

**FOUNDATION INVESTIGATION REPORT
FOR
WHITE CHURCH ROAD UNDERPASS
HIGHWAY 6 (NEW)
FROM HIGHWAY 403 SOUTHERLY TO EXISTING HIGHWAY 6
W.P. 603-00-01, STRUCTURE SITE NO. 36-494
CITY OF HAMILTON, ONTARIO**

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PML Ref: 00HF108
Geocres No. 30M4-96

March, 2002

TABLE OF CONTENTS

INTRODUCTION	1
SITE DESCRIPTION	1
INVESTIGATION PROCEDURES	2
SUMMARIZED SUBSURFACE CONDITIONS.....	3
Topsoil	4
Upper Silty Clay	4
Silt.....	4
Lower Silty Clay	5
Bedrock.....	5
Groundwater	6
CLOSURE	7

APPENDICES

- APPENDIX A - Table I – Rock Core Description
- APPENDIX B - Figures 1 and 2 - Grain Size Distribution Charts
 - Figure 3 - Plasticity Chart
- APPENDIX C - Record of Borehole Logs
 - Drawing 1

FOUNDATION INVESTIGATION REPORT

For
White Church Road Underpass
Highway 6 (New)
From Highway 403 Southerly to Existing Highway 6
W.P. 603-00-01, Structure Site No. 36-494
City of Hamilton, Ontario

INTRODUCTION

This report summarizes the results of the foundation investigation carried out for the underpass structure to be constructed at White Church Road and Highway 6 (New) in the former Township of Glanbrook, now in the City of Hamilton, Ontario. The investigation was conducted for Delcan Corporation on behalf of the Ontario Ministry of Transportation.

The alignment of Highway 6 (New) will cross under White Church Road at approximate Station 16+626, Highway 6 (New) chainage.

The report pertains to the proposed bridge structure and approach embankments within about 20 m of the abutments between approximate Station 9+940 and 10+060, White Church Road chainage.

SITE DESCRIPTION

The site is situated some 35 m north of existing White Church Road, approximately 650 m west of existing Highway 6 in the former Township of Glanbrook. The structure will carry White Church Road traffic over the proposed Highway 6 (New). At the proposed location of the structure, Highway 6 (New) runs roughly north-south.

The lands adjacent to the site are primarily agricultural.

The site is situated approximately 10 km south of the Niagara Escarpment, south of the west end of Lake Ontario, in the broad physiographic region known as the Haldimand Clay Plain. In general, the topography on the plain is gently rolling.

The overburden is some 20 to 25 m thick and typically comprises glaciolacustrine silts and clays deposited in glacial Lake Warren. The underlying bedrock consists of dolostone of the Guelph Formation.

INVESTIGATION PROCEDURES

The fieldwork was carried out during the period November 7 to 9, 2000 and December 14 to 21, 2001 and comprised five boreholes (numbered 16 to 20) drilled at the locations indicated on Drawing 1, appended. The boreholes at the foundation units were extended some 3.5 to 4.1 m into bedrock to total depths of 26.5 to 27.8 m. Two boreholes were drilled to 6.6 m depth in the east and west approach embankments, some 20 m beyond the abutment locations.

The alignment of the abutments and approaches were staked in the field by J.D. Barnes Limited. The position of the boreholes along the staked alignments was selected by Peto MacCallum Ltd. with regard for access limitations and utility lines. The locations of and ground surface elevations at the boreholes were determined relative to the survey stakes.

The boreholes were advanced using continuous flight solid and hollow stem augers, powered by track-mounted CME-75 and 55 drillrigs, supplied and operated by a specialist drilling contractor, working under the full-time supervision of a member of our engineering staff.

Representative samples of the overburden were recovered at frequent depth intervals using a conventional split spoon sampler during drilling. Standard penetration tests were conducted simultaneously with the sampling operation to assess the strength characteristics of the substrata. Penetrometer testing was carried out on the recovered samples to determine the undrained shear strength of the cohesive soils.

In the deep boreholes drilled at the foundation units, casing was extended to the bedrock surface and a 3.5 to 4.1 m length of rock core was recovered from each hole using NQ rock coring equipment.

The groundwater conditions in the boreholes were closely monitored during the course of the fieldwork. In addition, standpipes were installed in two boreholes to monitor groundwater levels. Details of the installation and subsequent water level readings are recorded on the Record of Borehole Sheets.

All of the recovered samples were returned to our laboratory for detailed visual examination, classification and routine moisture content determinations. Grain size distribution analyses and Atterberg Limits tests were carried out on selected samples and are presented on the Record of Borehole Sheets and Figures 1 to 3 attached.

SUMMARIZED SUBSURFACE CONDITIONS

Reference is made to the appended Record of Borehole sheets for details of the subsurface conditions including soil classifications, inferred stratigraphy, boundary elevations, standard penetration test "N" values, penetrometer shear strength results, and groundwater observations. The results of laboratory grain size distribution analyses, Atterberg Limits tests, and moisture content determinations are also shown.

The borehole locations and a stratigraphic profile prepared from the borehole data are presented on Drawing 1.

