

60-F-316C

W.P. 113-59

Hwy. # 401

SOUTH RAISIN RIVER



Memo to Mr. A. M. Toye,  
Bridge Engineer.  
From Materials & Research Section. Date February 10, 1960.  
Subject FOUNDATION INVESTIGATION - by  
Racey, MacCallum & Associates.

Attention: Mr. S. McCombie.

Re: South Raisin River, Near Cornwall,  
Lots 7 & 8, Hwy. #401, Ottawa, Ont.  
District #9 -- W.P. 113-59.

Attached please find a copy of the foundation report  
for the above site, submitted by Racey, MacCallum & Associates.

Reference to the contents of this report shows that  
the subsoil stratigraphy consists of a deposit of sensitive,  
normally consolidated marine clay, extending from ground surface  
to a depth averaging 30 feet. This stratum is underlain by a  
layer of dense, glacial till, generally 15 to 20 feet in thick-  
ness. The till is underlain by sound limestone bedrock.

Artesian pressure was noted at the contact of the  
bedrock and glacial till.

Based on the information presented in this report, it  
is our recommendation that the structure be supported on small  
displacement 'H' piles driven to practical refusal in the under-  
lying dense, glacial till stratum. Pile lengths should not ex-  
ceed 45 feet. Small displacement piles are preferable to timber  
or monotube piles - particularly at the abutment locations, due  
to the sensitive marine clay.

If you have any questions regarding the contents of this  
report, or our foregoing comments, please do not hesitate to call  
our Office.

LGS/MdF

Attach.

cc: Messrs. A. M. Toye (2)  
H. A. Tregaskes  
D. G. Ramsay  
H. J. Ford  
L. E. Walker  
J. E. Gruspier  
A. Watt  
Foundations Office  
Gen. Files.

*L. G. Soderman*

L. G. Soderman,  
PRINCIPAL SOILS & FOUNDATIONS ENGINEER

*BA 457-A.*

RACEY, MacCALLUM AND ASSOCIATES  
LIMITED

A COMPANY OWNED, DIRECTED AND OPERATED BY

**Consulting Engineers**  
AND ASSOCIATED STAFF

MONTREAL

VANCOUVER

TORONTO

TORONTO DIVISION  
27 CARLTON STREET

DONALD C. MACCALLUM, B.ENG., M.E.I.C., P.ENG.

K. JOHN RACEY, B.Sc., M.E.I.C., P.ENG.

GEORGE L. HOUGHTON, A.M.I.MECH.E., M.E.I.C., P.ENG.

Reference: S-500/T-2037

- Report -

9th February, 1960

60-F-316C

Department of Highways for Ontario,  
Materials and Research Section,  
c/o Parliament Buildings,  
TORONTO - Ontario.

Attention: Mr. L. G. Soderman

RE: SOIL INVESTIGATION AT  
SOUTH RAISIN RIVER, NEAR CORNWALL  
ONTARIO, W.P. 113-59

Dear Sir,

The enclosed report presents the results of our foundation investigation at the above location.

We hope the report is satisfactory to you; if you have any questions about it please do not hesitate to get in touch with us.

Thank you for this opportunity of being of service to you.

Yours very truly,  
RACEY, MacCALLUM AND ASSOCIATES LIMITED,

*J. J. Schoustra*  
J. J. Schoustra, P. Eng.,  
Divisional Soil Engineer.

JJS/JP

Department of Highways for Ontario,  
Materials and Research Section,  
c/o Parliament Buildings,  
Toronto - Ontario.

SCIL INVESTIGATION AT  
SOUTH RAISIN RIVER, NEAR CORNWALL  
ONTARIO, W.P. 113-59

Reference: S-500/3-2037  
- Report -

Racey, MacCallum and Associates  
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9th February, 1960

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TORONTO

TORONTO DIVISION  
27 CARLTON STREET

Reference: S-500/T-2037

- Report -

9th February, 1960

SOIL INVESTIGATION AT  
SOUTH RAISIN RIVER, NEAR CORNWALL  
ONTARIO, W.P. 113-59

INTRODUCTION :

The field investigation to determine the subsoil conditions at the site was carried out from 7th to 21st December, 1959 and consisted of seven borings and eight cone penetrometer tests. On arrival at the laboratory the samples were subjected to various tests to determine the strength and settlement characteristics of the soil.

The following paragraphs present a detailed description of the field and laboratory results and their consequences with regard to various subsoil problems. It is understood that a previous soil investigation had been conducted for the bridge structure proper and that a pile foundation had been decided on. No further study in this regard, therefore, was undertaken for this report. (It might be noted here, however, that some problems might occur if the piles are to be driven through the boulder till overlying the limestone bed rock.)

PRELIMINARY GEOLOGICAL STUDY :

The site under investigation is located in an area known as the St. Lawrence-Ottawa lowland. Following the recession of the last glacier, this area was covered by an arm of the sea, known as the Champlain Sea. The till plain was subsequently buried under the sediments of this sea. These water-lain deposits are deep silty-clays commonly known as "Leda" clays. With the removal of the glacier load, the uplift of the earth's crust together with the deposited sediments gradually progressed until exposed as the present-day clay plains.

Reference : S-500/T-2037  
- Report - Continued.

9th February, 1960

#### SCOPE OF FIELD INVESTIGATION

The borings (locations are shown on Enclosure 1) were carried out using a standard diamond-drilling rig equipped for sampling with a 2 inch outside diameter split spoon and 2 inch inside diameter thin-walled Shelby tubes. Boreholes were advanced by driving HX casing and washing, with samples being taken at regular intervals. In addition to obtaining samples, several vane-torsional tests were carried out at various depths to obtain the in-situ soil shear strength both in the undisturbed and remoulded state. Once the dense till was reached the boring was advanced by running AX casing. In the underlying bed rock a core bit was used.

Adjacent to each borehole a 60 degree point angle cone was driven to obtain a continuous record of soil density. The driving energy for both the split spoon and cone penetrations was a 110 pound hammer at a 30 inch drop.

The results of the borings and cone tests are shown on Enclosures No. 2 to 9.

#### SCOPE OF LABORATORY WORK

Laboratory work consisted of Unconfined Compression and Triaxial tests to determine the strength characteristics of the silty-clay; and Consolidation and Atterberg Limit tests to determine the settlement characteristics.

The results of the strength tests and Atterberg tests are shown on Enclosures No. 2 to 9; and the results of the consolidation tests are plotted as "e-log. p" curves on Enclosures No. 10 and 11.

#### SUBSOIL CONDITIONS

A soil profile along the proposed centre-line is shown on Enclosure No. 1. The thickness of the soft sensitive silty-clay is approximately 25 feet in the vicinity of Borehole No. 1 and gradually diminishes to zero westward i.e. at Borehole No. 8. The clay layer is overlain by approximately 5 feet of silty-sand to silty-clays with sand; and is underlain by a dense gravelly-sand glacial till down to a sound limestone bed-rock. The glacial till just overlying the bed-rock has an

Reference : S-500/T-2037  
- Report - Continued.

9th February, 1960

appreciable amount of boulders.

An artesian condition was encountered in all boreholes at approximately the inter-face of the bed rock and the over-lying boulder till. The pressure head was to approximately 3 feet above ground level or Elevation 188.0 feet.

As wash water was used in advancing the borings, no accurate prediction of the ground water level could be made. However, other evidence such as grey colouring and saturation of the clay samples would seem to indicate that the lowest ground water table usually exists in the upper few feet of the silty-clay stratum.

DISCUSSION OF RESULTS :

The results of consolidation tests indicate that the clay had been pre-consolidated to approximately 2800' to 3000' psf. According to the geology of the area it is doubtful that the clay had been subjected to any drying or overburden load. It would seem probable therefore that as it is a marine clay, the pre-consolidation might be attributed to chemical action.

The shear strength of the clay subsoil is relatively uniform throughout the whole depth. Values of shear strength as determined by the in-situ vane-torsional tests average out to approximately 600 psf, whereas those determined by the laboratory unconfined compression tests average 300 psf. The large variation may possibly be explained by some of the following factors.

- i) A general structural disturbance caused by sampling and preparation procedures.
- ii) A micro-structural disturbance not readily visible to the eye but which is in all probability present, as the silty-clay is quite sensitive.
- iii) The removal or reduction of in-situ stresses during sampling.

It has been shown by various authorities that vane-torsional test results give higher values of shear strength

Reference : S-500/T-2037  
- Report - Continued.

