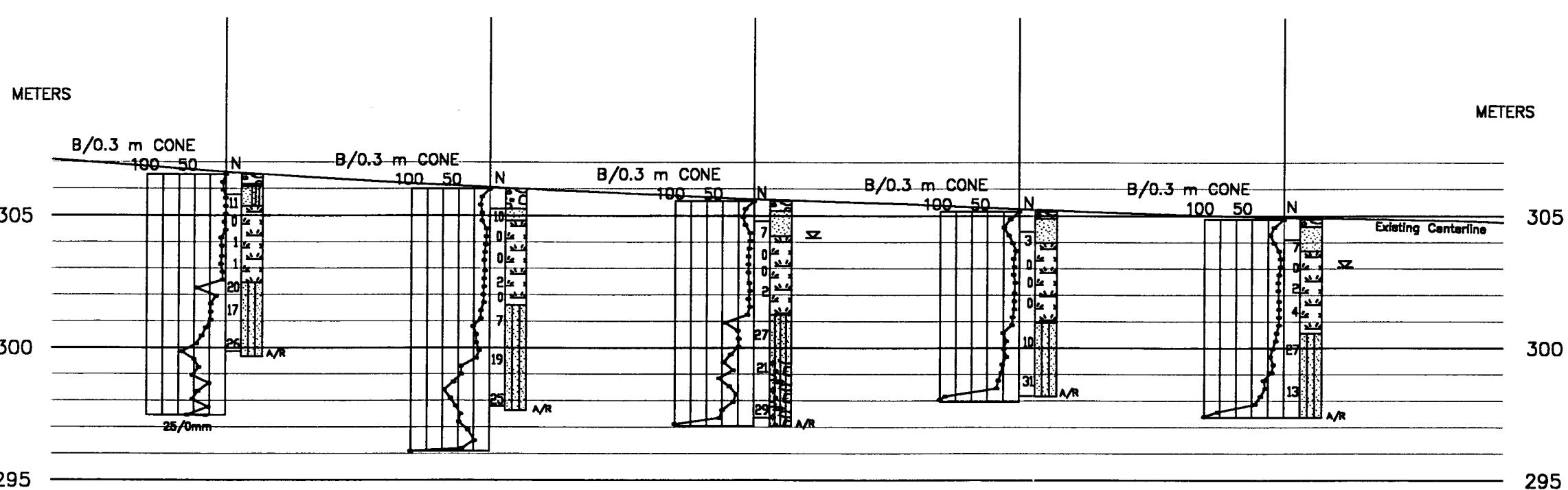
STRATIGRAPHY LEGEND

	TOPSOIL		SAND		SILTY SAND/ SANDY SILT
	PEAT		SAND & GRAVEL		SILT
	VARVED/ INTERLAYERED CLAYS & SILTS		CLAY		SILTY CLAY
	FILL		TILL		CRUSHED GRAVEL
	ASPHALT COATED				

LEGEND

- Borehole and Dynamic Cone Penetration Test
- Borehole
- N Blows/0.3 m
- Water Level at Time of Investigation
- A/R Auger Refusal at Elevation

Borehole No.	Co-ordinates		Elevation
	North	East	
BOREHOLE No. 00-37	5158593.167	330848.771	308.555m
BOREHOLE No. 00-38	5158640.877	330831.188	305.997m
BOREHOLE No. 00-39	5158688.187	330815.806	305.545m
BOREHOLE No. 00-40	5158735.897	330800.024	305.181m
BOREHOLE No. 00-41	5158783.207	330784.441	304.870m



NOTE 1:
The boundaries between soil strata have been established at the borehole locations only. The boundaries between boreholes are assumed based on borehole data.



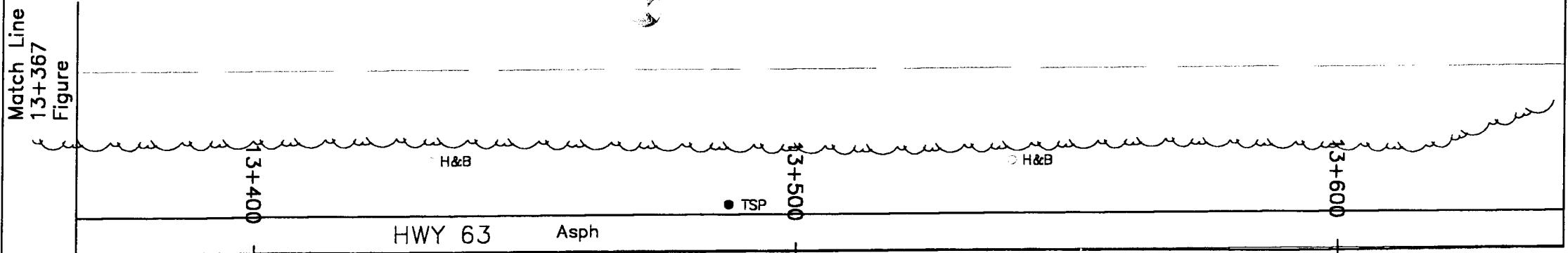
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PROJECT: HWY. 63, Foundation Investigation	REFERENCE NO. 00036F	DATE: August 28, 2000
DRAWN BY: M.R.	CHECKED BY: M.A.M.	

CONT NO.
W.P. NO. 167 - 90 - 00

HWY 63
FOUNDATION INVESTIGATION - AREA 1
BOREHOLE LOCATIONS AND SOIL STRATA

FIGURE
3B



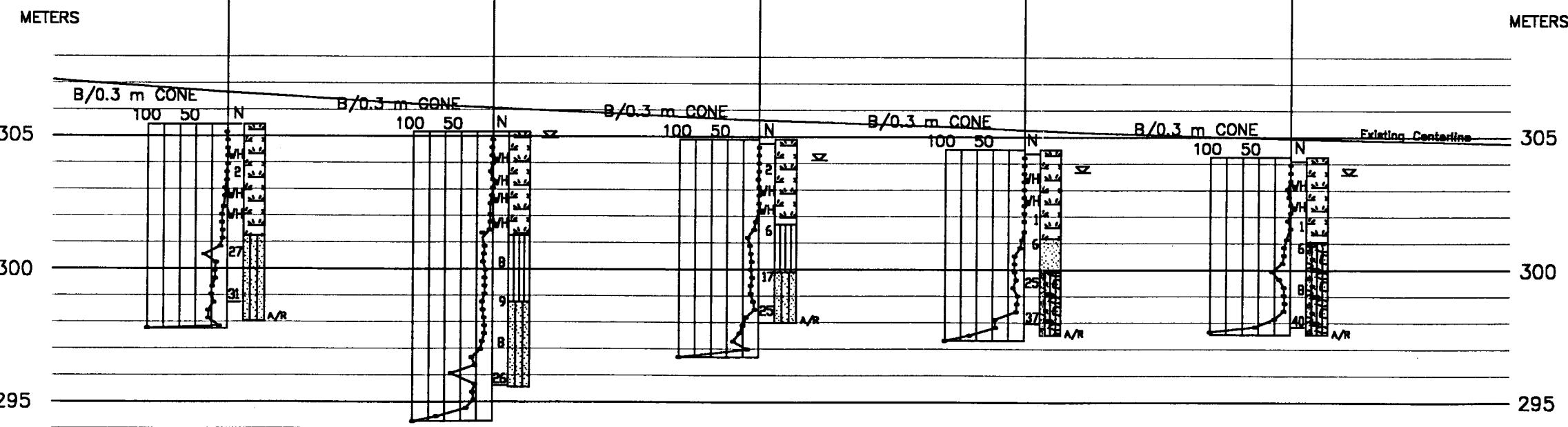
Match Line
13+642 &
Figures

SCALE

10m 0 20m HORT (1:1000)
2m 0 4m VERT (1:200)

STRATIGRAPHY LEGEND

	TOPSOIL		SAND		SILTY SAND/ SANDY SILT
	PEAT		SAND & GRAVEL		SILT
	VARVED/ INTERLAYERED CLAYS & SILTS		CLAY		SILTY CLAY
	FILL		TILL		CRUSHED GRAVEL
	ASPHALT COATED				



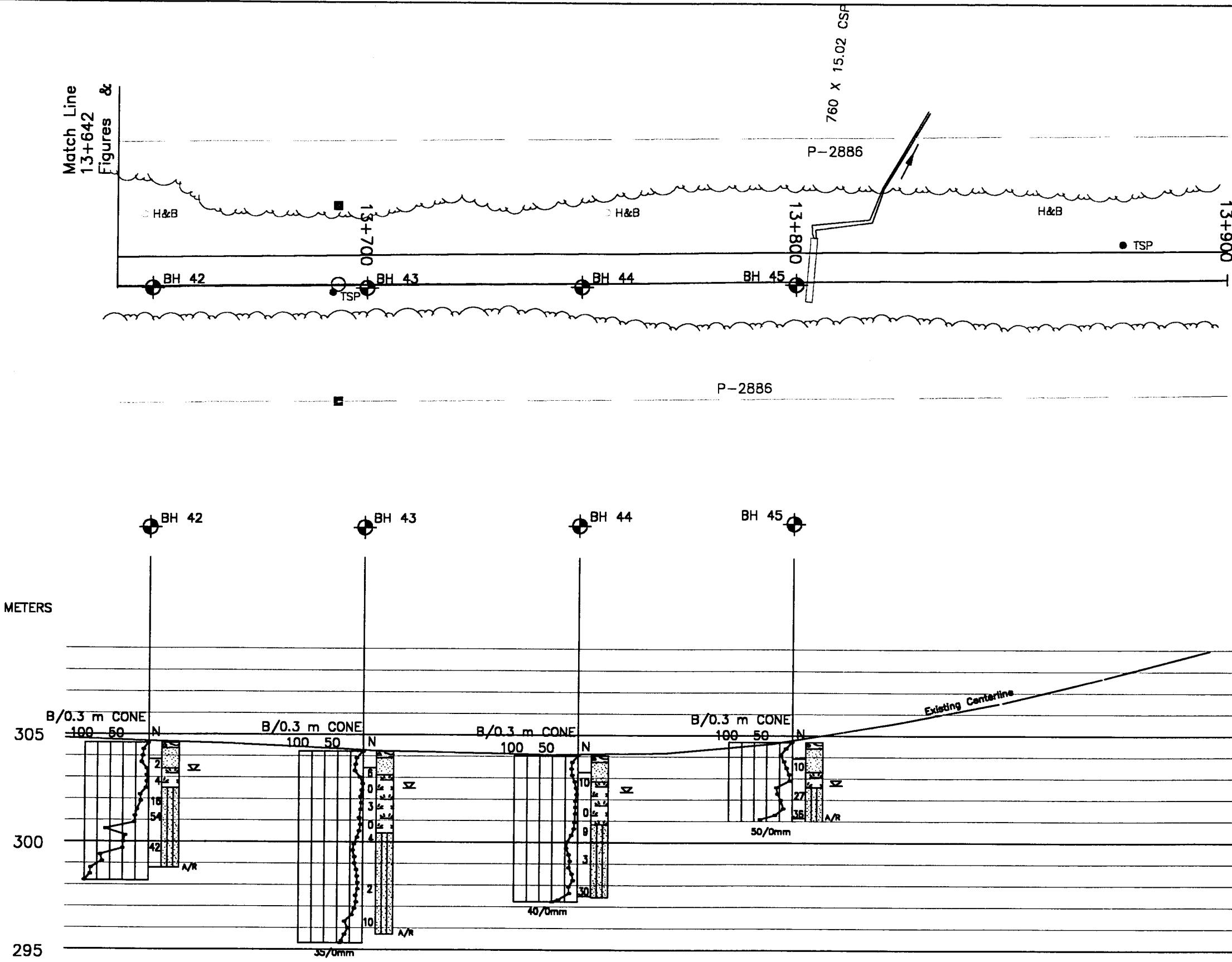
LEGEND			
	Borehole and Dynamic Cone Penetration Test		
	Borehole		
N	Blows/0.3 m		
	Water Level at Time of Investigation		
A/R	Auger Refusal at Elevation		
Borehole No.	Co-ordinates North	East	Elevation
BOREHOLE No. 00-16	5158598.598	330854.182	305.442m
BOREHOLE No. 00-17	5158643.108	330838.800	305.189m
BOREHOLE No. 00-18	5158690.818	330823.018	304.893m
BOREHOLE No. 00-19	5158738.128	330807.435	304.519m
BOREHOLE No. 00-20	5158785.837	330791.853	304.255m

NOTE 1:
The boundaries between soil strata have been established at the borehole locations only. The boundaries between boreholes are assumed based on borehole data.



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DRAWN BY: M.R.	CHECKED BY: MAM	

Match Line
13+642 &
Figures



CONT NO.
W.P. NO. 167 - 90 - 00

HWY 63
FOUNDATION INVESTIGATION - AREA 1
BOREHOLE LOCATIONS AND SOIL STRATA

FIGURE
4A

SCALE

10m 0 20m HORT (1:1000)
2m 0 4m VERT (1:200)

STRATIGRAPHY LEGEND

	TOPSOIL		SAND		SILTY SAND/ SANDY SILT
	PEAT		SAND & GRAVEL		SILT
	VARVED/ INTERLAYERED CLAYS & SILTS		CLAY		SILTY CLAY
	FILL		TILL		CRUSHED GRAVEL
	ASPHALT COATED				

LEGEND

- Borehole and Dynamic Cone Penetration Test
- Borehole
- N Blows/0.3 m
- Water Level at Time of Investigation
- A/R Auger Refusal at Elevation

Borehole No.	Co-ordinates		Elevation
	North	East	
BOREHOLE No. 00-42	5158830.717	330788.859	304.801m
BOREHOLE No. 00-43	5158878.228	330753.277	304.211m
BOREHOLE No. 00-44	5158925.736	330737.895	304.034m
BOREHOLE No. 00-45	5158973.246	330722.112	304.694m

NOTE 1:
The boundaries between soil strata have been established at the borehole locations only. The boundaries between boreholes are assumed based on borehole data.



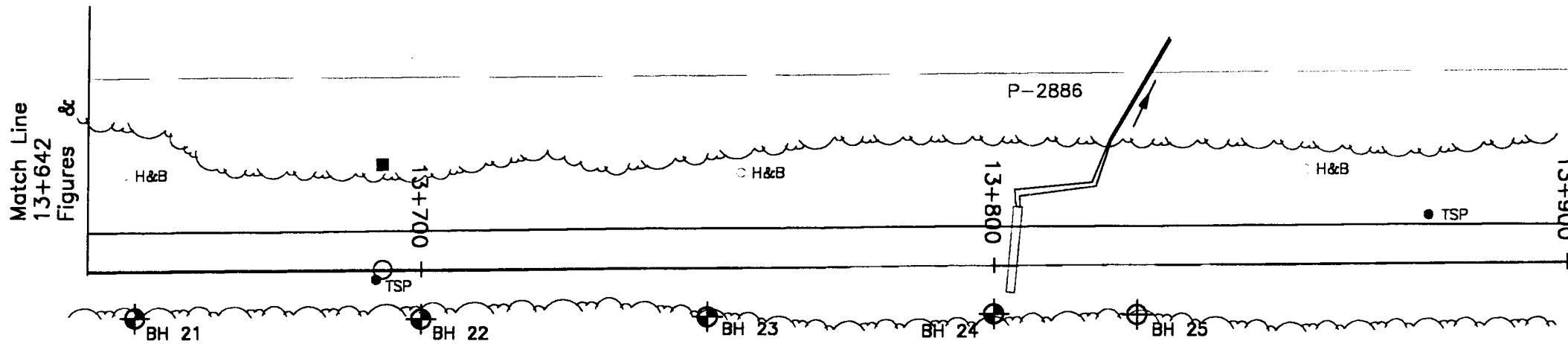
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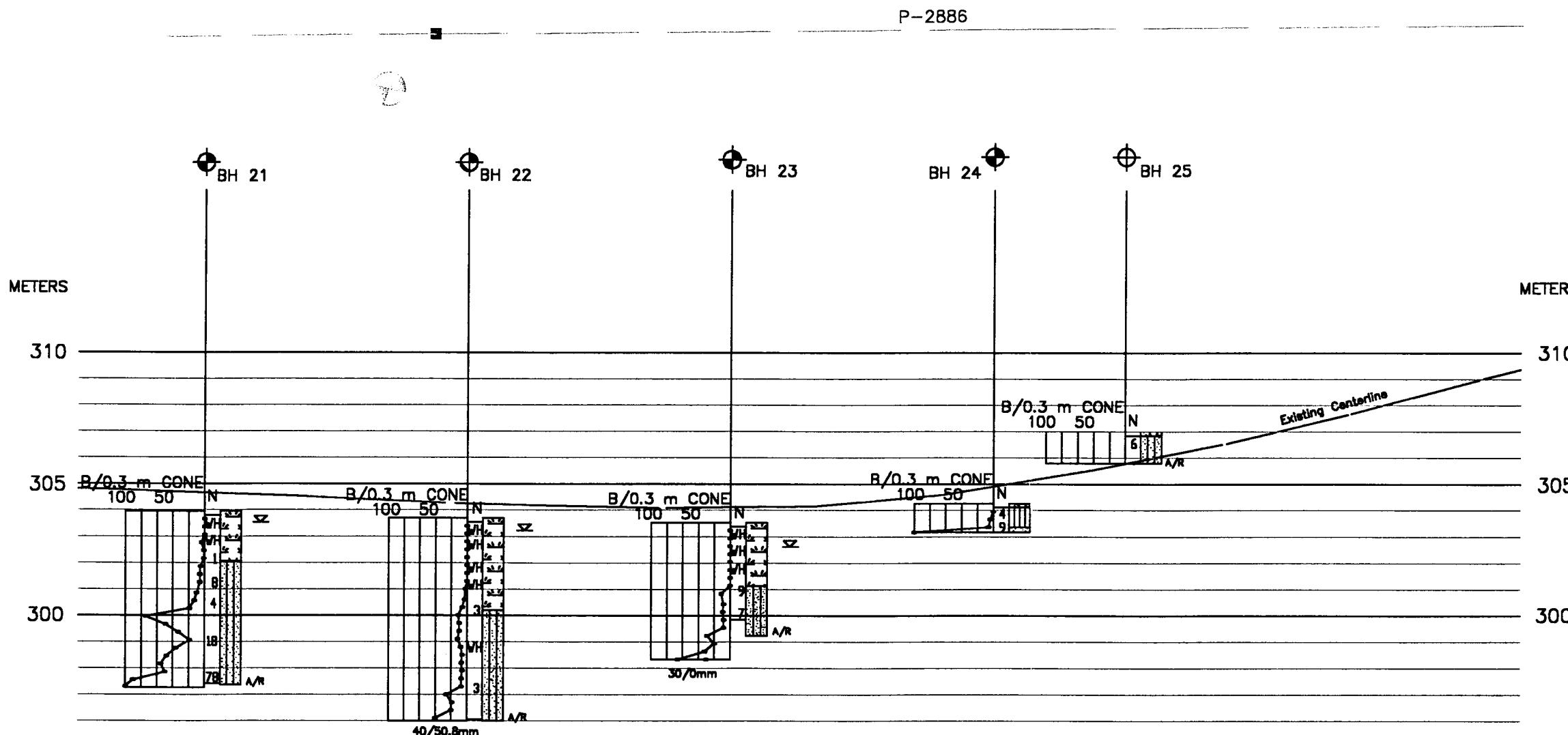
CONT NO.
W.P. NO. 167 - 90 - 00

HWY 63
FOUNDATION INVESTIGATION - AREA 1
BOREHOLE LOCATIONS AND SOIL STRATA

FIGURE
4B



P-2886



STRATIGRAPHY LEGEND

	TOPSOIL		SILTY SAND/ SANDY SILT
	PEAT		SAND & GRAVEL
	VARVED/ INTERLAYERED CLAYS & SILTS		SILT
	CLAY		SILTY CLAY
	FILL		TILL
	ASPHALT COATED		CRUSHED GRAVEL

LEGEND

- Borehole and Dynamic Cone Penetration Test
- Borehole
- N Blows/0.3 m
- SZ Water Level at Time of Investigation
- A/R Auger Refusal at Elevation

Borehole No.	Co-ordinates North	Co-ordinates East	Elevation
BOREHOLE No. 00-21	5158833.147	330776.271	303.983m
BOREHOLE No. 00-22	5158880.657	330760.688	303.703m
BOREHOLE No. 00-23	5158928.167	330745.108	303.537m
BOREHOLE No. 00-24	5158975.877	330729.524	304.270m
BOREHOLE No. 00-25	5158999.432	330721.733	306.999m

NOTE 1:
The boundaries between soil strata have been established at the borehole locations only. The boundaries between boreholes are assumed based on borehole data.



