

## MEMORANDUM

23-65-263

TO: Mr. A. M. Toye,  
Bridge Engineer,  
Bridge Division.

FROM: Foundation Section,  
Materials & Testing Div.,  
Room 107, Lab. Bldg.

Attention: Mr. S. McCombie

DATE: May 13, 1965

OUR FILE REF.

IN REPLY TO

SUBJECT:

## FOUNDATION INVESTIGATION REPORT

For

Proposed Retaining Walls #1 & #2 at  
Hwy. #401 and Islington Avenue,  
District #6, Toronto

W.J. 65-F-42

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W.P. 85-59-6

A request from Mr. J. Curtis of the Bridge Office, for a foundation investigation at the above site, was received by this Section.

The subsequent investigation consisted of 4 sampled boreholes, carried out in April 1965.

The subsoil at the site consists of a thin layer of topsoil, underlain by an extensive deposit of glacial till. This till consists generally of clayey silt with sand and occasional gravel. The consistency of the till as estimated from the results of the Standard Penetration Test ('N' values 13 blows/ft. to 200 blows/ft.) varies from stiff to hard. Water level observations in the boreholes, carried out during the time of investigation, indicated the ground water level to be approximately 0.5 ft. below the ground level at the location of Retaining Wall #1, while it was found to be approximately 4 ft. below the ground level at the location of Retaining Wall #2.

cont'd. /2 ...

Our recommendations pertaining to the retaining structures are as follows:

1) The footings for the proposed retaining walls may be placed 5 ft. below the finished grade of the roadway with a safe bearing pressure of 3.0 t.s.f.

2) If footings are placed within the proposed fill material, the fill material below the top of the footings should consist of well-compacted G.B.C. Class 'A' material and should extend for a horizontal distance of not less than 3 ft. on either side of the footing tops as shown on Dwg. 65-F-42B. The fill should be completed to the finished grade before re-excavating for the footings. A safe bearing pressure of 2 t.s.f. may be used for design purposes. The sequence of filling operations, together with the extent of granular material required, are shown on Dwg. 65-F-42B.

3) Because of the limited number of boreholes carried out for the long retaining structure, some slight variations in consistency of the subsoil can be anticipated during construction. In view of this, it would be advisable, whenever some doubt exists, to have the footing excavations inspected by the Foundation Section prior to pouring the concrete. Provision should also be made in the Contract for deepening the foundations should this prove to be necessary.

cont'd. /3 ...

The field work, along with the preparation of this report, was undertaken by Mr. R. Magi, Project Foundation Engineer. The investigation was carried out under the general supervision of Mr. M. Devata, Senior Foundation Engineer, who also reviewed this report.

Equipment was owned and operated by Master Soil Investigations, Ltd., of Toronto.

We believe the contents of this report will prove adequate for your requirements; however, should there be any queries in connection with this project, please do not hesitate to contact our Office.

RM/MdeF  
Attach.

cc: Messrs. A. M. Toye (2)  
H. A. Tregaskes  
H. D. McMillan  
G. K. Hunter (2)  
J. C. Thatcher  
T. J. Kovich  
A. Watt

  
K. Y. Lo,  
SUPERVISING FOUNDATION ENGINEER

Foundations Office  
Gen. Files

APPENDIX I.



FOUNDATION SECTION

ORIGINATED BY R.M.

COMPILED BY R.M.

CHECKED BY M.D. SK

[illegible]

DEPARTMENT OF HIGHWAYS - ONTARIO

MATERIALS & TESTING DIVISION

# RECORD OF BOREHOLE NO. 3

FOUNDATION SECTION

JOB 65-F-42 LOCATION Sta 410+88 215' Rt. ORIGINATED BY R.M.  
W.P. 85-59-6 BORING DATE April 26, 1965 COMPILED BY R.M.  
DATUM \_\_\_\_\_ BOREHOLE TYPE Washboring CHECKED BY M.D. dhl

