

\*59-F-223C

BRIDGE #12

FAIRMONT AVE.

& OTTAWA

QUEENSWAY

# MCROSTIE & ASSOCIATES

CONSULTING ENGINEERS AND SURVEYORS

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59-F-223C

## FAIRMONT AVENUE - BRIDGE NO. 12

### 1. TERMS OF REFERENCE

We were requested by the Ottawa Office of De Leuw Cather & Company to investigate foundation conditions at the site of a proposed bridge to carry the Queensway over Fairmont Avenue. Proposed grades for the Queensway and Fairmont Avenue, and preferred footing elevations were supplied, and a report was to be prepared on the investigation.

### 2. RECOMMENDATIONS

#### 2.1 Foundation Type

The structure happens to be located at a fault in the rock and this results in unusually variable conditions at the site. It has been necessary to consider each abutment separately since different types of support are recommended for each abutment.

##### East Abutment

Some type of pile or caisson support is recommended for this abutment. The soils below the abutment are unsuitable for the support of major structural loads for a considerable depth, thus a system of transferring the load of the structure to the fractured rock at depth is necessary.

If "H" piles are used they cannot be expected to develop sufficient resistance in the dense till soils to act as friction piles in this material.

They should be driven into the fractured rock or to end bearing on unbroken rock in the few places where it occurs. The high number of blows for the standard penetration test in some of the till layers has been found not to represent the degree of driving resistance in the Ottawa Area till soils which might be expected from experience elsewhere. Despite the possible lack of frictional driving resistance in the tills, driving difficulties due to boulders are to be expected. Test drilling efforts encountered boulders in several holes with sizes up to a few feet in diameter.

An alternate proposal should be requested on a fixed price basis for abutment support by means of expanded base, encased shaft, concrete piles of the "Franki" type. The specification for this type of pile should provide for a guaranteed load capacity such as 100 tons on a 16 inch shaft diameter with the pile length chosen by the contractor. A load test should be included in the fixed total cost with the test to be made on any pile chosen by the supervising engineer. The specification should also include the requirement for a permanent metal casing for the pile shaft to be fastened to the enlarged base in such a manner that the two will not separate. No metal casing should be filled with concrete until inspected.

#### Test Abutment

For this abutment we would recommend the use of footings to spread the abutment load on the fractured rock at about elevation 208. Random dips in the fractured rock surface were found to be filled with dense till soil but if suitably low bearing values are used on the fractured rock, the

till soils can support similar loads and the dips in the rock surface would not be critical. In addition the rigidity of the abutment itself would allow small areas of low density to be spanned.

The preceding recommendations do not apply however to the southerly wing-wall of the west abutment. Loose till soils overly the fractured rock in this location and the wing-wall footings should therefore follow the fractured rock surface. Towards the westerly end of the wing-wall, where the embankment retained by the wall becomes small, a shallower wing-wall supported on the dense higher soil layers could be considered.

## 2.2 Soil And Rock Strengths

Bearing values for units of the structure can be recommended as follows: -

### East Abutment

Soils at reasonable footing depths are not suitable for the support of a major structure.

### West Abutment

fractured rock at about elevation 208	15,000 POUNDS PER SQUARE FOOT
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dense till at about elevation 208	10,000 POUNDS PER SQUARE FOOT
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### West Abutment Southerly Wing-Wall

fractured rock at elevation 208 - 203	15,000 POUNDS PER SQUARE FOOT
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soils at elevation 217 - 214	6,000 POUNDS PER SQUARE FOOT
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loose soils below elevation 211	Not suitable for support of major elements of structure
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### Approach Embankment Foundation.

The organic layers encountered in the easterly abutment location would not have suitable strengths to act as a foundation for the approach embankment. These organic soils should be removed despite the fact that they are presently beneath several feet of fill.

### 2.3 Soil Compressibilities

The soils and rocks which are recommended for use as support of the structure are basically granular soil types and hence do not produce long term consolidation settlements. However, the layers of organic material several feet in thickness which were encountered beneath the easterly abutment would also exist beneath the new approach embankment fills hence large settlements of this fill would occur even if the strength of the organic layer was not exceeded. This fact provides an additional reason for the removal of the organic layers.

### 2.4 Construction Precautions

During the construction of the westerly abutment foundations, where the rock surface may be irregular, the contractor should be prevented from excavating in a manner that would disturb the bearing soils. Even in the fractured rock areas the material should be treated in a similar manner as an earth excavation so that the natural tendency of an excavator who feels that he is "going to rock" can be prevented. It is unlikely that any smooth working surface will result and if the loosest rock fragments cannot be removed by hand or by machine scraping, recompaction of the upper few inches of broken material may be required.

Another item which should be considered during construction is that the foundations of the existing bridge abutment may cause some interference with normal construction operations. This point should be drawn to the attention of the bidders.

An important point regarding the relative timing of the construction period for the easterly abutment and its approach fill is that the organic soils under the site of the structure should be removed before the structure or the embankment is built. These organic soils would be stressed by the weight of the approach embankment and could provide the mechanism for a failure by lateral yield. If the structure were to be built first, without the removal of the organic soils, it would be very difficult to have them removed at a later date.

### 3. SITE INVESTIGATION

#### 3.1 Field Work

The field work in this investigation was more extensive than normal since variable soil and rock conditions were gradually discovered. Investigation was made in four stages with a period of study of the previous findings inbetween each stage and with consultations with the designing office to discuss the significance of information as it became known.

The four stages of the program are outlined below:

Stage 1 - Six boreholes were made at the site in the normal pattern with our test drilling rig, samples were recovered and a study was made of the till soils to investigate the possibility of their use as foundation support for the structure.

Stage 2 - When soil and rock conditions were found to be variable, and footings on the till soils found unlikely to be suitable, and considerable depths of soil deposit found in the southeasterly corner of the east abutment, three additional holes were made in the deepest soil area. Two of the holes were made with our test drilling rig and the third was made by J. B. Dufresne Limited, Drilling Contractors, who were asked to bring heavy drilling equipment in an effort to overcome difficulties due to boulders. Great difficulty was experienced in all three holes due to boulders and the borehole (No. 8) made by J. B. Dufresne Limited was discontinued before reaching rock and little information was gained from it except that test drilling conditions were exceptionally difficult. At this time, test drilling was discontinued and a test pile scheme was studied as an alternate means of providing information on the load capacity and possible length of end bearing piles.

Stage 3 - The slope of the rock at the easterly edge of the footings for the westerly abutment and soil conditions for an extension of the southerly wing-wall were then studied by means of three boreholes ( Nos. 10, 11 and 12) made with our test drilling rig. In these holes the elevation of the rock surface was the main object of study.

Stage 4 - When unusual variations in rock depth and structure were observed in Stage 3, two further holes were made with our test drilling rig. These holes confirmed that soil and rock conditions were exceedingly variable and that special foundation measures would be required.

In all stages, 2" split barrel samples were recovered in the non-cohesive soil layers, standard penetration tests were performed in the boreholes, and groundwater levels were observed during the field program. During diamond drilling a watch for and record of drops and discontinuities in the drilling was kept so that as much information as possible could be obtained on the rock structure in place.

### 3.2 Laboratory Testing

As mentioned above, the samples recovered in Stage 1 of the investigation were tested for water content and mechanical analysis in order to provide aids to a judgement of their inplace densities. These results also aided in judging the suitability of the tills for use as support of friction piles.

### 3.3 Rock Core Logging

Since fractured rocks at a fault zone are involved and a complex rock surface was discovered which is of considerable significance in the design and construction of the new structure, a complete description



of the cores recovered and of the information obtained regarding the rock formation during drilling has been included in the report.

### 3.4 Observations

Details of soil and rock conditions are shown on the accompanying plates but can be generalized as follows. The site of the structure apparently lies across the edge of one of a group of rock faults which traverse the area and hence abrupt changes in the rock surface were observed. These changes involve rock depths which vary from a few feet to more than 50 feet within a space of 40 feet or less.

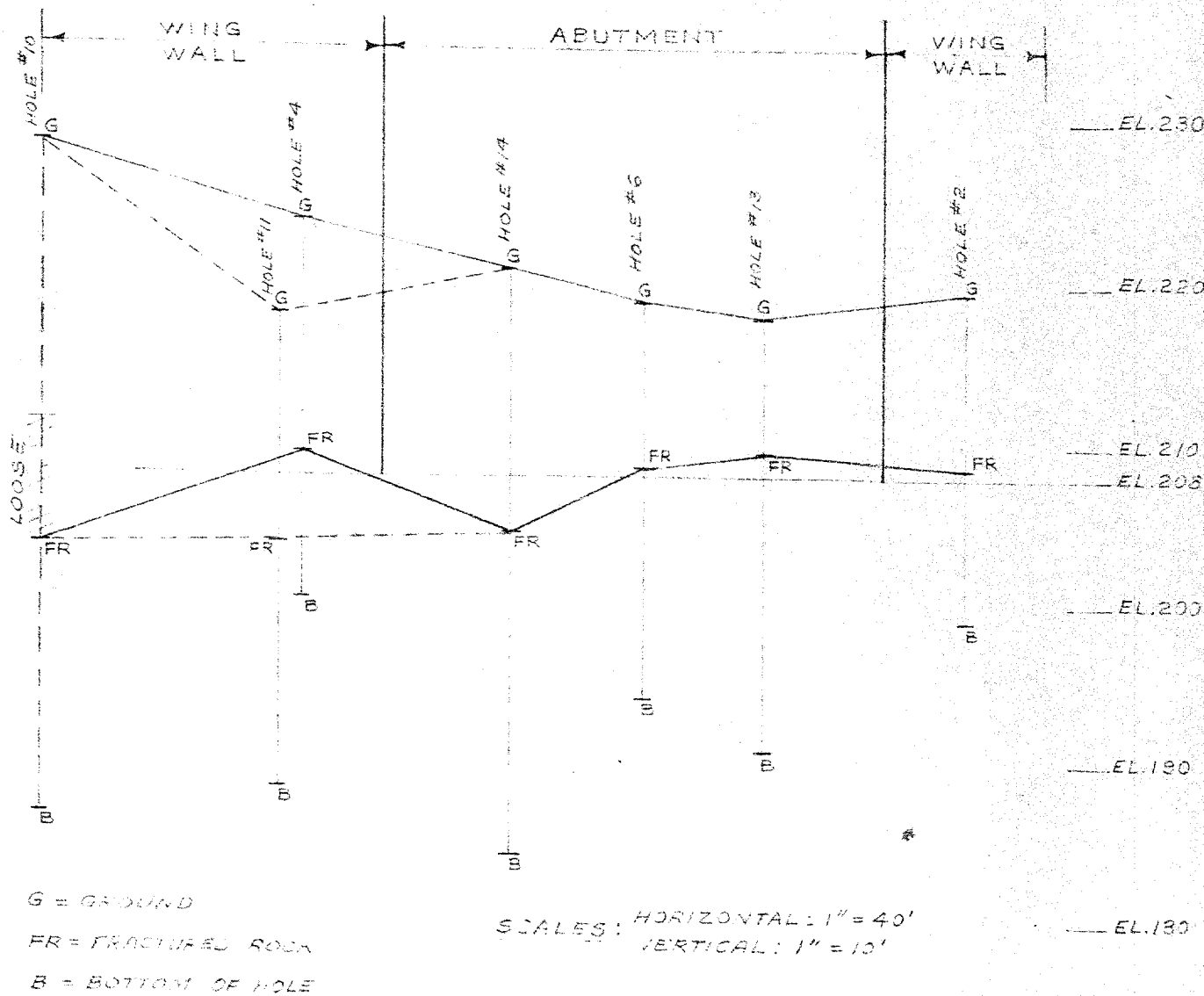
The rock itself, which is a limestone of the Ottawa Formation, is strongly fractured due to the fault action and the upper layers are weathered in addition to the fractures. Where soils exist to considerable depths, they are chiefly glacial tills overlain by sands, fills, or organic deposits, and the tills were observed to have densities varying from loose to very dense. A significant boulder content exists in the till, boulders up to 2 feet in diameter were encountered during the test drilling and doubtless larger boulders are present. Ground-water levels were observed at 5 to 10 feet below the surface and, with the exception of spring thaw conditions, appear to be controlled by the level of municipal sewers on adjacent streets.

The remains of a former railway bridge and the approach fills for this bridge occupy part of the site of the new structure. The effect of these existing features should be considered in the construction of both the new embankment and the new structure.

Finally, in summary, it could be noted that this site is both complex and difficult for investigation, design, and construction, but is fortunately not typical of what can be generally expected.



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SECTION THROUGH WEST ABUTMENT AND AROUND WING WALLS

QUEENSWAY & FAIRMONT

PLATE NO. 2





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#### SOIL PROFILE AND SUMMARY OF FIELD AND LABORATORY TESTS

Q.W.Y. &amp; FAIRMONT

ELEVATION OF GROUND SURFACE (ZERO DEPTH) 214.4' DATE 13-18 Nov. /58  
 REMARKS See PLATE No. 3 - FOR MECHANICAL ANALYSIS SEE  
PLATES No. 37 TO No. 41

HOLE NO.

3

UNCONFINED COMPRESSIVE STRENGTH KIPS/FT. <sup>2</sup>	SMALL SCALE PENETROMETER KIPS/FT. <sup>2</sup>	STANDARD PENETRATION BLOWS/FT.	SAMPLE NUMBER	DESCRIPTION OF SOIL	DEPTH IN FEET	ELEVATION	LB. HAMMER INCH DROP	NO CASING INCH DIA. ROD
				GROUND SURFACE				
					0.0	214.4'		
			49	FILL				OVERNIGHT W.L. EL. 212.2
			3		5.0			
			1701B	ORGANIC				
			35	MEDIUM DENSE SANDY TILL	10.0	204.4		
			1921A		12.5			
			1251A	DENSE TILL				
			96					
			601A	DENSE SANDY TILL	20.0	194.4		
			67	BOULDERS				
			76	DENSE TILL				
			72			184.4		
				BOULDER	32.8			
				DENSE TILL	34.0	180.4		
				SHALE Limestone				
				(CORE RECOVERY 85%)				
				SHALE Limestone				
				(CORE RECOVERY 81%)				
				CORE RECOVERY 93%				
				45° DIP				
				BOTTOM OF HOLE	44.2	170.2		
							0 20 40 60 80 100 % WATER CONTENT NATURAL ○ LIQUID LIMIT □ PLASTIC LIMIT △	
							PLATE 5	









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# SOIL PROFILE AND SUMMARY

## OF FIELD AND LABORATORY TESTS

QWY 5 FAIRMONT

ELEVATION OF GROUND SURFACE (ZERO DEPTH) 220.5 DATE 15-22 DEC. /58

HOLE NO.