9th February, 1960

than those computed from unconfined compression tests and may be as much as twice the unconfined value.

From the foregoing considerations it may be concluded that soil shear strength as determined by the in-situ vane-torsional test to be the more correct value.

Remoulded shear strength values as determined by in-situ vane torsional tests indicate the silty-clay as being sensitive. This fact tends to confirm the foregoing argument in that it shows the soil as having the potential to be easily disturbed by ordinary sampling and testing procedures. This peculiar property however is characteristic of most sensitive clays and once the disturbing effect has stopped or is removed, the soil should recover most or all of its original strength within a period of one or two months.

#### EMBANKMENT SETTLEMENT :

Settlement calculations based on the results of the consolidation tests indicate that the settlement under the centre of the embankment fill will be approximately 9 inches, and approximately 3 inches under the edge of the fill. These values are in all probability greater than actual due to sample disturbance, as pointed out in the preceding paragraphs. The settlement will be 50% and 90% complete in approximately 2 and 9 months respectively.

In the calculations the following conditions were assumed;

- i) Embankment height approximately 10 feet.
- ii) Embankment average width 70feet.
- iii) Unit weight of fill 140pcf.
- iv) Ground Water Table at ground surface.

#### EMBANKMENT STABILITY :

Stability analyses were carried out for both a general embankment fill and an abutment fill. Sketches of each case are shown on Enclosures No. 12 and 13. The results

Reference : S-500/T-2037  
- Report - Continued.

9th February, 1960

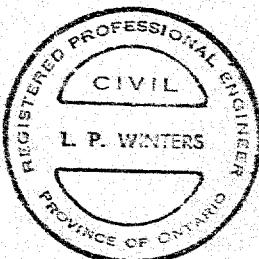
of the various trial solutions are shown on the respective enclosure. From these results it can be seen that the Safety Factor is roughly 2.1 for the embankment fill and 2.2 for the abutment fill. A base failure was assumed for each case.

CONCLUSIONS AND RECOMMENDATIONS :

Summarizing the foregoing results and considerations the following conclusions and recommendation seem warranted.

1. The soil profile consists of a stratum of sensitive silty-clay averaging 25 feet on the east side of the river, decreasing gradually westward. Underlying there is a dense gravel-sand-boulder till over a sound limestone bed-rock.
2. Evidence indicates that the ground water table usually exists within a few feet of ground surface. An artesian condition was encountered at the interface of the boulder till and limestone bed rock, with a pressure head approximately 3 feet above ground level.
3. The settlement under the embankment fill will be approximately 9 inches at the centre and 3 inches at the edges.
4. The Safety Factor against a slip-circle failure is roughly 2.1 under the road embankment fill and 2.2 under the abutment fill.

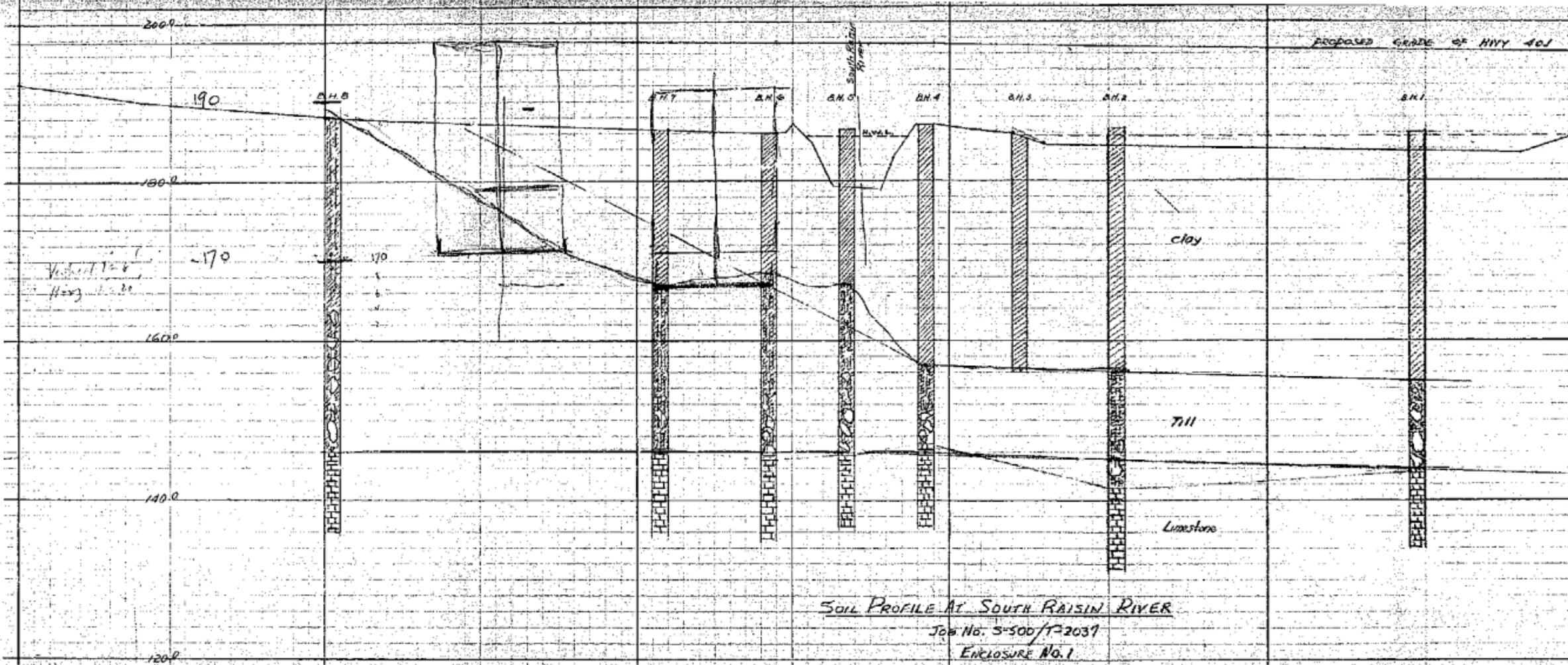
LPW/JP



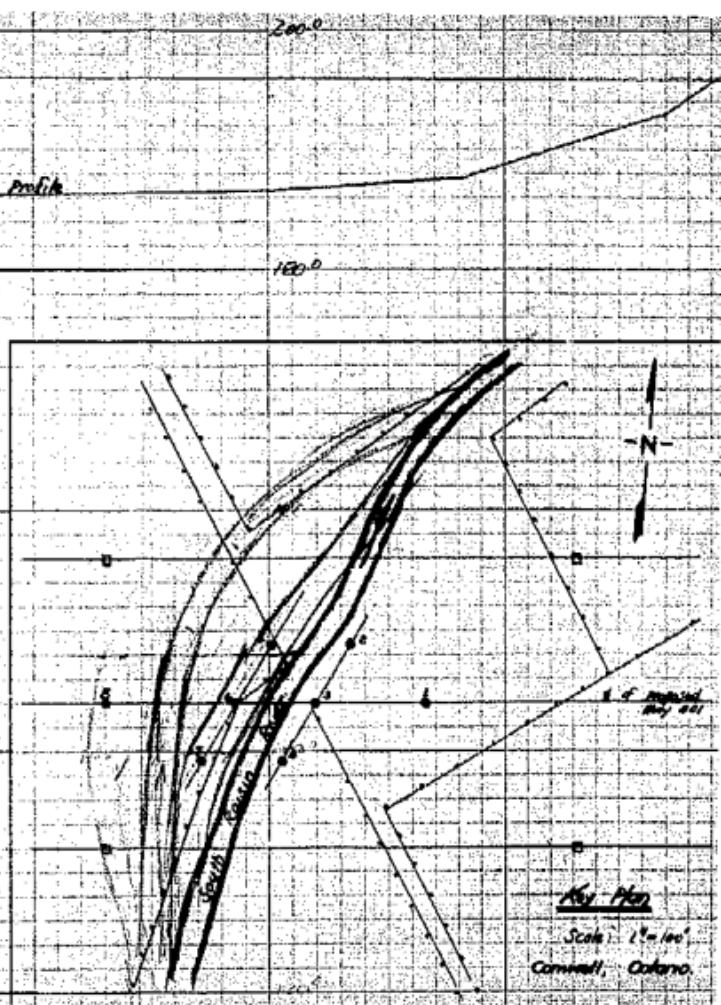
L. P. Winters

Lorne P. Winters, P.Eng.,  
Project Engineer.