SOIL PROFILE			SAMPLES			ELEV. SCALE	DYNAMIC PENETRATION RESISTANCE BLOWS / FOOT		LIQUID LIMIT — WL PLASTIC LIMIT — WP WATER CONTENT — W		BULK DENSITY P.C.F.	REMARKS
ELEV. DEPTH	DESCRIPTION	STRAT. PLOT	NUMBER	TYPE	BLOWS / FOOT		SHEAR STRENGTH P.S.F.		WATER CONTENT %			
490.0	Groundlevel											
489.0	Topsoil											
1	Glacial Till (Clayey silt with sand and occasional gravel).  Stiff to hard.		1	SS	35	485						WL Elev ▼ 485.9  Sa 22% Si 71% Cl 7%  Gr 1% Sa 23% Si 61% Cl 15%  Gr 5% Sa 11% Si 57% Cl 27%
			2	SS	42							
			3	SS	54	480						
			4	SS	65							
			5	SS	14	475						
			6	SS	25	470						
			7	SS	42	465						
			8	SS	155	460						
			9	SS	100	455						
453.5	End of borehole.				6"	450						

FOUNDATION SECTION

JOB 65-F-42 LOCATION Sta 411+87 223' Rt. ORIGINATED BY R.M.  
W. P. 85-59-6 BORING DATE April 26, 1965. COMPILED BY R.M.  
DATUM \_\_\_\_\_ BOREHOLE TYPE Washboring CHECKED BY M.D. *MR*

[illegible]



DEPARTMENT OF HIGHWAYS - ONTARIO

## MATERIALS &amp; TESTING DIVISION

JOB 65-F-42

LOCATION 188' Rt., Sta 4094-60

ORIGINATED BY T.C.

W. P. 85-59-6

BORING DATE May 27, 1964

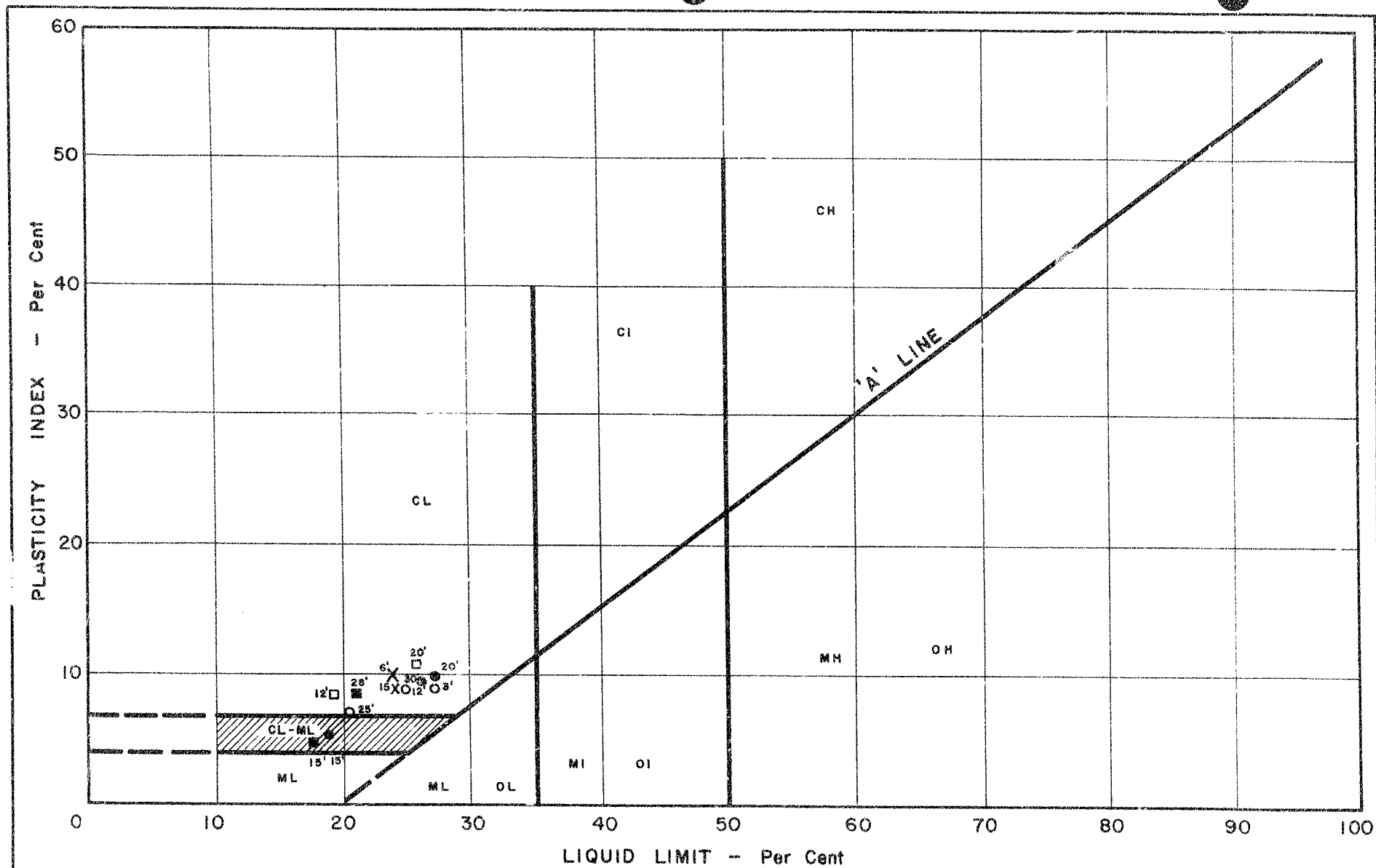
COMPILED BY T.C.