The subsurface stratigraphy revealed at the bridge site generally comprised a surficial topsoil layer overlying native clay and silt units, underlain by clay. Dolostone bedrock was contacted below the overburden at 22.4 to 24.3 m depths. The strata encountered are summarized below:

Topsoil

Clayey silt/silty clay topsoil was encountered surficially in four boreholes. The topsoil layer was 100 to 270 mm thick.

Upper Silty Clay

A unit of stiff to very stiff cohesive silty clay was encountered below the topsoil in four boreholes and surficially in borehole 20. The 'N' values of the deposit ranged from 8 to 25. The undrained shear strength of the clay determined by penetrometer testing ranged from about 150 to 210 kPa. Moisture contents in this deposit ranged from 17 to 24%. The upper clay unit was penetrated at 3.3 to 4.9 m depth in all boreholes.

The results of the particle size distribution analyses conducted on the clay are presented on Figure 2. Liquid and plastic limits of 35 and 47 and 16 and 23 respectively with plasticity indices ranging from 16 to 24 were measured indicating a low to medium plastic clay (refer to Figure 3).

Silt

Non-plastic silt was contacted below the upper clay unit in all boreholes. The non cohesive silt was compact to very dense, with 'N' values ranging from 11 to 77, and moisture contents ranging from 15 to 21%, locally 24 to 26% in the upper 1.0 m in borehole 17. The results of grain size distribution analyses conducted on the silt are presented on Figure 1 appended.

Representative samples of the silt were examined by the project engineer and were deemed to be non-plastic, consequently Atterberg Limits tests were not conducted.

Drilling was terminated within the silt at 6.6 m depth in boreholes 16 and 20. The silt deposit was penetrated at 9.5 to 10.8 m depths in the remaining boreholes.

Lower Silty Clay

Cohesive silty clay was contacted below the silt in boreholes 17, 18 and 19. The consistency of the clay was stiff to very stiff, with 'N' values ranging from 8 to 28. The undrained shear strength of the clay determined by penetrometer testing ranged from 25 to 130 kPa. Moisture contents varied from 20 to 34%. The clay deposit mantled bedrock.

The results of a particle size distribution analysis conducted on a sample of the clay are presented on Figure 2. Liquid and plastic limits of 33 to 41 and 20 to 21 respectively, with plasticity indices ranging from 13 to 20 were measured, indicating a low to medium plastic clay (refer to Figure 3).

Bedrock

Dolostone bedrock was contacted below the clay overburden in boreholes 17, 18 and 19 at the following depths:

Borehole	Depth to Bedrock (m)	Elevation
17	22.4	194.7
18	23.6	194.5
19	24.3	192.9

Rock core lengths of 3.5 to 4.1 m were recovered from boreholes 17, 18 and 19.

A description of the recovered rock core is provided on Table I. Core recovery was 48 and 58% in the first two 1.5 m lengths of core retrieved in borehole 17, and 70% in the upper 1.1 m length of core retrieved in borehole 18. The core recovery in the upper lengths of borehole 19 was 100%. The core recovery increased to 97 to 100% in the lower 1.1 to 3.0 m of recovery in

boreholes 17, 18 and 19. The RQD determined from the upper 3.0 m of all core recovered ranged from 13 to 62%, indicating a very poor to fair quality rock. The RQD improved to between 69 to 84% (fair to good quality) in the next 1.1 to 1.5 m.

The unconfined compressive strengths of selected core samples were as follows:

Borehole	Depth (m)	Unconfined Compressive Strength (MPa)
17	22.6	85.0
17	25.6	63.0

Groundwater

Water was encountered after sampling to 3.5 m in boreholes 16 and 17. Upon completion of augering, water was observed in the west and east embankment approach holes at 3.0 and 5.8 m depths. The following water levels were measured in the standpipes:

Borehole No.	November 14, 2000		January 29, 2002	
	Depth to Water (m)	Elevation	Depth to Water (m)	Elevation
16	0.9	216.2	Standpipe Destroyed	
17	2.1	215.0	4.8	212.3

Observed groundwater levels are subject to seasonal fluctuations and rainfall patterns.

CLOSURE

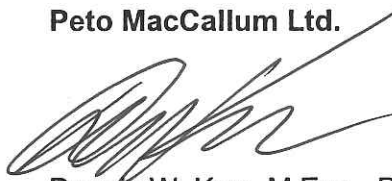
The fieldwork was carried out under the supervision of Mr. M. Rapsey and direction of Mr. M.R. Anderson, P.Eng. The equipment was supplied by Bart Chaston Water Haulage and Malone's Soil Samples Co. Ltd.

The report was prepared by Mr. P. Cullen, B.Eng. and Mr. M.R. Anderson, M.Eng., P.Eng., Senior Project Engineer and reviewed by Mr. B.R. Gray, M.Eng., P.Eng., President. Mr. D.W. Kerr, M.Eng., P.Eng., Manager of Geotechnical and Geo-Environmental Services, Hamilton carried out an independent review of the report.

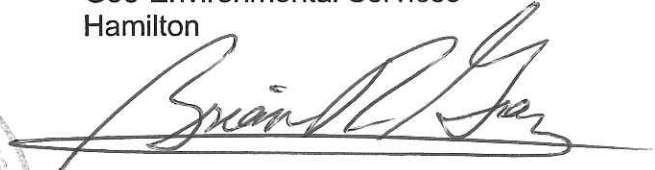
Yours very truly

Peto MacCallum Ltd.