2009



2009



Key Map

Scale 1"=100'

Compton, Ontario

## RACEY MacCALLUM AND ASSOCIATES LTD.

Foundation Engineering Division

## Engineering Data Sheet for Borehole 1

Project FOUNDRY INVEST. BRIDGE SITES OVER SOUTH RAISIN RIVER.

Location: CORNWALL, ONTARIO.

Hole Location: See Enclosure No 1.

Hole Elevation and Datum: 184.5 feet

Field Supervisor: J.W. Prep: J.W.

Driller: X.G. Checked: Date:

## LEGEND

Soil Strength 1

Unstratified sandstone

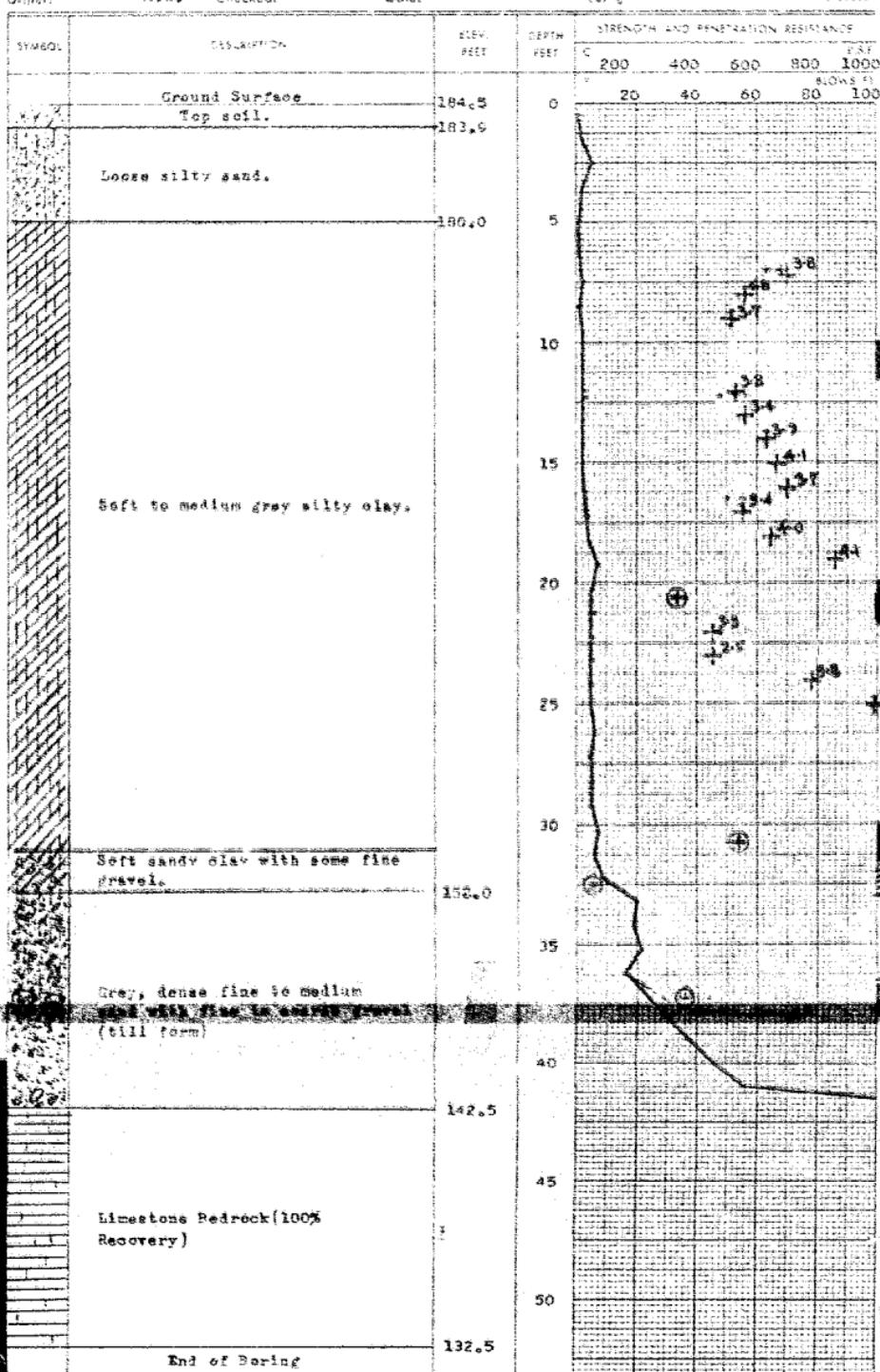
Value for 100 mm diameter 1.5

Penetration Resistance P

1" Split spoon

2" Dr. Core

Coring

LEGEND :

- Thin walled sample
- Split spoon sample

RACEY MacCALLUM AND ASSOCIATES LTD.

### **Foundation Engineering Division**

### **Engineering Data Sheet for Borehole:**

#### LEGEND

### Conclusion

### Natural moisture and Liquidity Index (LI)

### Liquid Limit Plastic Limit

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### **Sampling Methods**

### **2.2 Dig. split tube**



2018-03-01



DEPTH FEET	CONSISTENCY					SAMPLE	NATURAL UNIT WT. P.C.F.	REMARKS
	MOISTURE CONTENT % DRY WEIGHT							
0	20	40	60	80	100			Ground Surface
5								
10						1		
15								
20						2	99.0	
25								
30						3	100.5	
35						4		

## RACEY MacCALLUM AND ASSOCIATES LTD.

Foundation Engineering Division

## Engineering Data Sheet for Borehole- 2

Project: FOUNDN. INVEST. BRIDGE SITE OVER SOUTH RAI SIN RIVER,

Location: CORNWALL, ONTARIO.

Hole Location: See Enclosure No 1.

Hole Elevation and Datum: 185.2 Feet

Field Supervisor: J.W. Prep.: J.W.

Driller: M.G. Checked: Date:

LEGEND

Single Standard 10

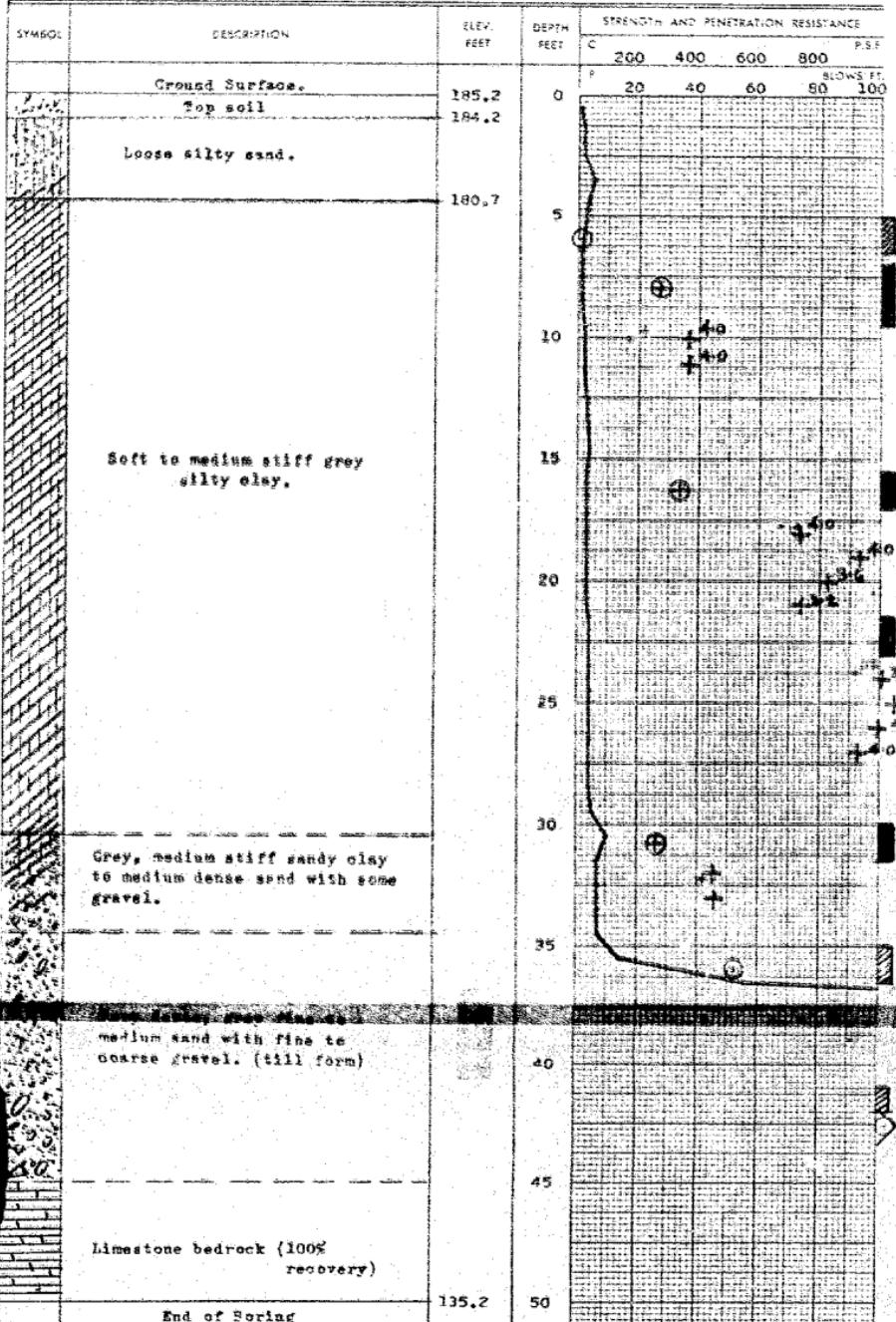
Unconfined compressive  
Value test and sensitivity S