REMARKS SEE PLATE No. 3 - FOR MECHANICAL ANALYSIS SEE  
PLATE No. 47

7

UNCONFINED COMPRESSIVE STRENGTH KIPS/FT. <sup>2</sup>	SMALL SCALE PENETROMETER KIPS/FT. <sup>2</sup>	STANDARD PENETRATION BLOWS/FT.	SAMPLE NUMBER	DESCRIPTION OF SOIL	DEPTH IN FEET	ELEVATION	LB. HAMMER	NO CASING
				GROUND SURFACE	0.0	220.5	INCH DROP	INCH DIA. ROD
				FILL				
			7-71				SAND	CLAY
			7-72	ORGANIC	90			
					100		OVERNIGHT W.L.	EL. 211.0
			8-73	LOOSE TILL				
			7-74		200	200.8		
			83-75	DENSE TILL				
			7-76		300	190.8		
			7-77	Boulders in Till	345			
			7-78	DENSE SANDY TILL	400	180.8		
				FRACTURED SHALEY LIMESTONE (CORE RECOVERY 33%)	425	175.8		
				CORE RECOVERY 55%	450			
				CORE RECOVERY 76%	475	170.8		
				CORE RECOVERY 45%	500			
				CORE RECOVERY 43%	525			
				CORE RECOVERY 29%	550			
				FRACTURED SHALEY LIMESTONE 30° DIP	600	160.8		
				CORE RECOVERY 52%	618	159.0		
				BOTTOM OF HOLE				
							% WATER CONTENT	PLATE
							NATURAL	9
							LIQUID LIMIT	
							PLASTIC LIMIT	

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# SOIL PROFILE AND SUMMARY

## OF FIELD AND LABORATORY TESTS

Q W Y / FAIRMONT

 ELEVATION OF GROUND SURFACE (ZERO DEPTH) 221.2 DATE 17-24 FEB /59  
 REMARKS See Plate No. 3

HOLE NO.

8

UNCONFINED COMPRESSIVE STRENGTH KIPS/FT. <sup>2</sup>	SMALL SCALE PENETROMETER KIPS/FT. <sup>2</sup>	STANDARD PENETRATION BLOWS/FT.	SAMPLE NUMBER	DESCRIPTION OF SOIL	DEPTH IN FEET	ELEVATION	NO CASING	
							.....LB. HAMMER	.....INCH DIA. ROD
				GROUND SURFACE			.....INCH DROP	
					0.0	221.2'		
							W.L. 20 FEB /59	EL. 218.3
							W.L. 18 FEB /59	EL. 216.3
			11	8-1				
				Fill				
			7	8-2	10.5	210.7'		
				Organic	12.5	208.7'		
			5	8-3			W.L. 21 FEB /59	EL. 207.7
							W.L. 19 FEB /59	EL. 204.7
				Loose Till	20.0	201.2'		
			9	8-4	25.0	196.2'		
					30.0	191.2'		
				Boulders in Soil				
					42.6	178.6'		
				Bottom of Hole				
							0 20 40 60 80 100 % WATER CONTENT NATURAL ○ LIQUID LIMIT □ PLASTIC LIMIT △	
							PLATE 10	

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# SOIL PROFILE AND SUMMARY

## OF FIELD AND LABORATORY TESTS

Q W Y FAIRMONT

ELEVATION OF GROUND SURFACE (ZERO DEPTH) 230.5

DATE 5-10 MARCH 1959

HOLE NO.

REMARKS See Plate No. 3

9

UNCONFINED COMPRESSIVE STRENGTH KIPS/FT. <sup>2</sup>	SMALL SCALE PENETROMETER KIPS/FT. <sup>2</sup>	STANDARD PENETRATION BLOWS/FT.	SAMPLE NUMBER	DESCRIPTION OF SOIL	DEPTH IN FEET	ELEVATION	LB. HAMMER INCH DROP	NO CASING INCH DIA. ROD
				GROUND SURFACE	0.0	230.5		
			14 91					
			9 92	Sandy Fill				
			8 93					
			16 94	ORGANIC	17.5	213.0		
			15 95		21.0	209.5		
			19 96	Dense Sand with Gravel	22.5	208.0		
			8 96	Loose Till	25.0	205.5		
			12 97	Medium Dense Till				
			34 98	Dense Sandy Till	30.0	200.5		
					32.0	198.5		
			29 99	Medium Dense Sandy Till				
			117 100	Dense Till	40.0	190.5		
					44.9	185.6		
				Boulders in Till	47.5	183.0		
				FRACTURED SHALEY LIMESTONE CORE RECOVERY 30%	52.5	178.0		
				60° DIP CORE RECOVERY 73%	55.0	175.5		
				FRACTURED LIMESTONE CORE RECOVERY 75%	60.8	169.7		
				FRACTURED SHALEY LIMESTONE CORE RECOVERY 21%	64.2	166.3		

OVERNIGHT W.L. EL 212.7

0	20	40	60	80	100
% WATER CONTENT					
NATURAL	○				
LIQUID LIMIT	□				
PLASTIC LIMIT	△				
PLATE					
11					

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#### SOIL PROFILE AND SUMMARY OF FIELD AND LABORATORY TESTS

Q W Y FAIRMONT

ELEVATION OF GROUND SURFACE (ZERO DEPTH) 228.7 DATE 19-20 & 28-29 May/59 HOLE NO.REMARKS SEE PLATE No. 3OVERNIGHT W.L. DRY 21 MAY/59

10

UNCONFINED COMPRESSIVE STRENGTH KIPS/FT. <sup>2</sup>	SMALL SCALE PENETROMETER KIPS/FT. <sup>2</sup>	STANDARD PENETRATION BLOWS/FT.	SAMPLE NUMBER	DESCRIPTION OF SOIL	DEPTH IN FEET	ELEVATION	LB. HAMMER INCH DROP	NO CASING INCH DIA. ROD
				GROUND SURFACE	0.0	228.7		
			14 10-1	FILL				
			6 10-2		6.5	222.2		
			4 10-3	LOOSE SILTY WELL GRADED SAND WITH SOME GRAVEL	8.0	220.7		
			29 10-4	MEDIUM DENSE SILTY WELL GRADED SAND WITH SOME GRAVEL				
			9 10-5					
			13 10-6	DENSE FILL	15.5	213.2		
			58 10-7	DENSE WELL GRADED SAND	16.5	212.2		
			6 10-7		17.5	211.2		
			4 10-8	LOOSE TILL				
			7 10-9					
				WEATHERED OR FRACTURED LIMESTONE	25.3	203.4		
				CORE RECOVERY 54%	28.1	200.6		
				CORE RECOVERY 74%	31.0	197.7		
				CORE RECOVERY 43%	32.5	195.2		
				CORE RECOVERY 45%				
				FRACTURED LIMESTONE	32.0	194.7		
				CORE RECOVERY 75%	39.0	189.7		
				CORE RECOVERY 75% LIMESTONE	39.8	188.9		
				CORE RECOVERY 93%	42.3	186.4		
				BOTTOM OF HOLE				
							0 20 40 60 80 100	% WATER CONTENT
								NATURAL <input type="radio"/>
								LIQUID LIMIT <input type="checkbox"/>
								PLASTIC LIMIT <input type="checkbox"/>
								PLATE
								12









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# SOIL PROFILE AND SUMMARY

## OF FIELD AND LABORATORY TESTS

Q W Y FAIRMONT

ELEVATION OF GROUND SURFACE (ZERO DEPTH) 220.8

DATE MAY 29<sup>th</sup> to June 3<sup>rd</sup> 1954

HOLE NO.

REMARKS See Plate No. 3

14

UNCONFINED COMPRESSIVE STRENGTH KIPS/FT. <sup>2</sup>	SMALL SCALE PENETROMETER KIPS/FT. <sup>2</sup>	STANDARD PENETRATION BLOWS/FT.	SAMPLE NUMBER	DESCRIPTION OF SOIL	DEPTH IN FEET	ELEVATION	LB. HAMMER	NO CASING
				GROUND SURFACE	0.0	220.8	INCH DROP	INCH DIA. ROD
			4 19-1	FILL				
			36.6 142	MEDIUM DENSE SILTY TILL	5.5	215.3		
			10 143	LOOSE TILL				
			62.4 144	(1" SILT LAYER AT 9-2)	10.8	210.0		
			15.6 145	BOULDERS IN TILL	12.5			
				MEDIUM DENSE TILL	13.5			
				DENSE TILL	16.3	204.5		
				WEATHERED OR FRACTURED				
				LIME TONE - 45° DIP	19.9			
				CORE RECOVERY 50%				
				CORE RECOVERY 50%	23.0	197.8		
				FRACTURED LIMESTONE	24.0			
				CORE RECOVERY 47%	26.1			
				CORE RECOVERY 69%				
				30° - 45° DIP				
				CORE RECOVERY 73%	31.7	189.1		
				LIMESTONE				
				45° - 60° DIP				
				CORE RECOVERY 81%	36.7	184.1		
				BOTTOM OF HOLE				
							0 20 40 60 80 100 % WATER CONTENT NATURAL ○ LIQUID LIMIT □ PLASTIC LIMIT △	
							PLATE 16	

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PROJECT Queensway at Fairmont  
 BOREHOLE NO. 2  
 SURFACE ELEV'N 219.5' (MSL)  
 BOREHOLE DEPTH 20.5'

DRILLER W. Deevy  
 RECORDER G. Bilodeau  
 BORING DATE 20 Nov. 1958  
 LOGGING BY G.L. Genest P.Eng.  
 CORE SIZE 7/8"

DRILLING & WATER CONDITIONS	ELEVATION, % RECOVERY	CORE DESCRIPTION
	219.5	GROUND SURFACE soil - fill, sand and till
No drop of rods no loss of drill water	208.6 50%	BEDROCK SURFACE fractured limestone, dark grey, medium grained, high angled joints, calcite filled to 1/16", thin shaley partings between bedding planes, some pyrite deposit, core lengths - from broken to 2", probable 60° dip
no drop of rods no loss of drill water	206.1 89%	limestone, dark grey, fine to medium grained, vertical fracture at El. 203.9 4", thick limestone filled and vertical hairline calcite infilling, near horizontal joints calcite and crystalline calcite filled to 1/8", average core lengths 1 1/2", probable 80° dip
no drop of rods no loss of drill water	204.6 61%	fractured limestone, dark grey, fine to medium grained, high angled joints calcite filled to 1/16", core lengths - from broken to 2", probable 45° dip
no drop of rods no loss of drill water	203.1 57%	fractured limestone, dark grey, medium grained, high angled joints calcite filled to 1/16", core lengths - from broken to 4", 60° - 80° dip
	199.0	BOTTOM OF HOLE

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PROJECT	Queensway at Fairmont	DRILLER	W. Deevy
BOREHOLE NO.	3	RECORDER	G. Bilodeau
SURFACE ELEV'N	214.4 (MSL)	BORING DATE	13-18 Nov, 1958
BOREHOLE DEPTH	44.2'	LOGGING BY	G.L. Genest P.Eng.
		CORE SIZE	7/8"

DRILLING & WATER CONDITIONS	ELEVATION, % RECOVERY	CORE DESCRIPTION
	214.4	GROUND SURFACE
		soil - fill and till
	180.4	BEDROCK SURFACE
no drop of rods no loss of drill water	85%	shaley limestone, dark grey, fine grained, vertical joints calcite filled 1/32" to 1/2", distorted bedding planes at El. 178.9, average core lengths 1 1/2", probable 60° dip
	178.2	
no drop of rods no loss of drill water	81%	shaley limestone, dark grey, fine grained, shale partings to 3/8", vertical joints calcite filled 1/32" to 1/2" at El. 176.6, average core lengths 2"
	173.6	
no drop of rods no loss of drill water	93%	shaley limestone, dark grey, fine grained, vertical joints calcite filled to 1/16", shale partings to 1/4", average core lengths 2 1/2", 45° dip
	170.2	
		BOTTOM OF HOLE

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PROJECT	Queensway at Fairmont	DRILLER	W. Deevy
BOREHOLE NO.	4	RECORDER	G. Bilodeau
SURFACE ELEV'N	223.8 (MSL)	BORING DATE	19-20 Nov., 1958
BOREHOLE DEPTH	23.6'	LOGGING BY	G.L. Genest P.Eng.
		CORE SIZE	7/8"

DRILLING & WATER CONDITIONS	ELEVATION, % RECOVERY	CORE DESCRIPTION
	223.8	GROUND SURFACE
		soil - fill and till
	209.6	BEDROCK SURFACE
1" drop of rods at El.207.1	74%	Weathered or fractured limestone, dark grey, fine grained, vertical joints, calcite filled to 1", core lengths - from broken to 2", 30° dip
Lost drill water at El.207.1		
	204.9	
no drop of rods losing drill water	77%	fractured limestone, dark grey, fine grained, high angled joints. calcite filled to 1/16", fracture zone at El.202.8, calcite filled to 3/4", core lengths - from broken to 4", probable near horizontal bedding.
	200.2	BOTTOM OF HOLE

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PROJECT	Queensway at Fairmont	DRILLER	W. Deevy
BOREHOLE NO.	5	RECORDER	G. Bilodeau
SURFACE ELEV'N	221.0 (MSL)	BORING DATE	4-5 Dec, 1958
BOREHOLE DEPTH	41.0'	LOGGING BY	G.L. Genest P.Eng.
		CORE SIZE	7/8"

DRILLING & WATER CONDITIONS	ELEVATION, % RECOVERY	CORE DESCRIPTION
	221.0	GROUND SURFACE soil - fill and till
no drop of rods no loss of drill water	194.0 48%	BEDROCK SURFACE weathered limestone, dark grey, fine to medium grained, vertical joints, calcite filled to 1/16", core lengths - from broken to 2½", near horizontal bedding.
3" drop of rods at El. 189.2 no loss of drill water	190.0 36%	Weathered limestone, dark grey, fine to medium grained, thin shaley partings calcite intrusions, core lengths - from broken to 3", 45° dip
no drop of rods no loss of drill water	187.0 81%	shaley limestone, dark grey, fine to coarse grained, high angled joints, calcite filled to 1/32", fracture zones at El. 186.3 and 185.0 shale infilling, average core lengths 2½", 30° dip
no drop of rods no loss of drill water	183.0 100%	shaley limestone, dark grey, fine grained, high angled joints, calcite filled to 1/16", vertical fracture at El 181.6 shale infilling, average core lengths 2½", 30° - 45° dip
	180.0	BOTTOM OF HOLE