Dennis W. Kerr, M.Eng., P.Eng.
Manager Geotechnical and
Geo-Environmental Services
Hamilton




Brian R. Gray, M.Eng., P.Eng.
President

PC:ld

APPENDIX A

TABLE I - ROCK CORE DESCRIPTION

TABLE I

ROCK CORE DESCRIPTION
WHITE CHURCH ROAD UNDERPASS AT HIGHWAY 6 (NEW)
W.P. 603-00-01, STRUCTURE SITE NO. 36-494
CITY OF HAMILTON, ONTARIO

BOREHOLE	CORE RECOVERY				CORE DESCRIPTION	
	CORE NO.	RUN (m)	RECOVERY (%)	RQD (%)	DEPTH (m)	DESCRIPTION
17	14	22.40 – 23.95	48	27	22.40 – 26.50	DOLOSTONE: Grey, fine crystalline, high strength; unweathered; highly porous layers, some voids, occ. shaley partings; close spaced flat partings, rough planar, tight and dipping to vertical joint, smooth planar, tight; very poor to poor quality.
	15	23.95 – 25.45	58	28		
	16	25.45 – 26.50	98	69		
18	14	23.60 – 24.70	70	13	23.60 – 27.70	DOLOSTONE: Grey, fine grained, medium to high strength; unweathered; occ. black shale partings, stylolitic partings, occ. vugs and pitting with calcite encrustation/infilling; close spaced flat bedding layers, smooth to rough planar, tight; very poor to fair quality. (Guelph Formation)
	15	24.70 – 26.20	97	57		
	16	26.20 – 27.70	100	63		
19	14	24.30 – 24.70	100	44	24.30 – 27.80	DOLOSTONE: Grey, fine grained, medium to high strength; unweathered; occ. irregular black shale partings, stylolitic partings, occ. vugs and pitting with calcite encrustation/infilling; close to moderate spaced flat bedding layers, rough planar, tight; poor to good quality. (Guelph Formation)
	15	24.70 – 26.20	100	62		
	16	26.20 – 27.80	100	84		

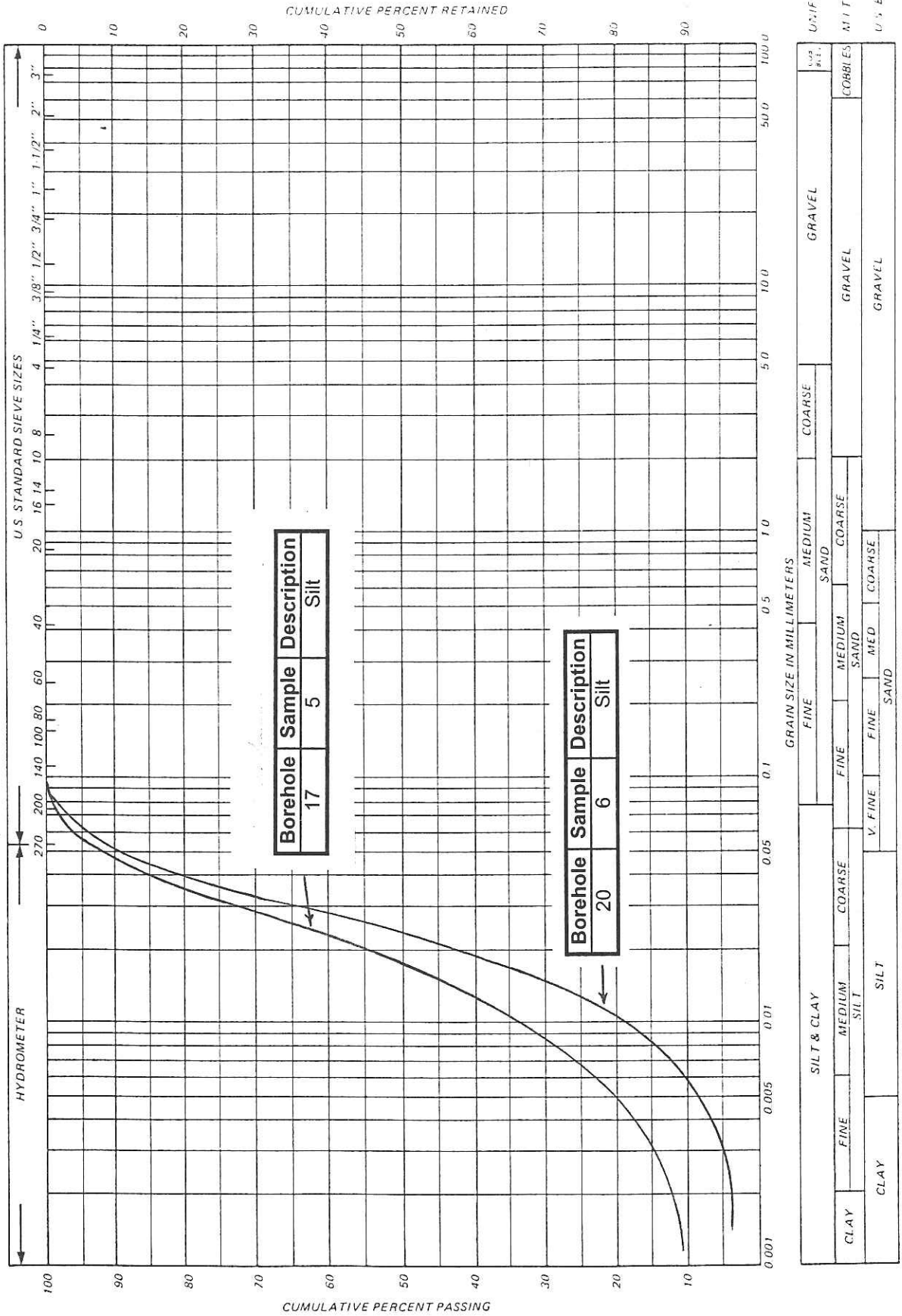
Logged by J.F. Wright using the Provincial Highways "A Guide to the Description of Rock for Engineering Purposes" dated October, 1982.