## Penetration Resistance

2 Split tube

2 D.I. Cone

Coring

LEGEND :

■ - Thin walled sample

■ - Split spoon sample

## RACEY MacCALLUM AND ASSOCIATES LTD.

Foundation Engineering Division

Engineering Data Sheet for Borehole: 2

## LEGEND

## Consistency

Natural moisture and  
liquidity index 18  
Liquid limit  
Plastic limit



x 11



-



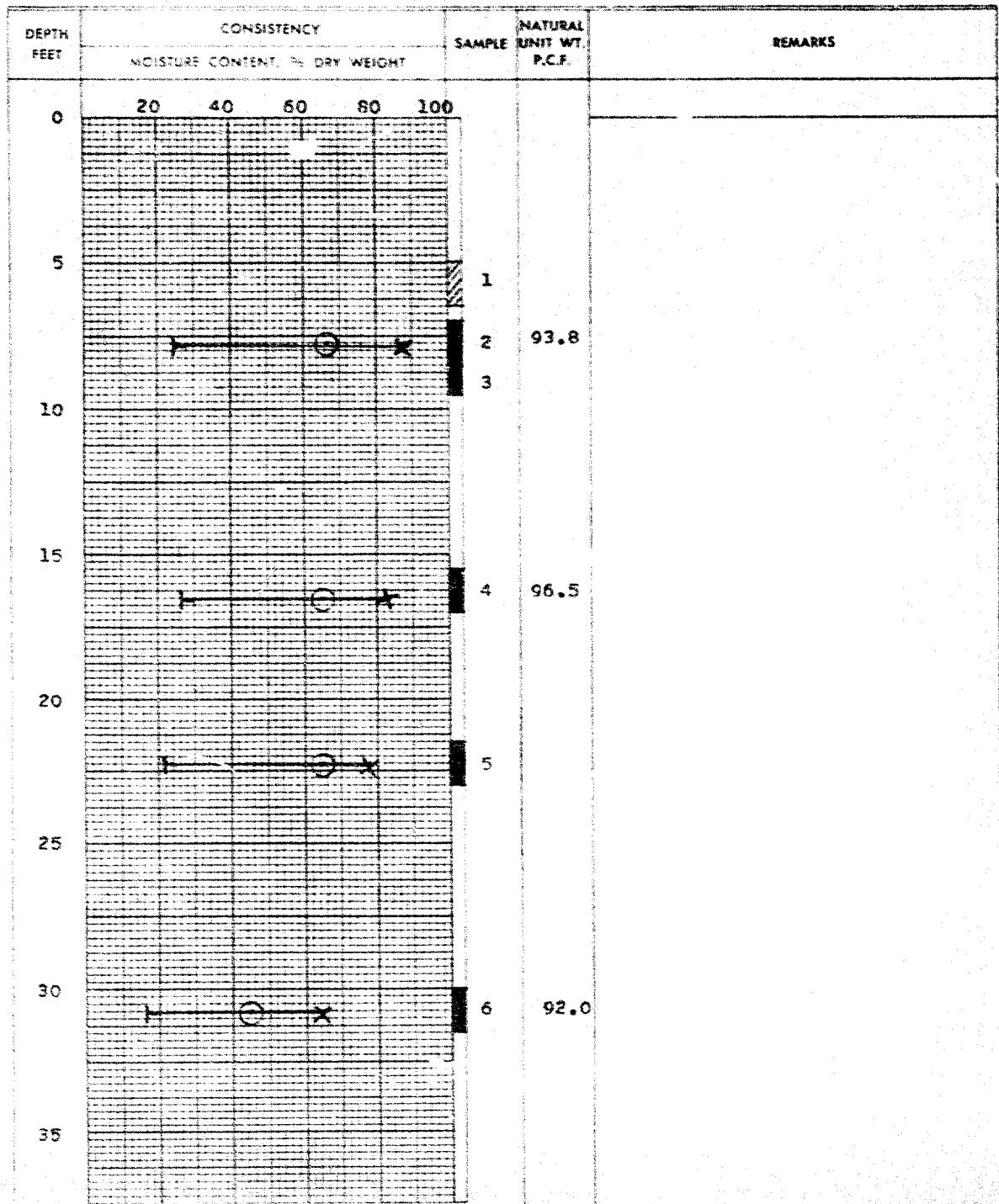
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## Sampling Method

2" Dia. split tube



2" Shelby tube



## RACEY MacCALLUM AND ASSOCIATES LTD.

Foundation Engineering Division

## Engineering Data Sheet for Borehole: 3

Project: FOUNDN. INVEST. BRIDGE SITE OVER SOUTH RAISIN RIVER.

Location: CORNWALL, ONTARIO.

Hole Location: See Enclosure No 1.

Hole Elevation and Datum: 184.8 feet

Field Supervisor: J.W. Prep.: J.W.

Driller: M.G. Checked:

Date:

## LEGEND

Shear Strength (C)

Unconfined compression

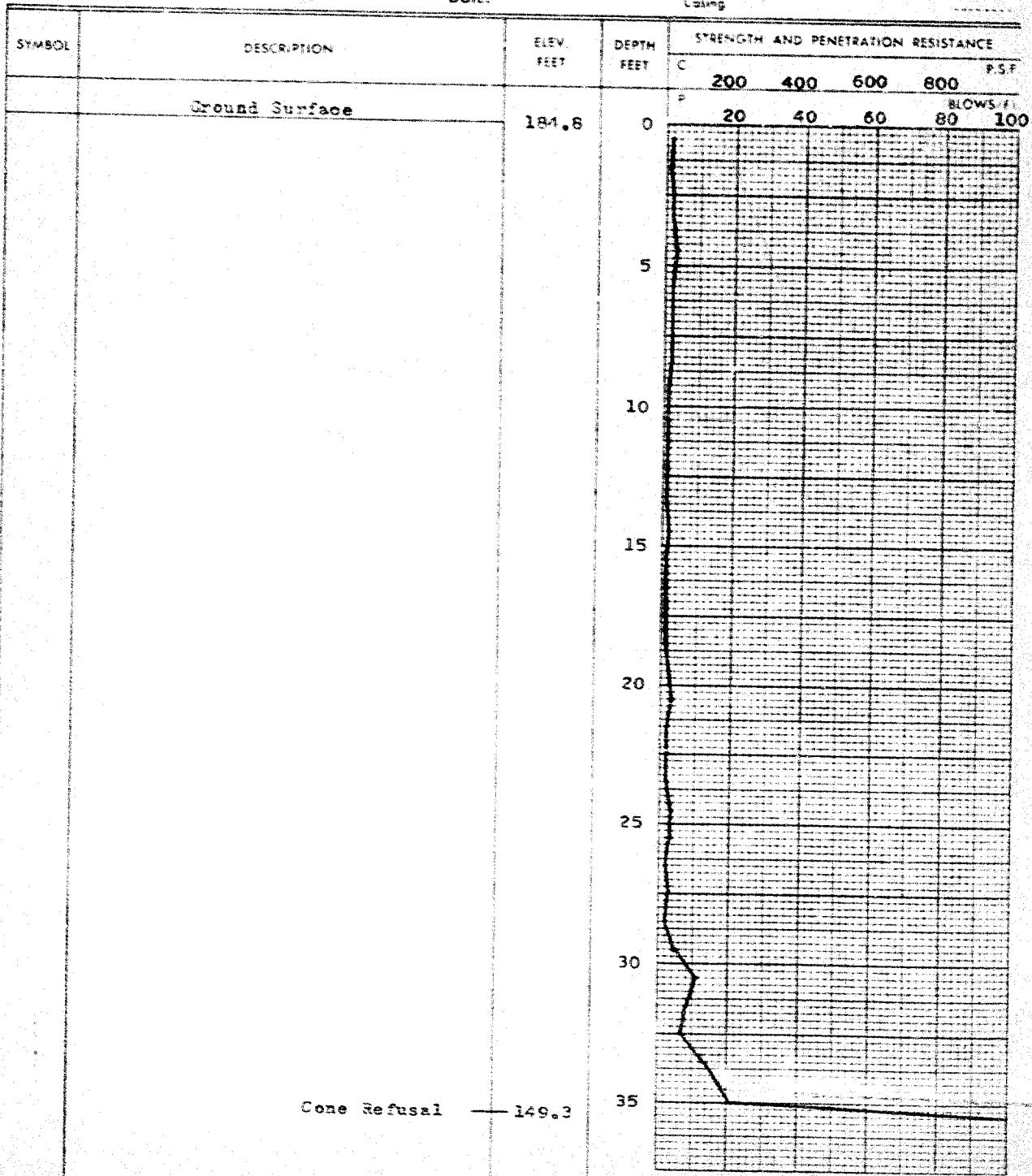
Vane test and sensitivity (S)