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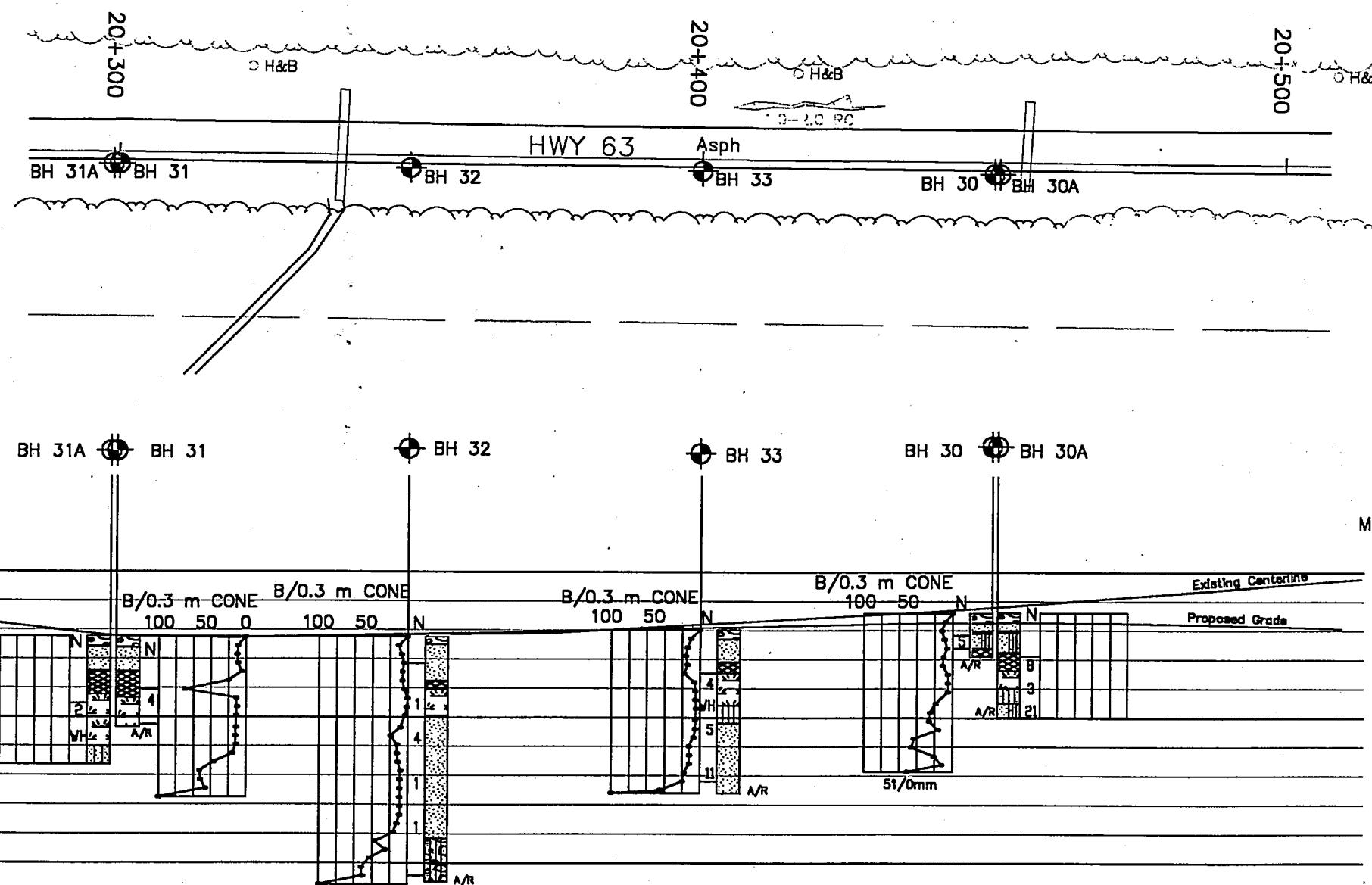
CONT NO.
W.P. NO. 167 - 90 - 00

HWY 63
FOUNDATION INVESTIGATION - AREA 2
BOREHOLE LOCATIONS AND SOIL STRATA

FIGURE
5A

610 X 19.17 CSP

610 X 15.41 CSP



NOTE: FOR DETAILED SUBSOIL AND BOREHOLE INFORMATION REFER TO RECORD OF BOREHOLE.

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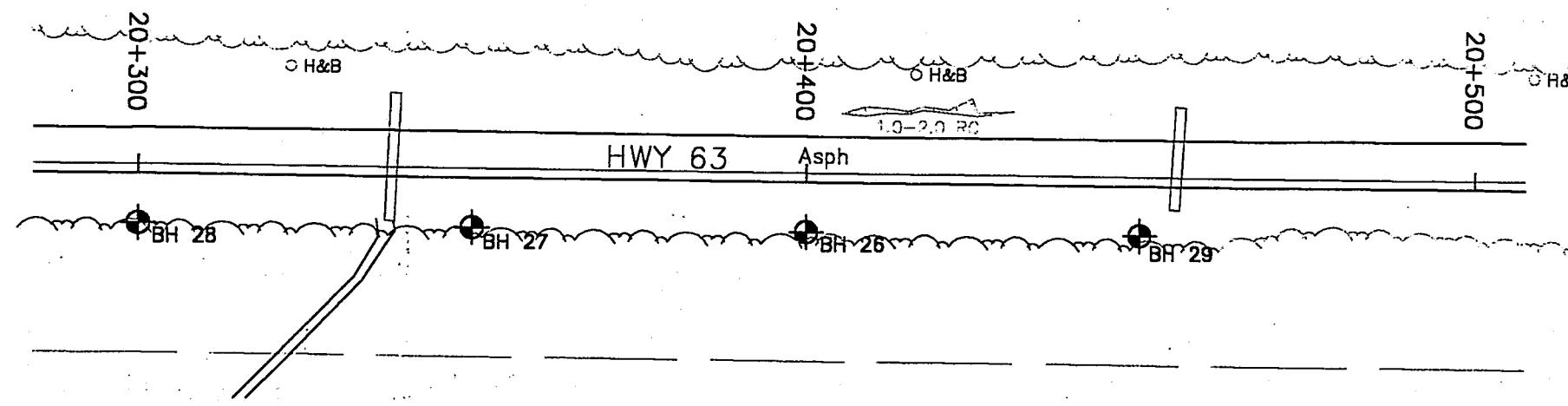
CONT NO.
W.P. NO. 167 - 90 - 00

HWY 63
FOUNDATION INVESTIGATION - AREA 2
BOREHOLE LOCATIONS AND SOIL STRATA

FIGURE
5B

610 X 19.17 CSP

610 X 15.41 CSP

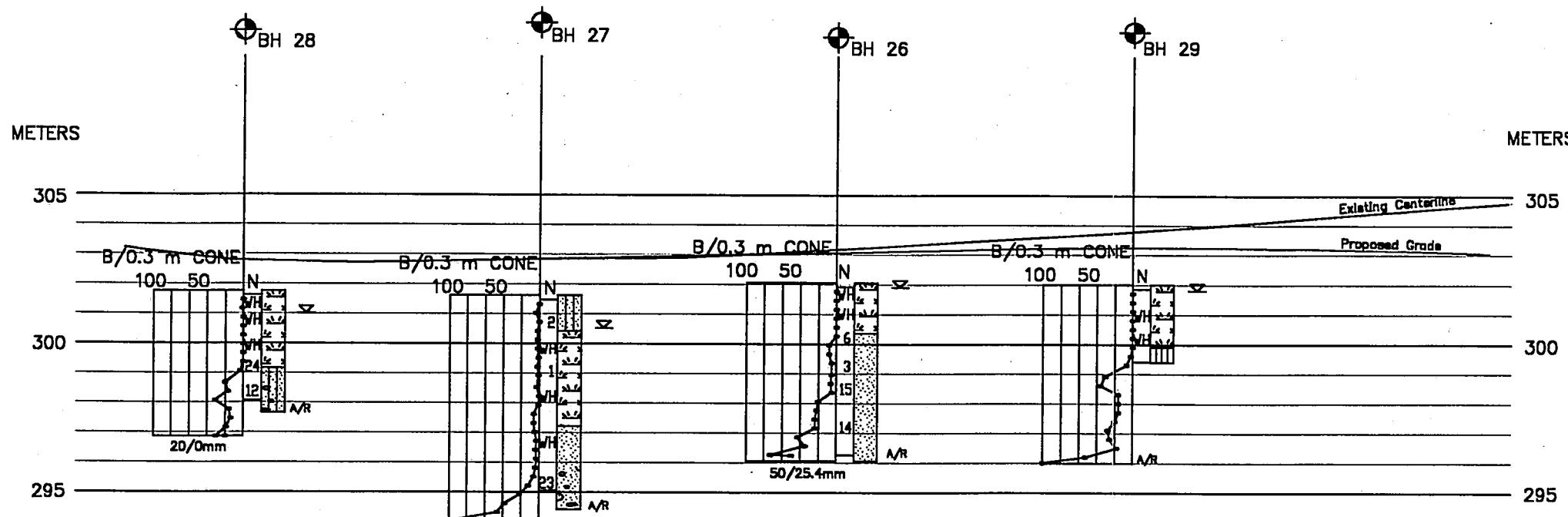


SCALE

10m 0 20m HORT (1:1000)
2m 0 4m VERT (1:200)

STRATIGRAPHY LEGEND

	TOPSOIL		SAND		SILTY SAND/ SANDY SILT
	PEAT		SAND & GRAVEL		SILT
	VARVED/ INTERLAYERED CLAYS & SILTS		CLAY		SILTY CLAY
	FILL (Shot Rock)		TILL		CRUSHED GRAVEL
	ASPHALT COATED				



LEGEND

- Borehole and Dynamic Cone Penetration Test
- Borehole
- N Blows/0.3 m
- Water Level at Time of Investigation
- A/R Auger Refusal at Elevation

Borehole No.	Co-ordinates North	Co-ordinates East	Elevation
BOREHOLE No. 00-28	5164692.568	331149.893	301.763m
BOREHOLE No. 00-27	5164721.345	331190.782	301.620m
BOREHOLE No. 00-26	5164750.121	331231.671	302.067m
BOREHOLE No. 00-29	5164778.898	331272.560	302.007m

NOTE 1:
The boundaries between soil strata have been established at the borehole locations only. The boundaries between boreholes are assumed based on borehole data.



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CONT NO.
W.P. NO. 167 - 90 - 00

HWY 63
FOUNDATION INVESTIGATION - AREA 3
BOREHOLE LOCATIONS AND SOIL STRATA

FIGURE
6

Match Line
20+821.85
Figure

SCALE

10m 0 20m HORT (1:1000)
2m 0 4m VERT (1:200)

STRATIGRAPHY LEGEND

	TOPSOIL		SAND		SILTY SAND/ SANDY SILT
	PEAT		SAND & GRAVEL		SILT
	VARVED/ INTERLAYERED CLAYS & SILTS		CLAY		SILTY CLAY
	FILL		TILL		CRUSHED GRAVEL
					ASPHALT COATED

METERS

305

Existing Contourline

300

Proposed Grade

295

290

285

280

305

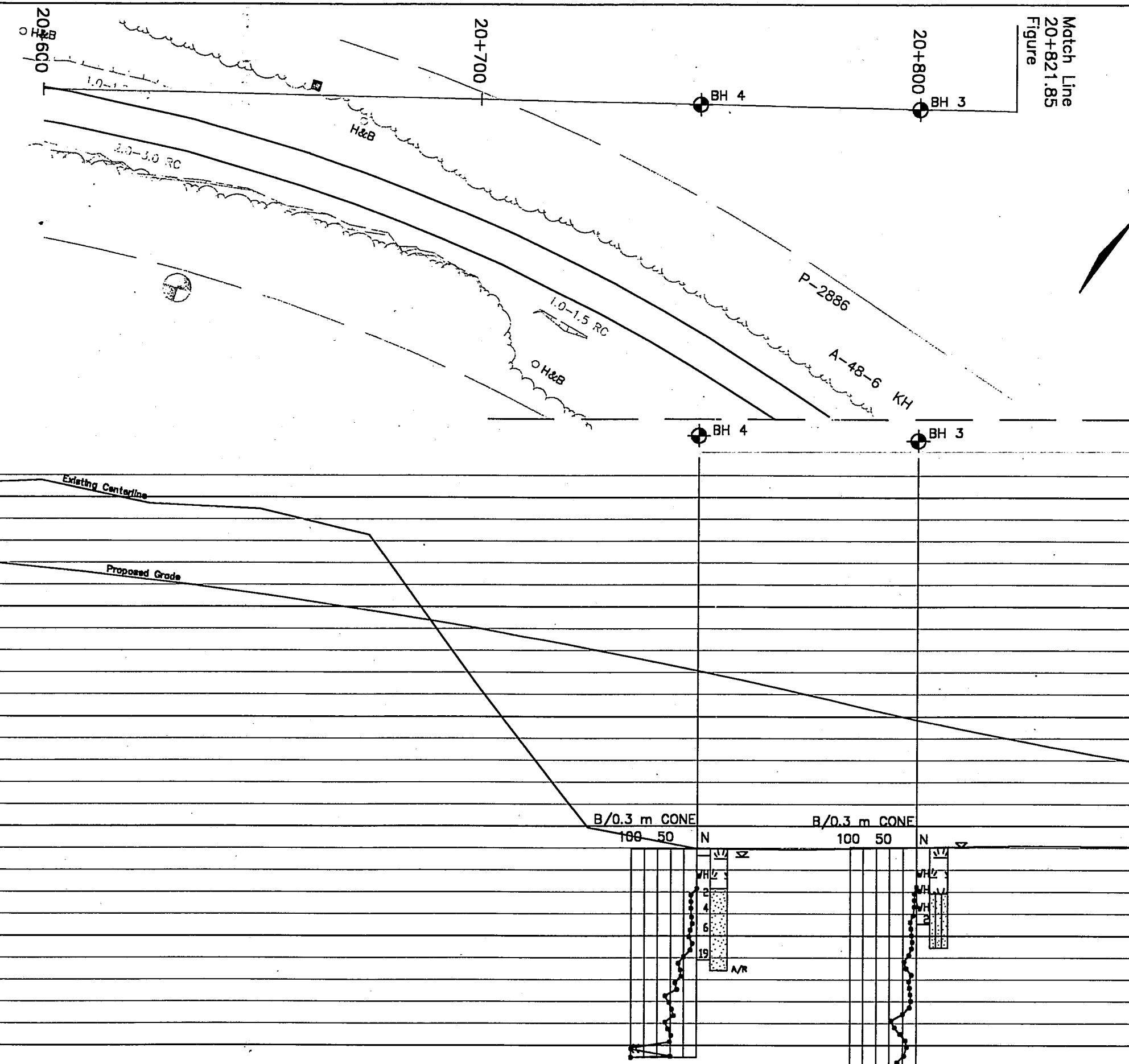
300

295

290

285

280



LEGEND			
	Borehole and Dynamic Cone Penetration Test		
	Borehole		
N	Blows/0.3 m		
	Water Level at Time of Investigation		
A/R	Auger Refusal at Elevation		
Borehole No.	Co-ordinates North	East	Elevation
BOREHOLE No. 00-04	5164961.839	331517.298	288.957m
BOREHOLE No. 00-03	5164990.816	331558.187	289.022m

NOTE 1:
The boundaries between soil strata have been established at the borehole locations only. The boundaries between boreholes are assumed based on borehole data.



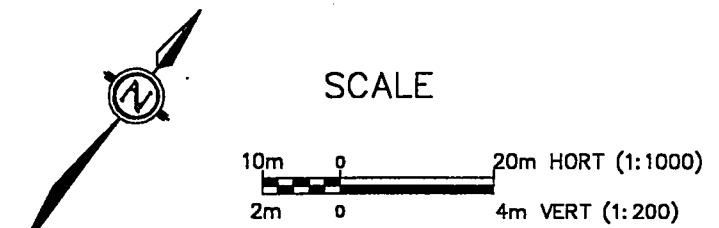
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CONT NO.
W.P. NO. 167 - 90 - 00

HWY 63
FOUNDATION INVESTIGATION - AREA 3
BOREHOLE LOCATIONS AND SOIL STRATA

FIGURE
7



Match Line
10+159.18
Figure

METERS
300

295

290

285

280

20+900

HOT 10+000.000 HWY 63
HOT 20+922.627 HWY 63

Match Line
20+821.85
Figure

METERS

300

295

290

285

280

B/0.3 m CONE

Existing Centerline

100

50

N

Proposed Grade

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B/0.3 m CONE

Borehole No. 00-02

5165033.781

331619.521

289.117m

BOREHOLE No. 00-01

5165080.985

331658.175

288.957m

BOREHOLE No. 00-05

5165089.781

331699.083

288.922m

BOREHOLE No. 00-08

5165118.538

331739.952

288.707m

BOREHOLE No. 00-07

5165147.315

331780.841

288.757m

NOTE 1:

The boundaries between soil strata have been established at the borehole locations only. The boundaries between boreholes are assumed based on borehole data.



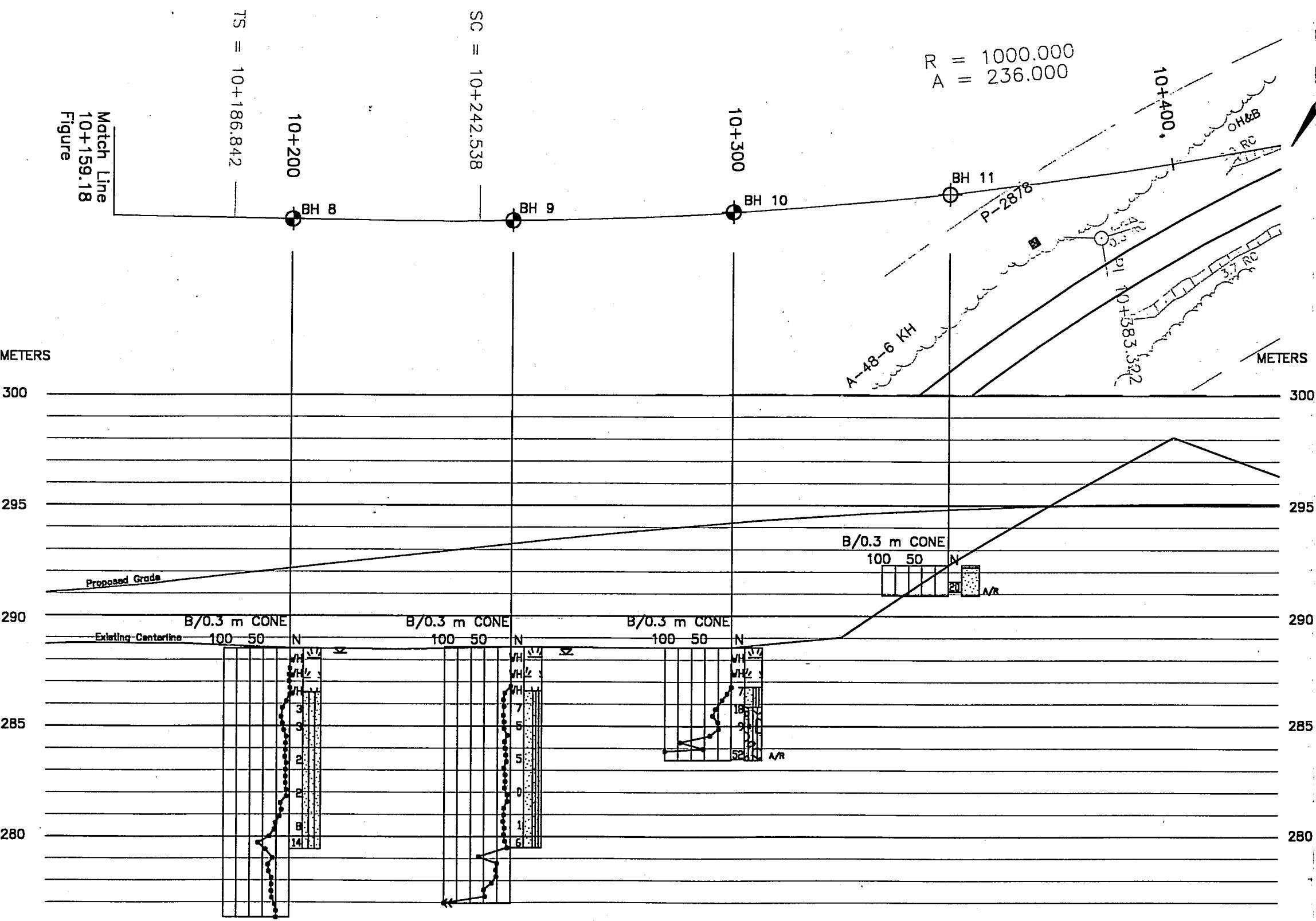
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DRAWN BY: M.R.	CHECKED BY: M.A.M.	