RQD = Rock Quality Designation

APPENDIX B

FIGURES 1 TO 3

PARTICLE SIZE DISTRIBUTION CHART

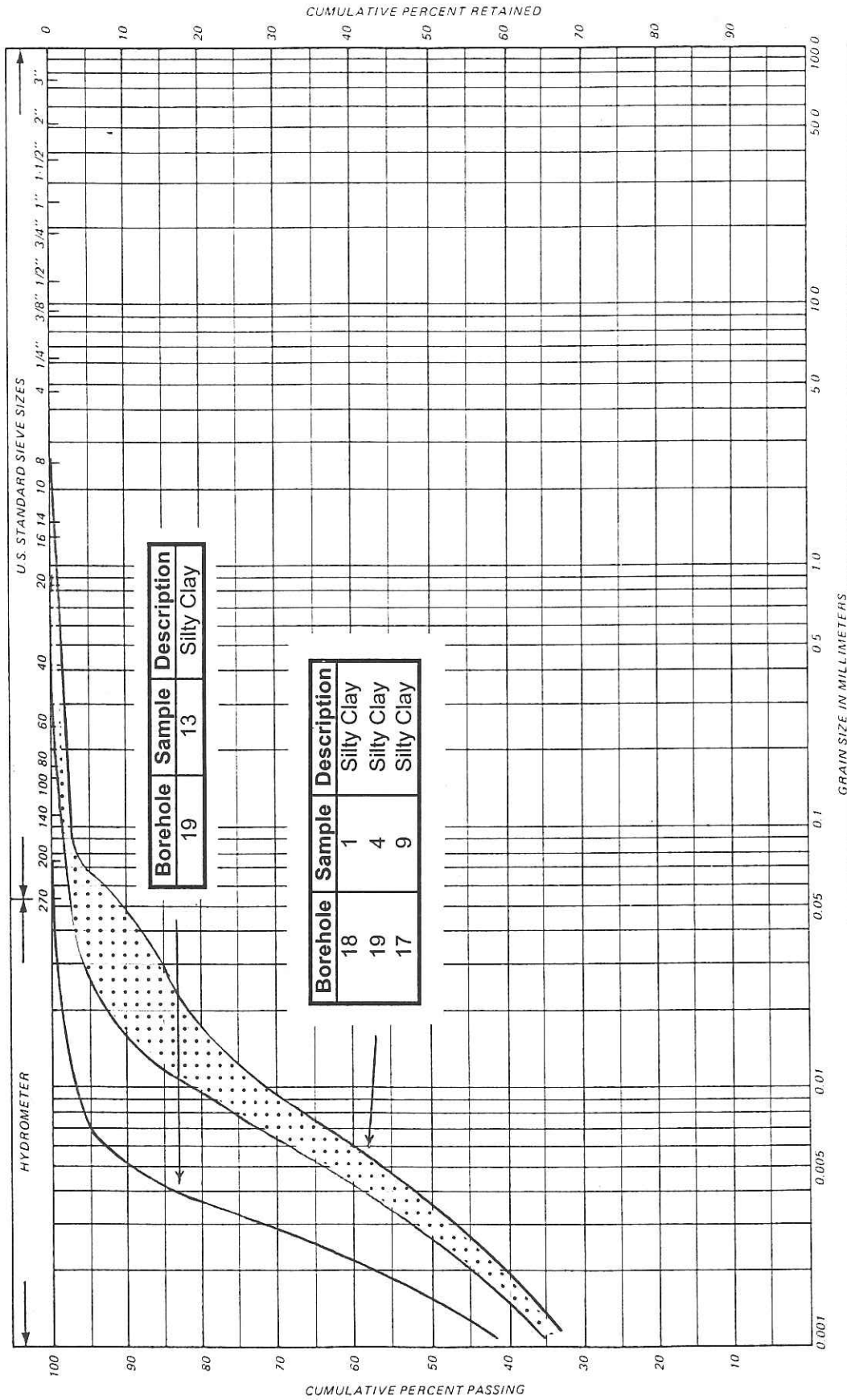


REMARKS

Silt

PML REF. 00HF108
REPORT NO. -
FIGURE 2

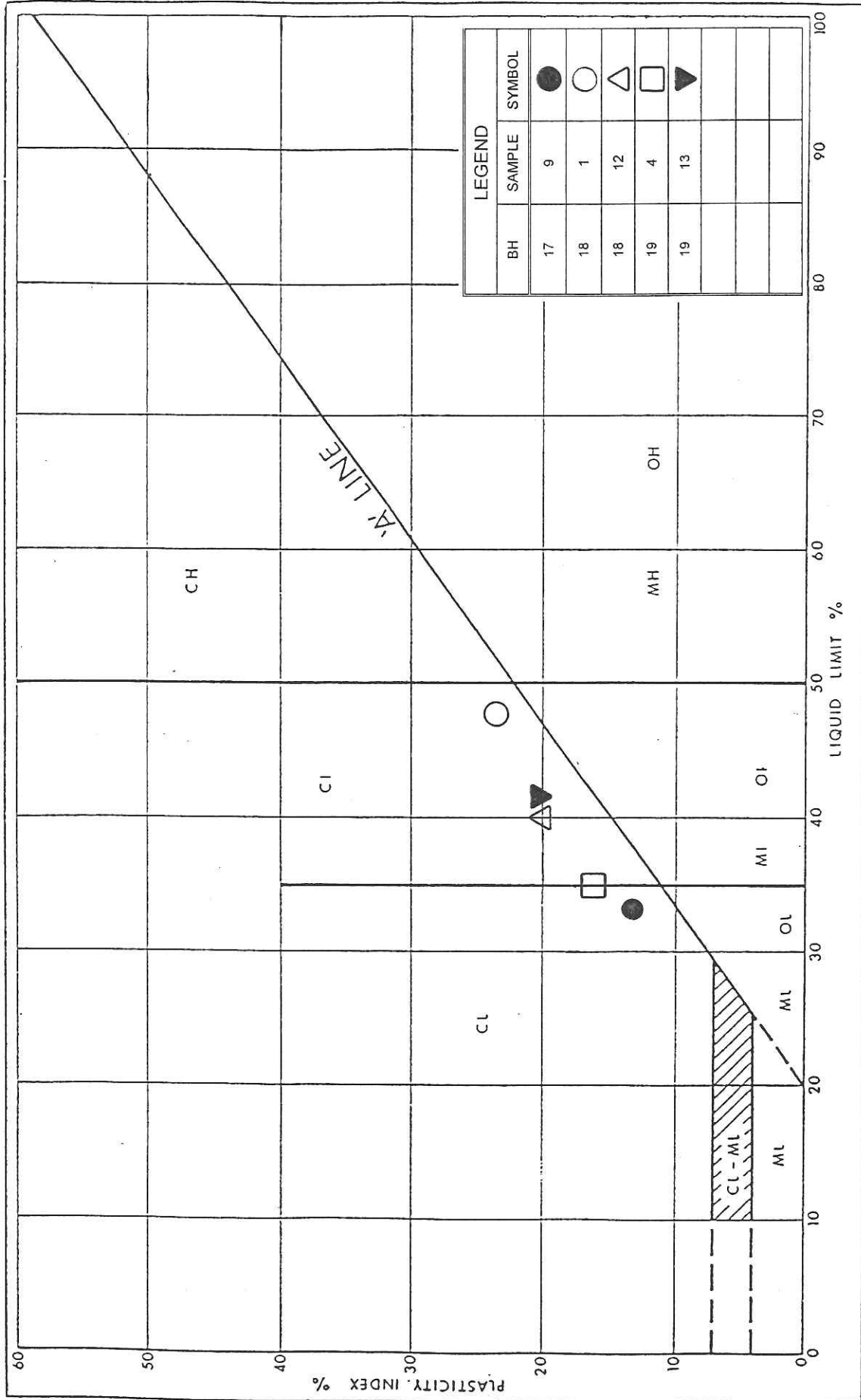
PARTICLE SIZE DISTRIBUTION CHART



CLAY				SILT & CLAY				SAND				GRAVEL				UNIFIED	
FINE				MEDIUM				COARSE				COARSE				MIT	
CLAY				SILT				SAND				GRAVEL				U.S. BUREAU	
CLAY				SILT				SAND				GRAVEL				U.S. BUREAU	

Silty Clay

REMARKS



APPENDIX C

RECORD OF BOREHOLE SHEETS
DRAWING NO. 1

LIST OF ABBREVIATIONS

PENETRATION RESISTANCE

STANDARD PENETRATION RESISTANCE 'N', - THE NUMBER OF BLOWS REQUIRED TO ADVANCE A STANDARD SPLIT SPOON SAMPLER 0.3m INTO THE SUBSOIL. DRIVEN BY MEANS OF A 63.5kg HAMMER FALLING FREELY A DISTANCE OF 0.76m.

DYNAMIC PENETRATION RESISTANCE : - THE NUMBER OF BLOWS REQUIRED TO ADVANCE A 51mm, 60 DEGREE CONE, FITTED TO THE END OF DRILL RODS. 0.3m INTO THE SUBSOIL. THE DRIVING ENERGY BEING 475 J PER BLOW.