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PROJECT	Queensway at Fairmont	DRILLER	W. Deevy
BOREHOLE NO.	6	RECORDER	G. Bilodeau
SURFACE ELEV'N	218.8 (MSL)	BORING DATE	8-9 Dec. 1958
BOREHOLE DEPTH	24.7	LOGGING BY	G.L. Genest, P. Eng.
		CORE SIZE	7/8"

DRILLING & WATER CONDITIONS	ELEVATION, % RECOVERY	CORE DESCRIPTION
	218.8	GROUND SURFACE soil - fill and till
1/4" drop of rods at El 207.0 no loss of drill water	208.4 54%	BEDROCK SURFACE weathered shaley limestone, dark grey, fine grained, high angled joints calcite filled to 1/16", core lengths - from broken to 2", 30° dip
no drop of rods no loss of drill water	206.4 84%	shaley limestone, dark grey, fine to medium grained, vertical joints calcite filled to 1/16", thin shale partings between bedding planes, average core lengths 2", 30° dip
no drop of rods no loss of drill water	203.1 89%	limestone, dark grey, fine grained hairline partings calcite filled, average core lengths 1", probable 45° dip
no drop of rods no loss of drill water	202.4 62%	fractured limestone, dark grey, fine grained, high angled joints calcite filled to 1/16", thin shale par- tings, core lengths - from broken to 2", 45° dip
no drop of rods no loss of drill water	200.0 73%	fractured limestone, dark grey, fine grained, vertical joints calcite filled to 1/16", thin shale part- ings, average core lengths 2", 30° dip
no drop of rods no loss of drill water	197.8 91%	limestone dark grey, fine grained, hairline joints calcite filled, thin shale partings, average core lengths 2", 45° dip
	194.1	BOTTOM OF HOLE

**McROSTIE & ASSOCIATES**  
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**OTTAWA CANADA**

PROJECT	Queensway at Fairmont	DRILLER	W. Deevy
BOREHOLE NO.	7	RECORDER	G. Bilodeau
SURFACE ELEV'N	220.8 (MSL)	BORING DATE	15-22 Dec. 1958
BOREHOLE DEPTH	61.8'	LOGGING BY	G.L. Genest, P.Eng.
		CORE SIZE	7/8"

DRILLING & WATER CONDITIONS	ELEVATION, % RECOVERY	CORE DESCRIPTION
	220.8	GROUND SURFACE soil - fill and till
no drop of rods no loss of drill water	178.3 33%	BEDROCK SURFACE fractured shaley limestone, dark grey, fine grained, high angled joints calcite filled and shale infilling to 1/16", core lengths - from broken to 3", distorted bedding planes.
no drop of rods no loss of drill water	173.0 55%	fractured shaley limestone, dark grey, fine grained, high angled joints calcite filled to 1/8", fracture zone at El 173.0 shale infilling, core lengths - from broken to 2"
no drop of rods no loss of drill water	171.3 76%	fractured shaley limestone, dark grey, fine grained high angled joints calcite filled to 1/8", fracture zone at El 171.1, shale infilling, core lengths - from broken to 5"
no drop of rods no loss of drill water	167.8 45%	fractured shaley limestone, dark grey, fine grained, high angled joints calcite filled to 1/16", several shale intrusions at El 167.8, core lengths - from broken to 1 1/2", prob- able 30° - 45° dip
no drop of rods no loss of drill water	166.0 43%	fractured shaley limestone, dark grey, fine grained, high angled joints calcite filled to 1/16", shale par- tings to 1/32" layers, core lengths - from broken to 1 1/2"
no drop of rods no loss of drill water	164.2 29%	fractured shaley limestone, dark grey, fine grained, thin shale partings, core lengths - from broken to 1 1/2"
	162.8	



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OTTAWA CANADA

BOREHOLE NO. 7 Page No. 2

	162.8	
no drop of rods		
no loss of drill	52%	fractured shaley limestone, dark grey,
water		fine grained, high angled joints cal-
		cite filled to 1/16", shale partings
		to 1/32" layers, core agths - from
		broken to 1 1/2", 30° dip
	159.0	
		BOTTOM OF HOLE

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**OTTAWA CANADA**

PROJECT	Queensway at Fairmont	DRILLER	W. Deevy
BOREHOLE NO.	9	RECORDER	G. Bilodeau
SURFACE ELEV'N	230.5 (MSL)	BORING DATE	4-10 March, 1959
BOREHOLE DEPTH	64.2'	LOGGING BY	G.L. Genest, P.Eng.
		CORE SIZE	7.8"

DRILLING & WATER CONDITIONS	ELEVATION, & RECOVERY	CORE DESCRIPTION
	230.5	GROUND SURFACE soil - fill and till
no drop of rods no loss of drill water	183.0 30%	BEDROCK SURFACE fractured shaley limestone, dark grey, fine grained, high angled joints calcite filled to 1/16", several shale intrusions, fracture zone at El 182.5, average core lengths 2"
no drop of rods no loss of drill water	178.0 73%	fractured shaley limestone, dark grey, fine grained, high angled joints at El 178.0 1/4" shale infilling, near vertical joints calcite filled to 1/16", fracture zone at El 177.7, thin shale partings, average core lengths 2", 60° dip
no drop of rods no loss of drill water	175.5 75%	fractured limestone, dark grey, fine to medium grained, high angled joints shale filled to 1/8" and cal- cite filled to 1/32", shaley lime- stone at El 170.8 to El 169.7, aver- age core lengths 2"
no drop of rods no loss of drill water	169.7 21%	fractured shaley limestone, dark grey fine grained, high angled joints calcite filled to 1/4", core lengths - from broken to 1"
	166.3	BOTTOM OF HOLE

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**OTTAWA CANADA**

PROJECT	Queensway at Fairmont	DRILLER	W. Deevy
BOREHOLE NO.	10	RECORDER	G. Bilodeau
SURFACE ELEV'N	228.7 (MSL)	BORING DATE	19-20 & 28-29 May/59
BOREHOLE DEPTH	42.3'	LOGGING BY	G.L. Genest, P. Eng.
		CORE SIZE	7/8"

DRILLING & WATER CONDITIONS	ELEVATION, % RECOVERY	CORE DESCRIPTION
	228.7	GROUND SURFACE soil - fill and till
no drop of rods no loss of drill water	203.4 54%	BEDROCK SURFACE weathered or fractured limestone, dark grey, fine grained, core lengths - from broken to 2", calcite seams, probable 45° dip
no drop of rods no loss of drill water	200.6 74%	weathered or fractured limestone, dark grey, shaley, fine grained, high an- gled joint 1/16" calcite filled at elevation 201.3, core lengths - from broken to 3", probable 45° dip
no drop of rods no loss of drill water	197.7 43%	weathered or fractured limestone, dark grey, fine grained, core lengths - from broken to 2", probable 45° dip
no drop of rods no loss of drill water	195.2 45%	weathered or fractured limestone, dark grey, fine grained, shaley partings to 1/8" layers, core lengths - from broken to 2", probable 45° - 60° dip
no drop of rods lost drill water at El. 190.9	191.7 75%	fractured limestone, dark grey, fine grained, core lengths - from broken to 2", probable 45° - 60° dip
no drop of rods	189.7 75%	fractured limestone, dark grey, fine grained, average core lengths 1", probable 45° dip
no drop of rods	188.9 93%	limestone, dark grey, fine grained, shaley partings to 1/8" layers, core lengths - from broken to 3", probable 45° dip
	186.4	BOTTOM OF HOLE

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**OTTAWA CANADA**

PROJECT	Queensway at Fairmont	DRILLER	W. Deevy
BOREHOLE NO.	11	RECORDER	G. Bilodeau
SURFACE ELEV'N	218.0 (MSL)	BORING DATE	21 May, 1959
BOREHOLE DEPTH	29.7'	LOGGING BY	G.L. Genest, P. Eng.
		CORE SIZE	7 7/8"

DRILLING & WATER CONDITIONS	ELEVATION, % RECOVERY	CORE DESCRIPTION
	218.0	GROUND SURFACE soil -
no drop of rods no loss of drill water	203.8 36%	BEDROCK SURFACE weathered or fractured limestone, dark grey, fine grained, core lengths- from broken to 1 1/2", probable 60° dip.
no drop of rods no loss of drill water	200.8 41%	weathered or fractured limestone, dark grey, fine grained, cores- lengths- from broken to 2", probable 45° dip.
no drop of rods no loss of drill water	199.4 87%	limestone, dark grey, fine grained, 1/16" - 1/8" calcite intrusions, distorted bedding planes, average core lengths 2 1/2".
no drop of rods no loss of drill water	198.2 86%	limestone, dark grey, fine grained, 1/16" - 1/8" calcite intrusions, distorted bedding planes, average core lengths 2 1/2".
no drop of rods no loss of drill water	195.8 43%	fractured limestone, dark grey, fine grained, high angled joints, calcite filled 1/16", core lengths - from broken to 1", probable 45° dip.
no drop of rods no loss of drill water	193.3 95%	limestone, dark grey, fine grained, no fractures, near vertical joints calcite filled 1/16", average core lengths 2 1/2", bedding planes near horizontal.
	188.3	BOTTOM OF HOLE

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**OTTAWA CANADA**

PROJECT	Queensway at Fairmont	DRILLER	W. Deevy
BOREHOLE NO.	12	RECORDER	G. Bilodeau
SURFACE ELEV'N	217.2 (MSL)	BORING DATE	22 May, 1959
BOREHOLE DEPTH	14.0'	LOGGING BY	G.L. Genest, P.Eng.
		CORE SIZE	7/8"

DRILLING & WATER CONDITIONS	ELEVATION, % RECOVERY	CORE DESCRIPTION
	217.2	GROUND SURFACE soil
no drop of rods no loss of drill water	212.4 60%	BEDROCK SURFACE weathered or fractured limestone, dark grey, medium grained, average core lengths 1 1/2"
no drop of rods no loss of drill water	211.1 60%	weathered or fractured limestone, dark grey, medium to fine grained, high angle joint at El 211.5. calcite filled 1/32", core lengths from broken to 1 1/2"
no drop of rods no loss of drill water	210.3 50%	fractured limestone, dark grey, fine grained, fracture zone, calcite filled 1/8", core lengths from broken to 1"
no drop of rods no loss of drill water	209.8 100%	limestone, dark grey, fine grained, no fracture, vertical joints, calcite filled 1/32", average core lengths 2"
no drop of rods no loss of drill water	207.8 100%	limestone, dark grey, medium grained, no fracture, high angled joints; calcite filled 1/16", average core lengths 2 1/2", probable 45° dip.
no drop of rods no loss of drill water	206.8 90%	limestone, dark grey, medium grained, vertical fracture at Elevation 206.9; calcite partings to 1/16", average core lengths 2"
no drop of rods no loss of drill water	205.2 96%	limestone, dark grey, fine grained, high angled joints; calcite filled to 1/8", average core lengths 1 1/2", bedding probably horizontal
	203.2	BOTTOM OF HOLE

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**OTTAWA CANADA**

PROJECT	Queensway at Fairmont	DRILLER	W. Deevy
BOREHOLE NO.	13	RECORDER	G. Bilodeau
SURFACE ELEV'N	217.9 (MSL)	BORING DATE	4 June, 1959
BOREHOLE DEPTH	27.0'	LOGGING BY	G.L. Genest, P. Eng.
		CORE SIZE	7/8"

DRILLING & WATER CONDITIONS	ELEVATION, % RECOVERY	CORE DESCRIPTION
	217.9	GROUND SURFACE soil - fill and till
no drop of rods no loss of drill water	209.3  55%	BEDROCK SURFACE weathered limestone, dark grey, fine to medium grained, vertical joints calcite filled 1/8", near horizon- tal partings calcite filled 1/16", core lengths - from broken to 3", 45° - 60° dip
no drop of rods no loss of drill water	206.9  72%	fractured limestone, dark grey, fine grained, vertical joints calcite filled 1/32", horizontal partings calcite filled 1/32", core lengths - from broken to 2 1/2", 45° dip
no drop of rods no loss of drill water	205.4  56%	fractured limestone, dark grey, med- ium grained, vertical joints cal- cite filled 1/16", horizontal part- ings calcite filled 1/32", core len- gths - from broken to 2 1/2", thin shaley partings between bedding planes, 45° dip
no drop of rods no loss of drill water	202.7  72%	fractured limestone, dark grey, fine to medium grained, vertical frac- ture at El 202.4, near vertical joints calcite filled to 1/16", hor- izontal partings calcite filled 1/16" core lengths - from broken to 3", 60° dip
no drop of rods most drill water at El 200.2	200.3  59%	fractured limestone, dark grey, fine to medium grained, vertical fractures, near vertical joints calcite filled to 1/8", near horizontal partings at El 199.3 calcite filled to 1/4", horizontal partings calcite filled to 1/32", Thin shaley partings be- tween bedding planes, core lengths - from broken to 3 1/2", 45° - 70° dip
	195.8	

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BOREHOLE NO. 13

Page No. 2.

no drop of rods  
no drill water  
return

195.8

90%

limestone, dark grey, fine to medium  
grained, vertical joints calcite  
filled to  $\frac{1}{4}$ " at El 194.4 and 191.4;  
high angled joints calcite filled  
to  $\frac{1}{16}$ ", average core lengths 2",  
thin shaley partings between bed-  
ding planes, 45° dip

