

Mr. A. Toye, Bridge Engineer.

August 3rd 1935

Re: Foundation Investigation

Highways Laboratory, Toronto.

St. Andrews Rd. & Hwy. 401 Cornwall.

Please find herewith two copies of the report
on the investigation of the above site.

The subsoil consists of a sandy till material
with varying degrees of stoniness and is suitable
for spread footings despite a high water table.

F.C. Brownridge,
Materials and Research Engineer.

Per:

M.M.D.

MM:fa

(H.E. Davis)

Atch: (2).

c.c. to -

Mr. A. Toye,
Mr. J. Walter,
Design Engineer,

Mr. J.S. Wilkes,
Div. Eng., Ottawa.

Mr. G. Robertson.

A. L. R. - J. C. B. - J. L.
65 F. 13
Preliminary Bridge Site Investigation

Highway 401 St. Andrews Road - Cornwall.

Station 389+00 Line 'C' Profile 401-J-27

Location 2½ miles north Hwy. 2 at Cornwall.

Introduction

Preliminary holes were drilled through the known till in this area to ascertain an accurate profile of the upper soil layers.

Soil Profile

Approximately 13" of topsoil and 'B' horizon brown sandy loam overlies a brown sandy loam till which is both moist and very stoney.

The above is underlain by a blue gray very fine sandy loam till which is also wet and stoney.

In one bore hole a saturated layer of brown sand and silt was observed at 6'0" below original ground level.

Four holes showed water entering at various depth but in apparently large quantities at 14'0".

Remarks

The water condition at this site may be a result of a natural east - west ground water drainage from the height of land on the east to the South Raisin river on the west. There is little doubt that the till to a depth of 15'0" would carry spread footing adequately, but as this is a overpass on 401 the size of the embankment - namely some 120' in width - requires subsoil investigation to a greater depth than is possible with the ordinary auger equipment. Also the properties of the lower soil stratas may be adversely affected by the water condition found by this preliminary investigation.

Recommendation

Normal core drill exploration to be carried out.

A. Thorley.

10/5/55.

cc: Mr. G. Farantatos.

Hole #1 1' E. Front Face Northwest Corner.

0-12" Black sandy loam topsoil
 12"-20" Dark brown sandy loam - "B"
 20"-44" Brown very fine sandy loam - Loam till (Very stony) Moist

Hole #2

0-12" Black sandy loam topsoil
 12"-20" Dark brown sandy loam "B"
 20"-4' Brown very fine sandy loam - Loam till (Very stony) Moist N.F.P.

Hole #3 1' S. E 401- Front Face West Side

0-14" Black sandy loam topsoil
 14"-24" Dark brown sandy loam "B"
 24"-7' Brown very fine sandy loam - Loam till (Very Stony) Moist N.F.P.

Hole #4 8' S. E 401 - Front Face West Side.

0-12" Black sandy loam topsoil
 12"-17" Dark brown sandy loam "B"
 17"-9½' Brown very fine sandy loam - Loam till, Moist (Very stony) H.M. 7'-8' 55-Z-101
 9½'-15' Blue grey very fine sandy loam - Loam till (Very stony-) H.M. 10'-11' 55-Z-102
 Water Enter 14' Moist) M. 12'-13' 55-Z-103

Hole #5 1' W. Front Face Southwest Corner.

0-11" Black sandy loam topsoil
 11"-21" Dark brown sandy loam - "B"
 21"-6' Brown very fine sandy loam - Loam till (Very Stony) Moist. N.F.P.

Hole #6 9' S. 1' W. Front Face Southwest Corner.

0-12" Black sandy loam topsoil
 12"-22" Dark Brown sandy loam "B"
 22"-6' Brown very fine sandy loam - Loam till (Very Stony) Moist. N.F.P.

Hole #7 5' S. 1' W. Front Face Southwest Corner.

0-10" Black sandy loam topsoil
 10"-22" Dark brown sandy loam - "B"
 22"-6' Brown very fine sandy loam - Loam till (Very Stony) Moist. N.F.P.

Hole #8 1' W. 6' N. Front Face Southwest Corner

0-10" Black sandy loam topsoil
 10"-18" Dark brown sandy loam - "B"
 18"-10' Brown very fine sandy loam - Loam till (Very stony) Moist - Wet
 10'-11' Blue grey very fine sandy loam - Loam till (Very Stony) Wet.
 11'-12½' Brown very fine sandy loam - Very fine sandy & silty (Sat.) (Stony) Water enter 11'
 12½'-15' Blue grey very fine sandy loam - Loam till (Stony) Wet.

Hole #9 1' W. Front Face Southeast Corner.
0-7" Black sandy loam topsoil
7"-14" Dark brown sandy loam "B"
14"-6' Brown very fine sandy loam - Loam till (Stony) Moist - Wet)
6'-15' Brown very fine sandy loam - Very fine sand & silty (Wet-Sat) Water enter 14'
H.M. 10'-11' 55-Z-104

Hole #10 1' S. E 401 Front Face East Side.
0-4" Black sandy loam topsoil
4"-13" Dark brown sandy loam "B"
13"-9' Brown very fine sandy loam - Loam till (Very stony) Moist
9'-10½' Blue grey very fine sandy loam - Loam till (Stony) Moist - Wet
10½'-12' Brown very fine sandy loam - Loam till (Very stony) Moist - Wet. N.F.P.