## Penetration Resistance (P)

2" Split tube

2" Dia. Cone

Casing

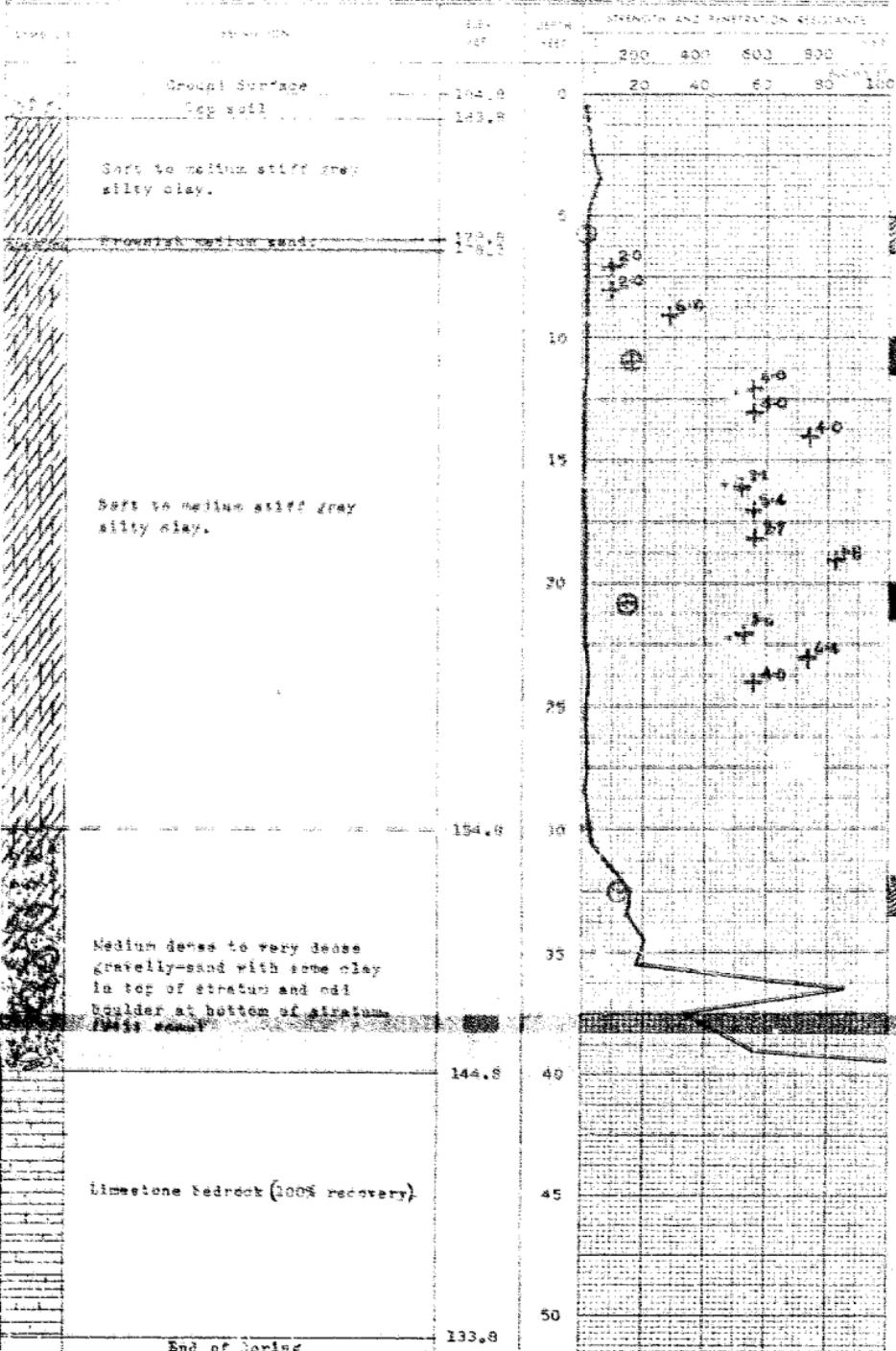


## KACEY McCALLUM AND ASSOCIATES LTD.

Project Name: ~~McCallum Engineering Services Inc.~~Site Name: ~~19th Street Bridge Site~~

Project Number: BRIDGE SITE OVER 19TH STREET RIVER.  
 Location: VERNON, CANADA  
 Hole Location: Sea Paradise No. 1.  
 Hole Diameter and Depth: 150.0 feet  
 Field Supervisor: J. F. Rep. J.M.  
 Driller: M.G. Checked Date:

Comments: (Handwritten notes)



**RACEY MacCALLUM AND ASSOCIATES LTD.**

## **Foundation Engineering Division**

### **Engineering Data Sheet for Borehole:**

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#### Summary Statement

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## RACEY MacCALLUM AND ASSOCIATES LTD.

Engineering Consulting Engineers

Geotechnical Data Sheet No. 5

FRENCH MINE, MINTON, MICHIGAN CITY, MIFF SOUTH RAILROAD RIVER, MICHIGAN

Lorachan, ONTARIO, CANADA

Hole Location: Line 1000, Block 1, No. 1.

Hole Elevation and Column UTM Co-Ord.

Field Supervisor: J.P., Prep: J.W.

Driller: H.J., Checked:

Date:

geotechnical data sheet no. 5

Sample No. 145-196-5A

Elev. 186.0 ft.

STRENGTH AND PENETRATION RESISTANCE

DEPT. OF 200 400 1600 800 PSF

F.EET 0 20 40 60 80 100

Crossed Surface

Top soil

Soft to medium stiff, mottled  
grey-brown silty clay with  
organic and traces of sand.Medium to coarse sand with silt  
and clay.