190.9

BOTTOM OF HOLE

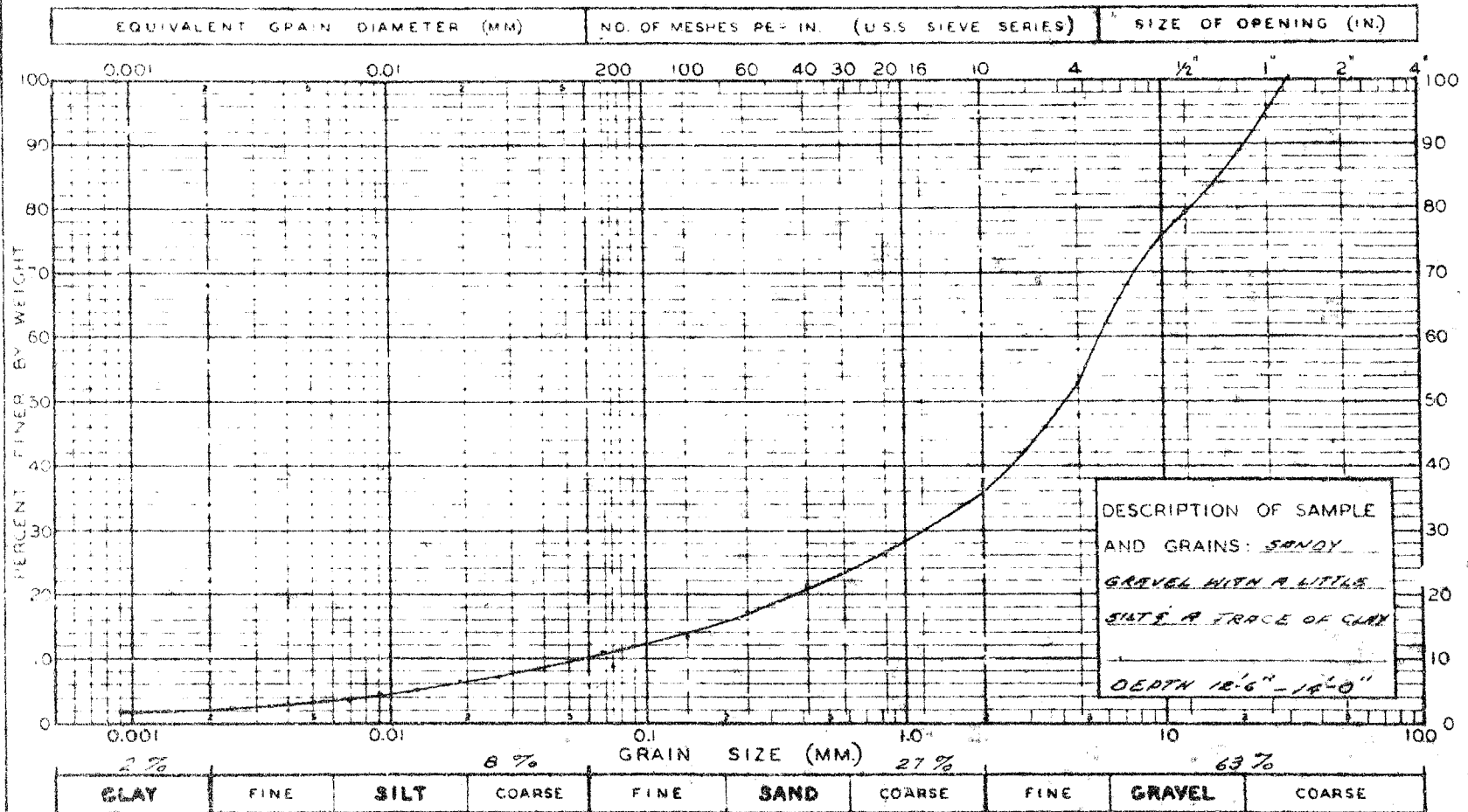
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**CONSULTING ENGINEERS**  
**OTTAWA CANADA**

PROJECT	Queensway at Fairmont	DRILLER	W. Deevy
BOREHOLE NO.	14	RECORDER	G. Bilodeau
SURFACE ELEV'N	220.8 (MSL)	BORING DATE	29 May-3 June, 1959
BOREHOLE DEPTH	36.7'	LOGGING BY	G.L. Genest, P.Eng.
		CORE SIZE	7/8"

DRILLING & WATER CONDITIONS	ELEVATION, % RECOVERY	CORE DESCRIPTION
	220.8	GROUND SURFACE soil - fill and till
no drop of rods no loss of drill water	204.5 50%	BEDROCK SURFACE weathered or fractured shaley lime- stone, dark grey, fine to medium grained, high angled joints, calcite filled to 1/8", thin partings, shale filled, core lengths - from broken to 3", 45° dip
no drop of rods no loss of drill water	200.9 30%	weathered or fractured limestone, dark grey, medium grained, high angled joints, calcite filled to 1/8", core lengths - from broken to 3", probable 45° dip
no drop of rods no loss of drill water	197.8 47%	fractured limestone, dark grey, fine grained, near vertical fractures, high angled joints calcite filled to 1/16", average core lengths 1 1/2", probable 45° dip
no drop of rods no loss of drill water	196.0 69%	fractured limestone, dark grey, medium grained, high angled joints calcite filled to 1/16", partings calcite filled to 1/16", average core lengths - 1 1/2"
no drop of rods no loss of drill water	194.7 73%	fractured limestone, dark grey, medium to fine grained, high angled fractures, shale filling, high angled joints calcite filled to 1/8", average core lengths 2 1/2", 30° - 45° dip
no drop of rods lost drill water at Fl. 194.7	189.1 81%	limestone, dark grey, fine to medium grained, high angled joints, calcite filled to 1/8", shaley partings, average core lengths 2", 45° - 60° dip
	184.1	BOTTOM OF HOLE



# MECHANICAL ANALYSIS OF SOILS



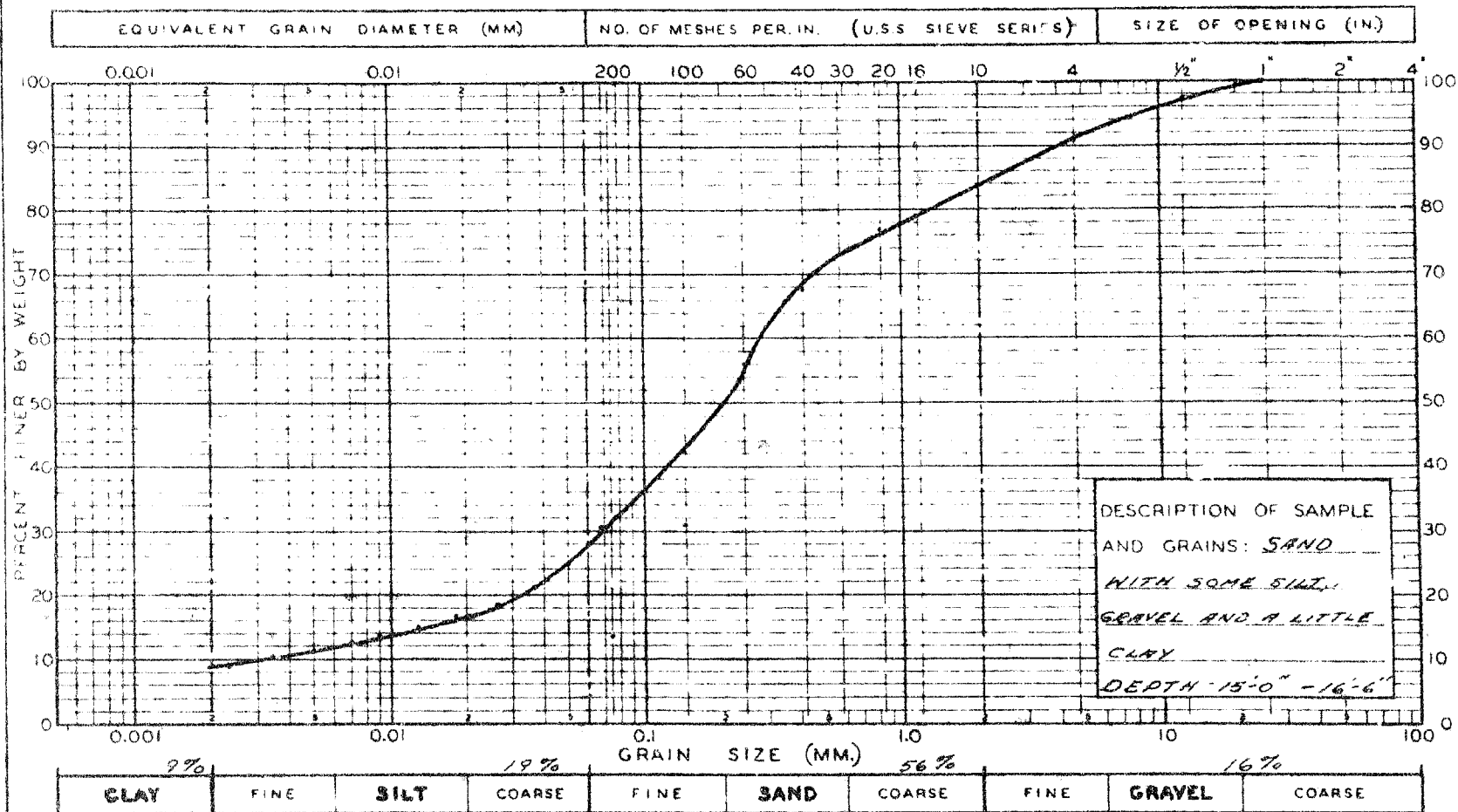
M.I.T. GRAIN SIZE CLASSIFICATION

PROJECT: <u>QUEENSWAY AT FAIRMONT</u>		SAMPLE NO. <u>1-5</u>	<b>McROSTIE &amp; ASSOCIATES</b> CONSULTING ENGINEERS
PLOTTED: <u>C.V.</u>	DATE: <u>DEC 1<sup>st</sup> 1958</u>	REMARKS: <u>0.02 TO .105 SIZE = 11%</u>	
CHECKED: <u>D.M.</u>	DATE: <u>DEC 12<sup>th</sup> 1958</u>		

PLATE NO. 31

SAMPLE NO. 1-5

# MECHANICAL ANALYSIS OF SOILS



M.I.T. GRAIN SIZE CLASSIFICATION

PROJECT: QUEENSWAY AT FAIRMONT

SAMPLE NO. 1-6

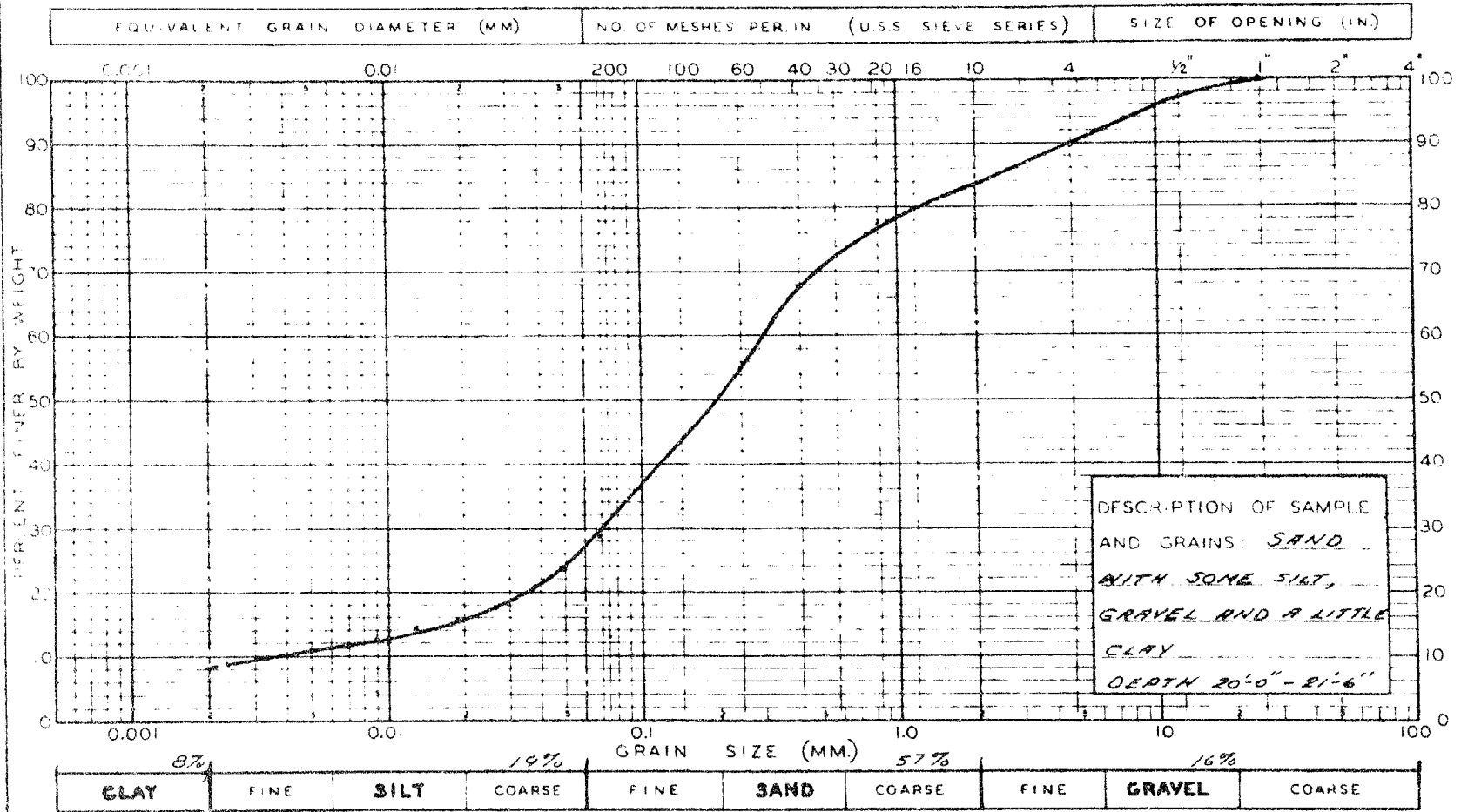
PLOTTED: D.M. DATE: DEC. 12/58

REMARKS: 0.02 TO .105 SIZE = 31%

CHECKED: C.V. DATE: DEC. 18/58

**McROSTIE & ASSOCIATES**  
**CONSULTING ENGINEERS**

# MECHANICAL ANALYSIS OF SOILS



DESCRIPTION OF SAMPLE  
AND GRAINS: SAND  
WITH SOME SILT,  
GRAVEL AND A LITTLE  
CLAY  
DEPTH 20'-0" - 21'-6"