Hole #11 1' W. Front Face Northeast Corner
0-5" Black sandy loam topsoil
5"-14" Dark brown sandy loam "B"
14"-4' Brown very fine sandy loam - Loam till (Very stony) Moist. N.F.P.

Hole #12 6' N. 4' W. Front Face Northeast Corner.
0-12" Black sandy loam topsoil
12"-23" Dark brown sandy loam "B"
23"-8' Brown very fine sandy loam - Loam till (Very stony) Moist - Wet
8'-15' Blue grey very fine sandy loam - Loam till (Very stony) Wet.

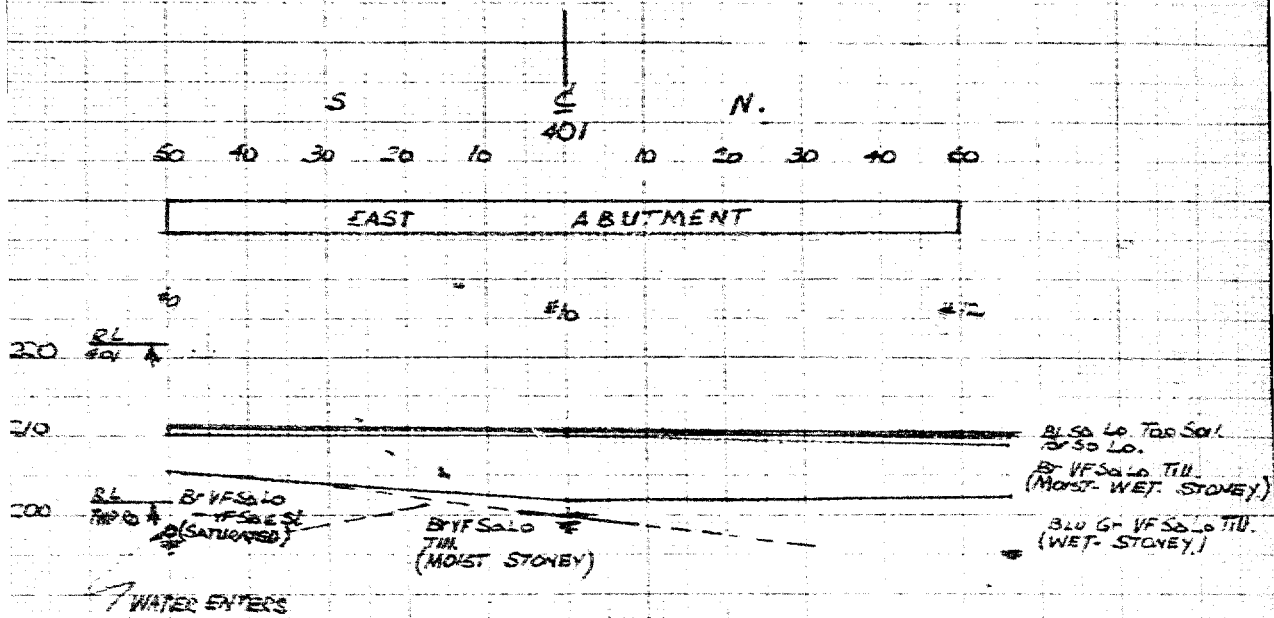
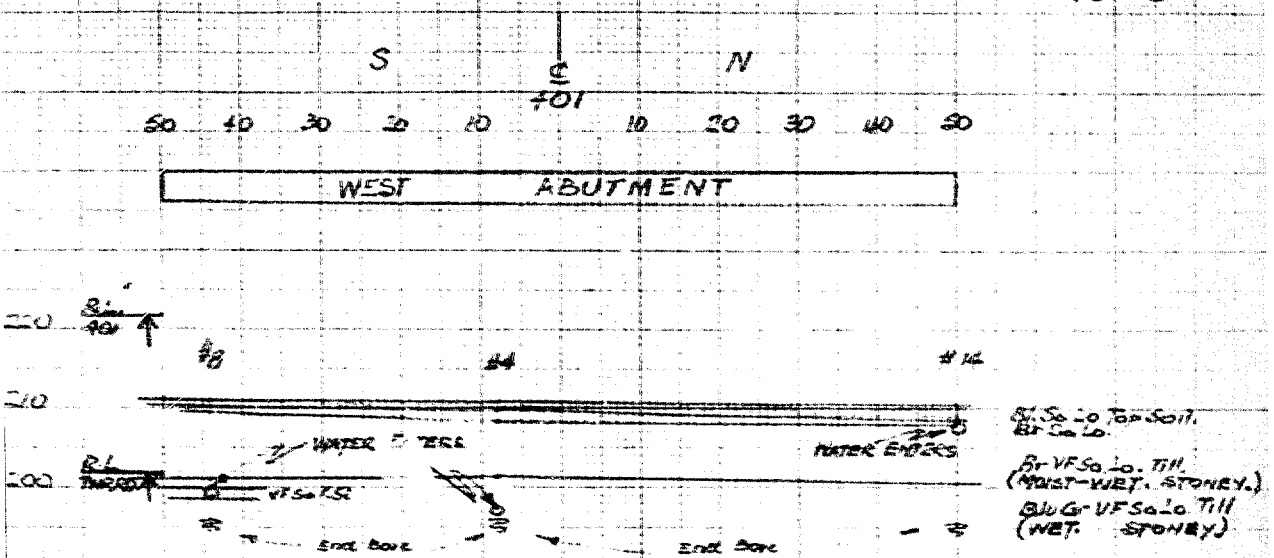
Hole #13 1' E. 5' N. Front Face Northwest Corner.
0-12" Black sandy loam topsoil
12"-23" Dark brown sandy loam "B"
23"-7½' Brown very fine sandy loam - Loam till (Very stoney) Moist. F.F.P.