DATUM

BOREHOLE TYPE Pennsylvania Type Auger

CHECKED BY M.D.

SOIL PROFILE			SAMPLES			DYNAMIC PENETRATION RESISTANCE BLOWS / FOOT		LIQUID LIMIT ——— WL PLASTIC LIMIT ——— WP WATER CONTENT ——— W		BULK DENSITY  P.C.F.	REMARKS
ELEV. DEPTH	DESCRIPTION	STRAT. PLOT	NUMBER	TYPE	BLOWS / FOOT	ELEV. SCALE	SHEAR STRENGTH P.S.F.		Wp      W      WL WATER CONTENT % 10      20      30		
487.2	Groundlevel										
486.2	Topsoil										
1	Glacial Till (Clayey silt with sand and occasional gravel)					485					WL Elev ▼483.2
		1	SS	28							
		2	SS	39	480						
		3	SS	63							
		4	SS	103	475						
		5	SS	35							
		6	SS	33	470						
		7	SS	27							
	V. stiff to hard					465					
		8	SS	54							
						455					
						450					
448.2			10	SS	62 1/5"						
39.0	End of borehole.										



NOTES BOREHOLE 1-X

" 2-O

" 3-●

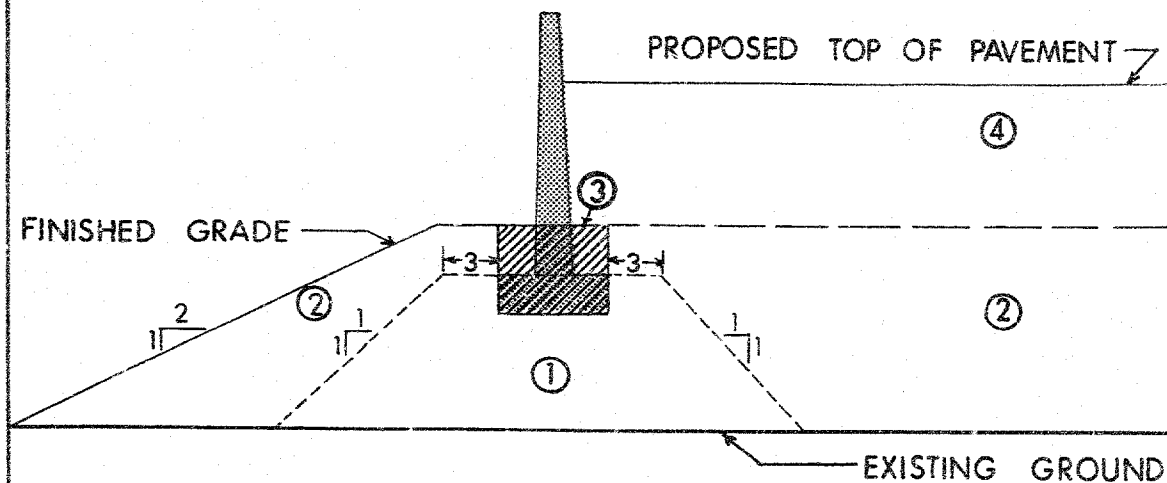
" 4-□

" 5-■

DEPARTMENT OF HIGHWAYS - ONTARIO  
 MATERIALS & RESEARCH DIVISION  
 PLASTICITY CHART

Job No. 65-F-42 W.P. No. 85-59-6

Location RETAINING WALLS 1 &amp; 2



### SEQUENCE OF CONSTRUCTION

- ① Construct granular fill (G.B.C.)
- ② Construct earth fill to the finished grade level.
- ③ Re-excavate and construct footing for the retaining structure. (MIN. 5' below finished grade)
- ④ Complete fill to the proposed grade.