M.I.T. GRAIN SIZE CLASSIFICATION

PROJECT: QUEENSWAY AT FAIRMONT

SAMPLE NO. 1-8

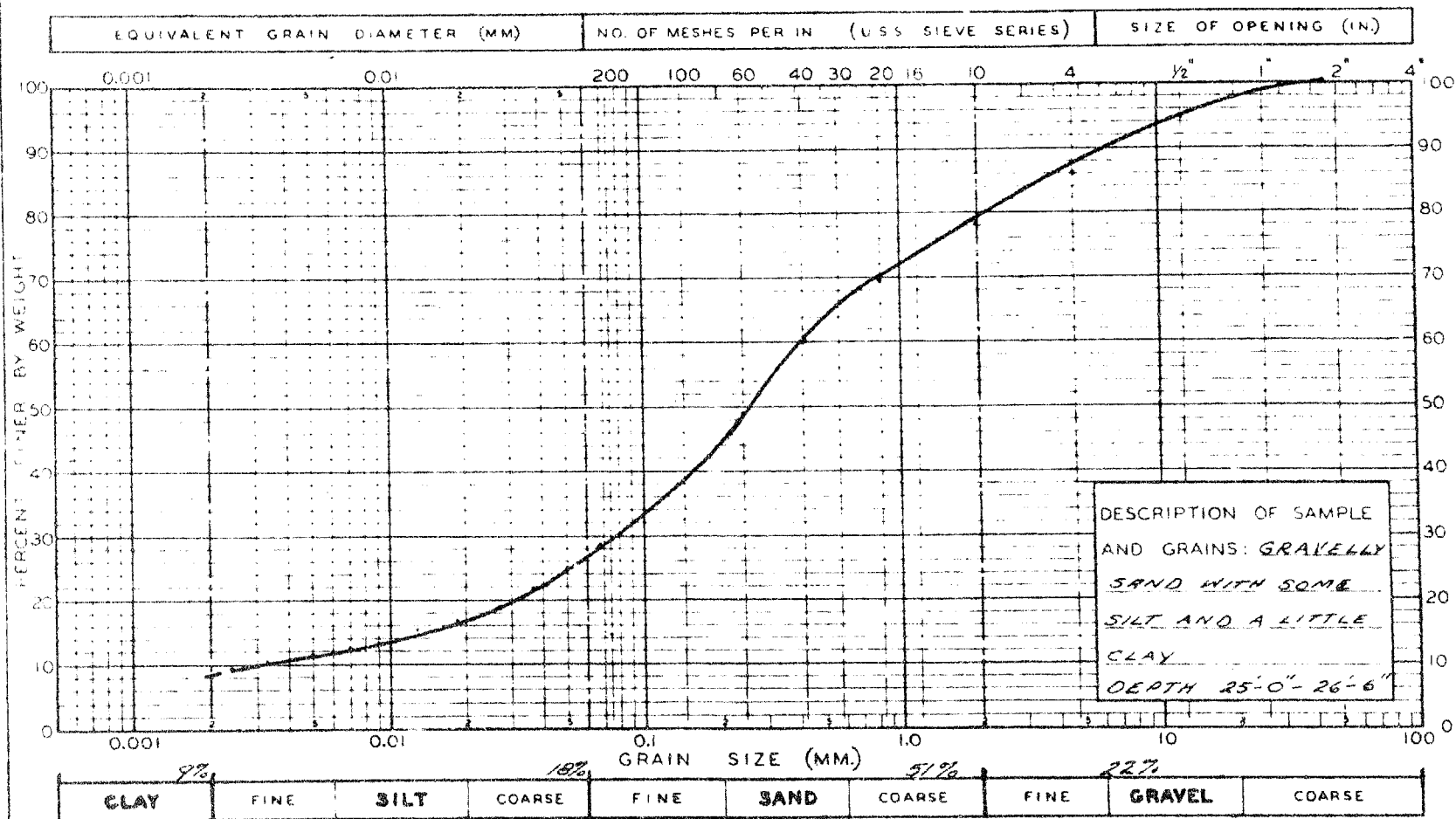
PLOTTED: D.M. DATE: DEC 12<sup>th</sup> 1958

REMARKS: 0.075 TO .105 SIZE = 32%

CHECKED: C.J. DATE: DEC 12<sup>th</sup> 1958

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# MECHANICAL ANALYSIS OF SOILS



M.I.T. GRAIN SIZE CLASSIFICATION

PROJECT: QUEENSBURY AT FAIRMONT

SAMPLE NO. 1-10

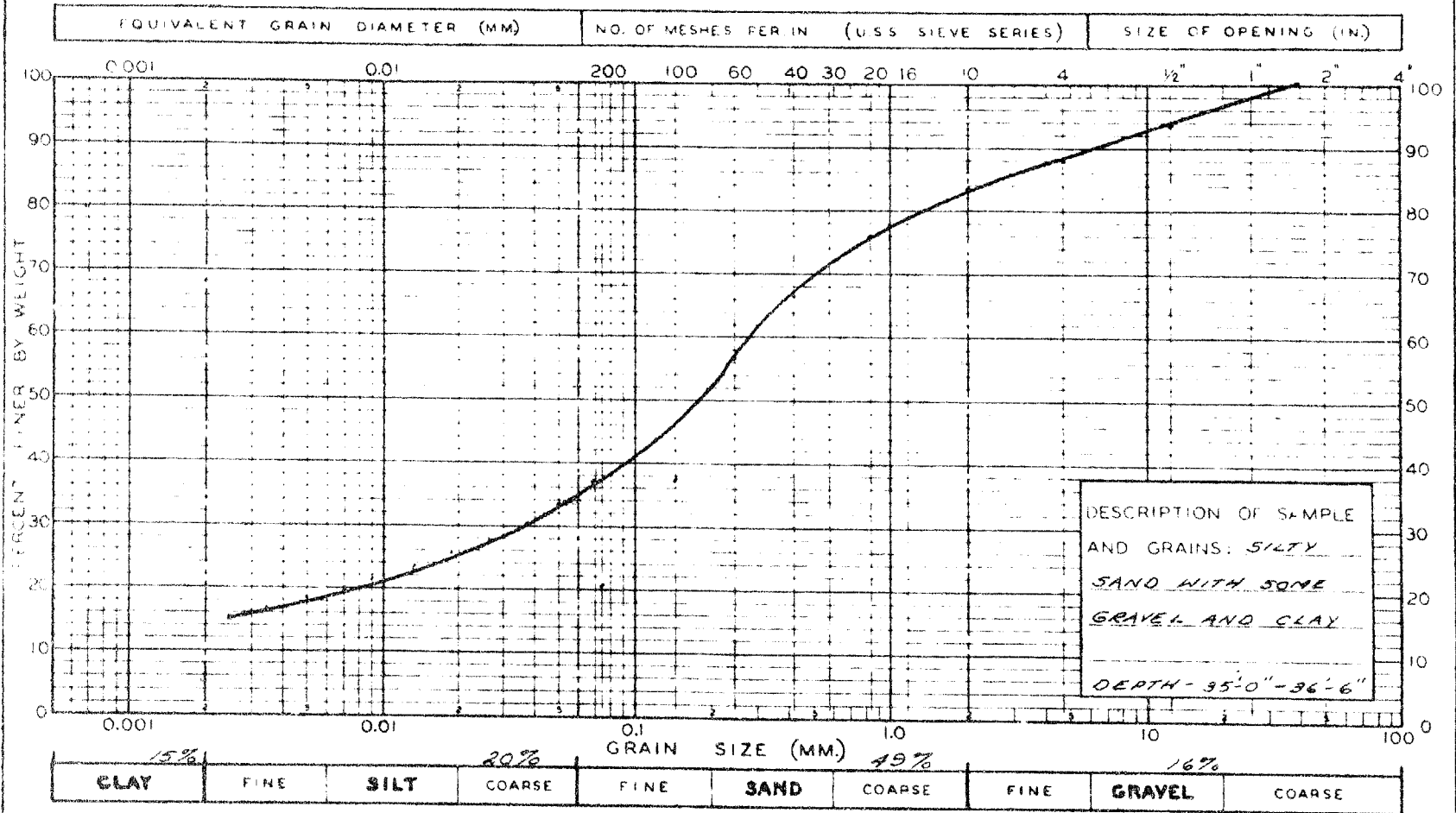
PLOTTED: D. M. DATE: DEC 11<sup>th</sup> 1958

REMARKS: 0.002 TO 105 SIZE = 27%

CHECKED: C. J. DATE: DEC 12<sup>th</sup> 1958

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# MECHANICAL ANALYSIS OF SOILS

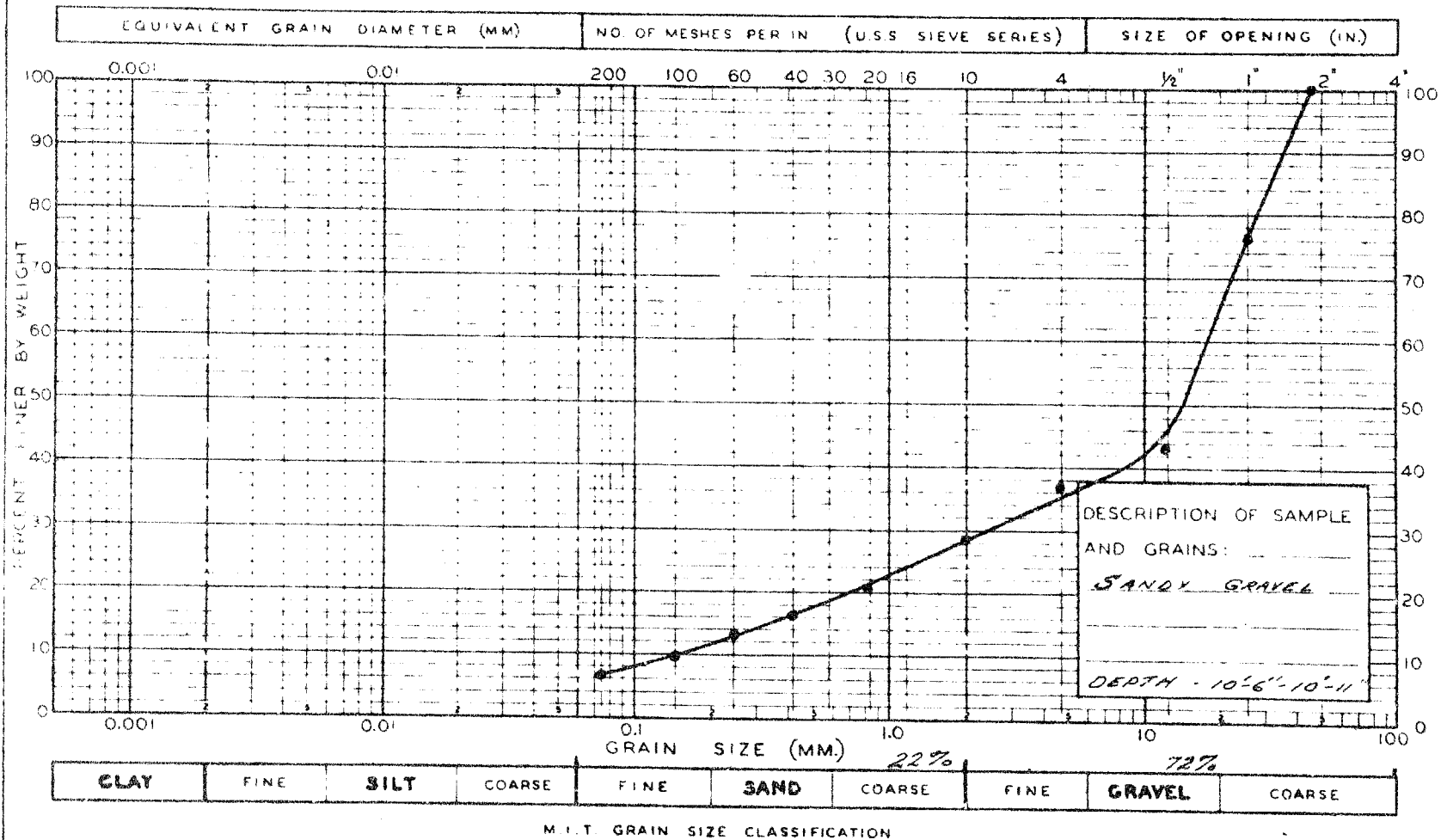


M.I.T. GRAIN SIZE CLASSIFICATION

PROJECT: QUEENSWAY AT FAIRMONT		SAMPLE NO. 1-12	
PLOTTED: O.M.	DATE: DEC 12 <sup>th</sup> /58	REMARKS: 0.075 TO .105 SIZE = 29%	
CHECKED: C.J.	DATE: DEC 12 <sup>th</sup> /58		

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# MECHANICAL ANALYSIS OF SOILS



PROJECT: <u>QUEENSWAY AT FAIRMONT</u>		SAMPLE NO. <u>2-4</u>
PLOTTED: <u>O.M.</u>	DATE: <u>29/11/58</u>	REMARKS: <u>90% TO .075 SIZE = 27%</u>
CHECKED: <u>C.J.</u>	DATE: <u>29/11/58</u>	

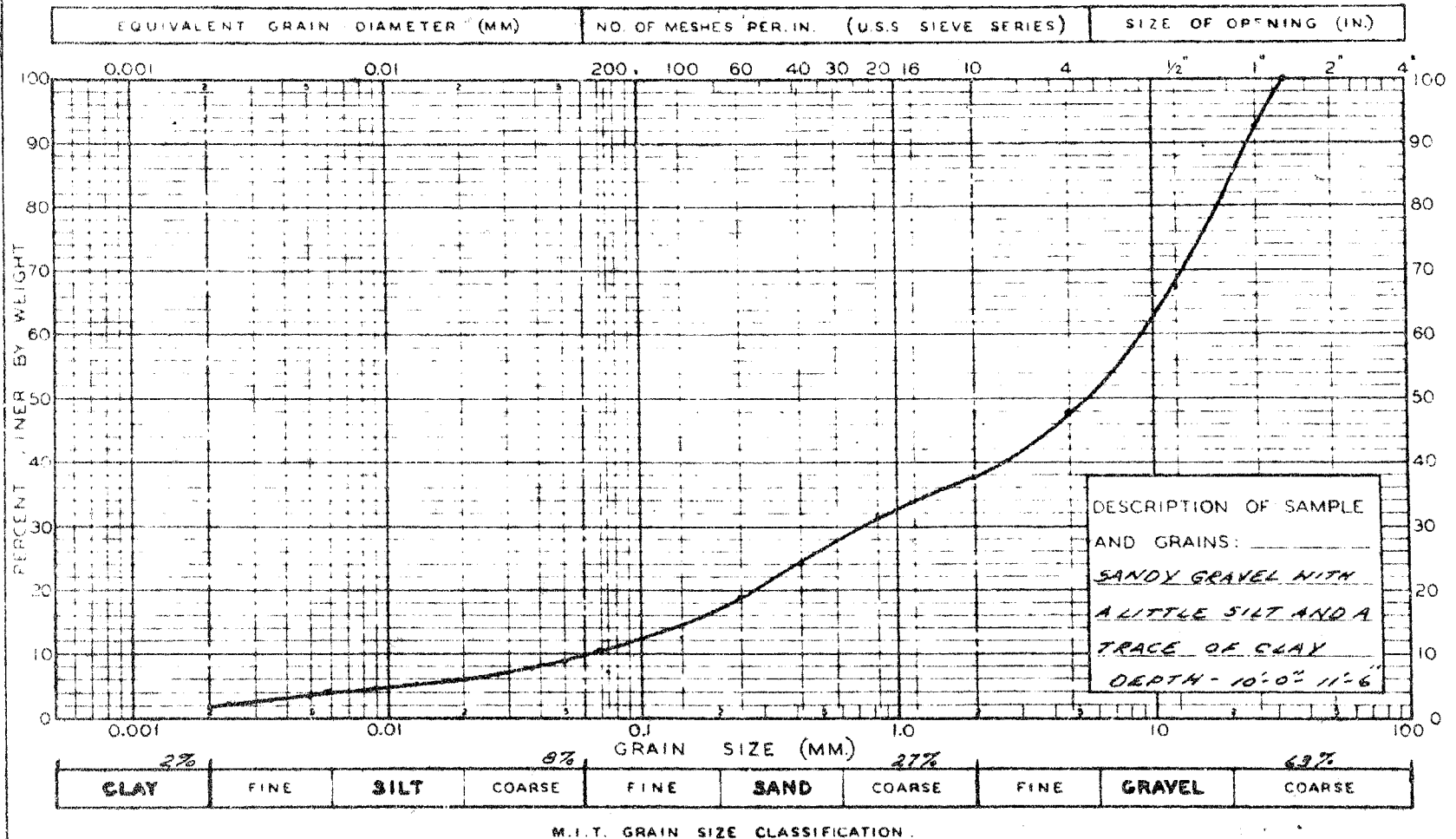
**McROSTIE & ASSOCIATES**  
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SAMPLE NO. 2-4