Hole #14 3' N. 1' W. Front Face Northwest Corner.
0-14" Black sandy loam topsoil
14"-25" Dark brown sandy loam "B" Horizon.
25"-5' Brown very fine sandy loam - Loam till (Very stony - Moist) N.F.P.

Hole #15 6' W. Front Face Northwest Corner.
0-25" Black sandy loam topsoil
25"-28" Dark brown sandy loam "B" Some water enter 28"
28"-10' Brown very fine sandy loam - Loam till (Very stony - Moist)
10'-15' Blue grey very fine sandy loam - Loam till (Very stony - Moist - Wet).

401 OVERPASS ST ANDREWS ROAD CORNWALL

PLAN 3165-9
PROF. 3165-6



A THORLEY 10/6/55

Report on
Foundation Investigation
of St. Andrews Road
and Highway 401
at Cornwall

Copies to: Mr. A. Teye
Bridge Engineer (2)

Mr. J. Walter
Design Engineer (1)

Mr. J. B. Wilkes
Div. Eng., Ottawa (1)

Mr. G. Parantatos (1)

File (1)

Project F-55-13

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Introduction

The following report is concerned with the foundations for the proposed Highway #401 overpass at St. Andrews Road, Cornwall. The sub-surface conditions have been explored in order to decide upon the type of foundation, bearing pressure and formation level.

Procedure

Three borings were put down at the positions shown on the attached plan 55-P-13A commencing May 7 and finishing June 9. The stony nature of the strata prevented a preliminary dynamic cone test, and in one case recourse was made to diamond drilling to begin the hole.

Soil Conditions

Sandy till was found for the entire depth of each borehole. In holes 1 and 2 this material was very stony in the upper and lower layers, with a less stony stratum sandwiched between.

In borehole 5 very stony sandy till was encountered throughout the entire depth of 33.0 feet.

Water Conditions

Ground water was encountered in boreholes 1 and 5 showing the water table to be between $4\frac{1}{2}$ and $7\frac{1}{2}$ feet below ground level.

Analysis of Results and Recommendations

The standard penetration tests showed that the penetration resistance of the softest strata was fifty blows per foot, and greater.

The stony layer, where the penetration test was impractical, must have a higher internal friction than the layers of fine sand underlying, so that fifty blows per foot is a reliable minimum penetration resistance.

For the condition that the settlement should not be greater than one inch, recourse has been made to Terzaghi's studies graph. This shows that for a saturated condition, a bearing value of $2\frac{1}{2}$ tons per square foot is permissible. However, using Meyerhoff's proposed equations, the safe bearing capacity, independent of settlement considerations, was found to be 15 tons per square foot. The maximum permissible value, according to the National Building Code of Canada, is 5 tons per square foot.

Recommendations

It is therefore recommended that for a rigid frame type of structure, a spread footing is satisfactory, using a bearing value of $2\frac{1}{2}$ tons per square foot. This bearing value can be increased to 5 tons per square foot for a simply supported structure.

Conclusion

The subsoil is suitable for a spread footing.

For a rigid frame structure, a bearing value of $2\frac{1}{2}$ tons may be used; for a simply supported structure, a bearing value of 5 tons per square foot is permissible.

F. C. Brownridge
Materials and Research Engineer

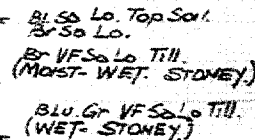
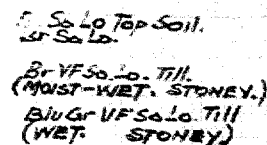
Per:


(G. Patantatos)

GF:GGP

APPENDIX I

PLAN 3165-7
PROF. 3165-6



A THORLEY 10/5/55

DATE APRIL 25/84

HOLE #1 1'E FRONT FACE N.W. CORNER

0-12" BL SALOTPSL
12-20" DK BR SALO-B
20-44" BR VF SALO-LoTILL (VERY STONY) Moist
N.F.P.

HOLE #2 1'E S'S FRONT FACE N.W. CORNER

0-12" BL SALOTPSL
12-20" DK BR SALO-B
20-4' BR VF SALO-LoTILL (VERY STONY) Moist
N.F.P.