DEPARTMENT OF HIGHWAYS  
MATERIALS and  
TESTING  
DIVISION

HWY. 401 & ISLINGTON AVE.  
TYPICAL SECTION OF RETAINING WALL  
ON COMPACTED FILL  
WP. 85-59-6 JOB. 65-F-42

DATE 1 JUNE 1965

APPROVED

DRAWING NO. 65-F-42B

## ABBREVIATIONS USED IN THIS REPORT

### PENETRATION RESISTANCE

STANDARD PENETRATION RESISTANCE 'N' - THE NUMBER OF BLOWS REQUIRED TO ADVANCE A STANDARD SPLIT SPOON SAMPLER 12 INCHES INTO THE SUBSOIL, DRIVEN BY MEANS OF A 140 POUND HAMMER FALLING FREELY A DISTANCE OF 30 INCHES.

DYNAMIC PENETRATION RESISTANCE - THE NUMBER OF BLOWS REQUIRED TO ADVANCE A 2 INCH, 60 DEGREE CONE, FITTED TO THE END OF DRILL RODS, 12 INCHES INTO THE SUBSOIL, THE DRIVING ENERGY BEING 350 FOOT POUNDS PER BLOW.

### DESCRIPTION OF SOIL

THE CONSISTENCY OF COHESIVE SOILS AND THE RELATIVE DENSITY OR DENSENESS OF COHESIONLESS SOILS ARE DESCRIBED IN THE FOLLOWING TERMS :-

<u>CONSISTENCY</u>	<u>'N' BLOWS / FT.</u>	<u>c LB. / SQ. FT.</u>	<u>DENSENESS</u>	<u>'N' BLOWS / FT.</u>
VERY SOFT	0 - 2	0 - 250	VERY LOOSE	0 - 4
SOFT	2 - 4	250 - 500	LOOSE	4 - 10
FIRM	4 - 8	500 - 1000	COMPACT	10 - 30
STIFF	8 - 15	1000 - 2000	DENSE	30 - 50
VERY STIFF	15 - 30	2000 - 4000	VERY DENSE	> 50
HARD	> 30	> 4000		

### TYPE OF SAMPLE

S.S.	SPLIT SPOON	T.W.	THINWALL OPEN
W.S.	WASHED SAMPLE	T.P.	THINWALL PISTON
S.B.	SCRAPER BUCKET SAMPLE	O.S.	OESTERBERG SAMPLE
A.S.	AUGER SAMPLE	F.S.	FOIL SAMPLE
C.S.	CHUNK SAMPLE	R.C.	ROCK CORE
S.T.	SLOTTED TUBE SAMPLE		
	P.H. SAMPLE ADVANCED HYDRAULICALLY		
	P.M. SAMPLE ADVANCED MANUALLY		

### SOIL TESTS

Q <sub>u</sub>	UNCONFINED COMPRESSION	L.V.	LABORATORY VANE
Q	UNDRAINED TRIAXIAL	F.V.	FIELD VANE
Q <sub>cu</sub>	CONSOLIDATED UNDRAINED TRIAXIAL	C	CONSOLIDATION
Q <sub>d</sub>	DRAINED TRIAXIAL	S	SENSITIVITY