185.0

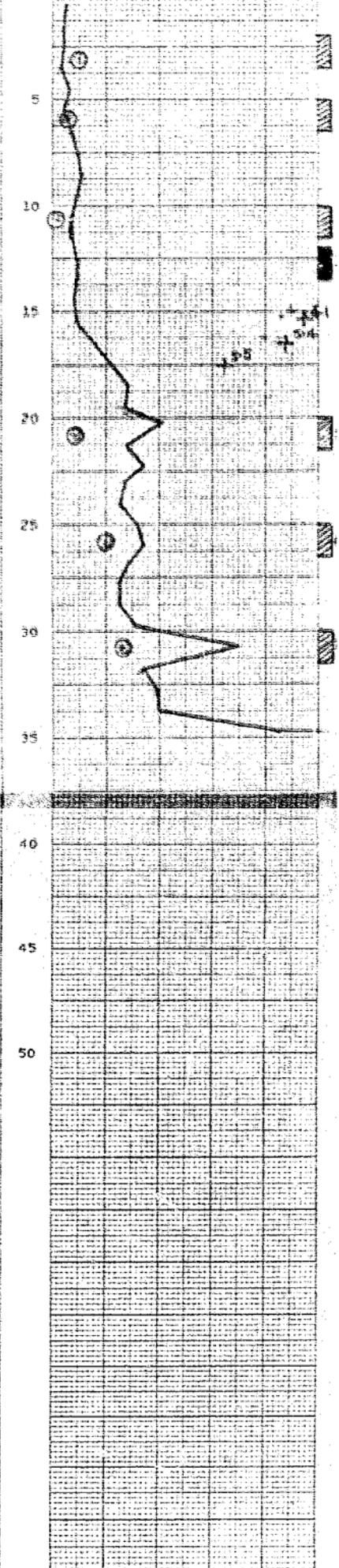
181.0

179.5

Soft to medium stiff grey  
silty clay.Dense to very dense gravelly-  
sand with some clay in upper  
portion. (till form)

Limestone bedrock (100% recovery).

End of Boring



## RACEY MacCALLUM AND ASSOCIATES LTD.

Foundation Engineering Division

## Boring Log Data Sheet for Boring No. 6

Project: FOUNDRY INVESTIGATION SITE ON THE SOUTH RAINBOW RIVER.  
Location: NEWHALL, BRITISH COLUMBIA.  
Site location: Box Enclosure No. 1.  
Bore Elevator and Screen: 165.3 feet  
Bore Supervisor: J.W. Prog: J.W.  
Driller: K.G. Checks Date:

## LEGEND

Soil classification

Soil test and soil type

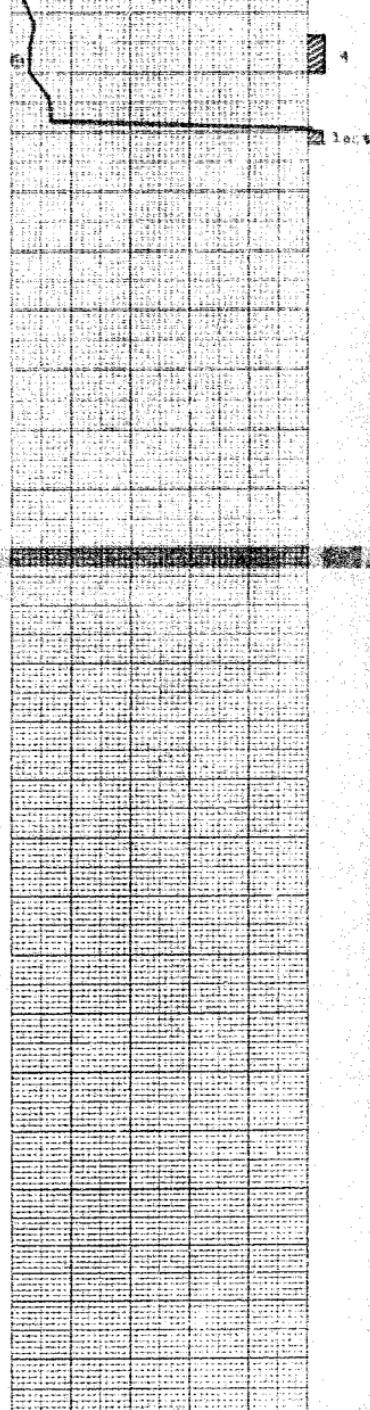
Strength Resistance

SPLAT value

2.5% Compressive load

Concreting

STATION	SOIL DESCRIPTION	ELEV. FEET	DEPTH FEET	STRENGTH AND PENETRATION RESISTANCE				
				200	400	600	800	1000
	Ground Surface	185.3	0	30	40	50	60	100
	Top soil	184.3						
	Loose medium to fine sand with silts.	182.3						
	Soft weathered brown clayey silt with some sands,	180.3						
	Soft to medium stiff grey silty clay.	177.3						
		177.0						
	Very dense gravelly-sand with boulders at lower depths. (till form)	174.3						
		172.3						
		170.3						
		168.3						
		167.0						
		165.3						
		164.3						
	Limestone bedrock (100% recovery).	133.7						
	End of Boring	133.7						



## RACEY MCCALLUM AND ASSOCIATES LTD.

Report on Engineering Services

The Results Data Sheet for Boring No. 1

Project: FORTIN, INGLET BRIDGE SITE OVER SOUTH RAISIN RIVER, ~~GRAND~~

Location: WINDMILL, ONTARIO.

Hole Location: See Enclosure No. 1.

Hole Diameter and Depth: 125.3

Field Supervisor and Crew: Peter J.W.

Driller: M.G. Checked: Dates:

Geological Observations

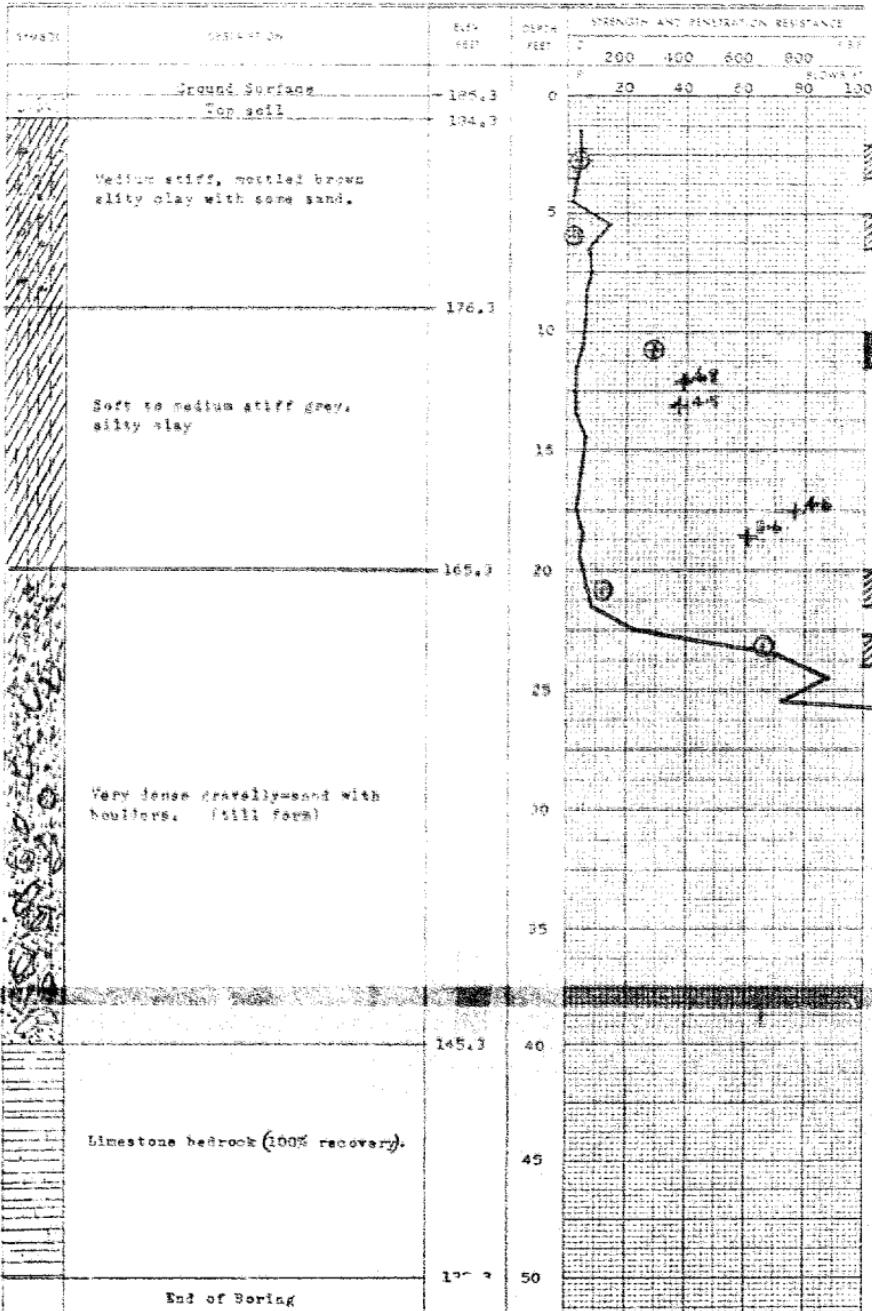
True Top and Bottom of Borehole

Penetration Resistances

1. Soil Test

2. Soil Comp.

Coring



**RACEY MacCALLUM AND ASSOCIATES LTD.**

Foundation Engineering Division

Engineering Data Sheet for Borehole: 7

**LEGEND**

## Consistency

Natural moisture and  
Liquid limit index (I<sub>L</sub>)  $\times 10$   
Liquid limit  $\circ$   
Plastic limit  $\square$