FORM 100

PLATE NO. 30

# MECHANICAL ANALYSIS OF SOILS



PROJECT: QUEENSWAY AT FAIRMONT

SAMPLE NO. 3-4

PLOTTED: D.M. DATE: 29/11/59

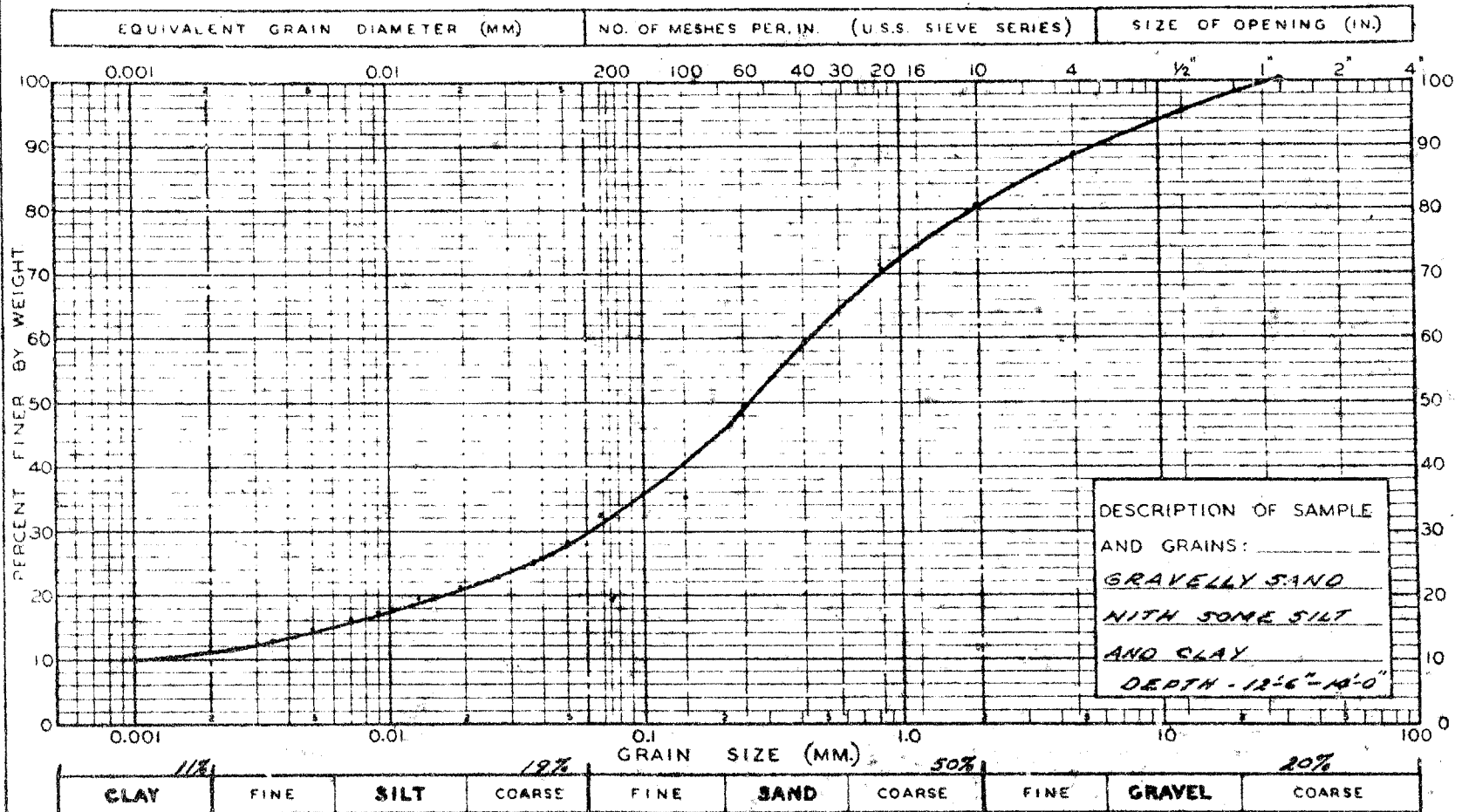
REMARKS: 0.075 TO 1.05 SIZE = 12%

CHECKED: B.M. DATE: 29/11/59

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SAMPLE NO. 3-4

# MECHANICAL ANALYSIS OF SOILS



M.I.T. GRAIN SIZE CLASSIFICATION

PROJECT: QUEENSWAY AT FAIRMONT

SAMPLE NO. 3-5

PLOTTED: D.M. DATE: 29/11/58

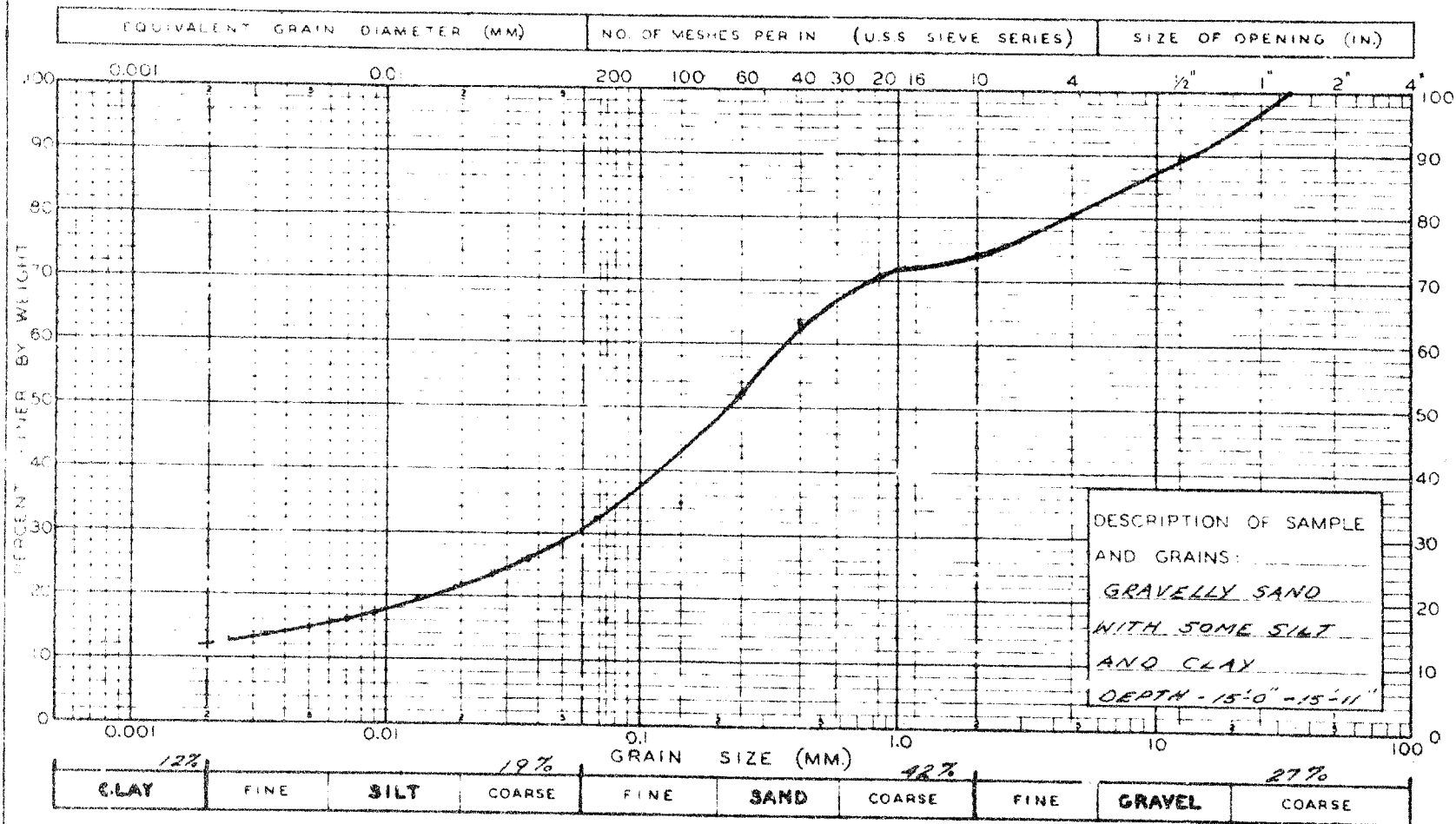
REMARKS: 0.02 TO .105 SIZE = 28%

CHECKED: B.M. DATE: 29/11/58

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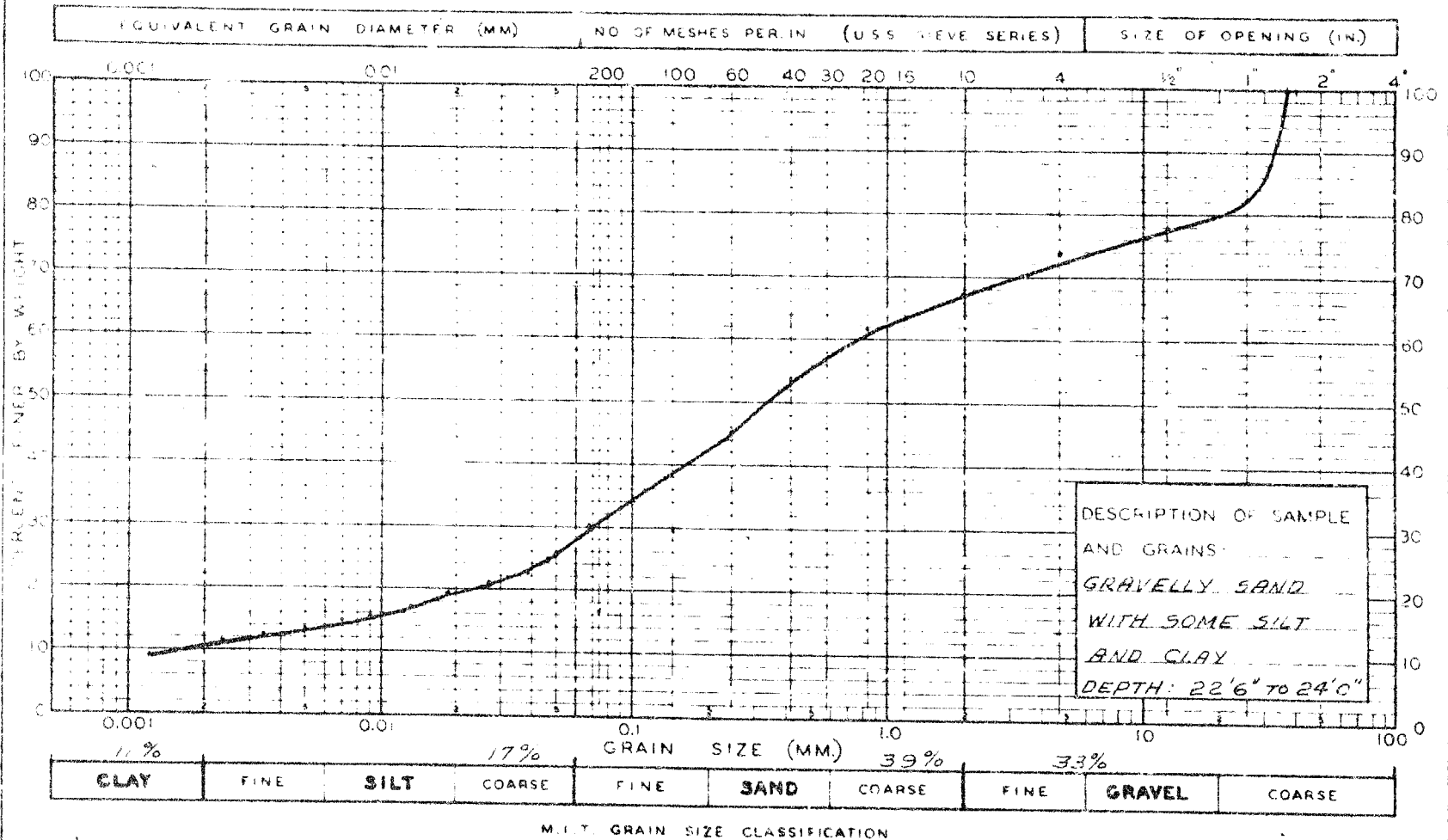
# MECHANICAL ANALYSIS OF SOILS



PROJECT: <u>QUEENSWAY AT FAIRMONT</u>		SAMPLE NO. <u>3-6</u>	
PLOTTED: <u>D M</u>	DATE: <u>12/12/58</u>	REMARKS: <u>.002 TO .105 SIZE = 28%</u>	
CHECKED: <u>C J</u>	DATE: <u>12/12/58</u>		