DESCRIPTION OF SOIL

THE CONSISTENCY OF COHESIVE SOILS AND THE RELATIVE DENSITY OR DENSENESS OF COHESIONLESS SOILS ARE DESCRIBED IN THE FOLLOWING TERMS :-

<u>CONSISTENCY</u>	<u>'N' BLOWS/0.3 m</u>	<u>c kPa</u>	<u>DENSENESS</u>	<u>'N' BLOWS/0.3 m</u>
VERY SOFT	0 - 2	0 - 12	VERY LOOSE	0 - 4
SOFT	2 - 4	12 - 25	LOOSE	4 - 10
FIRM	4 - 8	25 - 50	COMPACT	10 - 30
STIFF	8 - 15	50 - 100	DENSE	30 - 50
VERY STIFF	15 - 30	100 - 200	VERY DENSE	> 50
HARD	> 30	> 200		
W.T.P.L.	WETTER THAN PLASTIC LIMIT		D.T.P.L.	DRIER THAN PLASTIC LIMIT
	A.P.L. ABOUT PLASTIC LIMIT			

TYPE OF SAMPLE

S.S	SPLIT SPOON	T.W	THINWALL OPEN
W.S	WASHED SAMPLE	T.P	THINWALL PISTON
S.B	SCRAPER BUCKET SAMPLE	O.S	OESTERBERG SAMPLE
A.S	AUGER SAMPLE	F.S	FOIL SAMPLE
C.S	CHUNK SAMPLE	R.C	ROCK CORE
S.T	SLOTTED TUBE SAMPLE		
	P.H	SAMPLE ADVANCED HYDRAULICALLY	
	P.M	SAMPLE ADVANCED MANUALLY	

SOIL TESTS

Qu	UNCONFINED COMPRESSION	L.V	LABORATORY VANE
Q	UNDRAINED TRIAXIAL	F.V	FIELD VANE
Qcu	CONSOLIDATED UNDRAINED TRIAXIAL	C	CONSOLIDATION
Qd	DRAINED TRIAXIAL		

▲, Δ - Undisturbed and remoulded shear strength determined from in situ vane test.

■ - Undrained shear strength determined from pocket penetrometer test.

RECORD OF BOREHOLE No 16

1 of 1 METRIC

G.W.P. 603-00-01 LOCATION Co-ords. 4 778 462 N; 269 969 E ORIGINATED BY P.C.
DIST CR HWY 6 (NEW) BOREHOLE TYPE Continuous Flight Solid Stem Augers COMPILED BY M.R.A.
DATUM Geodetic DATE November 09, 2000 CHECKED BY D.W.K.

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			20	40					
217.11	Ground surface													
0.00	Topsoil													
0.27	Silty Clay, trace of sand and gravel		1	SS	20									
			2	SS	17									
			3	SS	14									
			4	SS	13									
213.81	Silt, trace of clay and fine sand													
3.30	Very dense Greyish brown		5	SS	77									
210.56	End of borehole		6	SS	57									
6.55	DATE Groundwater 11/14/00 Elevation 216.2 Standpipe destroyed													

RECORD OF BOREHOLE No 17

1 of 2 METRIC

G.W.P. 603-00-01 LOCATION Co-ords. 4 778 459 N; 269 988 E ORIGINATED BY P.C.
DIST CR HWY 6 (NEW) BOREHOLE TYPE Continuous Flight Hollow Stem Augers, NQ Coring COMPILED BY M.R.A.
DATUM Geodetic DATE November 07, 2000 CHECKED BY D.W.K.

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)	
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			SHEAR STRENGTH kPa							WATER CONTENT (%)
217.14	Topsoil						20	40	60	80	100	20	40	60	Water encountered after sample 4
0.00	Silty Clay, trace of sand														
0.20	Stiff to Khaki very brown stiff		1	SS	16										
		2	SS	13											
214.74	Silt, trace of clay and fine sand	3	SS	11											
2.40	Compact Brown and grey	4	SS	11											
		5	SS	28											
		6	SS	42											
		7	SS	51											

Cont'd

RECORD OF BOREHOLE No 17

2 of 2 METRIC

G.W.P. 603-00-01 LOCATION Co-ords. 4 778 459 N; 269 988 E ORIGINATED BY P.C.
DIST CR HWY 6 (NEW) BOREHOLE TYPE Continuous Flight Hollow Stem Augers, NQ Coring COMPILED BY M.R.A.
DATUM Geodetic DATE November 07, 2000 CHECKED BY D.W.K.

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC NATURAL LIQUID LIMIT MOISTURE CONTENT LIMIT			UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL	
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	SHEAR STRENGTH kPa ○ UNCONFINED + FIELD VANE ● QUICK TRIAXIAL X LAB VANE		WATER CONTENT (%) W _p W W _L				
217.14	occasional partings of silt		11	SS	9									
			12	SS	28									
			13	SS	8									
194.74	Dolostone bedrock		14	RC										
22.40														
			15	RC										
			16	RC										
190.64	End of borehole													
26.50														
DATE Groundwater Elevation														
9 Nov. 2000 214.7														
14 Nov. 2000 215.0														
29 Jan. 2002 212.3														

1 of 2 METRIC

[illegible]

RECORD OF BOREHOLE No 19

1 of 2 METRIC

G.W.P. 603-00-01 LOCATION Co-ords. 4 778 443 N; 270 053 E ORIGINATED BY R.B.
DIST CR HWY 6 (New) BOREHOLE TYPE Continuous Flight Hollow Stem Augers & NQ Coring COMPILED BY P.C.
DATUM Geodetic DATE December 20, 2001 CHECKED BY B.R.G.