## Sampling Method

2" Dia. split tube  
2" Shallow tube



DEPTH FEET	CONSISTENCY MOISTURE CONTENT % DRY WEIGHT	NATURAL SAMPLE UNIT WT. P.C.F.	REMARKS				
			20	40	60	80	100
0							
5							
10							
10	1	1					
10	2	2					
10	3	3					
10	99.2	99.2					
15							
20							
25							
30							
35							

## RACEY MacCALLUM AND ASSOCIATES LTD.

Soil Testing Engineering Division

Engineering Data Sheet for Boring No. 8

Project: PORTAGE INVEST. SPRING SITE OVER SOUTH RAYSIIN RIVER

Location: VERNON, ONTARIO

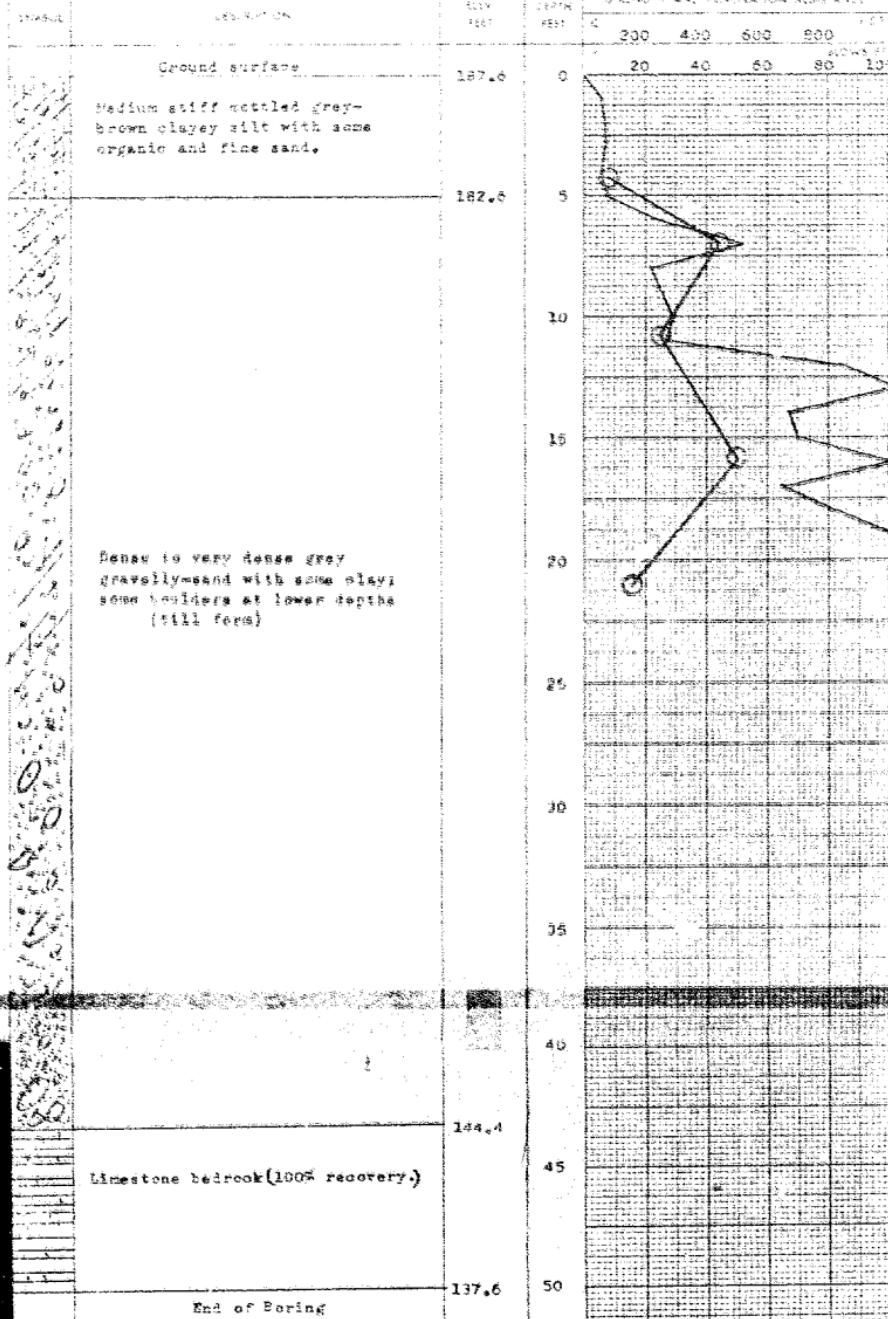
Site location: See Enclosure No. 1.

Hole elevation and Survey: 187.6

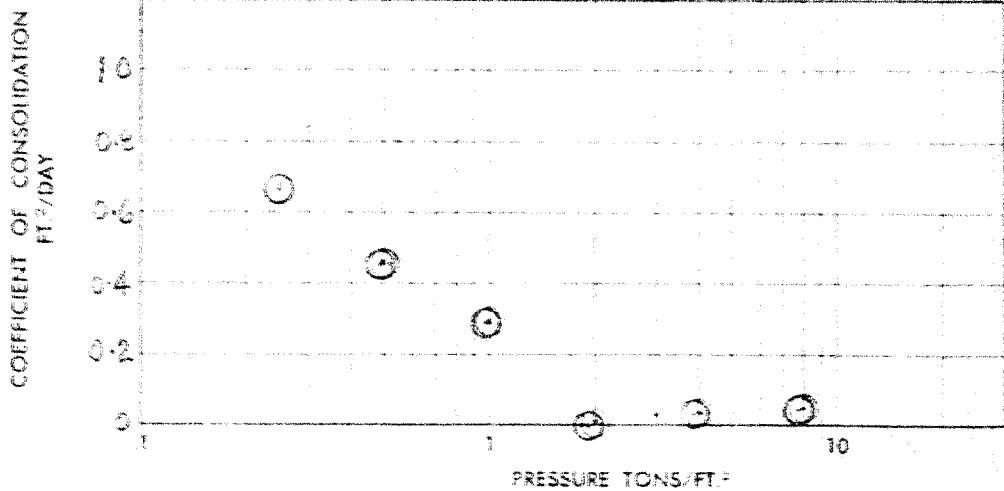
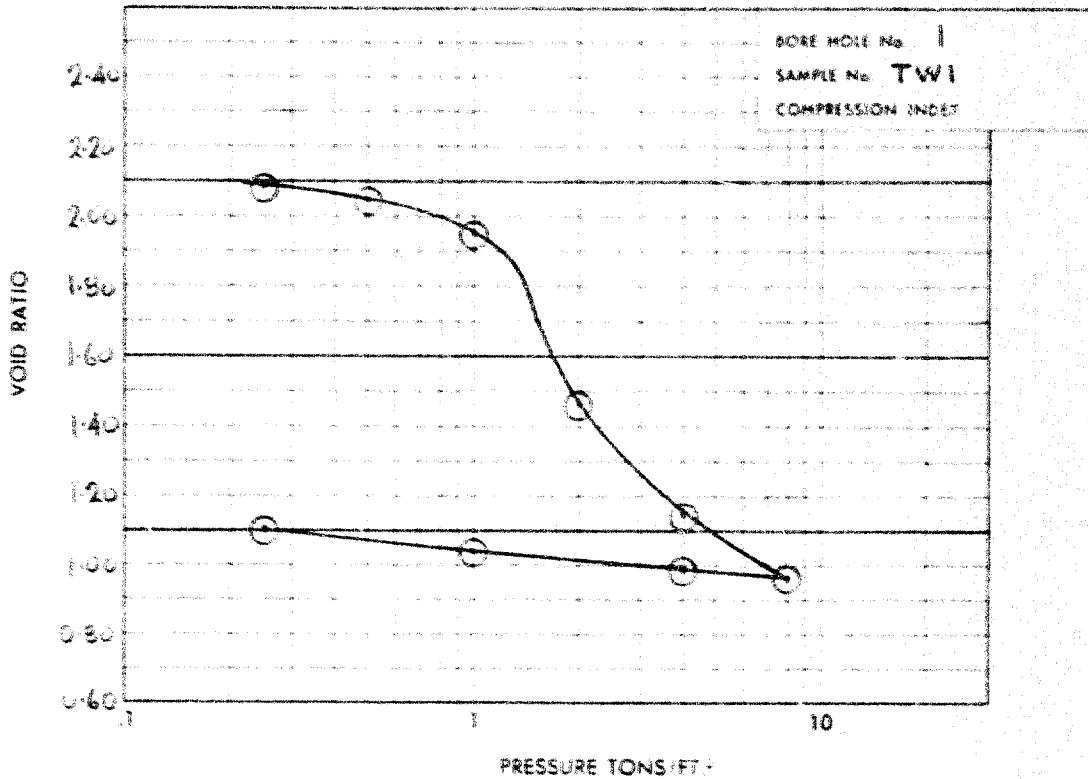
Field Supervisor: J.W. Doug. P.M.