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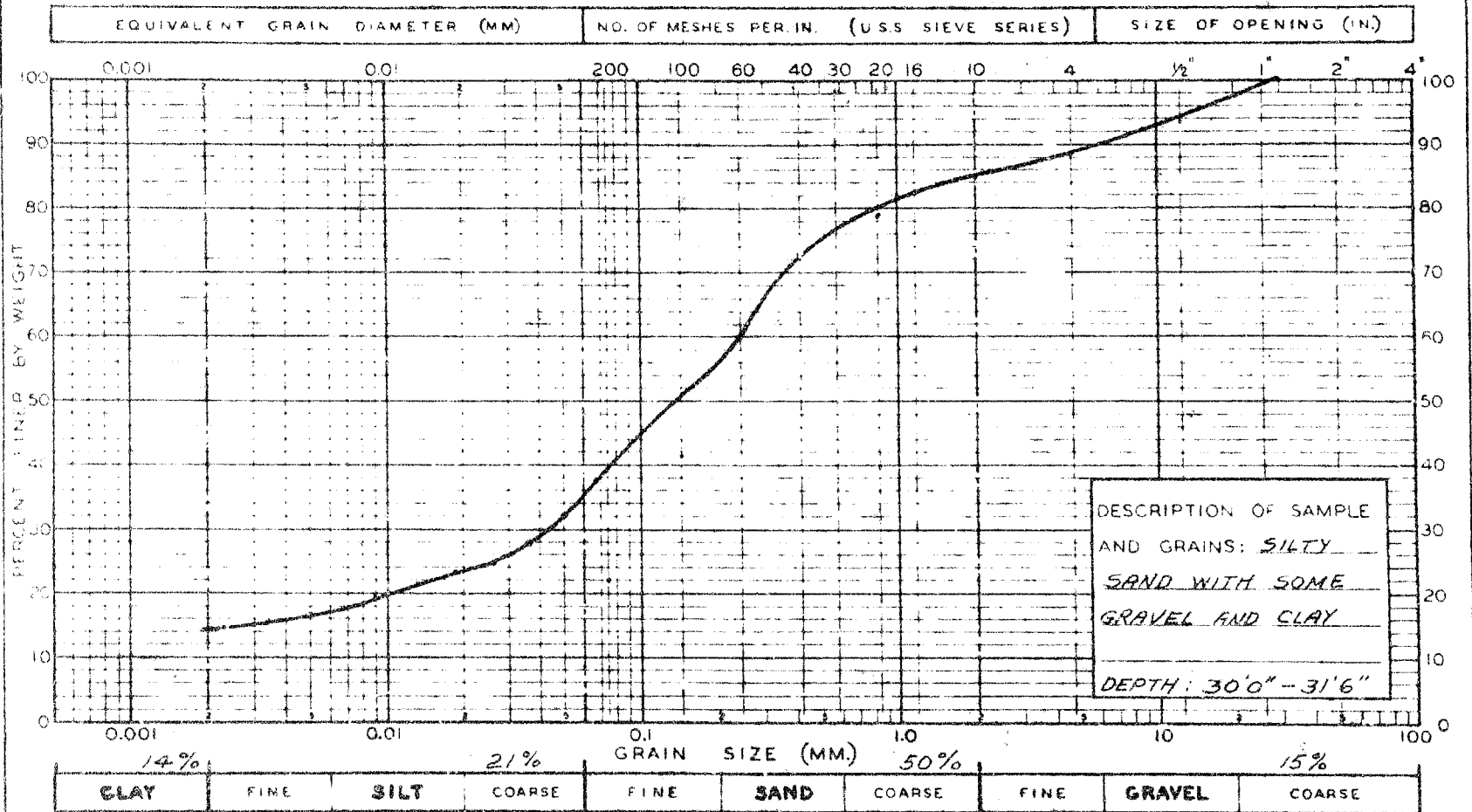
# MECHANICAL ANALYSIS OF SOILS



PROJECT: QUEENSWAY AT FAIRMONT		SAMPLE NO. 3-9
PLOTTED: C.J. CHECKED: D.M.	DATE: 12-12-58 DATE: 12-12-58	REMARKS: .002 TO .105 SIZE = 25%

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# MECHANICAL ANALYSIS OF SOILS

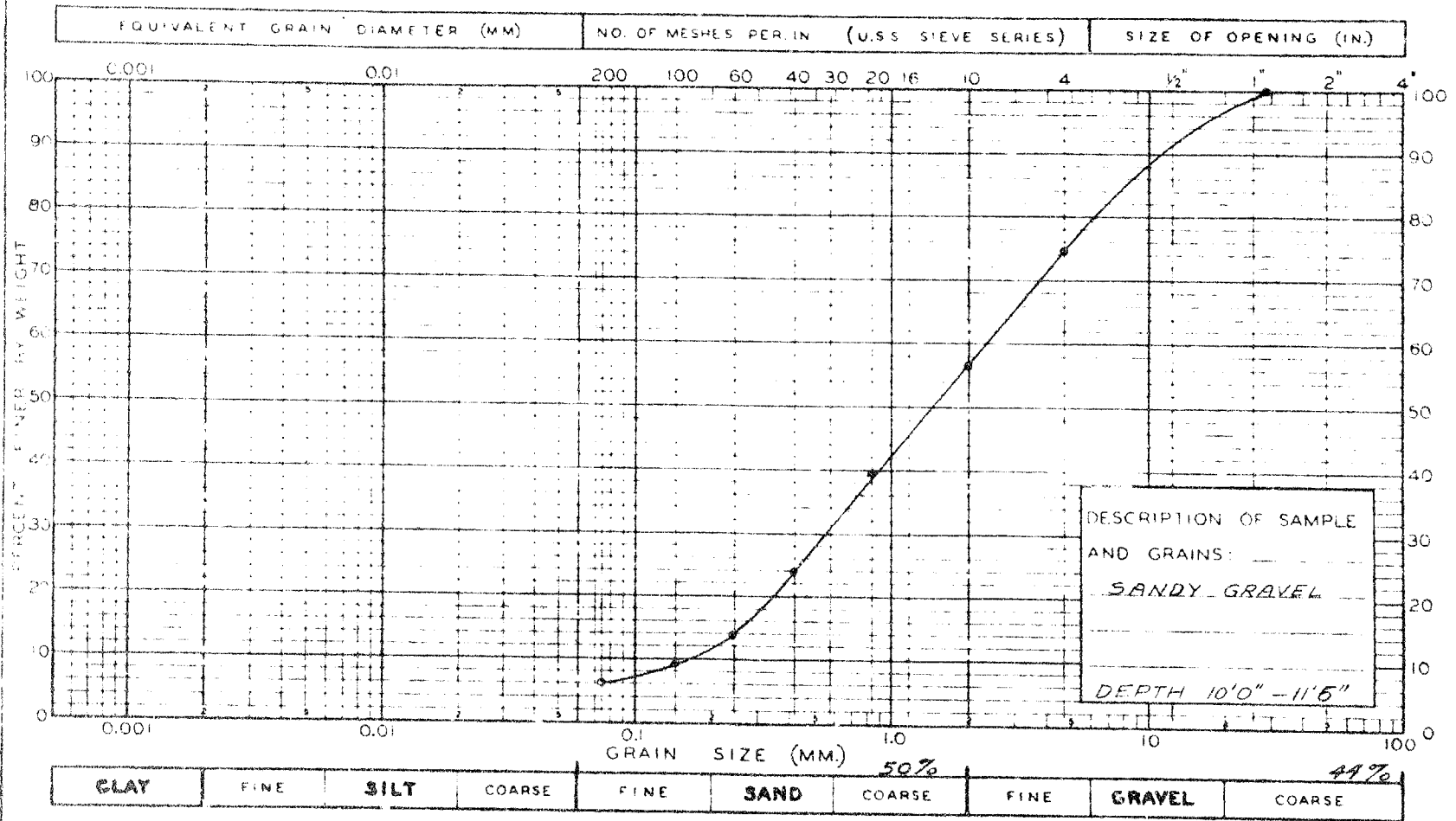


M.I.T. GRAIN SIZE CLASSIFICATION

PROJECT: <u>QUEENSWAY AT FAIRMONT</u>		SAMPLE NO. <u>3-11</u>	
PLOTTED: <u>D.M.</u>	DATE: <u>12-12-58</u>	REMARKS: <u>0.002 TO .105 SIZE = 34%</u>	
CHECKED: <u>C.J.</u>	DATE: <u>12-12-58</u>		

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# MECHANICAL ANALYSIS OF SOILS



PROJECT: QUEENSWAY AT FAIRMONT

SAMPLE NO. 4-4

PLOTTED: D.M. DATE: 28/11/58

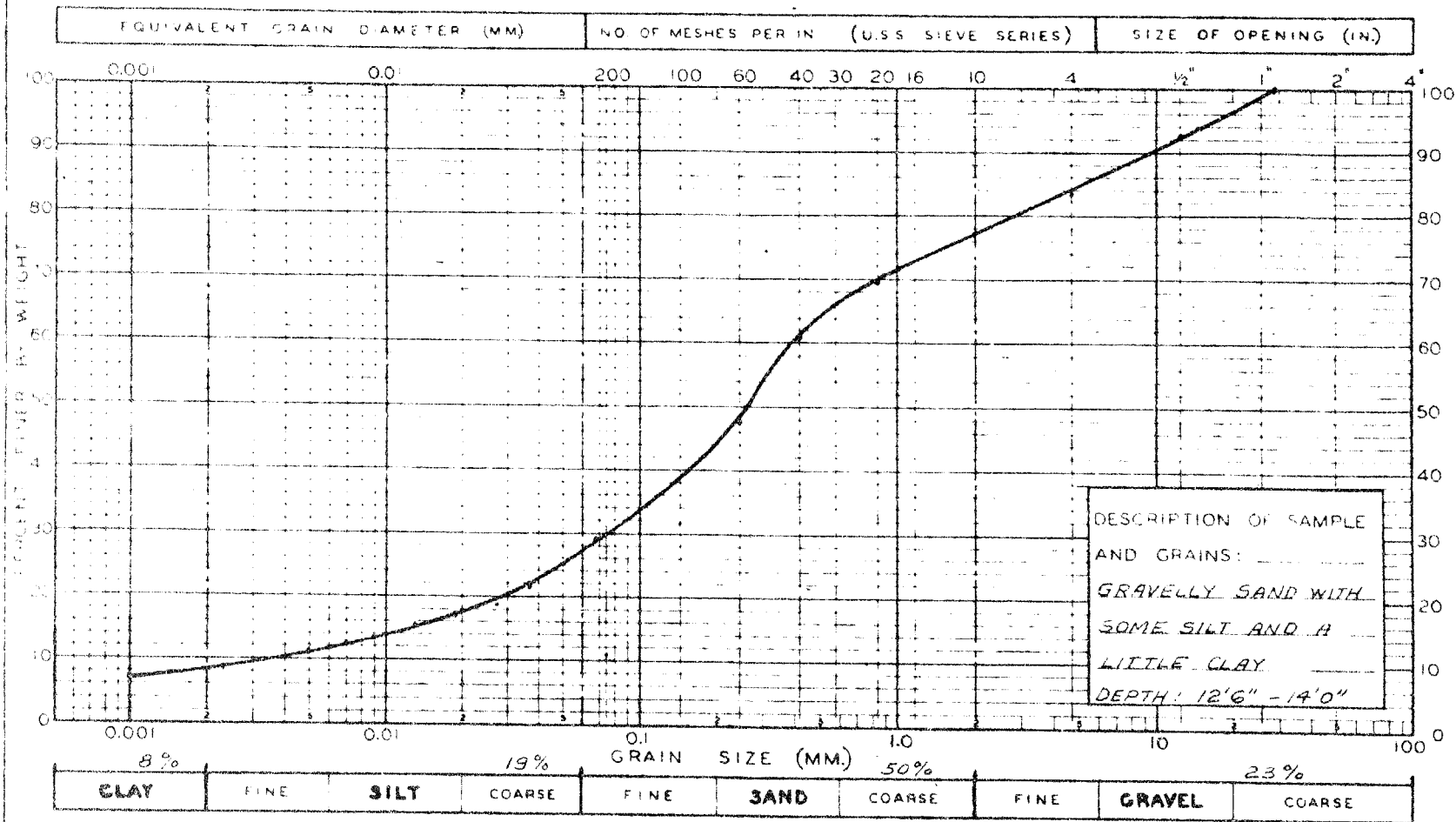
REMARKS: 002 TO 105 SIZE = 2%

CHECKED: C.V. DATE: 28/11/58

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SAMPLE NO. 4-4

# MECHANICAL ANALYSIS OF SOILS



PROJECT: QUEENSWAY AT FAIRMONT

SAMPLE NO. 4-5

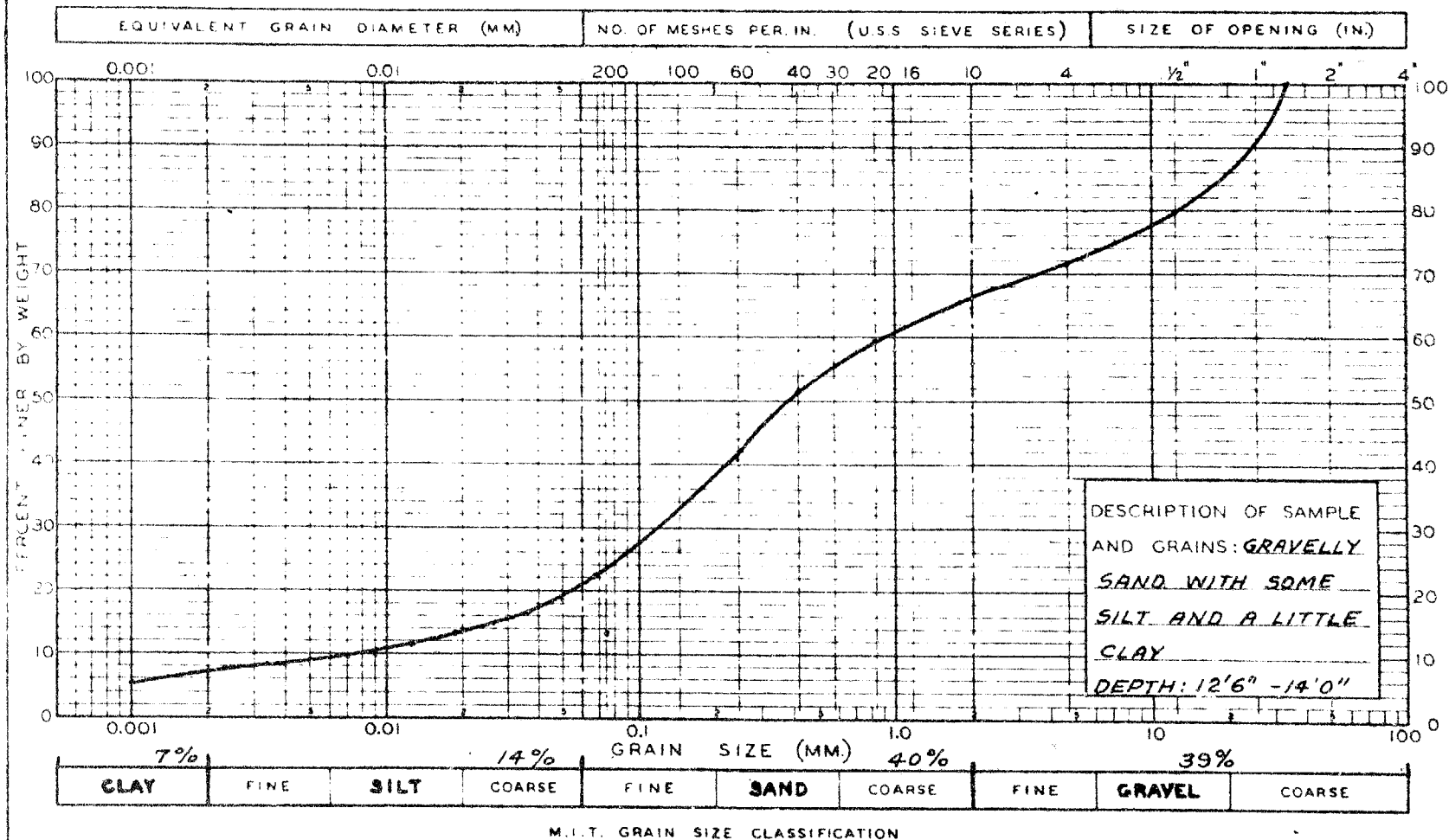
PLOTTED: D.M. DATE: 29-11-58

REMARKS: .002 TO .105 SIZE = 29%

CHECKED: B.M. DATE: 29-11-58

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# MECHANICAL ANALYSIS OF SOILS