HOLE #3 1'S & 401-FRONT FACE WEST SIDE

0-14" FL SALOTPSL
14-24" DK BR SALO-B
24-7' BR VF SALO-LoTILL (VERY STONY) Moist
N.F.P.

HOLE #4 3'S & 401-FRONT FACE WEST SIDE

0-12" OL SALOTPSL
12-17" DK BR SALO-B
17'-9 1/2" BR VF SALO-LoTILL Moist (VERY STONY) H.M. 7'-8' SS2101
9 1/2-15' BL GR VF SALO-LoTILL (V. STONY HARD) H.M. 10'-11' SS2102
WATER ENTER 14' H. 12'-13' SS2103

HOLE #5 1'W FRONT FACE S.W. CORNER

0-11" BL SALOTPSL
11'-21" DK BR SALO-B
21'-6" BR VF SALO-LoTILL (V. STONY) Moist
N.F.P.

HOLE #6 9'S 1'W FRONT FACE S.W. CORNER

0-12" BL SALOTPSL
12-20" DK BR SALO-B
20-6' BR VF SALO-LoTILL (V. STONY) Moist
N.F.P.

HOLE #7 5'S 1'W FRONT FACE S.W. CORNER

0-10" BL SALOTPSL
10-22" DK BR SALO-B
22'-6" BR VF SALO-LoTILL (V. STONY) Moist
N.F.P.

DATE April 25/05

HOLE #8 1/4 N FRONT FACE SW CORNER

0-10" Bl. Sal. Till
10'-18" Dr. Bl. Sal. Till
18'-10' Br. VF Sal. - Lo Till (V. Stony) Moist-Wet
10'-11" Bl. Gr. VF Sal. - Lo Till (V. Stony) Wet
11'-12 1/2' Br. VF Sal. - Lo Till (V. Stony) Water Filter II
12 1/2'-15' Bl. Gr. VF Sal. - Lo Till (Stony) Wet

HOLE #9 1' W FROM FACE - SE CORNER

0-7" Bl. Sal. Till
7'-11" Dr. Bl. Sal. Till
11'-6' Br. VF Sal. - Lo Till (Stony) Moist-Wet
6'-15' Br. VF Sal. - VF Sal. Sil. Wet. Cat. Water Filter 14' (11' - 14') 15' - 17'

HOLE #10 1 S & 4 W FROM FACE ENT. SAIL

0-4" Bl. Sal. Till
4'-13" Dr. Bl. Sal. Till
13'-9' Br. VF Sal. - Lo Till (V. Stony) Moist
9'-10 1/2' Bl. Gr. VF Sal. - Lo Till (Stony) Moist-Wet
10 1/2'-12' Br. VF Sal. - Lo Till (V. Stony) Moist-Wet
N.F.P.

HOLE #11 1 W FROM FACE NE CORNER

0-5" Bl. Sal. Till
5'-14" Dr. Bl. Sal. Till
14'-4' Br. VF Sal. - Lo Till (V. Stony) Moist
N.F.P.

HOLE #12 6 N & 4 W FROM FACE NE CORNER

0-12" Bl. Sal. Till
12'-23" Dr. Bl. Sal. Till
23'-8' Br. VF Sal. - Lo Till (V. Stony) Moist-Wet
8'-15' Bl. Gr. VF Sal. - Lo Till (V. Stony) Wet

HOLE #13 1 E & N FROM FACE NW CORNER

0-12" Bl. Sal. Till
12'-23" Dr. Bl. Sal. Till
23'-7 1/2' Br. VF Sal. - Lo Till (V. Stony) Moist
N.F.P.

Hole #14 3 NW FRONT FACE NW CORNER

0-14" 1/2 SALTED
 4'-25" 1/2 SALTED
 25'-5" 1/2 SALTED - 1/2" STAIN - (HIST)
 N.F.P.

Hole #15 6 W FRONT FACE NW CORNER

0-25" 1/2 SALTED
 25'-6" 1/2 SALTED - 1/2" STAIN - (HIST)
 25'-10" 1/2 SALTED - 1/2" STAIN - (HIST)
 10'-5" 1/2 SALTED - 1/2" STAIN - (HIST-WET)