Drafter: K.L. Checked: Date:

Note: This sheet is a copy of the original engineering data sheet.

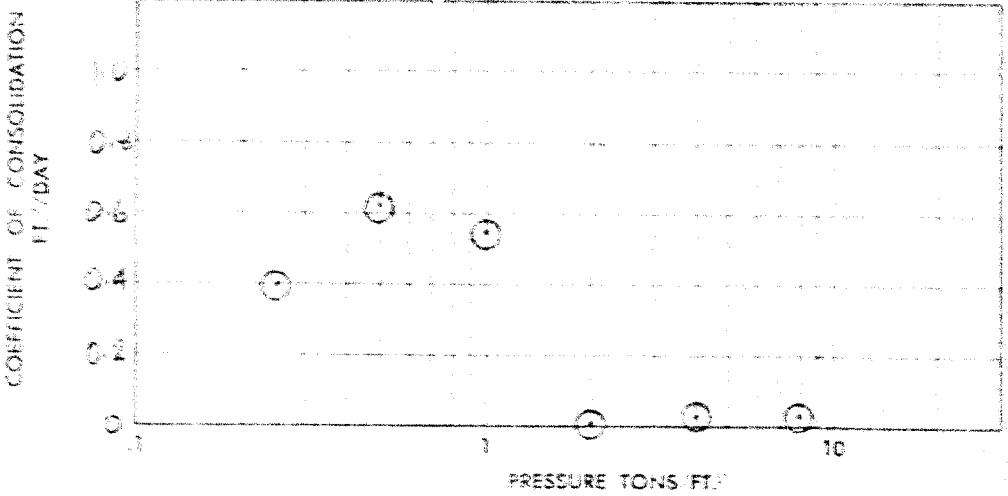
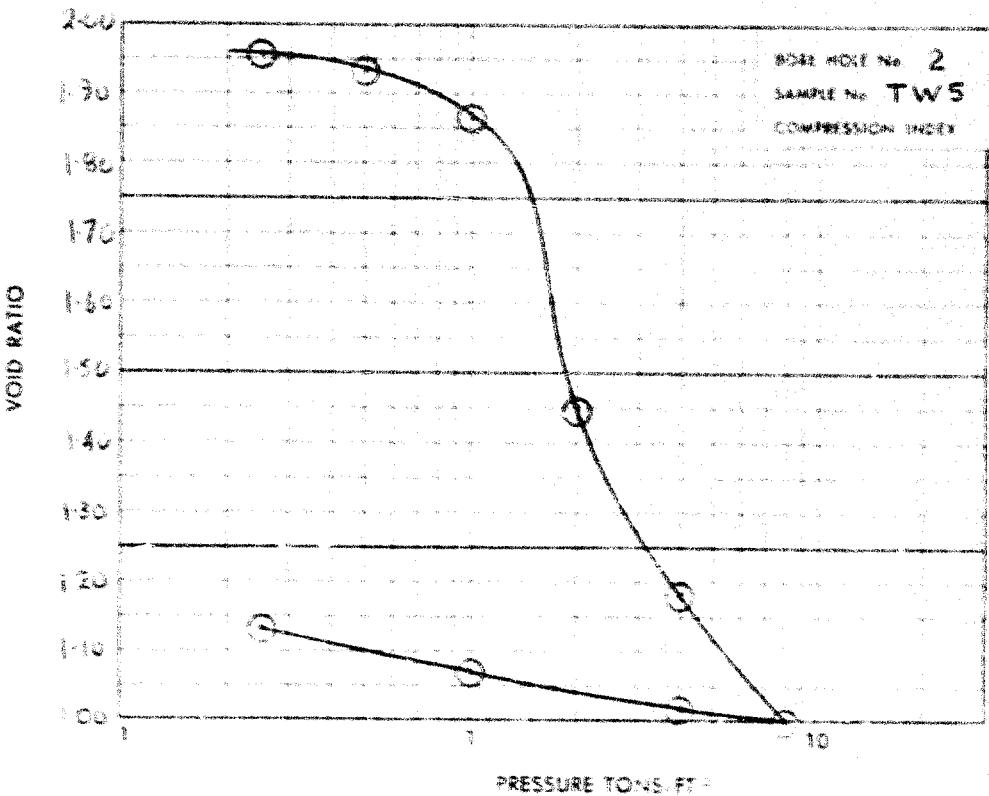


**RACEY MacCALLUM AND ASSOCIATES LTD.**  
**CONSOLIDATION TEST**



## RACEY McCALLUM AND ASSOCIATES LTD.

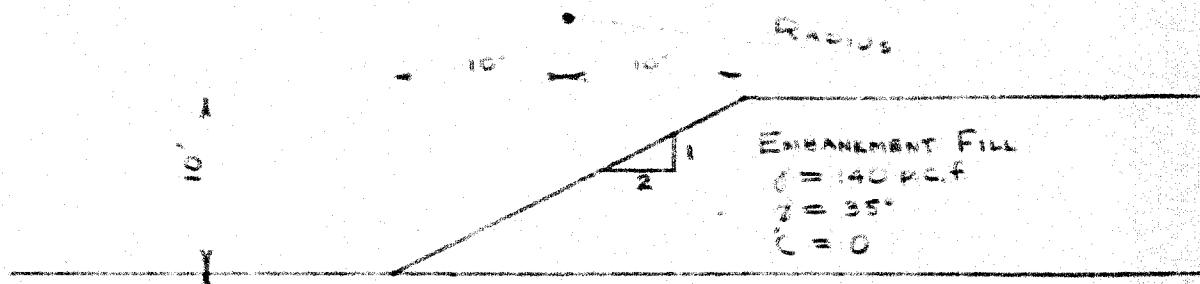
## CONSOLIDATION TEST



Prep. by L.P.W.

CASE 1 - STABILITY UNDER EMBANKMENT FILL

CENTRE OF CRITICAL CIRCLE



SILTY CLAY

$c = 97 \text{ p.c.f.}$

$C_{soil} = 35 \text{ p.c.f.}$

$C = 600 \text{ p.s.t.}$

$\phi = 0^\circ$

GRAVEL-SAND

GLACIAL TILL

TRIAL SOLUTIONS

RADIUS	DISTANCE FROM E. SLOPE	SAFETY FACTOR
30'	0	2.35
* 35'	0	2.11
44'	0	2.20
55'	0	2.22
35'	5' INWARDS	2.25

\* APPROXIMATE CRITICAL CIRCLE

Prep. By L.P.W.

CASE 2 - STABILITY AT ABUTMENT

CENTRE OF CRITICAL CIRCLE

RADIUS

EMBANKMENT FILL  
 $\gamma = 140$  p.c.f.  
 $\phi = 35^\circ$   
 $C = 0$

SILTY CLAY  
 $\gamma = 97$  p.c.f.  
 $\gamma_{soil} = 35$  p.c.f.  
 $C = 600$  p.s.f.  
 $\phi = 0^\circ$

GRAVEL-SAND  
 GLACIAL TILL

TRIAL SOLUTIONS

RADIUS	DISTANCE FROM ABUTMENT	SAFETY FACTOR
30'	0	2.27
40'	0	2.24
* 50'	0	2.18

\* APPROXIMATE CRITICAL CIRCLE