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT w _p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w _L	UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL			
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			SHEAR STRENGTH kPa									
								○ UNCONFINED + FIELD VANE									
								● QUICK TRIAXIAL X LAB VANE									
							WATER CONTENT (%)										
							20 40 60 80 100					20 40 60					
217.22							217										
0.10	Topsoil						216										
	Silty clay, trace of sand, with bluish grey fissures		1	SS	8												
	Stiff to Brown very stiff		2	SS	21												
			3	SS	19												
			4	SS	16												
213.22	Silt, trace of sand, trace of gravel						213										
4.00	Dense Grey Damp		5	SS	43												
			6	SS	42												
			7	SS	42												
			8	SS	32												
207.12	Silty clay, trace of sand, mottled						207										
10.10	Stiff Grey		9	SS	10												
			10	SS	12												
							206										
							205										
							204										
							203										

Cont'd

2 of 2

METRIC

DATUM Geodetic DATE December 20, 2001 CHECKED BY B.R.G.

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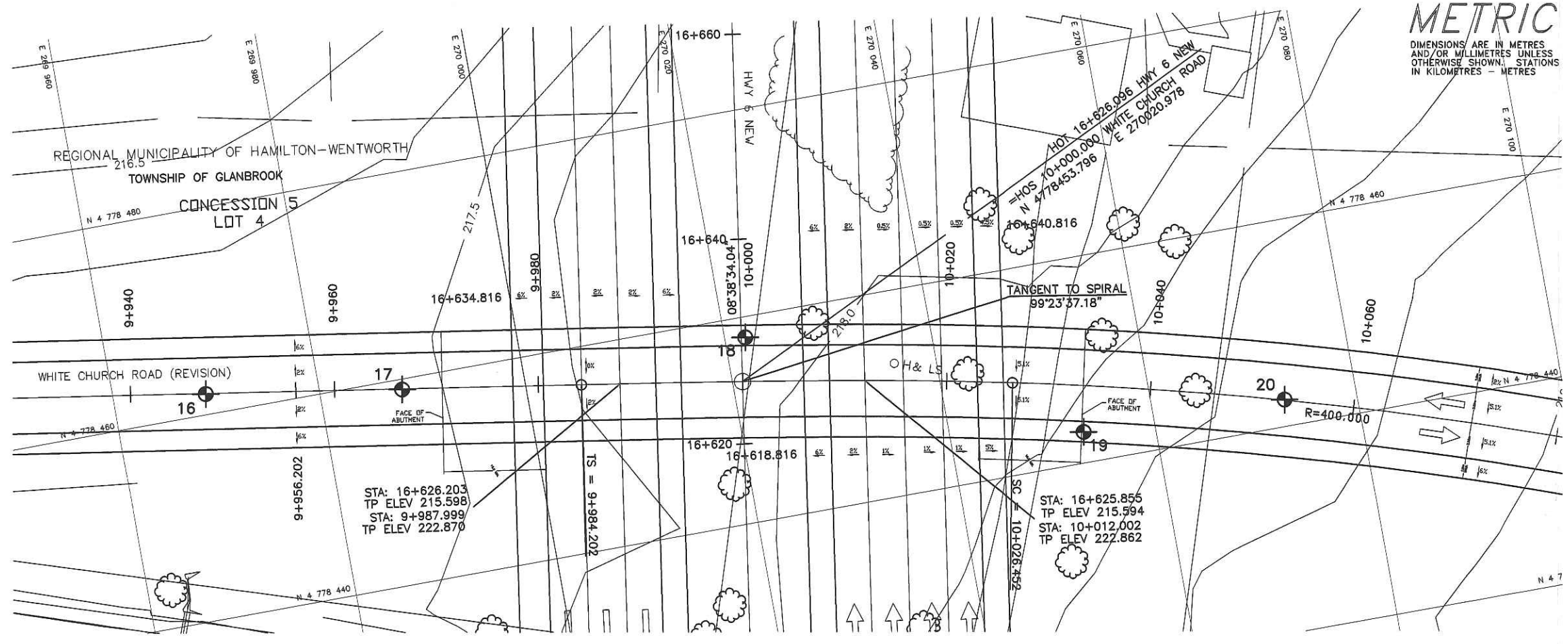
(%) STRAIN AT FAILURE

RECORD OF BOREHOLE No 20

1 of 1 METRIC

G.W.P. 603-00-01 LOCATION Co-ords. 4 778 443 N; 270 073 E ORIGINATED BY R.B.
DIST CR HWY 6 (New) BOREHOLE TYPE Continuous Flight Hollow Stem Augers COMPILED BY P.C.
DATUM Geodetic DATE December 21, 2001 CHECKED BY B.R.G.