CONT NO.
W.P. NO. 167 - 90 - 00

HWY 63
FOUNDATION INVESTIGATION - AREA 3
BOREHOLE LOCATIONS AND SOIL STRATA

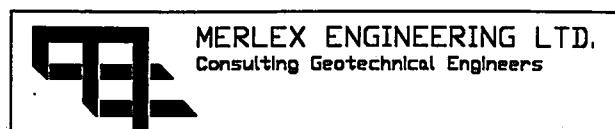
FIGURE
8



STRATIGRAPHY LEGEND		
TOPSOIL	SAND	SILTY SAND / SANDY SILT
PEAT	SAND & GRAVEL	SILT
VARVED / INTERLAYERED CLAYS & SILTS	CLAY	SILTY CLAY
FILL	TILL	CRUSHED GRAVEL
ASPHALT COATED		

LEGEND			
Borehole No.	Co-ordinates	East	Elevation
BOREHOLE No. 00-08	5185178.097	331821.728	288.517m
BOREHOLE No. 00-09	5185205.479	331882.180	288.587m
BOREHOLE No. 00-10	5185238.684	331801.255	288.582m
BOREHOLE No. 00-11	5185269.764	331838.724	292.424m

NOTE 1:
The boundaries between soil strata have been established at the borehole locations only. The boundaries between boreholes are assumed based on borehole data.



PROJECT: HWY. 63, Foundation Investigation	REFERENCE NO.: 00036F	DATE: August 28, 2000
DRAWN BY: M.R.	CHECKED BY: MAM	

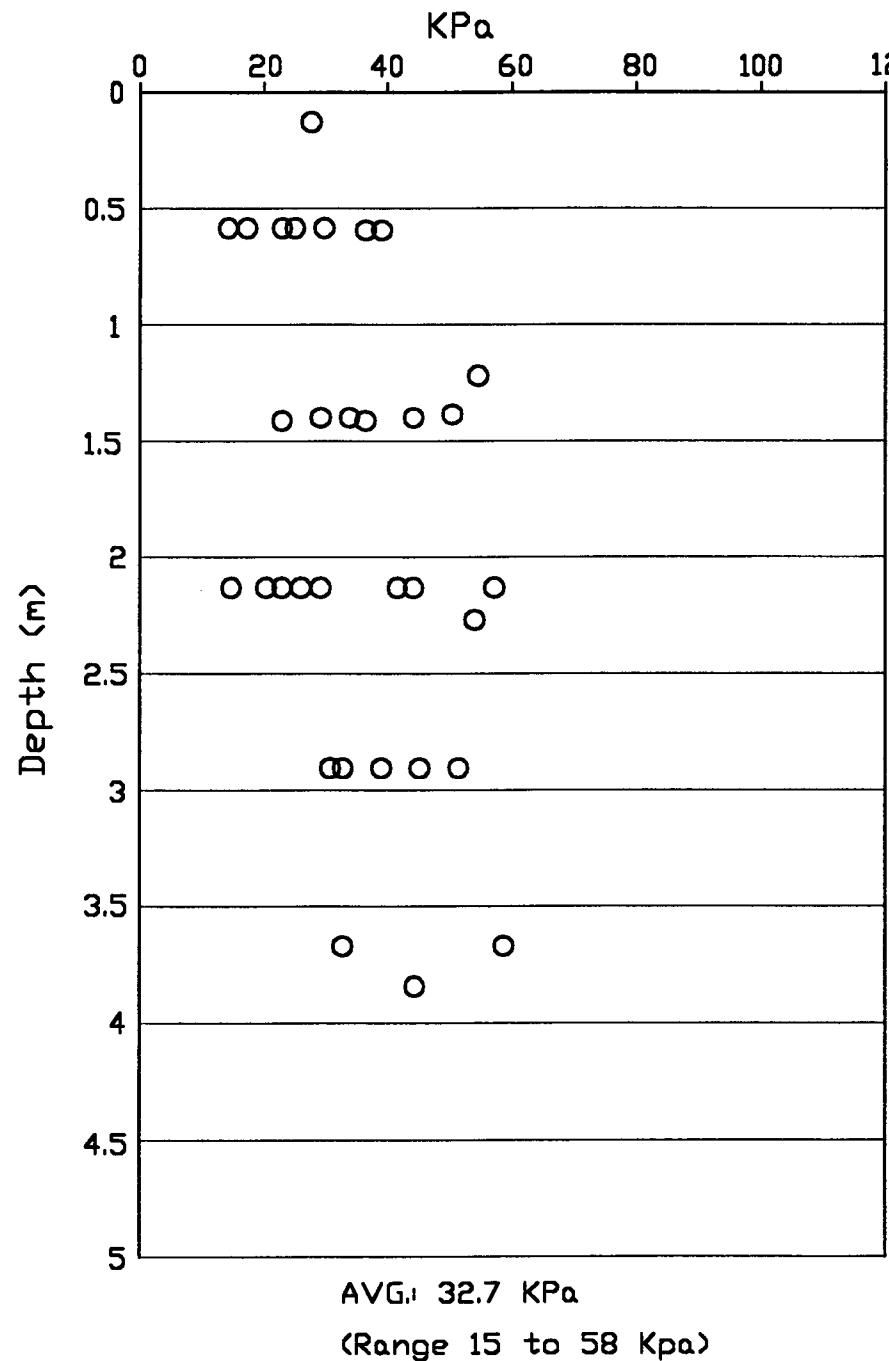
FIGURE 9

Undrained Shear Strength – Peat (No Surcharge)

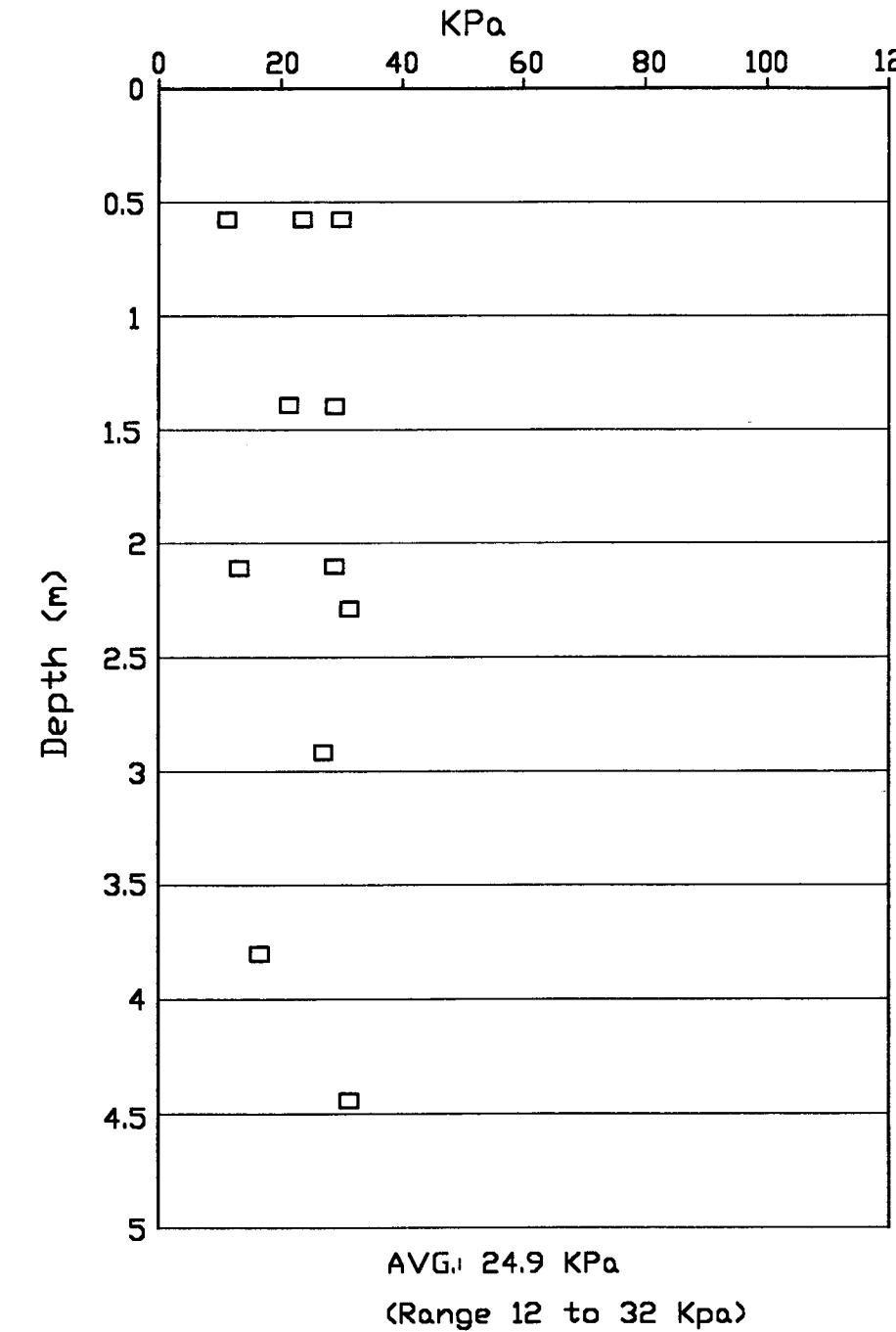
PEAT UNDRAINED SHEAR STRENGTH
AREAS 1, 2, and 3 (NO SURCHARGE)
HWY 63 - W.P. 167-90-00

FIGURE 9

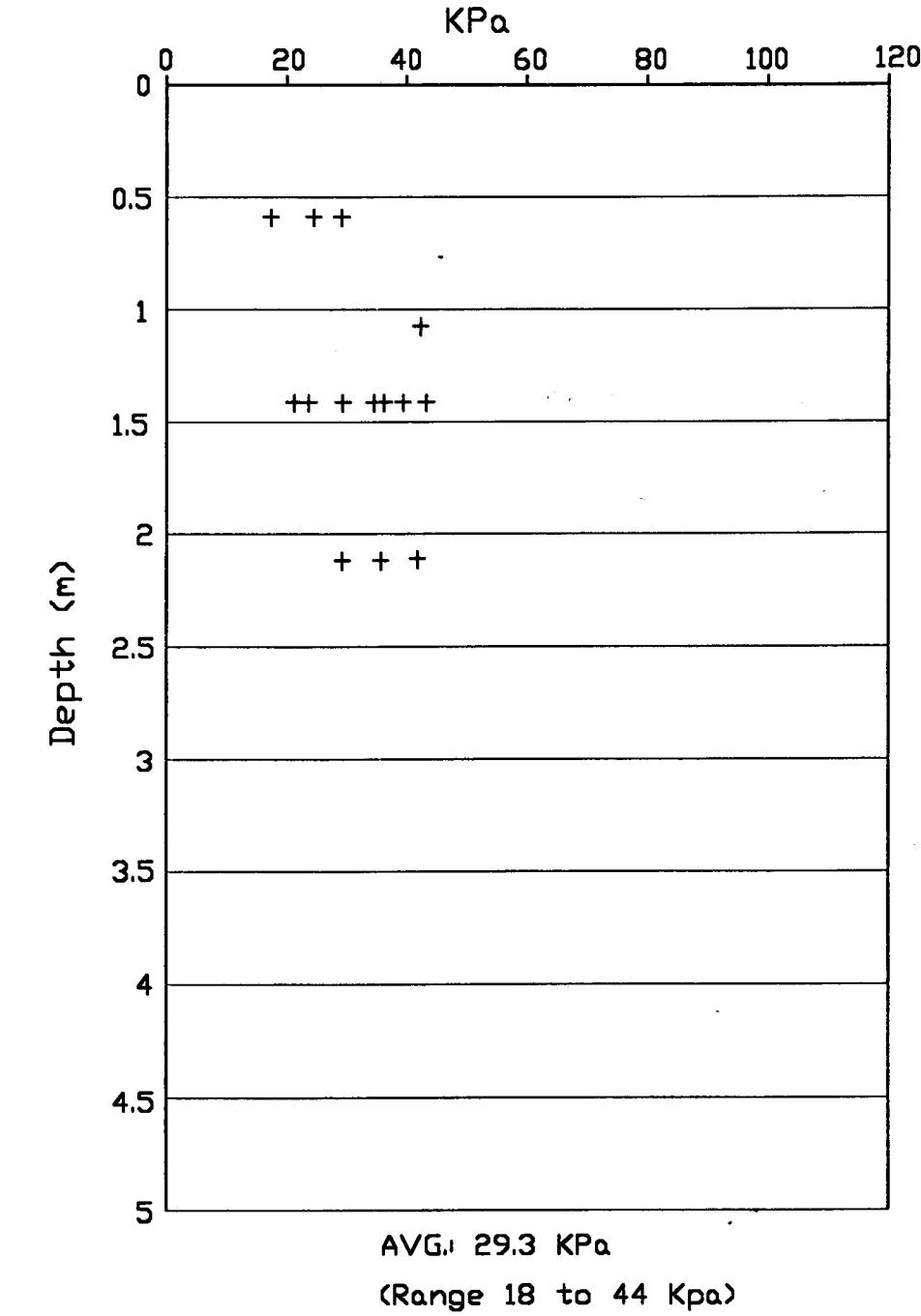
AREA 1- Sta. 13+250 to 13+825
Township of Jocko



AREA 2- Sta. 20+300 to 20+450
Township of Jocko



AREA 3- Sta. 20+750(Twp Jocko) to
10+350(Twp of Clarkson)



NOTE: No Surcharge refers to areas outside the existing area affected by the overlying roadway.

Date: November 13, 2000



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Drawn: M.R.

Project: 00036

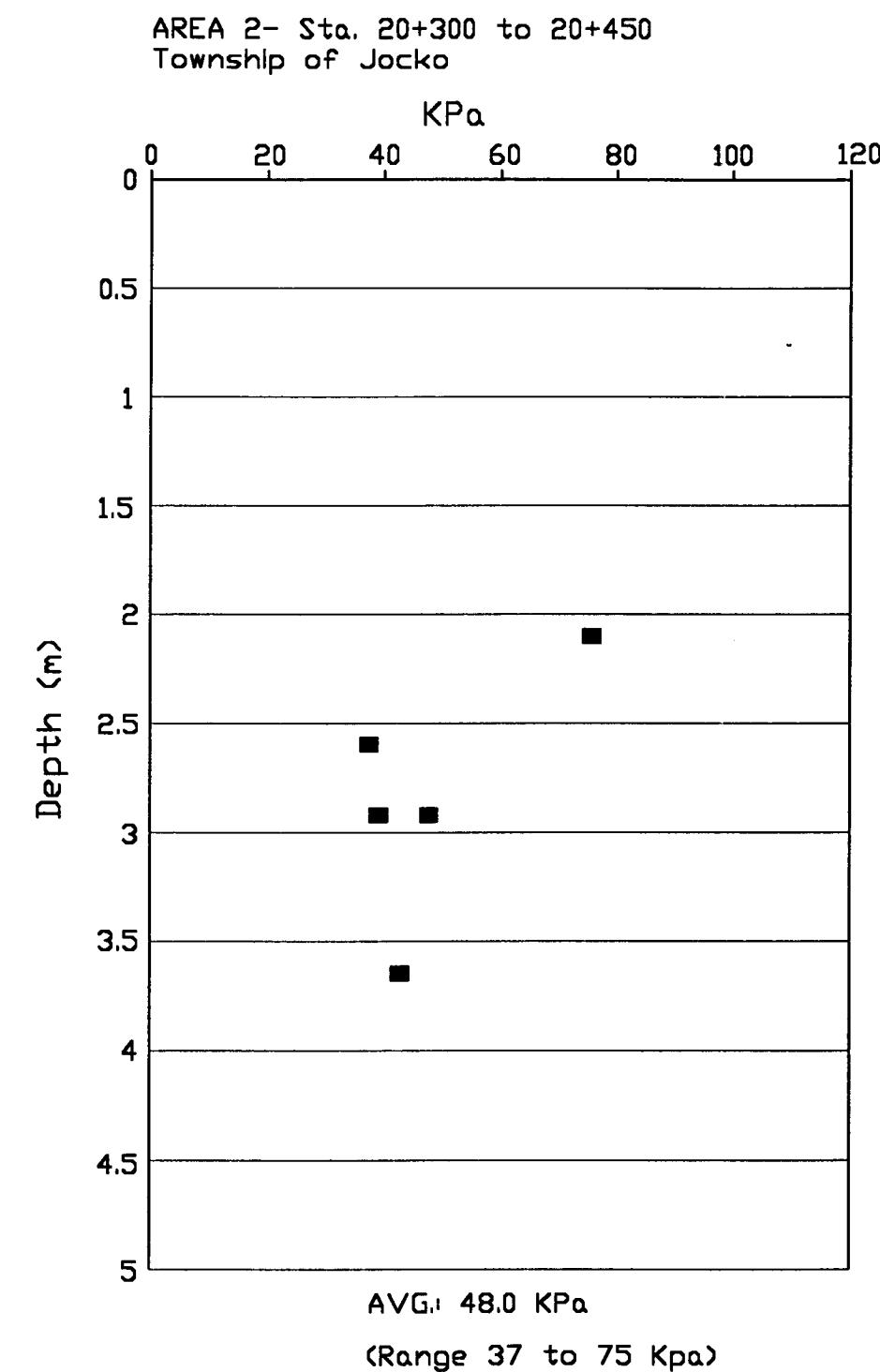
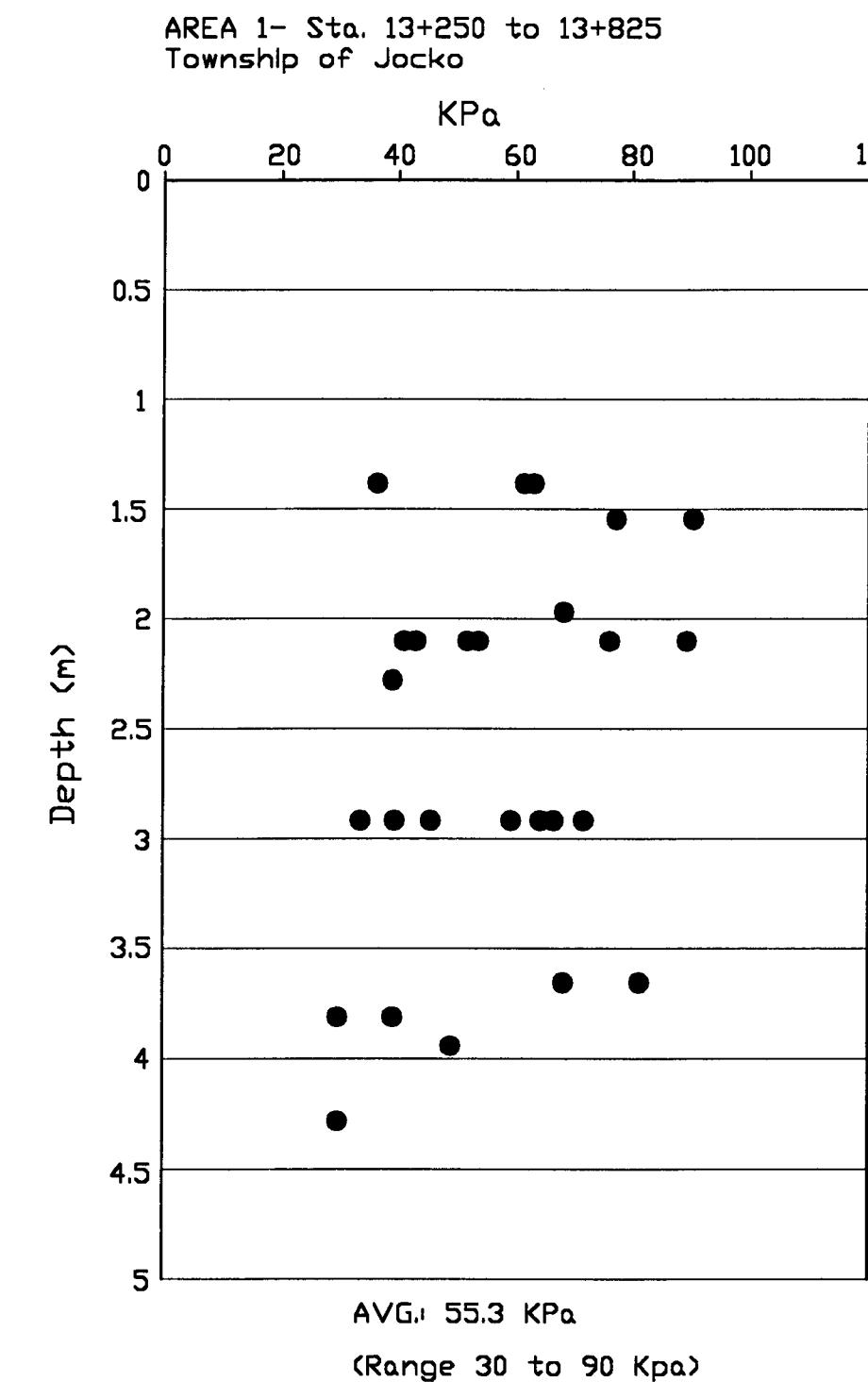
Chkd: M.A.M.