PROJECT: QUEENSWAY AT FAIRMONT

SAMPLE NO. 5-5

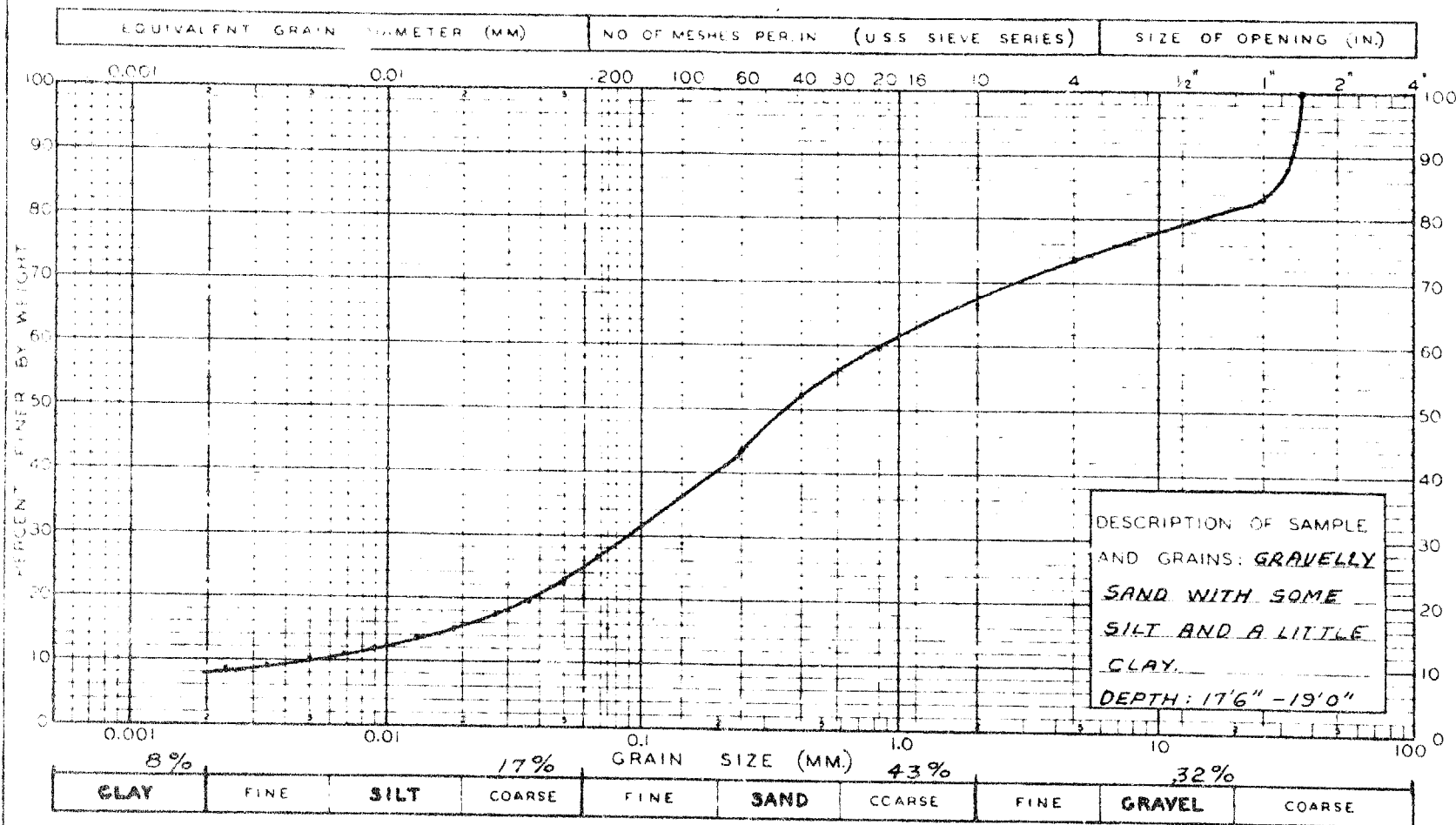
PLOTTED: D.M.      DATE: 12-12-58

REMARKS: 0.002 TO .105 SIZE = 23%

CHECKED: C.U.      DATE: 12-12-58

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# MECHANICAL ANALYSIS OF SILTS



PROJECT: QUEENSWAY AT FAIRMONT

SAMPLE NO. 5-7

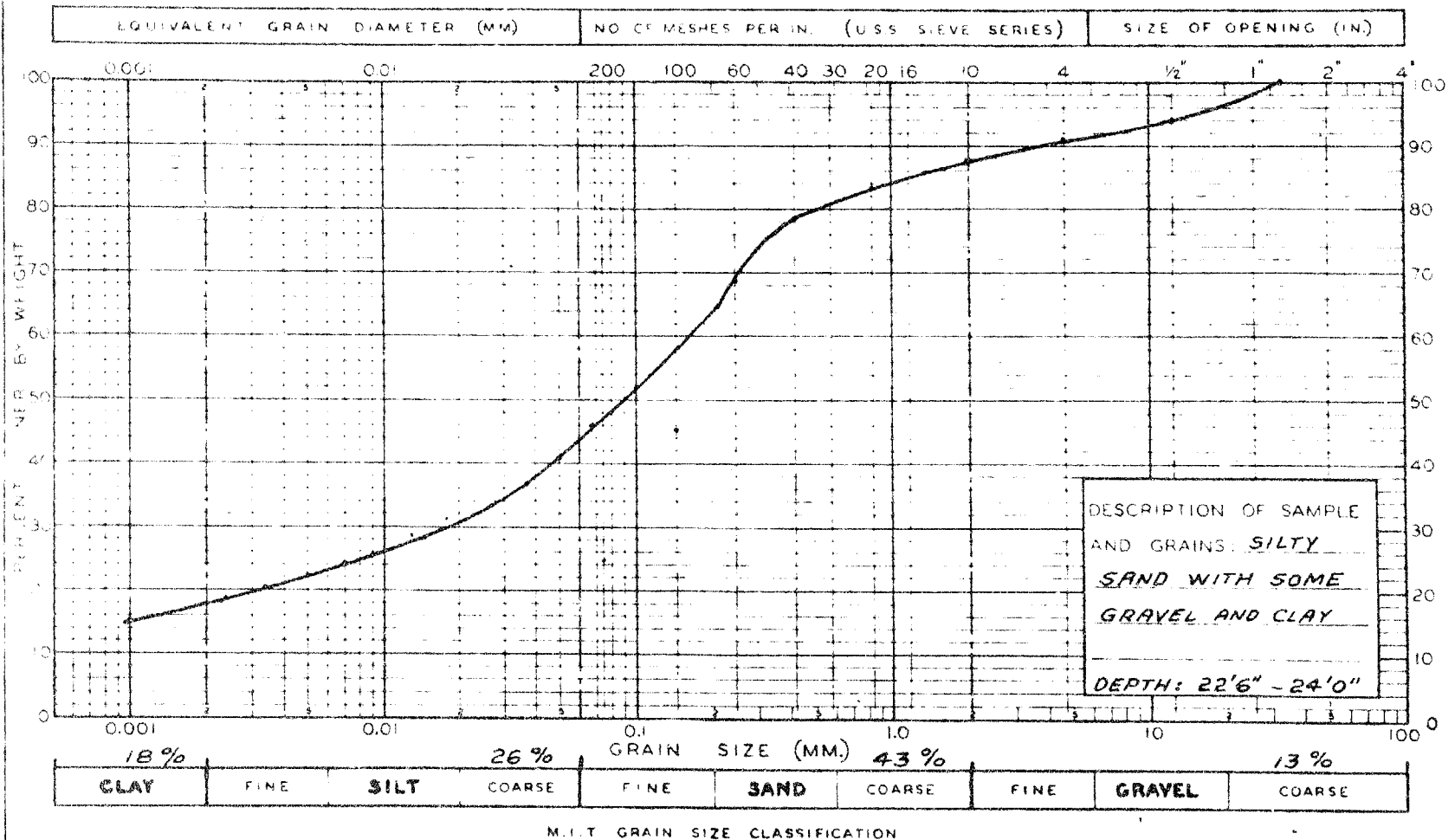
PLOTTED: D.M. DATE: 12-12-58

REMARKS: .002 TO .105 SIZE = 26%

CHECKED: C.J. DATE: 12-12-58

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# MECHANICAL ANALYSIS OF SOILS

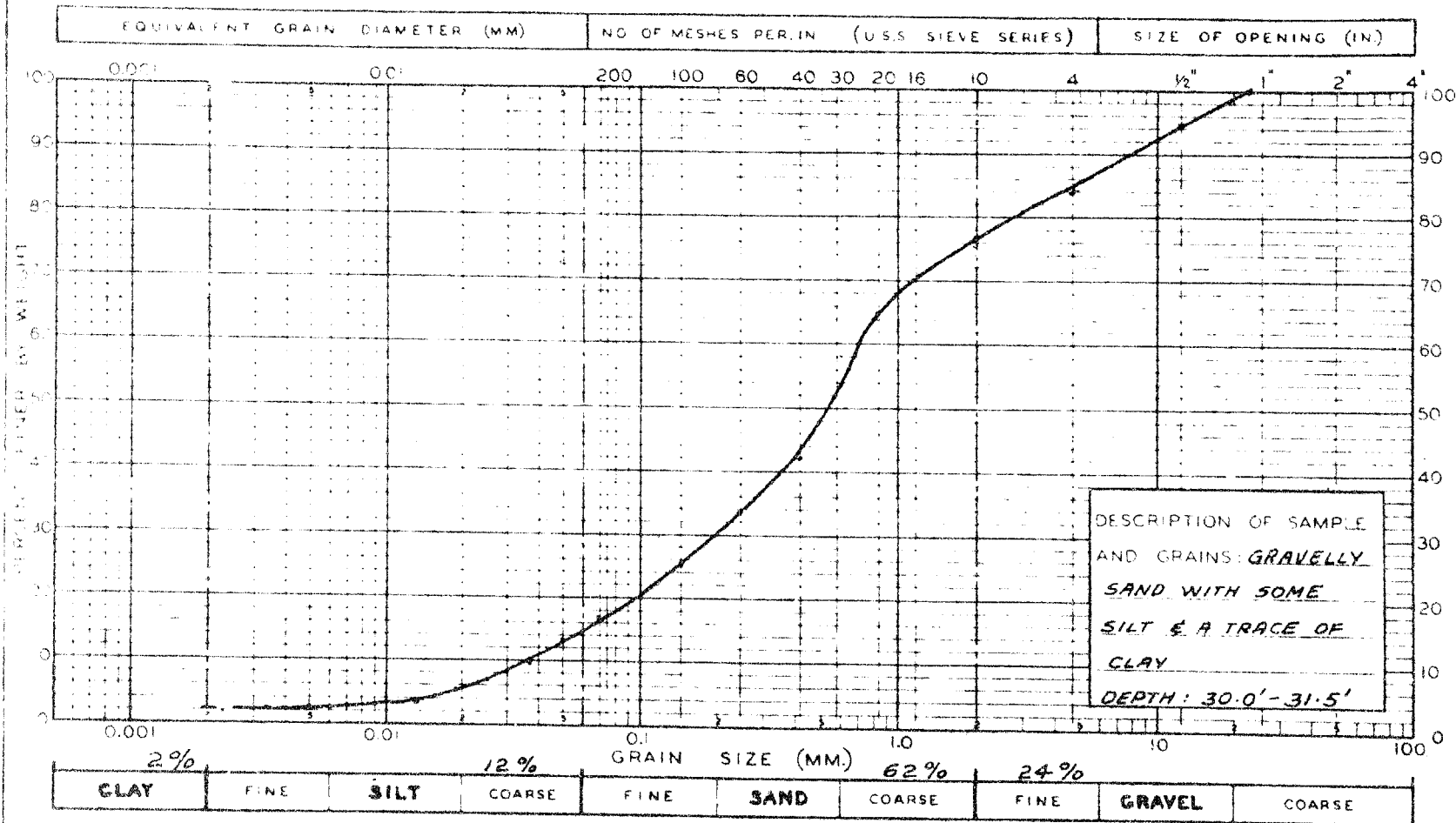


PROJECT: <u>QUEENSWAY AT FAIRMONT</u>		SAMPLE NO. <u>5-9</u>
PLOTTED: <u>B.M.</u>	DATE: <u>12-12-58</u>	REMARKS: <u>.002 TO .105 SIZE = 37%</u>
CHECKED: <u>C.J.</u>	DATE: <u>12-12-58</u>	

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# MECHANICAL ANALYSIS OF SOILS



M. I. T. GRAIN SIZE CLASSIFICATION

PROJECT: QUEENSWAY AT FAIRMONT

SAMPLE NO. 7-6

PLOTTED: D.M. DATE: 13-1-59

REMARKS: .002 TO .105 SIZE = 21%

CHECKED: G.B. DATE: 13-1-59

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