# ABBREVIATIONS USED IN THIS REPORT

## SOIL PROPERTIES

$\gamma$	UNIT WEIGHT OF SOIL (BULK DENSITY)
$\gamma_s$	UNIT WEIGHT OF SOLID PARTICLES
$\gamma_w$	UNIT WEIGHT OF WATER
$\gamma_d$	UNIT DRY WEIGHT OF SOIL (DRY DENSITY)
$\gamma'$	UNIT WEIGHT OF SUBMERGED SOIL
G	SPECIFIC GRAVITY OF SOLID PARTICLES $G = \frac{\gamma_s}{\gamma_w}$
e	VOID RATIO
n	POROSITY
w	WATER CONTENT
$S_r$	DEGREE OF SATURATION
$w_L$	LIQUID LIMIT
$w_p$	PLASTIC LIMIT
$I_p$	PLASTICITY INDEX
s	SHRINKAGE LIMIT
$I_L$	LIQUIDITY INDEX = $\frac{w - w_p}{I_p}$
$I_c$	CONSISTENCY INDEX = $\frac{w_L - w}{I_p}$
$e_{max}$	VOID RATIO IN LOOSEST STATE
$e_{min}$	VOID RATIO IN DENSEST STATE
$I_D$	DENSITY INDEX = $\frac{e_{max} - e}{e_{max} - e_{min}}$
	RELATIVE DENSITY $D_r$ IS ALSO USED
h	HYDRAULIC HEAD OR POTENTIAL
q	RATE OF DISCHARGE
v	VELOCITY OF FLOW
i	HYDRAULIC GRADIENT
k	COEFFICIENT OF PERMEABILITY
j	SEEPAGE FORCE PER UNIT VOLUME
$m_v$	COEFFICIENT OF VOLUME CHANGE = $\frac{-\Delta e}{(1+e)\Delta\sigma}$
$c_v$	COEFFICIENT OF CONSOLIDATION
$C_c$	COMPRESSION INDEX = $\frac{\Delta e}{\Delta \log_{10} \sigma}$
$T_v$	TIME FACTOR = $\frac{c_v t}{d^2}$ (d, DRAINAGE PATH)
U	DEGREE OF CONSOLIDATION
$\tau_f$	SHEAR STRENGTH
$c'$	EFFECTIVE COHESION INTERCEPT
$\phi'$	EFFECTIVE ANGLE OF SHEARING RESISTANCE, OR FRICTION
$c_u$	APPARENT COHESION
$\phi_u$	APPARENT ANGLE OF SHEARING RESISTANCE, OR FRICTION
$\mu$	COEFFICIENT OF FRICTION
$S_t$	SENSITIVITY

## GENERAL

$\pi$	= 3.1416
e	BASE OF NATURAL LOGARITHMS 2.7183
$\log_e a$ OR $\ln a$	NATURAL LOGARITHM OF a
$\log_{10} a$ OR $\log a$	LOGARITHM OF a TO BASE 10
t	TIME
g	ACCELERATION DUE TO GRAVITY
V	VOLUME
W	WEIGHT
M	MOMENT
F	FACTOR OF SAFETY

## STRESS AND STRAIN

u	PORE PRESSURE
$\sigma$	NORMAL STRESS
$\sigma'$	NORMAL EFFECTIVE STRESS ( $\bar{\sigma}$ IS ALSO USED)
$\tau$	SHEAR STRESS
$\epsilon$	LINEAR STRAIN
$\gamma$	SHEAR STRAIN
$\nu$	POISSON'S RATIO ( $\mu$ IS ALSO USED)
E	MODULUS OF LINEAR DEFORMATION (YOUNG'S MODULUS)
G	MODULUS OF SHEAR DEFORMATION
K	MODULUS OF COMPRESSIBILITY
$\eta$	COEFFICIENT OF VISCOSITY

## EARTH PRESSURE

d	DISTANCE FROM TOP OF WALL TO POINT OF APPLICATION OF PRESSURE
$\delta$	ANGLE OF WALL FRICTION
K	DIMENSIONLESS COEFFICIENT TO BE USED WITH VARIOUS SUFFIXES IN EXPRESSIONS REFERRING TO NORMAL STRESS ON WALLS
$K_o$	COEFFICIENT OF EARTH PRESSURE AT REST

## FOUNDATIONS

B	BREADTH OF FOUNDATION
L	LENGTH OF FOUNDATION
D	DEPTH OF FOUNDATION BENEATH GROUND
N	DIMENSIONLESS COEFFICIENT USED WITH A SUFFIX APPLYING TO SPECIFIC GRAVITY, DEPTH AND COHESION ETC. IN THE FORMULA FOR BEARING CAPACITY
$k_s$	MODULUS OF SUBGRADE REACTION