#55-F-13
Hwy. #401 E.
ST. ANDREWS RD.
CORNWALL

EDITED
FOR MICROFILMING
BY *K.T.* DATE *2/7/80*

TL 129
54-90

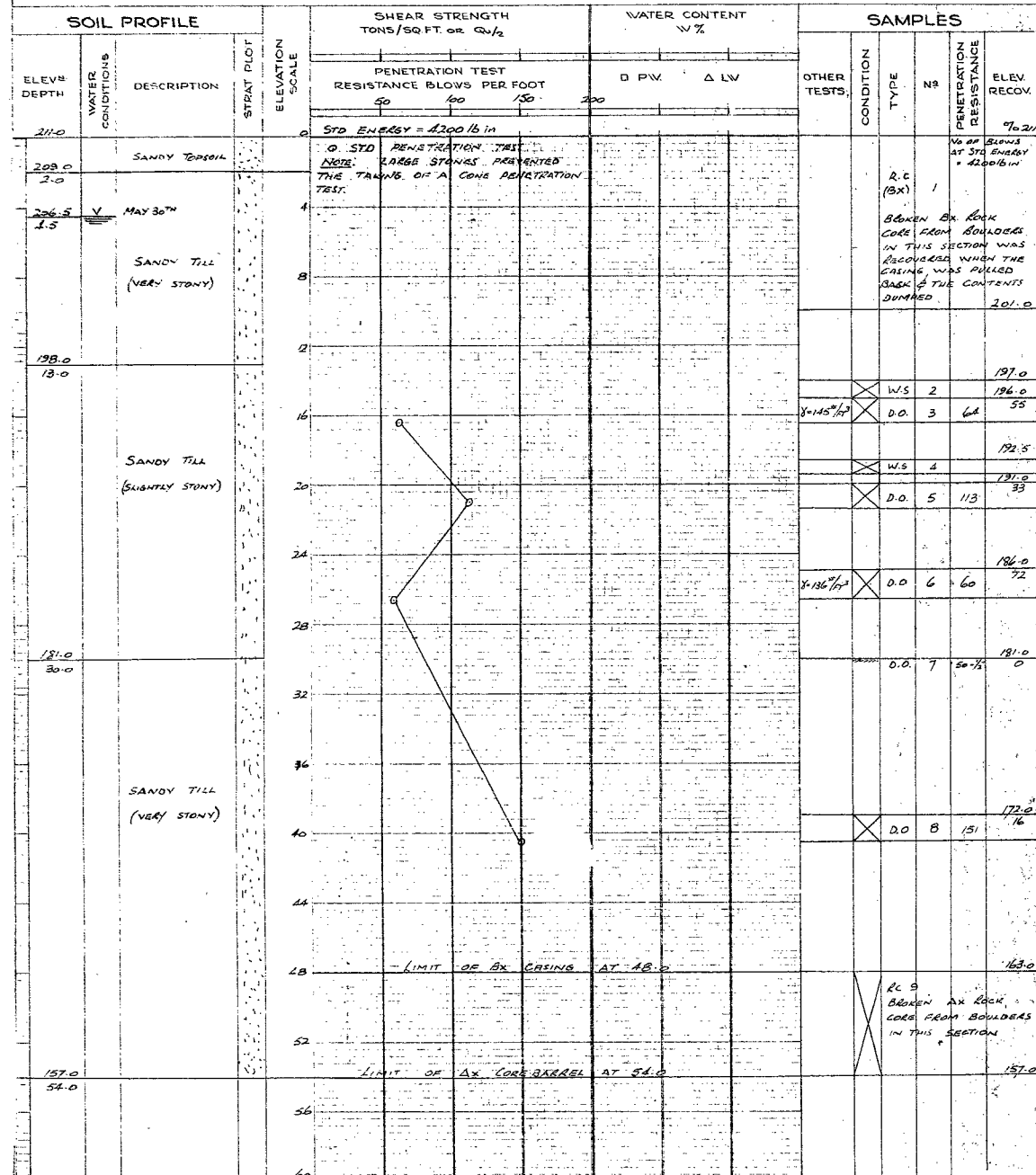
MATERIALS LABORATORY - DEPARTMENT OF HIGHWAYS - ONTARIO
OFFICE REPORT ON SOIL EXPLORATION

DRILL RIG CORE DRILL #4 JOB SS-F-3 CORNWALL BORING NO. 1
CASING 5X (STANDARD SAMPLERS TO FIT UNLESS NOTED) DATUM STA 389+14 AT 50' AT 116° 75' DATE REPORT
SAMPLER HAMMER WT. 250 DROPS INCHES COMPILED BY B.H. CHECKED BY B.H. BORING DATE MAY 21, 1955

SAMPLE CONDITION
DISTURBED
GOOD
LOST

SAMPLE TYPES
C.S. - CHUNK
D.O. - DRIVE OPEN
D.F. - DRIVE FOOT VALVE
T.O. - THIN WALLED OPEN
W.S. - WASHED SAMPLE
R.C. - ROCK CORE

ABBREVIATIONS
V - INSITU VANE SHEAR TEST
M - MECHANICAL ANALYSIS
U - UNCONFINED COMPRESSION
Q_c - TRIAXIAL CONSOLIDATED QUICK
Q - TRIAXIAL QUICK
S - TRIAXIAL SLOW
γ - UNIT WEIGHT
K - PERMEABILITY
C - CONSOLIDATION
CA - CASING
WL - WATER LEVEL IN CASING
WT - WATER TABLE IN SOIL