FIGURE 10

Undrained Shear Strength – Peat (With Surcharge)

PEAT UNDRAINED SHEAR STRENGTH
AREAS 1, 2, and 3 (UNDER EXIST PLATFORM)
HWY 63 - W.P. 167-90-00

FIGURE 10



Date: November 13, 2000

Project: 00036



Drawn: M.R.

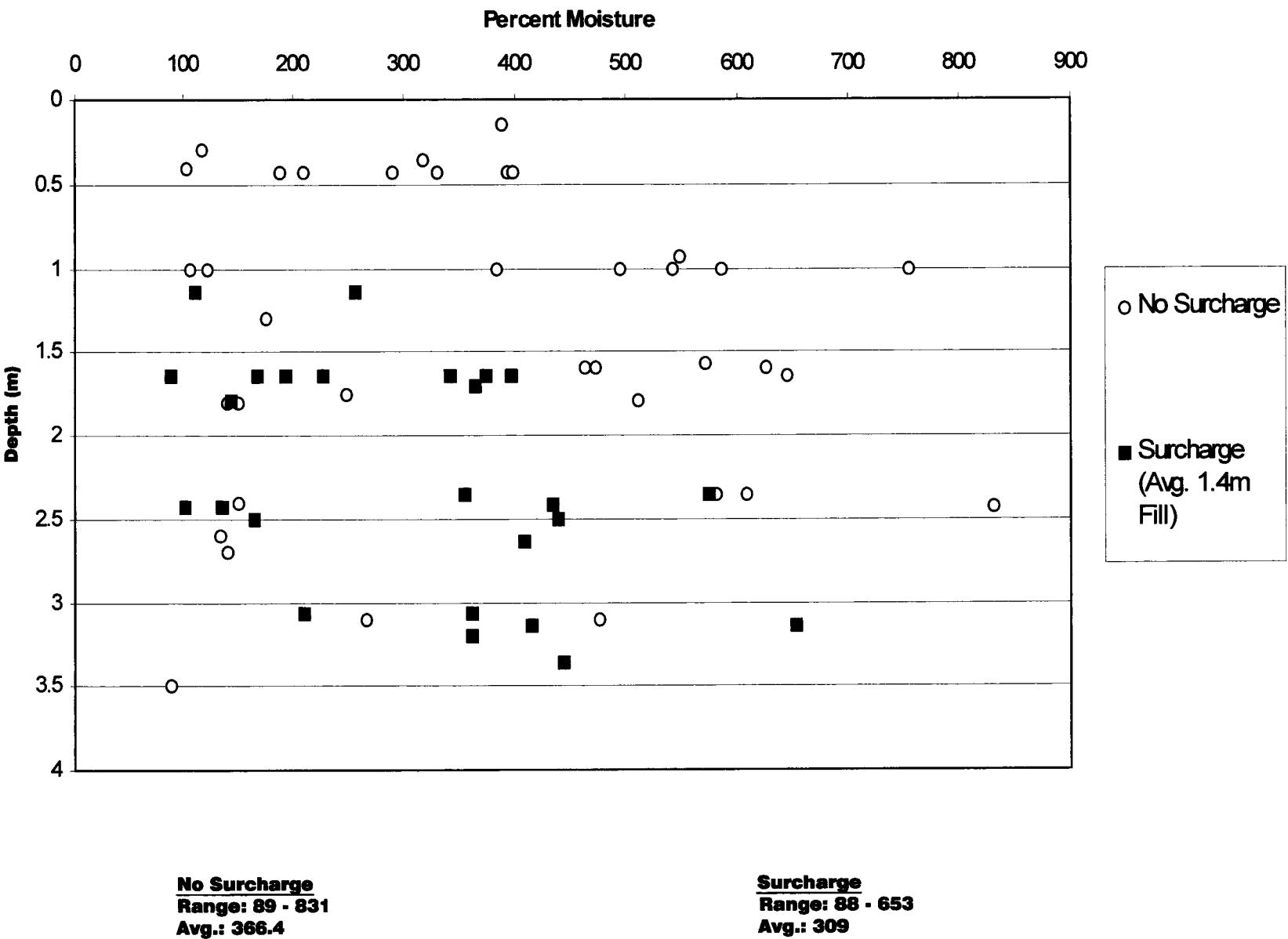
Chkd: M.A.M.

FIGURE 11 TO 13

Natural Moisture Content – Peat (Areas 1, 2 and 3)

Natural Moisture Content of Peat
 Area 1 Sta. 13+250 to 13+825
 Twp. Jocko

FIGURE 11



Date: November 13, 2000
 Project: 00036

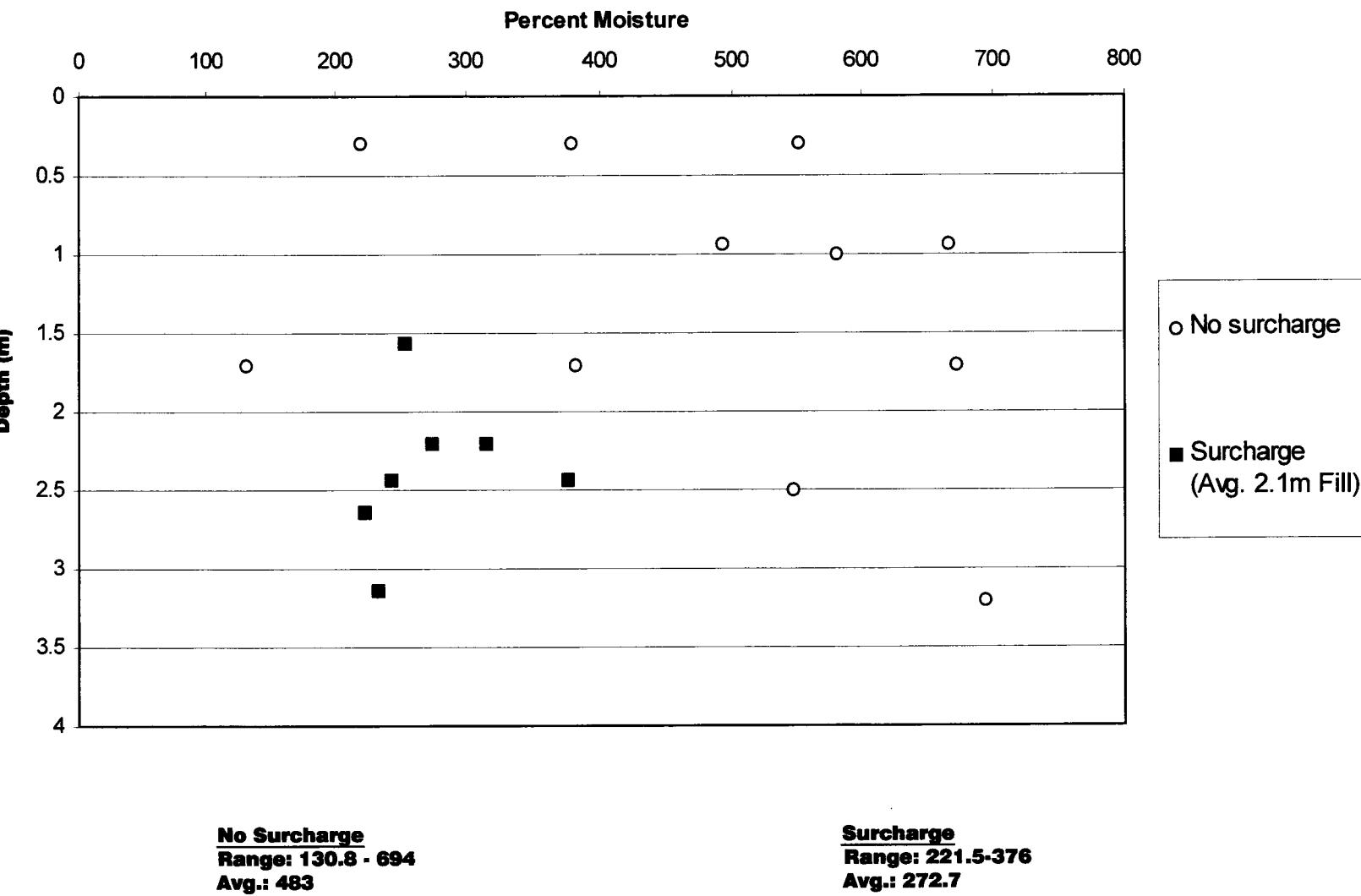


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 Consulting Geotechnical Engineers

Drawn: MR
 Chkd: MAM

Natural Moisture Content of Peat
Area 2 Sta. 20+300 to 20+450
Twp. Jocko

FIGURE 12



Date: November 13, 2000

Project: 00036



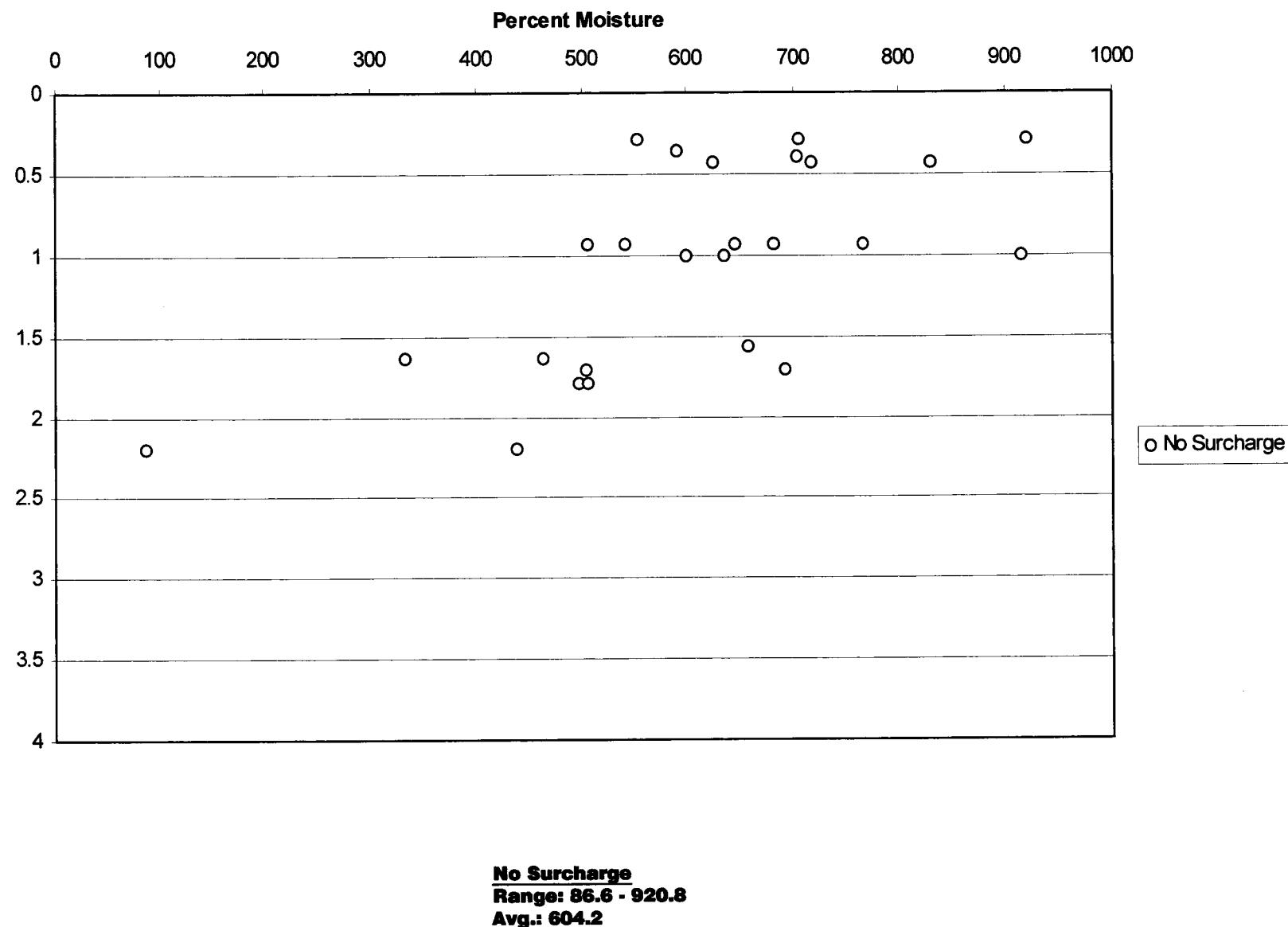
MERLEX ENGINEERING LTD.
Consulting Geotechnical Engineers

Drawn: MR

Chkd: MAM

Natural Moisture Content of Peat
Area 3 Sta. 20+750 (Twp Jocko) to 10+350 (Twp Clarkson)

FIGURE 13



Date: November 13, 2000

Project: 00036



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Consulting Geotechnical Engineers

Drawn: MR

Chkd: MAM

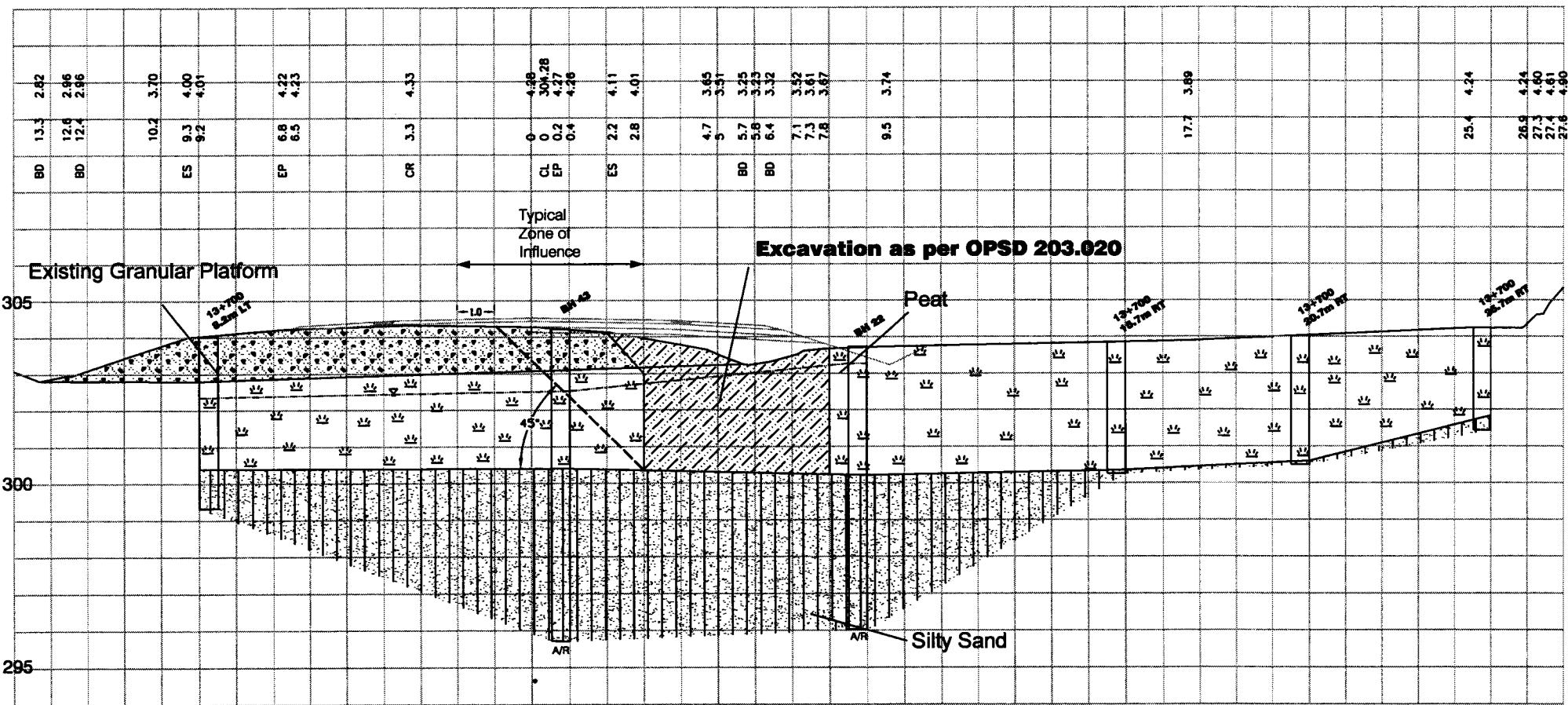
FIGURE 14

Cross-Sectional Schematic – Station 13+700 (Typ.)

**Cross-sectional Schematic
Sta. 13+700 (Typical)**

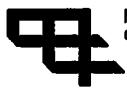
FIGURE 14

1 Squ.= 1 m



Date: January 3, 2000

Project: 00036.....



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Consulting Geotechnical Engineers

Drawn: MR.....

Chkd: MAM.....

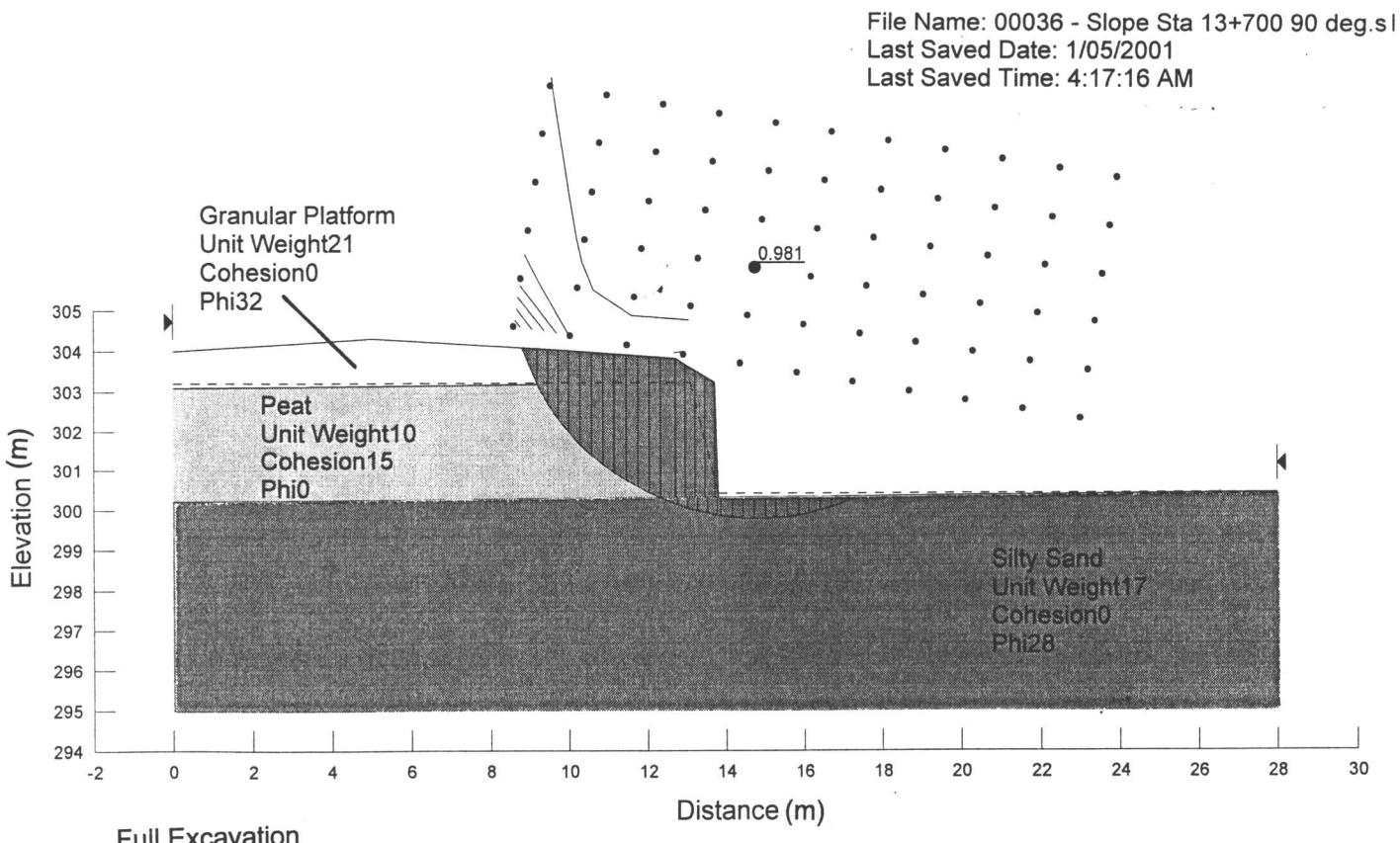
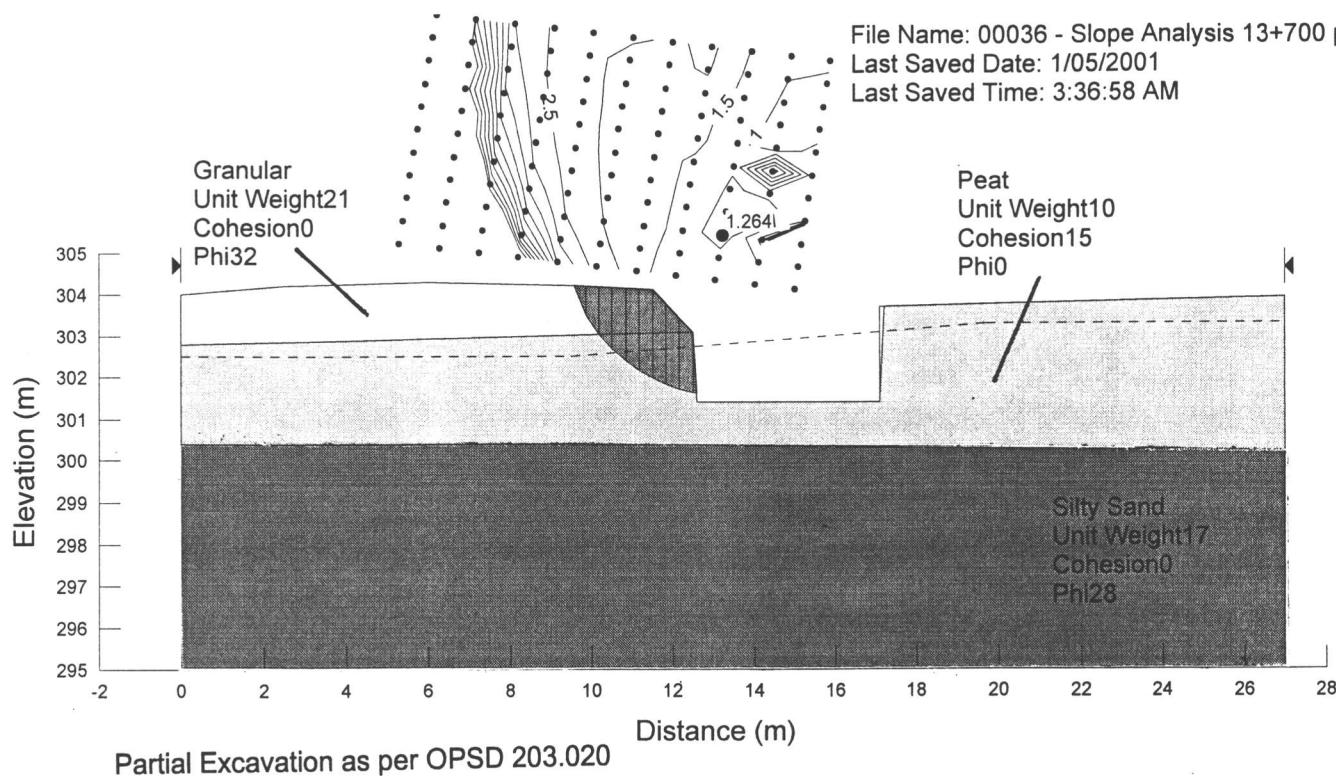
FIGURE 15