## SLOPES

H	VERTICAL HEIGHT OF SLOPE
D	DEPTH BELOW TOE OF SLOPE TO HARD STRATUM
$\rho$	ANGLE OF SLOPE TO HORIZONTAL

#65-F-42

W.P.#85-59-6

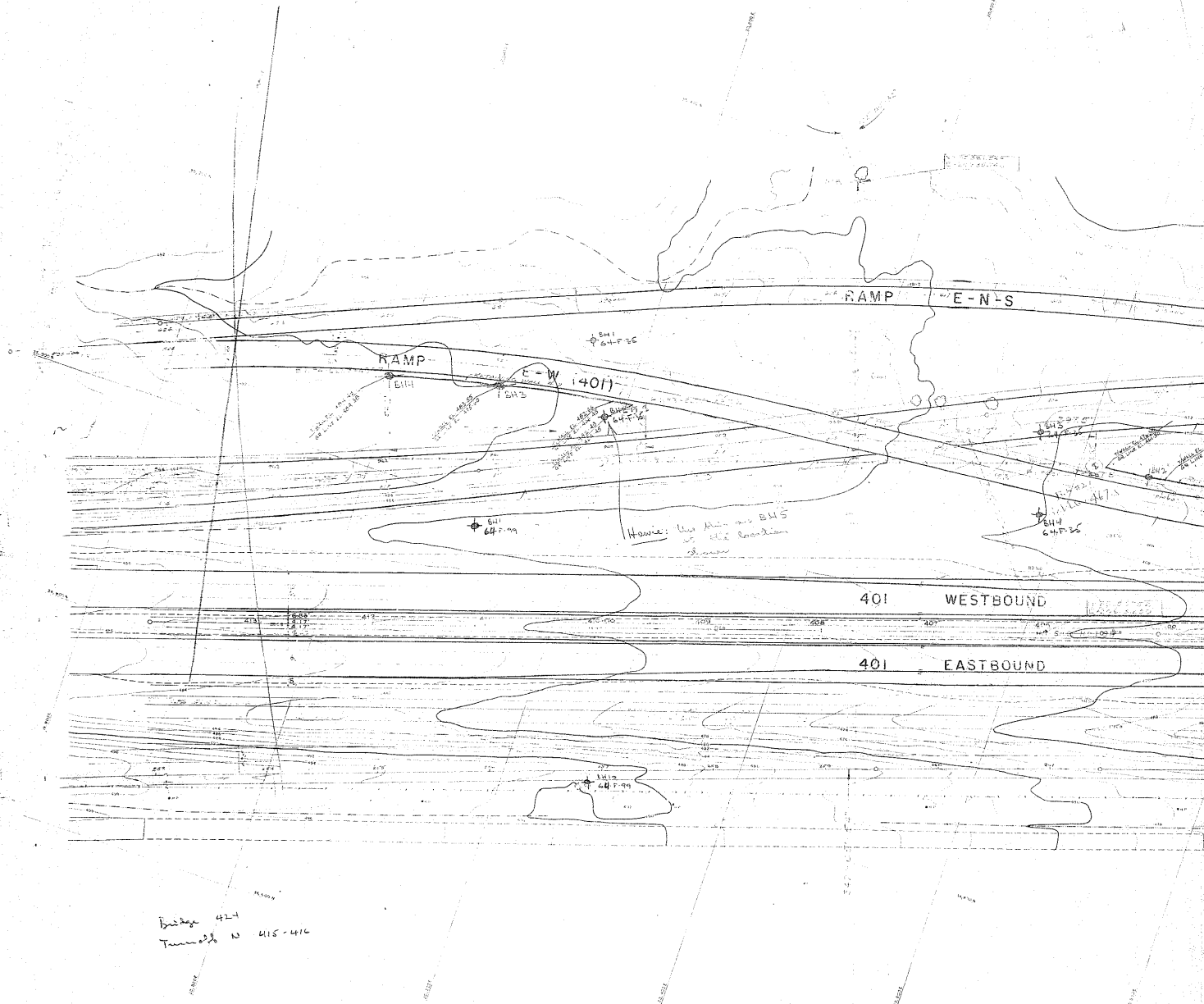
Hwy. #401 E

ISLINGTON

AVE. RETAINING

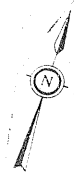
WALLS #1 E #2

(PROPOSED)



Bridge 42-1  
Tunnel N 415-416





205.72  
205.40  
434.103  
10.188  
311.87

W.B. COLLECTOR

BOUND

BOUND

E.B. COLLECTOR

DE LEUW CATHER AND COMPANY LIMITED

HWY. # 401 IMPROVEMENT  
DEPARTMENT OF HIGHWAYS - ONTARIO

SCALE 40 FT TO 1 INCH  
CONTOUR INTERVAL 2 FT

REVIEW PHOTOGRAPHY BY  
HILL, KELLEY AND ASSOCIATES  
CONTROL BY  
P.L.C. ON GEODETIC DATUM

DATE: 1962  
DRAWN: [Signature]  
APPROVED: [Signature]



Project	HWY. # 401 IMPROVEMENT
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Contour Interval	2 FT
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Project	HWY. # 401 IMPROVEMENT
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Contour Interval	2 FT
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