TL 129
54-90

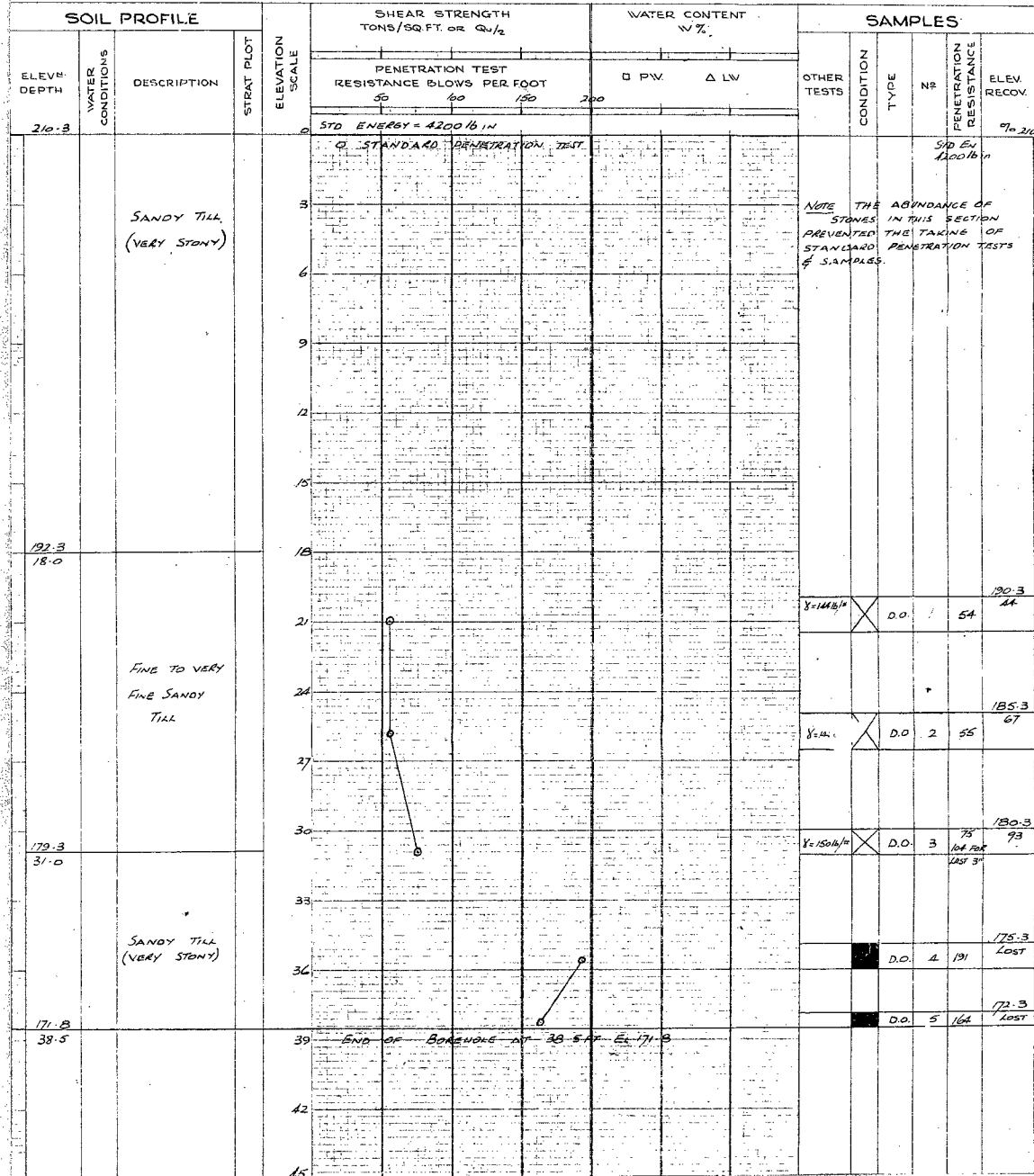
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OFFICE REPORT ON SOIL EXPLORATION