Slope Stability Cross-Section (Area 1)

Slope Stability Analysis - Area 1

Station 13+700 Hwy 63

FIGURE 15



Date: January 4, 2001

Project: 00036

Drawn: MR

Chkd: MAM



MERLEX ENGINEERING LTD.
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APPENDIX A

Geotechnical Data and Pedo – Area 1
Geotechnical Data and Pedo – Area 2
Pedological Sketches – Area 3

GEOTECHNICAL SURVEY DATA
W.P. 167 - 90 - 00
JOCKO TWP

AREA 1

METRIC

13+250 13.3 m Lt C/L D-1.4 0 - 2.0 Fib Muck Amor wet @ 300 2.0 - 3.2 Si F Sa Tr Gr	13+300 7.7 m Rt C/L D-1.5 0 - 2.0 Muck Amor 2.0 NFP Bl/BR	13+475 8.3 m Lt C/L D-0 0 - 2.0 Cr Gr 280 - 330 PST 330 - 800 Med F Sa Tr Gr Tr Sl OCC Cob 800 - 1.5 F Sa W Sl (wet@1.2) 1.5 - 4.8 Muck Amor 3.5 - 3.7 Si F Sa Tr Gr	13+625 13.3 m Lt C/L D-1.0 0 - 2.0 Fib Muck Amor wet @ 300 2.5 - 3.2 Si F Sa Tr Gr	13+797 6.9 m Lt C/L D-0 0 - 300 Cr Gr 300 - 550 Med F Sa Tr Sl Tr Cob 550 - 700 F Sa Some Si 700 - 1.5 Si F Sa wet @ 1.0 1.5 - 2.0 Muck Amor 2.3 NFP Bl/BR
13+250 8.3 m Lt C/L D-0 0 - 300 Cr Gr 300 - 750 Med F Sa Tr Gr Tr Sl OCC Cob 750 - 1.5 F Sa W Sl 1.5 - 3.5 Muck Amor 3.5 - 3.7 Si F Sa Tr Gr	13+325 13.3 m Lt C/L D-1.7 0 - 500 Fib Muck Amor wet @ 200 500 NFP Bl/BR	13+500 13.3 m Lt C/L D-1.1 0 - 2.1 Fib Muck Amor 2.1 - 3.2 Si F Sa	13+650 13.3 m Lt C/L D-1.3 0 - 1.3 Fib Muck Amor wet @ Surf 1.3 - 2.0 Si F Sa Tr Gr	13+800 1.6 m Rt C/L D-0 0 - 290 Cr Gr 290 - 550 Med F Sa Tr Gr Tr Sl Tr Cob 550 - 1.2 F Sa W Sl Tr Gr 1.2 NFP Bl/BR
13+250 1.7 m Rt C/L D-0 0 - 140 Cr Gr 140 - 240 Asph 240 - 620 Med F Sa Tr Gr Tr Sl 620 - 1.4 F Sa W Sl 1.4 - 1.7 Muck Amor 1.7 - 2.0 F Sa W Sl	13+325 1.7 m Rt C/L D-0 0 - 240 Asph 240 - 350 AC Gran 350 - 700 Med F Sa Tr Gr Tr Sl 700 - 1.5 Si F Sa 1.5 - 2.0 Muck Amor 2.0 - 3.0 Med F Sa Some Si 3.0 NFP Bl/BR	13+500 8.3 m Lt C/L D-0 0 - 280 Cr Gr 280 - 300 PST 300 - 750 Med F Sa Tr Gr Tr Sl OCC Cob 750 - 1.4 F Sa W Sl 1.4 - 4.8 Muck Amor 4.8 - 5.0 Si F Sa Tr Gr	13+650 8.1 m Lt C/L D-0 0 - 260 Cr Gr 260 - 280 PST 280 - 550 Med F Sa Some Gr Tr Sl 550 - 1.5 F Sa W Sl 1.4 - 4.2 Muck Amor 4.2 - 4.5 Si F Sa	13+800 6.7 m Rt C/L D-1.7 0 - 300 Wat 300 - 1.6 Si F Sa Tr Gr 1.6 NFP Bl/BR
13+250 7.7 m Rt C/L D-1.4 0 - 3.8 Muck Amor 3.8 - 4.6 Si Sa	13+325 7.7 m Rt C/L D-1.4 0 - 1.7 Muck Amor 1.7 - 2.0 Si Sa 2.0 NFP Bl/BR	13+500 5.5 m Lt C/L D-0 0 - 80 Asph 60 - 150 Cr Gr 150 - 180 Asph 180 - 320 Cr Gr	13+650 1.7 m Rt C/L D-0 0 - 240 Cr Gr 240 - 600 Med F Sa Tr Gr Tr Sl Tr Cob 600 - 1.3 F Sa W Sl Tr Gr 1.3 - 3.7 Muck Amor 3.7 - 4.0 Si F Sa	13+802.812 8.1 m Lt C/L D-0 0 - 280 Cr Gr 280 - 500 Med F Sa Tr Gr Tr Sl Tr Cob 500 - 1.4 Si F Sa 1.4 - 2.2 Muck Amor 2.2 - 3.0 Si Some F Sa
13+425 7.7 m Rt C/L D-1.0 0 - 3.7 Muck Amor 3.7 - 4.5 Si F Sa	13+350 13.3 m Lt C/L D-1.7 0 - 1.0 Fib Muck Amor wet @ 300 1.0 - 1.5 Si F Sa Tr Gr	13+500 13.3 m Lt C/L D-1.1 0 - 1.0 Fib Muck Amor 1.5 - 4.3 Muck Amor 4.3 - 5.0 Si F Sa	13+650 7.7 m Rt C/L D-1.1 0 - 1.7 Muck Amor 1.7 - 2.5 Si F Sa	13+803 15.3 m Lt C/L D-1.7 0 - 1.3 Muck Amor 1.3 - 2.0 Si Some F Sa
13+450 13.3 m Lt C/L D-1.2 0 - 2.2 Fib Muck Amor 2.2 - 3.2 Si Some F Sa	13+350 8.1 m Lt C/L D-0 0 - 300 Cr Gr 300 - 900 Med F Sa Tr Gr Tr Sl OCC Cob 900 - 1.7 F Sa W Sl 1.7 - 3.0 Muck Amor 3.0 - 4.0 Si F Sa Tr Cl	13+500 1.7 m Rt C/L D-0 0 - 220 Cr Gr 220 - 320 Asph 320 - 750 Med F Sa Tr Gr Tr Sl 750 - 1.4 F Sa W Sl 1.4 - 4.2 Muck Amor 4.2 - 5.0 Si F Sa	13+700 13.3 m Lt C/L D-900 0 - 280 Cr Gr 280 - 290 PST 290 - 800 Med F Sa Tr Gr Tr Sl 800 - 1.2 F Sa W Sl 1.2 - 3.6 Muck Amor 3.6 - 4.7 Si F Sa	13+808 6.9 m Lt C/L D-0 0 - 220 Cr Gr 220 - 650 Med F Sa Tr Sl Tr Gr 650 - 750 F Sa Some Si 750 - 1.8 Si F Sa 1.8 - 2.2 Muck Amor 2.2 - 2.5 Si Some F Sa
13+450 8.1 m Lt C/L D-0 0 - 280 Cr Gr 280 - 330 PST 330 - 800 Med F Sa Tr Gr Tr Sl OCC Cob 800 - 1.5 F Sa W Sl wet @ 1.2 1.5 - 4.8 Muck Amor 4.8 - 5.2 Si F Sa Tr Cl	13+350 1.7 m Rt C/L D-0 0 - 370 Cr Gr 370 - 860 Med F Sa Tr Gr Tr Sl 660 - 700 PST 700 - 1.8 F Sa W Sl 1.8 - 4.5 Muck Amor 4.5 - 4.6 Org Si 4.6 - 4.7 Med F Sa Some Si 4.7 NFP Bl/BR	13+500 7.7 m Rt C/L D-900 0 - 3.5 Muck Amor wet @ Surf 3.5 - 4.5 Si F Sa	13+700 1.7 m Lt C/L D-0 0 - 260 Cr Gr 260 - 280 PST 280 - 800 Med F Sa Tr Gr Tr Sl 800 - 1.2 F Sa W Sl 1.2 - 3.6 Muck Amor 3.6 - 4.7 Si F Sa	13+808 8.1 m Lt C/L D-0 0 - 280 Cr Gr 280 - 750 Med F Sa Tr Gr Tr Sl OCC Cob 750 - 1.6 F Sa W Sl 1.6 - 2.2 Muck Amor 2.2 - 2.7 Si F Sa
13+250 7.7 m Rt C/L D-1.3 0 - 100 Si Org 100 - 1.8 Si F Sa wet @ 200	13+350 7.7 m Rt C/L D-1.6 0 - 300 Wat 300 - 3.0 Muck Amor 3.0 - 3.1 Med F Sa Some Si 3.1 NFP Bl/BR	13+500 1.7 m Lt C/L D-1.1 0 - 2.0 Fib Muck Amor Fr Wt @ 200 2.0 - 2.5 Si F Sa Tr Gr Tr Cob 2.5 NFP Bl/BR	13+700 1.7 m Lt C/L D-0 0 - 300 Cr Gr 300 - 750 Med F Sa Tr Gr Tr Sl Tr Cob 750 - 1.3 F Sa W Sl Tr Gr 1.3 - 3.7 Muck Amor 3.7 - 4.8 Si F Sa	13+813 8.1 m Lt C/L D-0 0 - 280 Cr Gr 280 - 750 Med F Sa Tr Gr Tr Sl OCC Cob 750 - 1.6 F Sa W Sl 1.6 - 2.2 Muck Amor 2.2 - 2.7 Si F Sa
13+275 13.3 m Lt C/L D-1.5 0 - 1.0 Fib Muck Amor Fr Wat @ Surf 1.0 - 1.4 Muck Amor RF 1.4 - 1.7 Si F Sa Tr Gr	13+375 13.3 m Lt C/L D-1.7 0 - 1.8 Fib Muck Amor 1.8 - 3.2 Si F Sa Tr Gr	13+500 13.3 m Lt C/L D-1.3 0 - 2.0 Fib Muck Amor 36ELS115 w @ 200 = 610.9 2.0 - 3.0 Si F Sa Tr Gr	13+700 7.7 m Lt C/L D-800 0 - 3.4 Muck Amor 3.4 - 4.5 Si F Sa	13+823 8.2 m Lt C/L D-0 0 - 240 Cr Gr 240 - 270 PST 270 - 900 Med F Sa Tr Gr Tr Sl OCC Cob 900 - 1.7 F Sa W Sl 1.7 - 2.0 Si Org 2.0 - 2.3 F Sa W Sl
13+275 8.3 m Lt C/L D-0 0 - 150 Cr Gr 150 - 200 Asph 200 - 750 Med F Sa Tr Gr Tr Sl OCC Cob 750 - 1.4 F Sa W Sl 1.4 - 3.8 Muck Amor 3.8 - 4.0 Si F Sa Tr Gr	13+375 1.7 m Lt C/L D-0 0 - 270 Cr Gr 270 - 1.7 Med F Sa Tr Gr Tr Sl wet @ 1.2 1.7 - 5.5 Muck Amor 5.5 - 5.7 Si Sa	13+500 9.8 m Lt C/L D-400 0 - 280 Cr Gr 280 - 600 Med F Sa Tr Gr Tr Sl OCC Cob 600 - 1.0 F Sa W Sl 1.0 - 3.4 Muck Amor 3.4 - 4.0 Si F Sa Tr Gr	13+725 7.7 m Lt C/L D-800 0 - 200 Wat 200 - 3.4 Muck Amor 3.4 - 4.2 Si F Sa	13+850 19.3 m Lt C/L D-2.6 0 - 200 Si Org 200 - 2.6 F Sa W Sl wet @ 500
13+275 1.7 m Lt C/L D-0 0 - 260 Asph 260 - 340 AC Gran 340 - 600 Med F Sa Tr Gr Tr Sl 600 - 1.5 Si F Sa wet @ 1.5 1.5 - 2.2 Muck Amor 2.2 - 2.8 Med F Sa Some Si 2.8 NFP Bl/BR	13+375 7.7 m Lt C/L D-1.4 0 - 3.8 Muck Amor 3.8 - 4.6 Si Sa	13+500 7.7 m Lt C/L D-0 0 - 280 Cr Gr 300 - 750 Med F Sa Tr Gr Tr Sl OCC Cob 750 - 1.4 F Sa W Sl 1.4 - 3.7 Muck Amor 3.7 - 5.5 Si F Sa	13+750 8.3 m Lt C/L D-0 0 - 240 Cr Gr 240 - 290 PST 290 - 850 Med F Sa Tr Gr Tr Sl 850 - 1.3 F Sa W Sl 1.3 - 3.3 Muck Amor 3.3 - 4.7 Si F Sa	13+850 8.0 m Lt C/L D-0 0 - 240 Cr Gr 240 - 290 PST 290 - 850 Med F Sa Tr Gr Tr Sl 850 - 1.3 F Sa W Sl 1.3 - 3.3 Muck Amor 3.3 - 4.7 Si F Sa
13+275 7.7 m Lt C/L D-1.1 0 - 1.4 Fib Muck Amor, wet 1.4 NFP Bl/BR	13+400 7.7 m Lt C/L D-0 0 - 280 Cr Gr 280 - 480 Asph 480 - 800 Med F Sa Tr Gr Tr Sl OCC Cob 800 - 1.6 F Sa W Sl 1.6 - 3.0 Muck Amor 3.0 - 4.2 Fib Muck Amor 4.2 - 5.0 Si F Sa Tr Cl	13+500 1.7 m Lt C/L D-0 0 - 220 Cr Gr 220 - 270 Asph 270 - 750 Med F Sa Tr Gr Tr Sl 750 - 1.4 F Sa W Sl Tr Gr 1.4 - 4.2 Muck Amor 4.2 - 4.5 Si F Sa	13+750 1.5 m Lt C/L D-0 0 - 290 Cr Gr 290 - 700 Med F Sa Tr Gr Tr Sl Tr Cob 700 - 1.3 F Sa W Sl Tr Gr 1.3 - 3.5 Muck Amor 3.5 - 3.8 Si F Sa	13+850 1.6 m Lt C/L D-0 0 - 250 Cr Gr 250 - 500 Med F Sa Tr Gr Tr Sl Tr Cob wet @ 500 500 - 1.5 Si F Sa W Sl Tr Gr 1.5 NFP Bl/BR
13+300 13.3 m Lt C/L D-1.6 0 - 1.0 Fib Muck Amor wet @ 500 1.0 - 1.5 Muck Amor RF 1.5 - 3.3 Si F Sa Tr Gr	13+400 7.7 m Lt C/L D-0 0 - 280 Cr Gr 280 - 480 Asph 480 - 800 Med F Sa Tr Gr Tr Sl OCC Cob 800 - 1.6 F Sa W Sl 1.6 - 3.0 Muck Amor 3.0 - 4.2 Fib Muck Amor 4.2 - 5.0 Si F Sa Tr Cl	13+500 7.7 m Lt C/L D-800 0 - 3.6 Muck Amor 3.6 - 4.7 Si F Sa	13+750 7.7 m Lt C/L D-800 0 - 300 Wat 200 - 3.7 Muck Amor 3.7 - 4.7 Si F Sa	13+850 3.3 m Lt C/L D-300 0 - 200 Cr Gr 200 - 500 Med F Sa Tr Gr Tr Sl Tr Cob 500 - 1.2 F Sa W Sl Tr Gr 1.2 NFP Bl/BR
13+300 6.9 m Lt C/L D-0 0 - 200 Cr Gr 200 - 600 Med F Sa Tr Gr Tr Sl OCC Cob 600 - 1.4 F Sa W Sl 1.4 - 3.1 Muck Amor 3.1 NFP Bl/BR	13+400 6.9 m Lt C/L D-0 0 - 380 Cr Gr 380 - 480 Asph 480 - 800 Med F Sa Tr Gr Tr Sl 800 - 850 AC Gran 850 - 1.6 F Sa W Sl 1.6 - 4.2 Muck Amor 4.2 - 5.0 Med F Sa Some Si	13+500 7.7 m Lt C/L D-0 0 - 2.8 Fib Muck Amor wet @ 300 2.8 - 3.2 Si F Sa Tr Gr	13+755 7.7 m Lt C/L D-800 0 - 300 Wat 200 - 3.7 Muck Amor 3.7 - 4.7 Si F Sa	13+850 5.7 m Lt C/L D+500 0 - 50 Si Org 50 - 2.0 Med F Sa Some Si
13+300 1.7 m Lt C/L D-0 0 - 260 Asph 260 - 340 AC Gran 340 - 600 Med F Sa Tr Gr Tr Sl 600 - 1.5 Si F Sa wet @ 1.5 1.5 - 2.2 Muck Amor 2.2 - 2.8 Med F Sa Some Si 2.8 NFP Bl/BR	13+450 1.7 m Lt C/L D-0 0 - 300 Cr Gr 300 - 350 Asph 350 - 800 Med F Sa Tr Gr Tr Sl OCC Cob 800 - 1.4 F Sa W Sl 1.4 - 4.0 Muck Amor 4.0 - 5.0 Si F Sa	13+500 1.7 m Lt C/L D-0 0 - 280 Cr Gr 280 - 290 PST 290 - 760 Med F Sa Tr Gr Tr Sl 760 - 1.5 F Sa W Sl 1.5 - 4.0 Muck Amor 4.0 - 5.5 Si F Sa	13+782 8.3 m Lt C/L D-0 0 - 280 Cr Gr 280 - 650 Med F Sa Tr Gr Tr Sl 650 - 1.5 F Sa W Sl 1.5 - 4.0 Muck Amor 4.0 - 5.5 Si F Sa	13+880 7.7 m Lt C/L D+700 0 - 50 Si Org 50 - 2.2 Med F Sa Some Si 2.2 NFP Bl/BR
13+300 7.7 m Lt C/L D-1.2 0 - 3.7 Muck Amor 3.7 - 4.5 Si F Sa	13+450 7.7 m Lt C/L D-1.2 0 - 3.7 Muck Amor 3.7 - 4.5 Si F Sa	13+500 1.7 m Lt C/L D-0 0 - 290 Cr Gr 290 - 650 Med F Sa Tr Gr Tr Sl W Cob 900 - 1.4 F Sa W Sl Tr Gr 1.4 - 4.2 Muck Amor 4.2 - 4.7 Si F Sa	13+792 8.3 m Lt C/L D-0 0 - 280 Cr Gr 280 - 650 Med F Sa Tr Gr Tr Sl 650 - 1.5 Si F Sa 1.5 - 2.3 Muck Amor 2.3 - 2.7 Si Some F Sa	13+898 5.7 m Lt C/L D+1.0 0 - 50 Si Org 50 - 2.2 Med F Sa Some Si 2.2 NFP Bl/BR
13+600 7.7 m Lt C/L D-1.0 0 - 3.2 Muck Amor 3.2 - 4.7 Si F Sa	13+600 7.7 m Lt C/L D-1.0 0 - 3.2 Muck Amor 3.2 - 4.7 Si F Sa	13+600 7.7 m Lt C/L D-0 0 - 280 Cr Gr 280 - 290 PST 290 - 760 Med F Sa Tr Gr Tr Sl 760 - 1.5 F Sa W Sl 1.5 - 4.0 Muck Amor 4.0 - 5.5 Si F Sa	13+792 8.3 m Lt C/L D-0 0 - 280 Cr Gr 280 - 650 Med F Sa Tr Gr Tr Sl 650 - 1.5 Si F Sa 1.5 - 2.2 Muck Amor 2.2 - 2.8 Si Some F Sa	13+900 19.3 m Lt C/L D-3.5 0 - 100 Si Org 100 - 500 Sa Si, wet 500 NFP Bl/BR