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT w _p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w _L	UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			SHEAR STRENGTH kPa									
								○ UNCONFINED + FIELD VANE ● QUICK TRIAXIAL × LAB VANE									
216.68 0.00	Silty clay, trace of sand, trace of gravel Very stiff Brown						20	40	60	80	100						
			1	SS	22												
			2	SS	22												
			3	SS	25												
			4	SS	19												
212.68 4.00	Silt, trace of fine sand, trace of clay Dense Brown Damp to grey to moist																
			5	SS	44												
210.08 6.60	End of Borehole		6	SS	30											0 2 94 4	



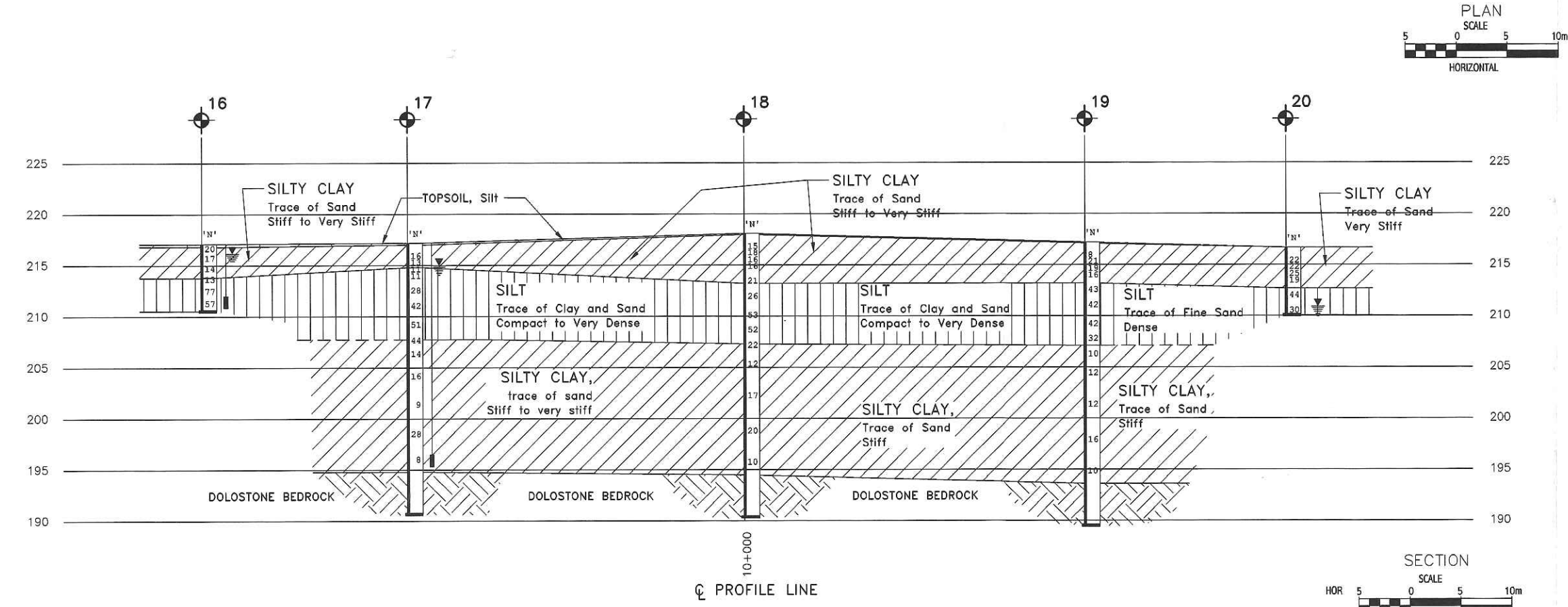
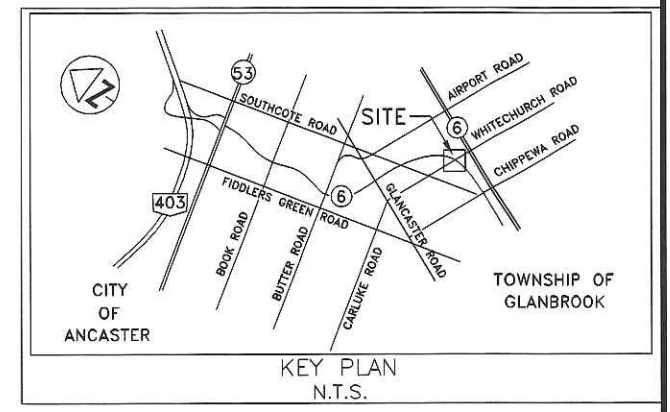
METRIC
DIMENSIONS ARE IN METRES
AND/OR MILLIMETRES UNLESS
OTHERWISE SHOWN. STATIONS
IN KILOMETRES - METRES

CONT No.
WP No. 603-00-01

HWY 6 (NEW) FROM HWY 403
TO EXISTING HWY 6
WHITECHURCH ROAD UNDERPASS
BOREHOLE LOCATION & SOIL STRATA

SHEET

Peto MacCallum Ltd.
CONSULTING ENGINEERS



LEGEND

Borehole
N Blows/0.3m (Std. Pen Test, 475 l / blow)
 W L at time of investigation
or in piezometer
 Piezometer

No	ELEVATION	CO-ORDINATES	
		NORTH	EAST
16	217.11	4 778 462	269 969
17	217.14	4 778 459	269 988
18	218.10	4 778 458	270 022
19	217.22	4 778 443	270 053
20	216.68	4 778 443	270 073

NOTE
The boundaries between soil strata have been established only at Borehole locations. Between Boreholes the boundaries are assumed from geological evidence.

REV.	DATE	BY
Geocres No. 30M4-96		
HWY No. 6	DIST	
SUBM'D P.C.	CHECKED M.R.A. DATE FEB. 2002	SITE 36-494
DRAWN C.B.	CHECKED B.R.G. APPROVED D.W.K.	DWG 1