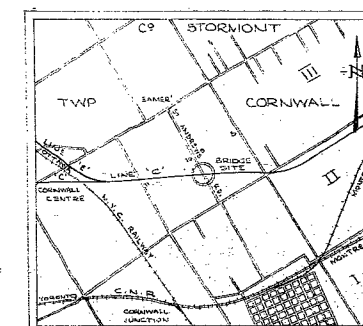
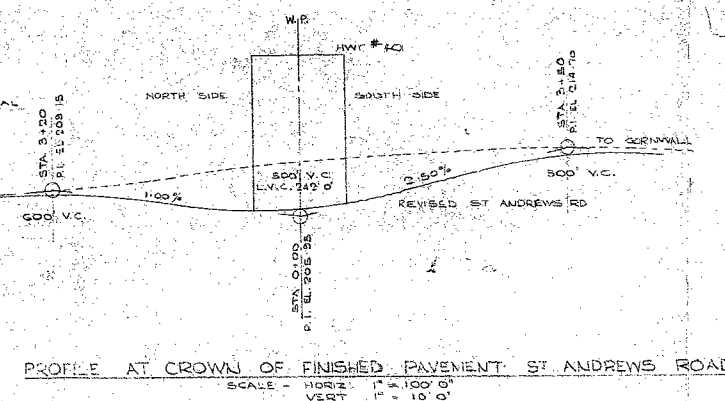
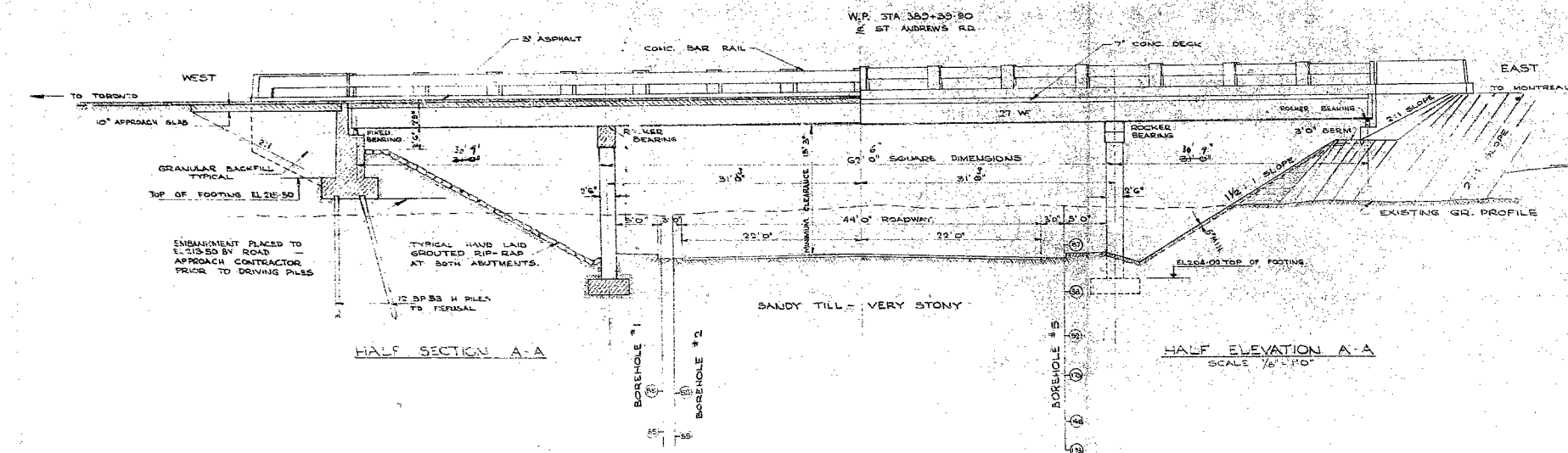
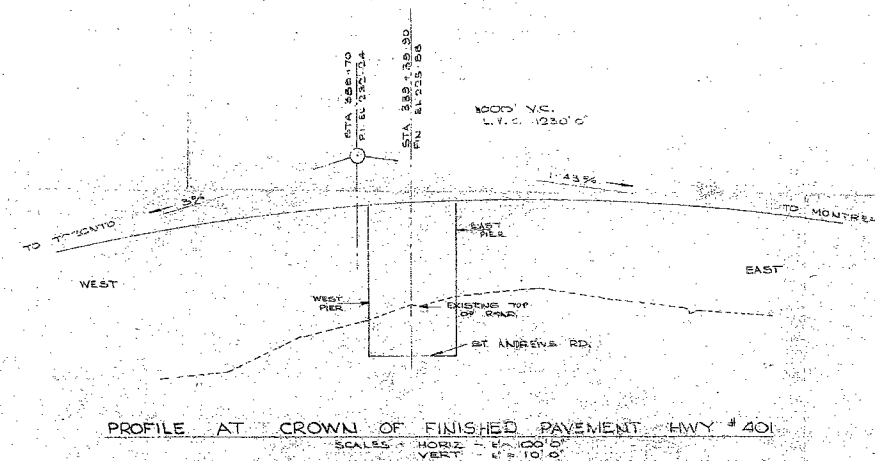
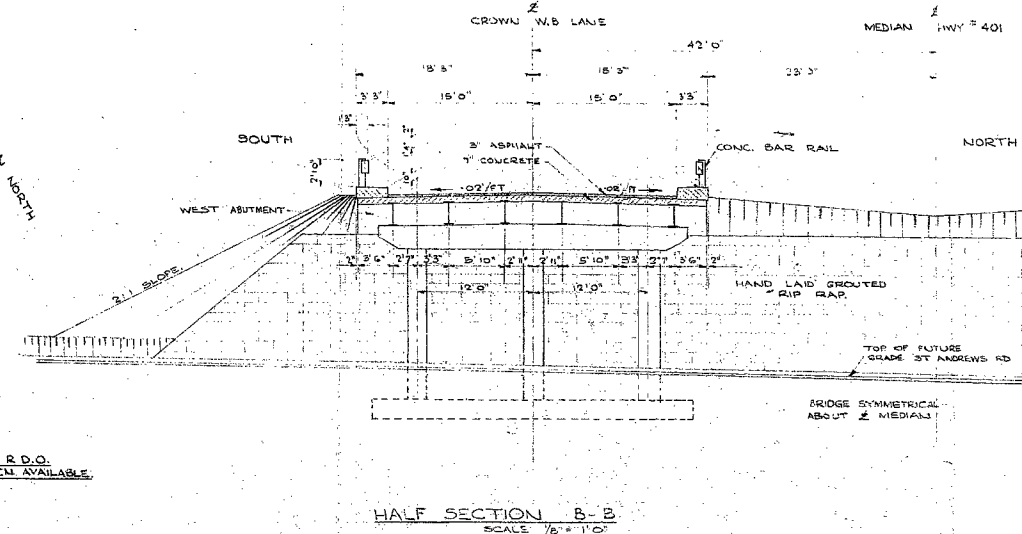
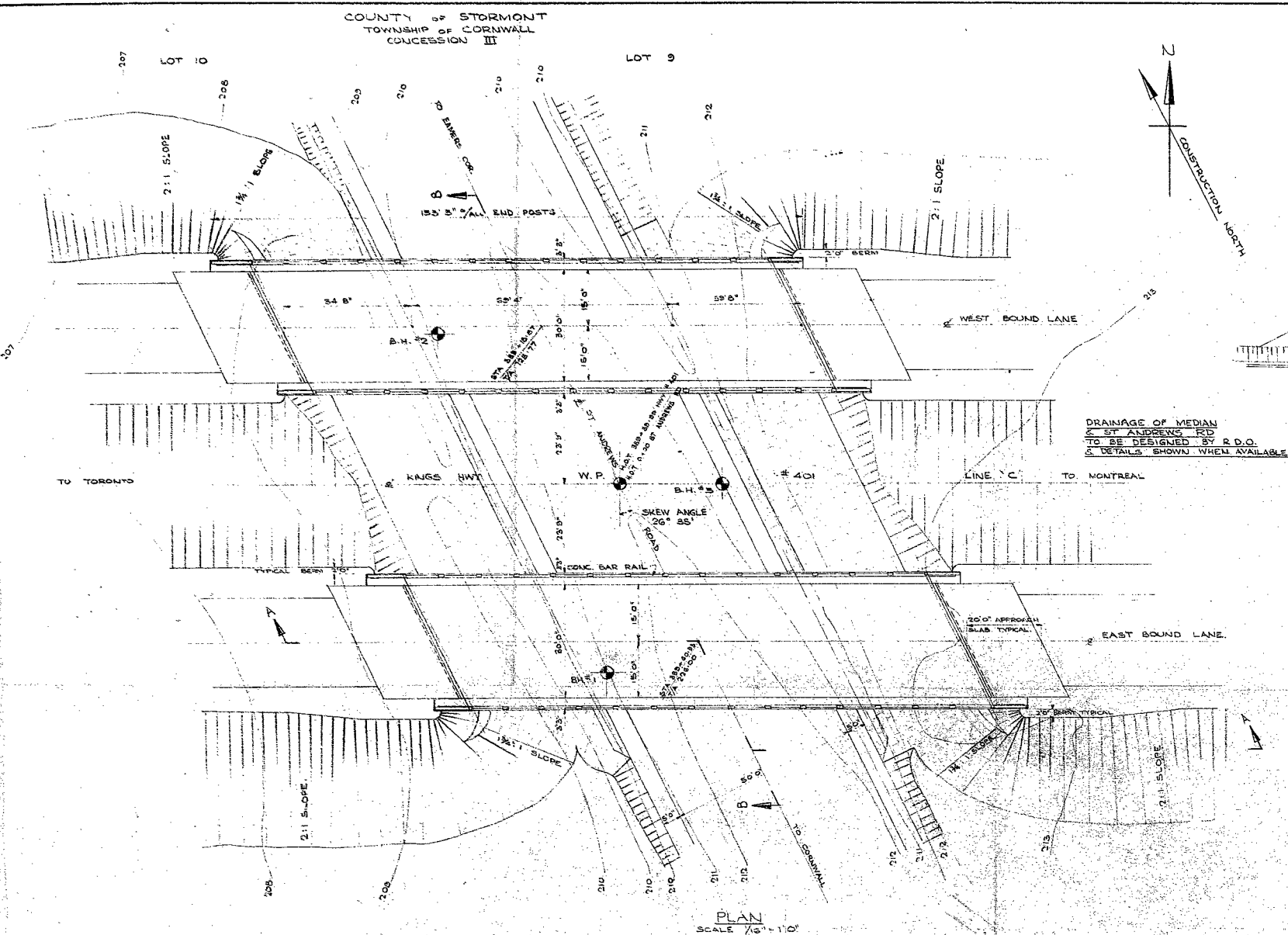
DRILL RIG CORE DRILL #4 JOB SS-F-3 CORNWALL BORING NO. 2
CASING 5X (STANDARD SAMPLERS TO FIT UNLESS NOTED) DATUM STA 389+14 AT 50' AT 116° 25' DATE REPORT
SAMPLER HAMMER WT. 250 DROPS INCHES COMPILED BY B.H. CHECKED BY B.H. BORING DATE MAY 21, 1955

SAMPLE CONDITION
DISTURBED
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LOST

SAMPLE TYPES
C.S. - CHUNK
D.O. - DRIVE OPEN
D.F. - DRIVE FOOT VALVE
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W.S. - WASHED SAMPLE
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EO 53257 PROCTOR & REDFERN CONSULTING ENGINEERS TORONTO		DWS N° A-53257- TORONTO
DEPARTMENT OF HIGHWAYS: ONTARIO- BRIDGE OFFICE-TORONTO		
CORNWALL TOWNSHIP BRIDGE N° 14 OVER ST ANDREWS RP		
THE KING'S HIGHWAY No. 401 CO. STORNONT		DIST. No. 3
TWP. CORNWALL	LOT 3 & 10	CON. III
PRELIMINARY GENERAL ARRANGEMENT		
APPROVED		
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