Date: November 17, 2000

Drawn: MR

Project: 00036

Chkd: MAM



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GEOTECHNICAL SURVEY DATA
W.P. 167 - 90 - 00
JOCKO TWP

METRIC

AREA 2

20+319.6 12.3 m Lt C/L D-600	20+344.6 1.3 m Rt C/L D-0	20+394.6 1.3 m Rt C/L D-0	20+444.6 1.2 m Rt C/L D-0
0 - 3.7 Muck Amor, wet 3.7 - 4.5 F Sa W Si	0 - 270 Cr Gr 270 - 1.0 Med F Sa Tr Gr Tr Si 1.0 - 1.3 F Sa Some Si Some Si 1.3 - 1.8 RF	0 - 390 Cr Gr 390 - 850 Med F Sa Tr Gr Tr Si 850 - 1.3 F Sa Some Si 1.3 NFP RF	0 - 360 Cr Gr 360 - 850 Med F Sa Tr Gr Tr Si 650 - 700 PST 700 - 1.2 F Sa Some Si 1.2 NFP RF
20+319.6 6.1 m Lt C/L D-0	1.8 - 3.0 Muck Amor 3.0 - 3.5 F Sa Some Si	20+394.6 11.3 m Rt C/L D-1.3	20+444.6 11.3 m Rt C/L D-1.5
0 - 250 Cr Gr 250 - 800 Med F Sa Some Si Tr Gr 800 - 1.8 F Sa Some Si 1.8 - 4.3 Muck Amor 4.3 - 4.8 F Sa W Si	20+346.6 1.1 m Rt C/L D-0	0 - 100 Si Org 100 - 1.7 Muck Amor 1.7 - 3.0 F Sa W Si	0 - 2.0 Muck Amor. 2.0 - 2.6 F Sa W Si 2.6 NFP Bld
20+319.6 1.3 m Rt C/L D-0	1.0 - 1.3 Med F Sa Some Si Some Gr wet @ 1.2 1.3 NFP RF	20+414.6 12.3 m Lt C/L D+2.1	20+447.6 5.6 m Lt C/L D-0
0 - 370 Cr Gr 370 - 800 Med F Sa Tr Gr Tr Si 800 - 1.1 F Sa Some Si 1.1 - 1.5 F Sa Some Si Some Gr wet @ 1.4 1.5 - 1.8 RF	20+351.6 1.2 m Rt C/L D-0	0 NFP BR	0 - 120 Asph 120 - 240 Cr Gr 240 - 830 Med F Sa Tr Si Tr Gr 830 - 900 PST 900 - 1.1 F Sa Some Si 1.1 NFP RF
20+319.6 11.3 m Rt C/L D-850	0 - 280 Cr Gr 280 - 1.0 Med F Sa Tr Gr Tr Si 1.0 - 1.3 Med F Sa Some Si Some Gr wet @ 1.2 1.3 NFP RF	20+414.6 5.7 m Lt C/L D-0	20+450 C/L
0 - 50 Si Org 50 - 5.4 Muck Amor 5.4 - 6.0 Med F Sa Some Si	20+356.6 1.2 m Rt C/L D-0	1.0 NFP Sh Rk/BR	0 - 350 Cr Gr 350 - 700 Med F Sa Tr Gr Tr Si 700 - 1.4 F Sa Some Si 1.4 - 2.0 Sh Rk/Sa & Peat 2.0 - 2.6 Muck Amor
20+326.6 8.8 m Lt C/L D-0	0 - 280 Cr Gr 280 - 1.0 Med F Sa Tr Gr Tr Si 1.0 - 1.4 Med F Sa Some Si Some Gr wet @ 1.2 1.4 NFP RF	20+414.6 1.2 m Rt C/L D-0	2.6 - 3.1 Si Some F Sa 3.1 - 3.6 F Sa W Si Cob @ 3.2
0 - 140 Cr Gr 140 - 200 AC Gran 200 - 570 Cr Gr 570 - 980 Med F Sa Tr Gr Tr Si 980 - 1.02 PST 1.02 - 2.0 Si F Sa Tr Gr Fr Wat @ 1.02	20+369.6 12.3 m Lt C/L D-700	0 - 340 Cr Gr 340 - 730 Med F Sa Tr Gr Tr Si 730 - 760 PST 760 - 1.3 F Sa Some Si 1.3 NFP RF	3.6 NFP Bld/BR
20+331.6 1.0 m Rt C/L D-0	0 - 280 Cr Gr 280 - 750 Med F Sa Tr Gr Tr Si 750 - 800 Si Org 800 - 1.5 F Sa Some Si Some Gr	20+369.6 1.7 m Rt C/L D-0	20+419.6 11.3 m Rt C/L D-400
0 - 280 Cr Gr 280 - 750 Med F Sa Tr Gr Tr Si 750 - 800 Si Org 800 - 1.5 F Sa Some Si Some Gr	0 - 300 Cr Gr 300 - 1.3 Med F Sa Tr Gr Tr Si 1.3 - 2.8 Muck Amor 2.8 - 4.2 Med F Sa Some Si	0 - 300 Si Org Fr Wat @ Surf 300 NFP Bld/BR	0 - 100 Si Org 100 NFP Bld/RF
20+336.6 1.2 m Rt C/L D-0	0 - 270 Cr Gr 270 - 1.3 Med F Sa Tr Gr Tr Si Fr Wat @ 860 1.3 - 1.5 F Sa Some Si Some Gr 36ELS142 Accep GRANULAR B TYPE I 1.5 NFP RF	20+369.6 11.3 m Rt C/L D-1.2	20+434.6 12.3 m Lt C/L D-900
0 - 270 Cr Gr 270 - 1.3 Med F Sa Tr Gr Tr Si Fr Wat @ 860 1.3 - 1.5 F Sa Some Si Some Gr 36ELS142 Accep GRANULAR B TYPE I 1.5 NFP RF	0 - 100 Si Org 100 - 2.9 Muck Amor 2.9 - 3.2 Med F Sa Some Si	0 - 240 Cr Gr 240 - 730 Med F Sa Tr Si Tr Gr 730 - 800 PST 800 - 1.0 F Sa Some Si 1.0 NFP Sh Rk/BR	20+434.6 6.2 m Lt C/L D-0
20+341.6 12.3 m Lt C/L D-700	0 - 120 Asph 120 - 240 Cr Gr 240 - 900 Med F Sa Tr Si Tr Gr Fr Wat @ 800 900 - 1.0 F Sa Some Si 1.0 NFP RF	0 - 120 Asph 120 - 240 Cr Gr 240 - 830 Med F Sa Tr Gr Tr Si 830 - 880 PST 880 - 1.3 F Sa Some Si 1.3 NFP Sh Rk/BR	20+434.6 1.5 m Rt C/L D-0
0 - 1.9 Muck Amor, wet 1.9 - 2.3 Med F Sa Some Si	900 - 1.0 F Sa Some Si 1.0 NFP RF	0 - 160 Asph 160 - 460 Cr Gr 460 - 830 Med F Sa Tr Gr Tr Si 830 - 880 PST 880 - 1.3 F Sa Some Si 1.3 NFP Sh Rk/BR	20+434.6 5.6 m Lt C/L D-0
20+341.6 10.3 m Rt C/L D-1.5	0 - 300 Wat 300 - 4.3 Muck Amor 4.3 - 4.6 Med F Sa Some Si	20+394.6 12.3 m Lt C/L D-600	0 - 120 Asph 120 - 240 Cr Gr 240 - 830 Med F Sa Tr Si Tr Gr 830 - 900 PST 900 - 1.2 F Sa Some Si 1.2 NFP RF
0 - 240 Cr Gr 240 - 1.5 Med F Sa Tr Gr Tr Si 1.5 - 1.8 Med F Sa Some Si wet @ 1.5 1.8 - 3.0 Muck Amor 3.0 - 3.5 F Sa Some Si	0 - 120 Asph 120 - 240 Cr Gr 240 - 600 Med F Sa Tr Si Tr Gr 600 - 670 PST 670 - 1.0 F Sa Some Si 1.0 NFP RF	20+394.6 5.7 m Lt C/L D-0	20+442.6 5.6 m Lt C/L D-0

Date: November 17, 2000

Drawn: MR

Project: 00036

Chkd: MAM



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PAGE NO.

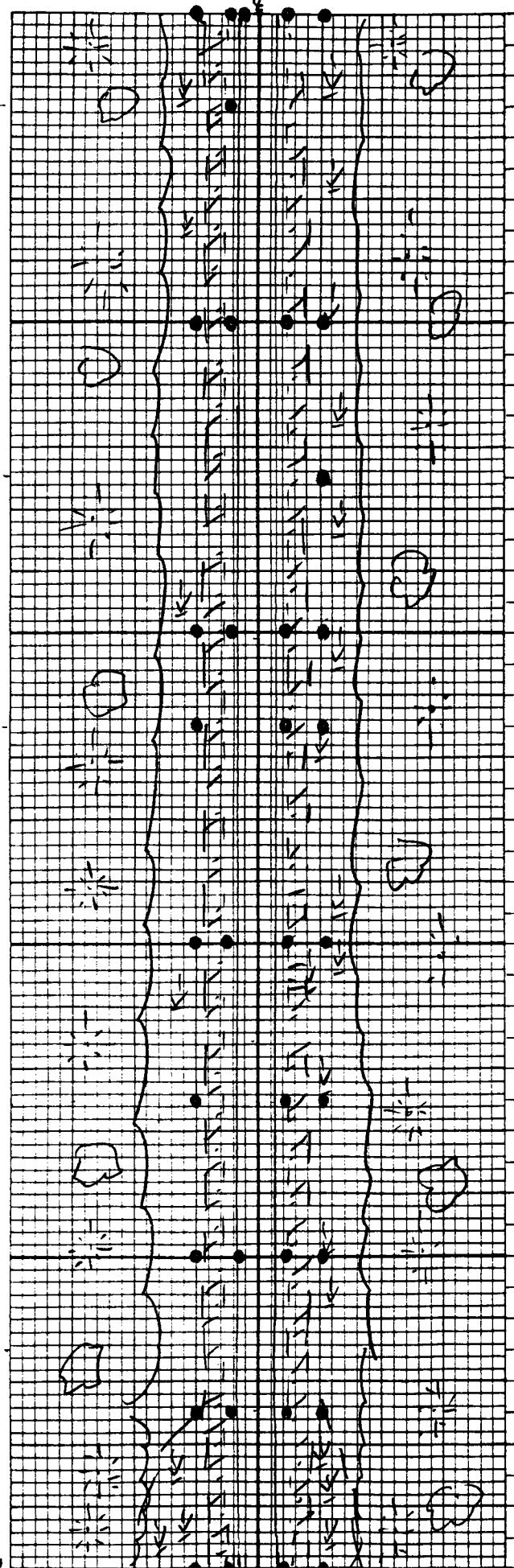
TWP.

J040

W.P. NO. 167-90-00

DATE JUN 27/00

13+500



HWY. NO.

LOCATION Hwy 533 TO QUEBEC BOUNDARY

ENGINEER

RJD

PAGE NO.

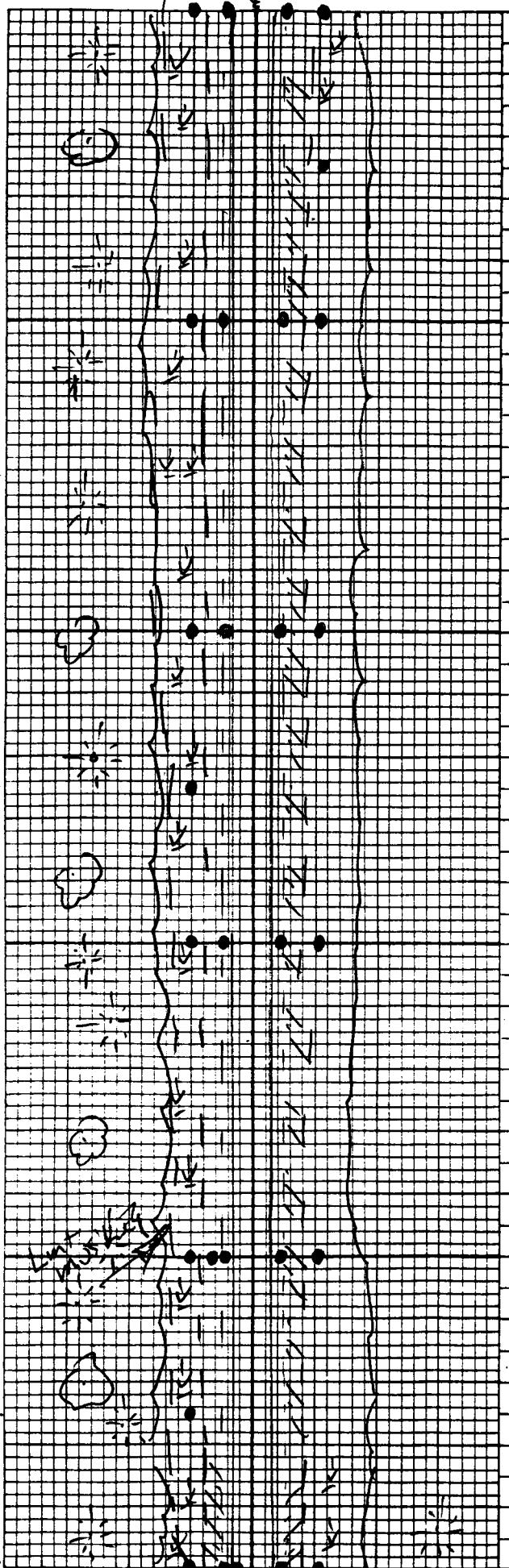
TWP.

Jocko

W.P. NO. 167-90-00

DATE Jun 27/00

134750



134650

134600

134550

8

134500

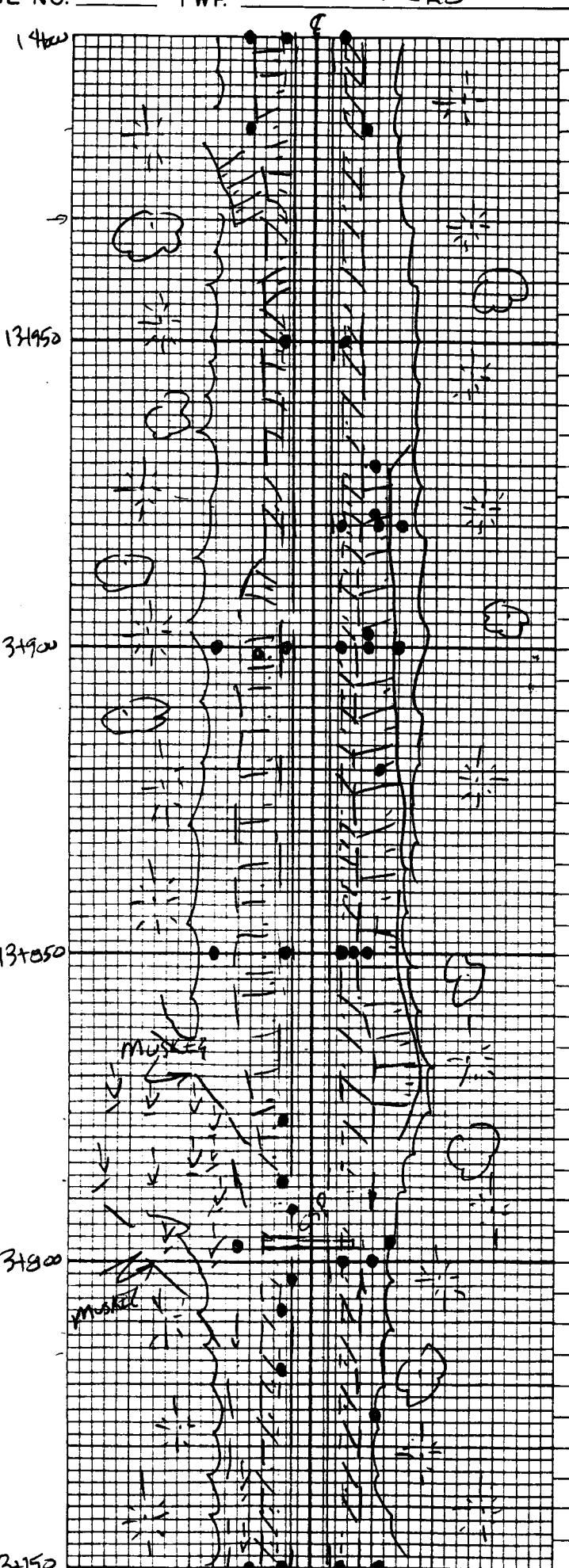
HWY. NO. 63

LOCATION Hwy 533 TO QUEBEC BOUNDARY

ENGINEER

RSD

PAGE NO. _____ TWP. _____ W.P. NO. 167-90-00 DATE JUN 27/00



Boulders in Cut (Right)

HWY. NO. _____

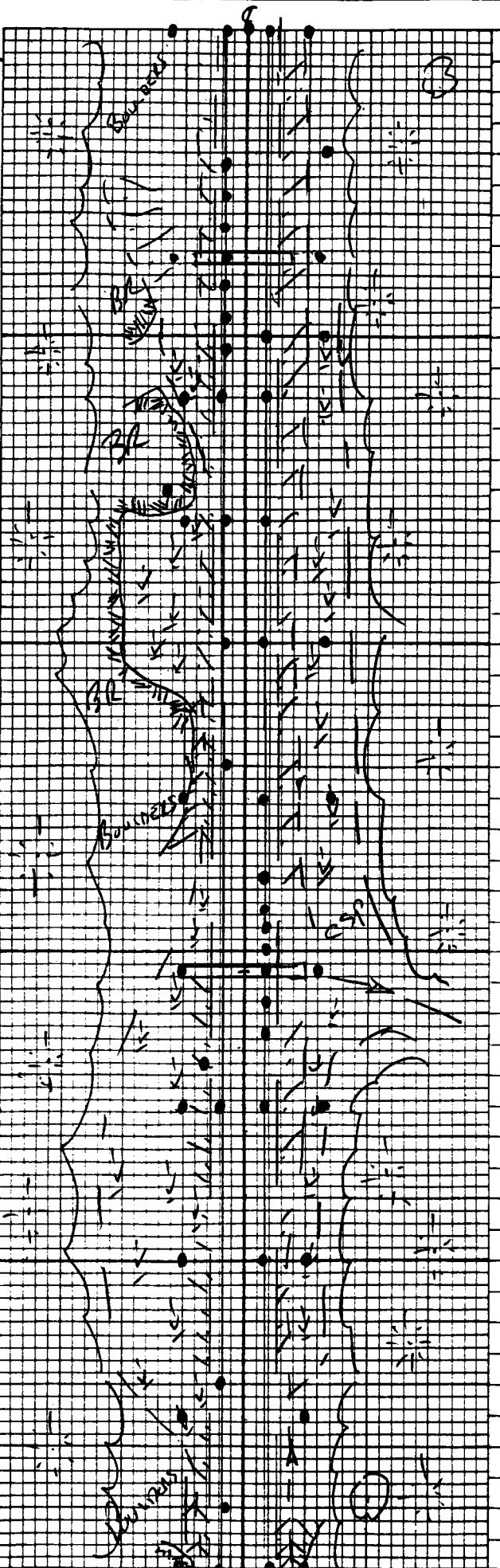
LOCATION Hwy 533 TO CULDEC BOUNDARY

ENGINEER _____

RBB

PAGE NO. _____ TWP. _____ JOCKO _____ W.P. NO. 167-90-00 _____ DATE Jul 03/00

20+500



20+450

20+400

20+350

20+300

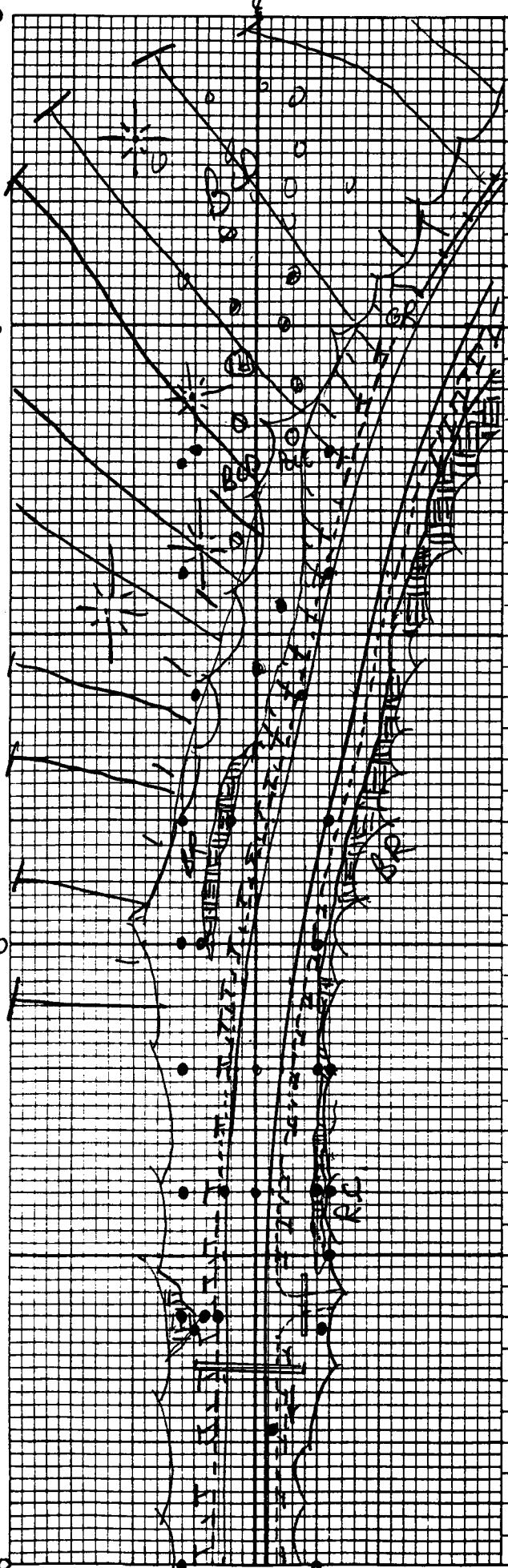
20+250

(20+347 csp)

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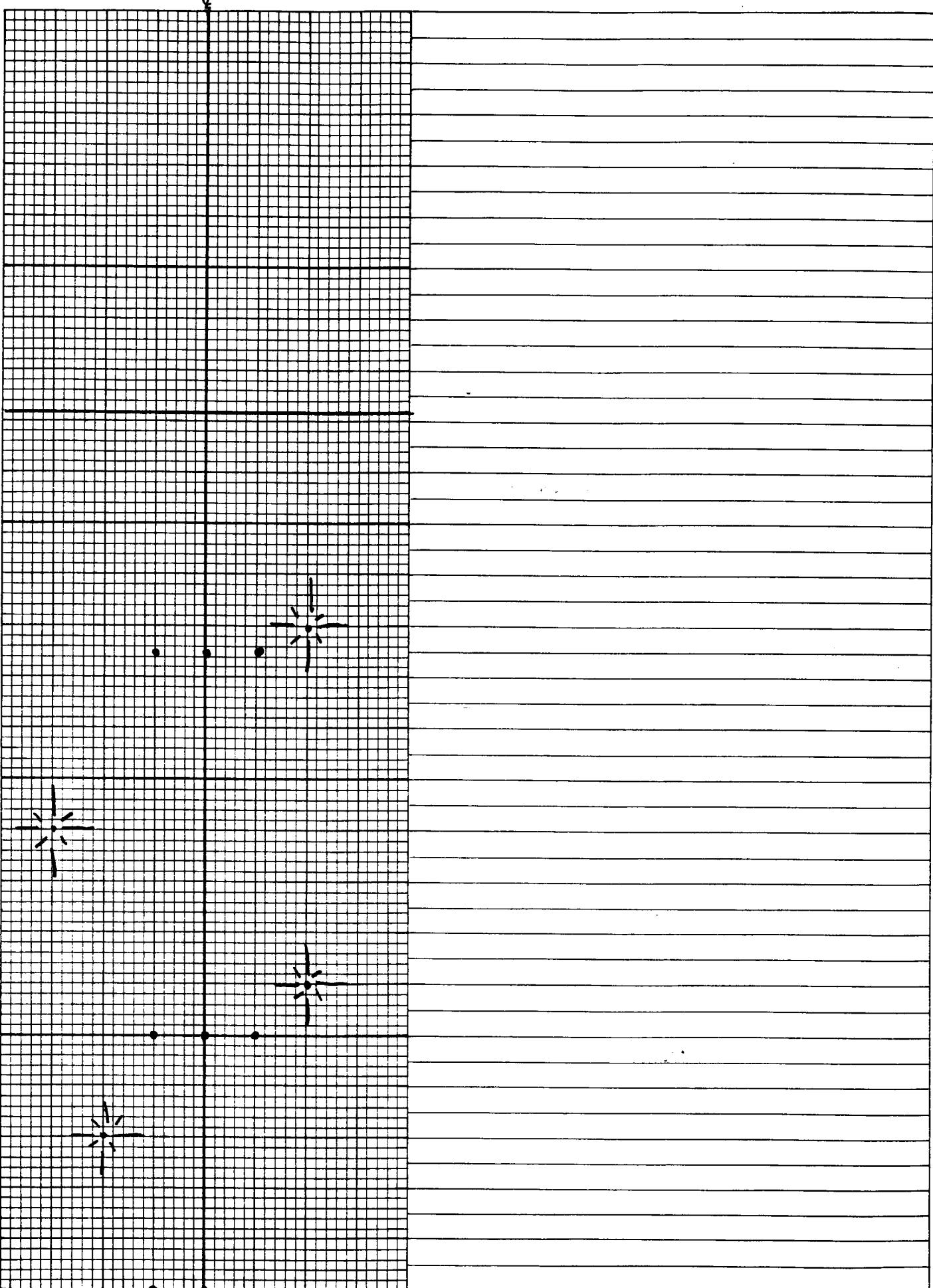
20+750



20+500

HWY. NO. 63 LOCATION Hwy 533 - P.Q Boundary ENGINEER ECS

PAGE NO. _____ TWP. JACKO (NEW) W.P. NO. 167-90-00 DATE _____



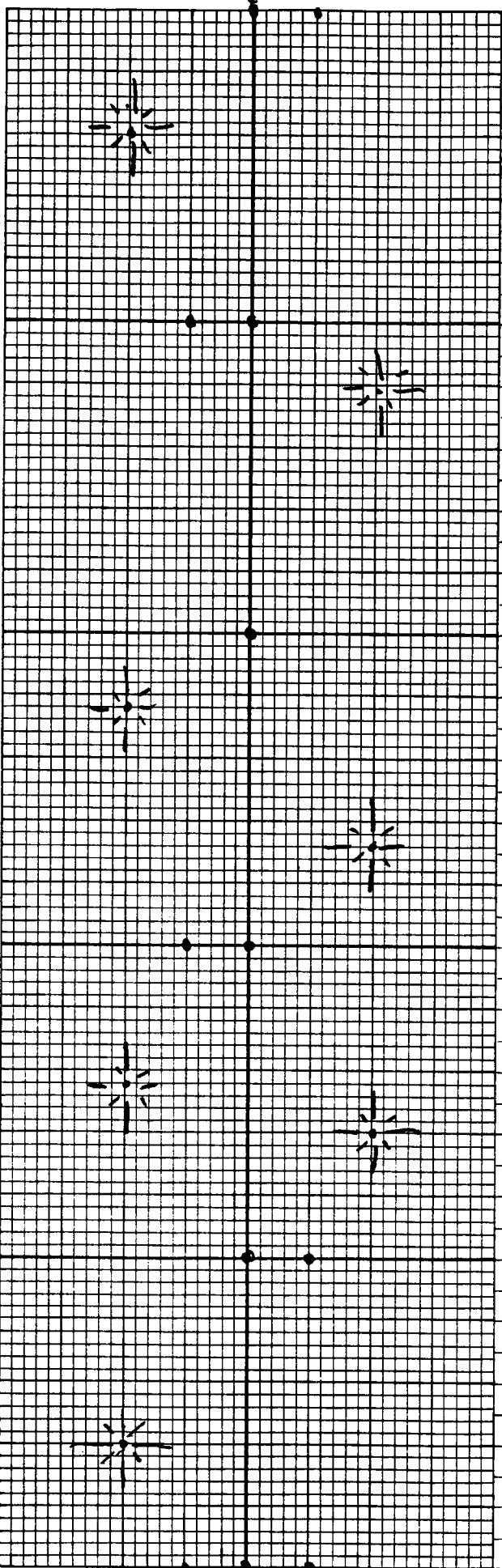
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TWP. CLARKSON (NEW)

W.P. NO. 167-90-00

DATE

10+250



PH-0-25 90-08

10+000

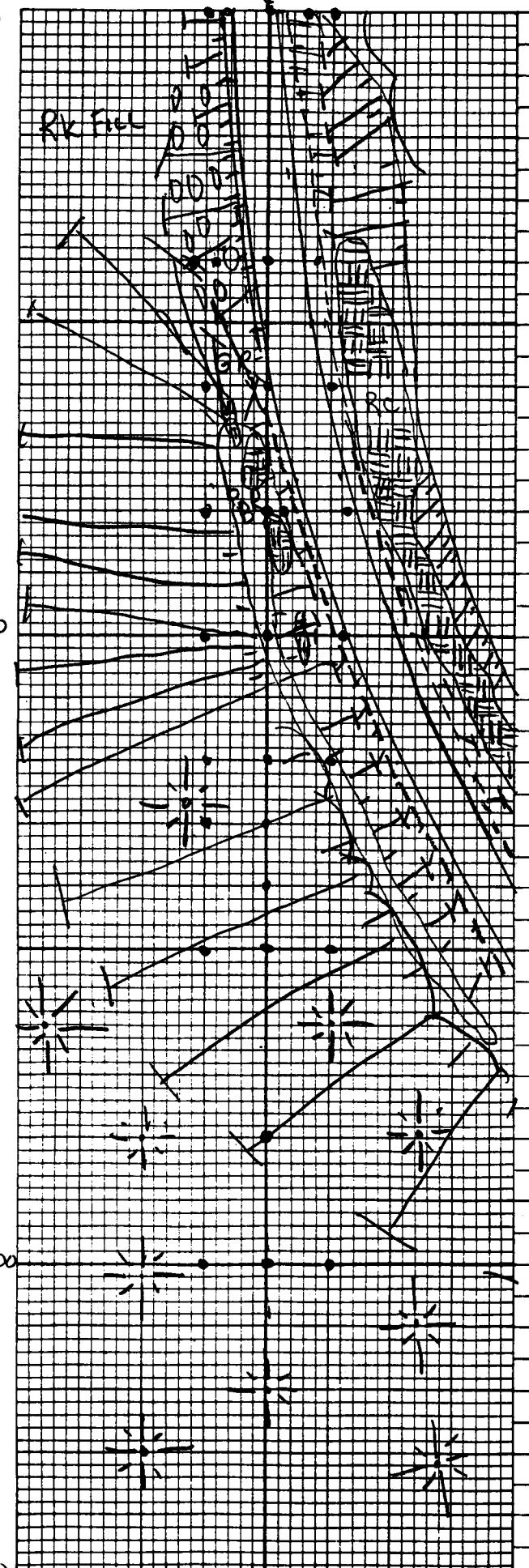
HWY. NO 63

LOCATION HWY 533 - P.Q BOUNDARY

ENGINEER EIS

PAGE NO. TWP. CLARKSON (NEW) W.P. NO. 167-90-00 DATE

10+500



Hwy. No. 63

LOCATION Hwy 533 - P.Q BOUNDARY

ENGINEER ECS

0-25
0-00

APPENDIX B

Geotechnical Survey Data – Possible Detour Areas

HWY 63		13+300	25.7 m Rt C/L D-1.3
FROM 1.0 KM N OF JCT. OF HWY 533			
N'LY TO QUEBEC BORDER	0 - 1.5	F Fib Peat	
WP 167-90-00	1.5 - 1.8	Med F Sa Some Si Tr Gr	
JOCKO TOWNSHIP		13+325	20.7 m Rt C/L D-1.3
13+250	15.7 m Rt C/L D-1.4		
0 - 250	Si Org	0 - 1.5	F Fib Peat Moist
250 - 1.0	Si F Sa	1.5 - 1.7	Si Some F Sa Wet
1.0	NFP Bld	13+350	15.7 m Rt C/L D-1.4
13+250	20.7 m Rt C/L D-1.4	0 - 2.3	F Fib Peat
0 - 200	Si Org	2.3 - 2.4	Gry Si Some F Sa Wet
200 - 1.0	Si F Sa	13+350	20.7 m Rt C/L D-1.2
1.0	NFP Bld	0 - 1.5	F Fib Peat
13+250	25.7 m Rt C/L D-1.4	1.5 - 1.6	Gry Si Some F Sa Wet
0 - 200	Si Org	13+350	25.7 m Rt C/L D-1.1
200 - 1.0	Si F Sa	0 - 1.4	F Fib Peat
1.0	NFP Bld	1.4 - 1.6	Gry Si Some F Sa Wet
13+275	20.7 m Rt C/L D-1.6	13+375	20.7 m Rt C/L D-1.2
0 - 50	Si Org		
50 - 1.7	F Fib Peat	0 - 2.4	F Fib Peat
1.7 - 2.0	Gry Si Some F Sa Wet	2.4 - 2.8	Gry Si Some F Sa Wet
2.0	NFB Bld	13+400	15.7 m Rt C/L D-1.3
13+300	15.7 m Rt C/L D-1.3	0 - 3.9	F Fib Peat OCC Wd
0 - 50	Si Org	3.9 - 4.0	Si Some F Sa Wet
50 - 2.5	F Fib Peat	13+400	20.7 m Rt C/L D-1.3
2.5	NFP Bld	0 - 4.5	F Fib Peat
13+300	20.7 m Rt C/L D-1.3	4.5	NFP Bld
0 - 2.5	F Fib Peat	13+400	25.7 m Rt C/L D-1.3
2.5 - 2.8	Si Some F Sa wet	0 - 3.4	F Fib Peat OCC Wd
2.8	NFP Bld	3.4 - 3.5	Gry Si Some F Sa Wet

WP 167-90-00 HWY 63 JOCKO TOWNSHIP
FOUNDATION AREA #1 DETOUR

Reference No.: 00036
Date: January 2001

13+400	30.7 m Rt C/L D-1.3	13+525	20.7 m Rt C/L D-1.0
0 - 1.4 1.4 - 1.6	F Fib Peat OCC Wd Gry Si Some F Sa Wet	0 - 3.6 3.6 - 3.8	F Fib Peat Gry Si F Sa Wet
13+425	20.7 m Rt C/L D-1.3	13+550	15.7 m Rt C/L D-1.1
0 - 4.0 4.0 - 4.4	F Fib Peat Gry Si Some F Sa Wet	0 - 3.5 3.5 - 3.6	F Fib Peat OCC Wd Gry Si Some F Sa Wet
13+450	15.7 m Rt C/L D-1.0	13+550	20.7 m Rt C/L D-1.1
0 - 4.2 4.2 - 4.4	F Fib Peat Med F Sa Some Si Tr Gr Wet	0 - 3.0 3.0 - 3.1	F Fib Peat OCC Wd Gry Si Some F Sa Wet
13+450	20.7 m Rt C/L D-1.0	13+550	25.7 m Rt C/L D-1.1
0 - 3.8 3.8 - 3.9	F Fib Peat Gry Si Some F Sa Wet	0 - 2.4 2.4 - 2.6	F Fib Peat OCC Wd Gry Si Some F Sa Wet
13+450	25.7 m Rt C/L D-1.1	13+575	20.7 m Rt C/L D-1.1
0 - 3.3 3.3 - 3.6	F Fib Peat Gry Si Some F Sa Wet	0 - 2.5 2.5	F Fib Peat OCC Wd NFP Bld
13+475	20.7 m Rt C/L D-1.1	13+575	22.7 m Rt C/L D-1.1
0 - 3.0 3.0 - 3.1	F Fib Peat OCC Wd Gry Si Some F Sa Wet	0 - 2.5 2.5 - 2.6	F Fib Peat OCC Wd Gry Si Some F Sa Wet
13+500	15.7 m Rt C/L D-1.0	13+600	15.7 m Rt C/L D-1.1
0 - 3.3 3.3 - 3.4	F Fib Peat Gry Si F Sa Wet	0 - 4.3 4.3 - 4.4	F Fib Peat OCC Wd Gry Si SomeF Sa Wet
13+500	20.7 m Rt C/L D-1.0	13+600	20.7 m Rt C/L D-1.1
0 - 3.1 3.1 - 3.3	F Fib Peat Gry Si Some F Sa Wet	0 - 3.3 3.3 - 3.4	F Fib Peat OCC Wd Gry Si Some F Sa Wet
13+500	25.7 m Rt C/L D-1.0	13+600	25.7 m Rt C/L D-1.1
0 - 3.8 3.8 - 3.9	F Fib Peat Gry Si F Sa Wet	0 - 3.3 3.3	F Fib Peat OCC Wd NFP Bld

WP 167-90-00 HWY 63 JOCKO TOWNSHIP
FOUNDATION AREA #1 DETOUR

Reference No.: 00036
Date: January 2001

13+625	20.7 m Rt C/L D-800	13+725	18.7 m Rt C/L D-800
0 - 4.0 4.2 - 4.2	F Fib Peat OCC Wd Gry Si Some F Sa Wet	0 - 2.4 2.4	F Fib Peat OCC Wd NFP Bld
13+650	15.7 m Rt C/L D-700	13+725	20.7 m Rt C/L D-800
0 - 3.6 3.6 - 3.8	F Fib Peat Gry Si Some F Sa wet	0 - 2.3 2.3	F Fib Peat OCC Wd NFP Bld
13+650	20.7 m Rt C/L D-700	13+750	15.7 m Rt C/L D-700
0 - 4.0 4.0 - 4.2	F Fib Peat OCC Wd Gry Si Some F Sa Wet	0 - 1.6 1.6	F Fib Peat NFP Bld
13+650	25.7 m Rt C/L D-700	13+750	20.7 m Rt C/L D-700
0 - 4.3 4.3 - 4.4	F Fib Peat OCC Wd Gry Si Some F Sa Wet	0 - 1.4 1.4	F Fib Peat OCC Wd NFP Bld
13+675	19.7 m Rt C/L D-700	13+750	25.7 m Rt C/L D-400
0 - 3.4 3.4 - 3.6	F Fib Peat OCC Wd Gry Si F Sa Wet	0 - 400 400	Si Org NFP Bld/BR
13+675	20.7 m Rt C/L D-700	13+775	15.7 m Rt C/L D-400
0 - 2.8 2.8	F Fib Peat OCC Wd NFP Bld	0 - 400 400	Si Org NFP Bld
13+700	15.7 m Rt C/L D-500	13+775	17.7 m Rt C/L D-0
0 - 3.4 3.4 - 3.5	F Fib Peat Gry Si F Sa wet	0 - 100 100 - 800 800	Si Org Med F Sa With Si Tr Gr NFP Bld
13+700	20.7 m Rt C/L D-300		
0 - 3.5 3.5 - 3.6	F Fib Peat OCC Wd Gry Si F Sa Wet		
13+700	25.7 m Rt C/L D-100		
0 - 2.4 2.4 - 2.8	F Fib Peat OCC Wd Gry Si F Sa Wet		

HWY 63				
FROM 1.0 KM N OF JCT. OF HWY 533 N'LY TO QUEBEC BORDER		20+294.6	21.8 m Rt C/L	D-1.3
WP 167-90-00		0 - 3.4	F Fib Peat OCC Wd	
		3.4 - 3.6	Gry Med F Sa Some Si	
JOCKO TOWNSHIP			Some Gr Wet	
20+244.6	16.8 m Rt C/L D-0			
0 - 50	Si Org	20+294.6	26.8 m Rt C/L	D-1.3
50 - 200	Si F Sa	0 - 3.8	F Fib Peat OCC Wd	
200	NFP Bld	3.8 - 3.9	Gry Med F Sa Some Si	
			Some Gr Wet	
20+244.6	17.8 m Rt C/L D-0			
0 - 50	Si Org	20+319.6	21.8 m Rt C/L	D-1.1
50 - 300	Si F Sa	0 - 5.0	F Fib Peat OCC Wd	
300	NFP Bld	5.0 - 5.1	Gry Med F Sa Some Si	
			Some Gr Wet	
20+244.6	21.8 m Rt C/L D-1.8			
0 - 300	Si Org	20+344.6	16.8 m Rt C/L	D-1.1
300	NFP Bld	0 - 4.8	F Fib Peat OCC Wd	
		48 - 4.9	Gry Med F Sa Some Si	
			Some Gr Wet	
20+244.6	26.8 m Rt C/L D-1.8			
0 - 700	F Fib Peat	20+344.6	21.8 m Rt C/L	D-1.1
700	NFP Bld	0 - 5.0	F Fib Peat OCC Wd	
		5.0 - 5.1	Gry Med F Sa Some Si	
			Some Gr Wet	
20+244.6	27.8 m Rt C/L D-1.8			
0 - 800	F Fib Peat	20+344.6	26.8 m Rt C/L	D-1.1
800	NFP Bld	0 - 5.5	F Fib Peat OCC Wd	
		5.5 - 5.6	Gry Med F Sa Some Si	
			Some Gr Wet	
20+269.6	21.8 m Rt C/L D-1.5			
0 - 1.6	F Fib Peat	20+344.6	21.8 m Rt C/L	D-1.3
1.6 - 1.8	Gry F Sa Some Si Wet	0 - 5.5	F Fib Peat OCC Wd	
		5.5 - 5.6	Gry Med F Sa Some Si	
			Some Gr Wet	
20+294.6	16.8 m Rt C/L D-1.3			
0 - 4.0	F Fib Peat OCC Wd	20+369.6	21.8 m Rt C/L	D-1.3
4.0 - 4.1	Gry Med F Sa Some Si	0 - 4.2	F Fib Peat OCC Wd	
	Some Gr Wet	4.2 - 4.3	Gry Med F Sa Some Si	
			Wet	

WP 167-90-00 HWY 63 JOCKO TOWNSHIP
FOUNDATION AREA #2 DETOUR

Reference No.: 00036
Date: January 2001

20+394.6	16.8 m Rt C/L D-1.0	20+469.6	23.8 m Rt C/L D-1.0
0 - 2.2	F Fib Peat OCC Wd	0 - 50	Si Org
2.2 - 2.4	Gry Med F Sa W Si	50 - 700	Br Si F Sa Wet
Wet		700	NFP Bld/BR
20+394.6	21.8 m Rt C/L D-1.0		
0 - 3.4	F Fib Peat OCC Wd		
3.4 - 3.6	Gry Med F Sa Some Si		
Wet			
20+394.6	26.8 m Rt C/L D-1.0		
0 - 3.0	F Fib Peat OCC Wd		
3.0	NFP Bld		
20+419.6	21.8 m Rt C/L D-1.3		
0 - 3.6	F Fib Peat OCC Wd		
Wet			
3.6 - 3.7	@ 200 Gry Med F Sa Some Si Some Gr Wet		
20+444.6	16.8 m Rt C/L D-1.8		
0 - 2.0	F Fib Peat OCC Wd		
2.0 - 2.1	Si F Sa Wet		
2.1	NFP Bld		
20+444.6	21.8 m Rt C/L D-1.8		
0 - 2.9	F Fib Peat OCC Wd		
2.9 - 3.0	Si F Sa Wet		
20+444.6	26.8 m Rt C/L D-1.8		
0 - 4.0	F Fib Peat OCC Wd		
4.0 - 4.1	Si F Sa Wet		
20+469.6	21.8 m Rt C/L D-800		
0 - 50	Si Org		
50 - 600	Br Si F Sa Wet		
600	NFP Bld/BR		

APPENDIX C

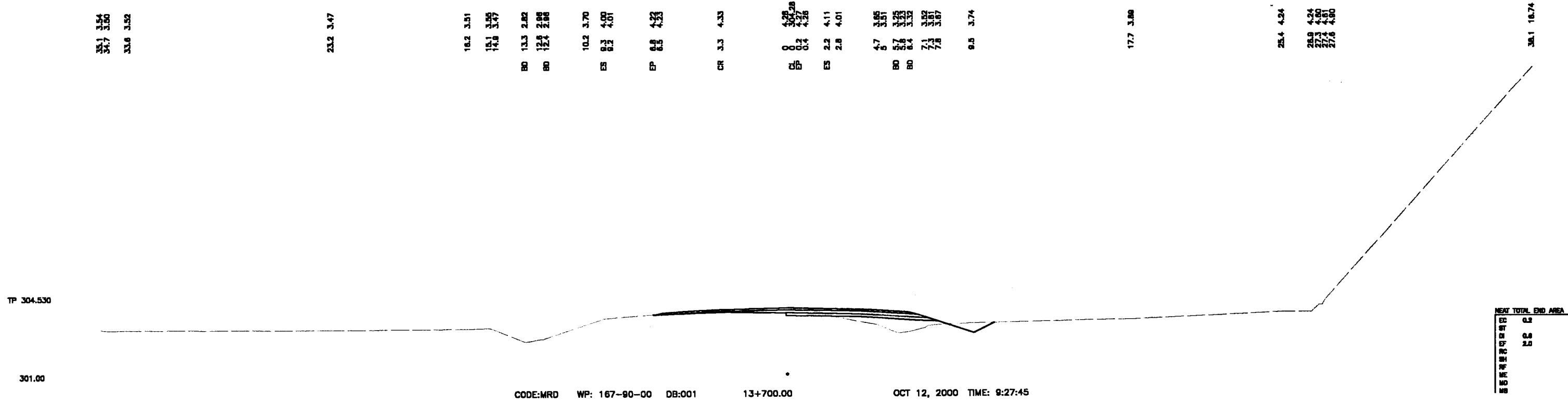
Typical Cross Sections

Figure C-1 Area 1

Figure C-2 Area 2

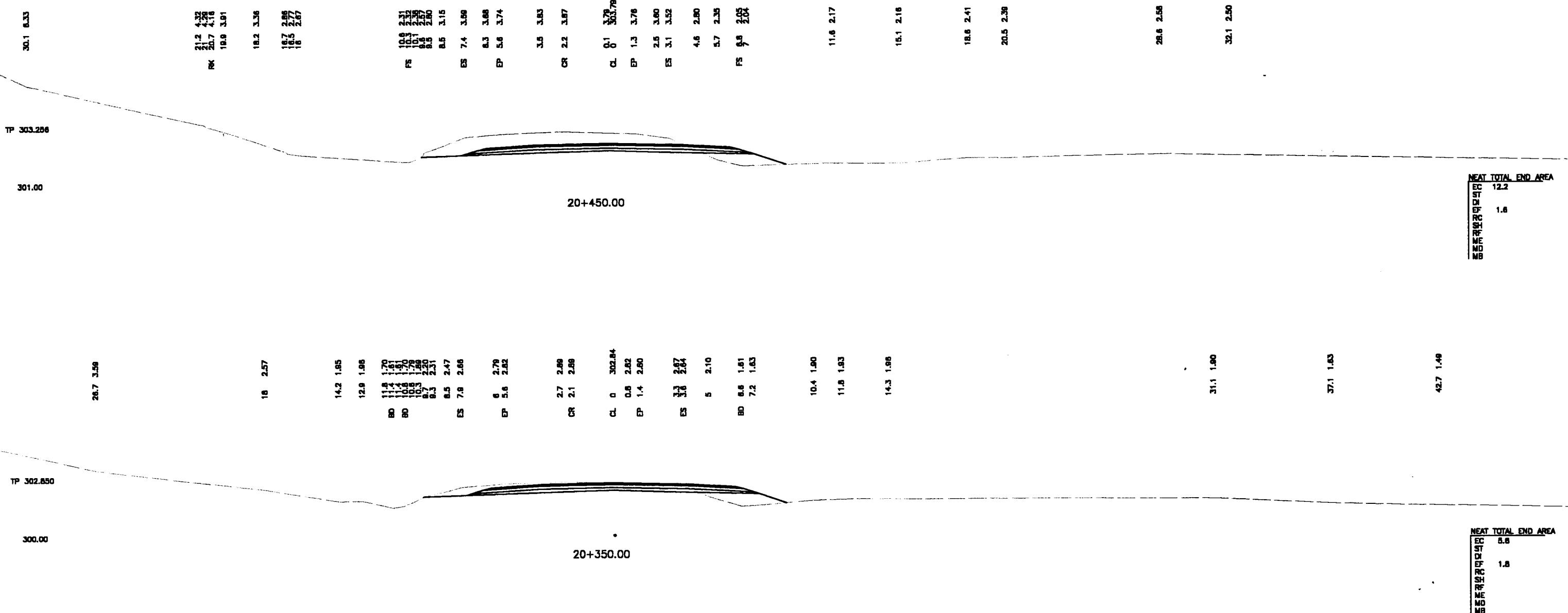
HWY 63 – W.P. 167-90-00
Typical Cross-Section Area 1

FIGURE C-1
Reference No. 00036
Scale 1:200



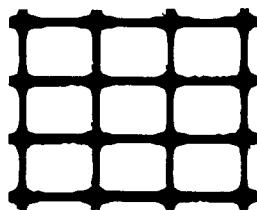
HWY 63 - W.P. 167-90-00
Typical Cross-Section Area 2

FIGURE C-2
Reference No. 00036
Scale 1:200



APPENDIX D

Fill Widening Reinforcement



Tensar Earth Technologies, Inc.

5883 Glenridge Drive
Suite 200
Atlanta, Georgia 30328
Tel: 404-250-1290
Fax: 404-250-9185

DESIGN CALCULATIONS

Prepared for

MERLEX ENGINEERING LTD.

HIGHWAY 63

CANADA

TET # E00501

CONTENTS

Design Assumptions	Page 1 - 2
Stability Analysis	Page 3 - 6

Calculated by:

Jack Fu, PhD

Checked by:

Kevin Lee, PE

January 5, 2001

DESIGN ASSUMPTIONS

Project Name: Hwy 63, Canada
Project Number E00501

Date: 01/05/01
Engineer: XJF

THE FOLLOWING ASSUMPTIONS HAVE BEEN ADOPTED BY TET FOR THE PURPOSE OF DEVELOPING THIS PREMININARY DESIGN. ALL ASSUMPTIONS MUST BE VERIFIED IN WRITING PRIOR TO FINAL DESIGN AND CONSTRUCTION.

1. Design Methodology

Tensar Design Guideline.

2. Slope Geometry

Approximately 1.3 m high new fill will be placed on the existing grade with approximately 3(H):1(V) side slope.

3. Soil Properties

Soil	Unit Weight γ , (kN/m ³)	Friction Angle ϕ' , (deg)	Cohesion c, (kPa)
New and Existing Fill	21	32	0
Foundation 1 (Peat)	10	0	15
Foundation 2 (Silty Sand)	17	28	0

4. Loading

Traffic loading = 12 kPa

5. Minimum Factors of Safety

Factor of safety for Global stability Static = 1.5

6. Geogrid Reinforcement

Geogrid Type	Ultimate Tensile Strength, (kN/m)	Creep Limit Strength, (kN/m)	RF _{ID}	RF _D	Design Strength, (kN/m)	Percent Coverage, R _c (%)
BX1100	19	2.55	1.0	1.15	2.22	100

Soil-geogrid interaction coefficient

Static

= 0.6

7. Groundwater

Water table is assumed to be at El. 303.

8. Geogrid Placement

Place the geogrid on the existing grade in the direction parallel to the center line of roadway, from the merge of existing grade and new fill to toe of proposed new fill slope.

9. Notes

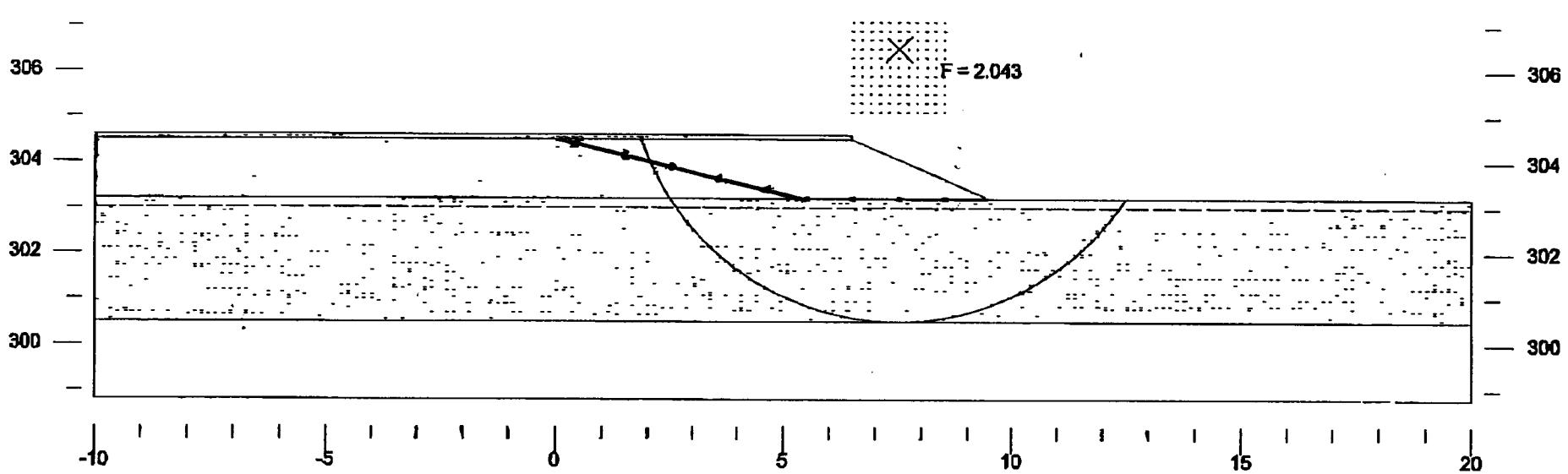
- A. Seismicity, flood conditions and rapid drawdown were not considered in this design.
- B. The design presented herein is based on the information provided by Merlex Engineering LTD. Tensar Earth Technologies, Inc. accepts no liability for the information or verification of information.
- C. Tensar Earth Technologies, Inc. assumes no liability for interpretation of subsurface conditions, suitability of soil design parameters, and subsurface groundwater conditions.
- D. Bearing capacity, total and differential settlement and their effects on this system are the responsibility of the owner or owner's representative. Tensar Earth Technologies, Inc. accepts no responsibility or liability for the evaluation of settlements.
- E. The owner or owner's representative is responsible to review and verify in writing the design parameters described in sections 1 - 7 prior to construction.

	Gamma kN/m ³	C kPa	Phi deg	Piezo Surf.	Ru
Traffic Load	120	0	0	1	0
New Fill	21	0	32	1	0
Existing Fill	21	0	32	1	0
Foundation 1	10	15	0	1	0
Foundation 2	17	0	28	1	0

Tensar Earth Technologies - Atlanta
E00501

Hwy 63 Extend road way
1/5/2001

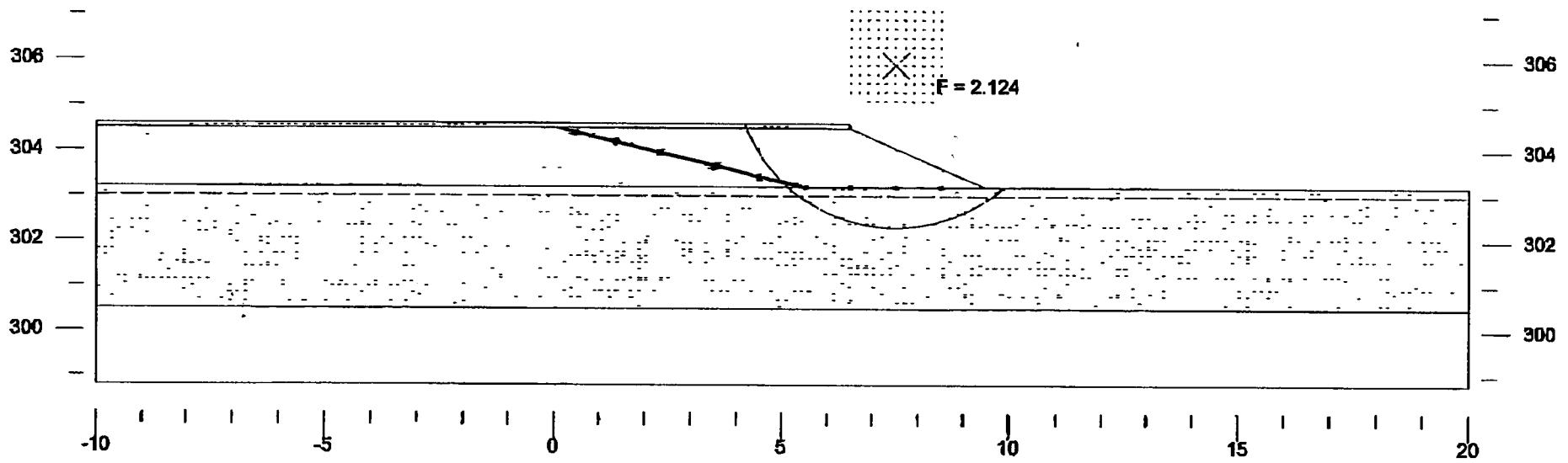
H=1.3 ft



	Gamma kN/m ³	C kPa	Phi deg	Piezo Surf.	Ru
Traffic Load	120	0	0	1	0
New Fill	21	0	32	1	0
Existing Fill	21	0	32	1	0
Foundation 1	10	15	0	1	0
Foundation 2	17	0	28	1	0

Tensar Earth Technologies - Atlanta
E00501
Hwy 63 Extend road way
1/5/2001

H=1.3 ft



DATA FILE NAME..... K:\E00501\HWY63.GSL

Job Number	E00501
Title	Hwy 63 Extend road way
Date	1/5/2001
Label A	
Label B	H=1.3 ft

Maximum Slice Width	1
Number of Soil Layers: (1 to 20)	5
Earthquake Acceleration:	0
No. of External Forces: (0 to 100)	0
Piezometric Surfaces: (0 to 9)	1
Unit weight of Water:	9.81
Reinforcement Layers: (0 to 100)	1
FoS against Pullout:	1.5

Material	Unit Wt	Cohesion	Friction Angle	Piezo Surf.	Ru	Interaction Coefficient
1 Traffic Load	120	0	0	1	0	.6
2 New Fill	21	0	32	1	0	.6
3 Existing Fill	21	0	32	1	0	.6
4 Foundation 1	10	15	0	1	0	.6
5 Foundation 2	17	0	28	1	0	.6

Upper Surface of Material # 1 (Traffic Load)

X-Coord	Y-Coord
-10	304.8
0	304.6
6.49	304.6
6.5	304.5
9.5	303.2
20	303.2

Upper Surface of Material # 2 (New Fill)

X-Coord	Y-Coord
-10	304.5
0	304.5
6.5	304.5
9.5	303.2
20	303.2

Upper Surface of Material # 3 (Existing Fill)

X-Coord	Y-Coord
-10	304.5
0	304.5
5.5	303.2
9.5	303.2
20	303.2

Upper Surface of Material # 4 (Foundation 1)

X-Coord	Y-Coord
-10	303.2
0	303.2
6.5	303.2
9.5	303.2

Upper Surface of Material # 5 (Foundation 2)

X-Coord	Y-Coord
-10	300.5
0	300.5
6.5	300.5
9.5	300.5
20	300.5

Piezometric Surface No. 1

X-Coord	Y-Coord
-10	303
20	303

There are no explicit external forces in the data set.

Reinforcement Layer No.	Horizontal Extents X1 <----> X2	Reinforcement Layer Elevation	Tallowable per unit width	Tconnection per unit width
1	5.5 9.5	303.2	2.22	0