



FINAL REPORT

FOUNDATION INVESTIGATION REPORT

New Patrol Yard Structure at MTO Jarvis Patrol Yard, Haldimand County

Agreement No. 3015-E-0017

Assignment No. 6

GWP 3075-16-00

Geocres No. 40116-28

Prepared for:

Ontario Ministry of Transportation

Regional Director's Office -West Region

Geotechnical Section

659 Exeter Road

London, ON N6E 1L3

Attn: Muhammad Kamran Khan, P.Eng., PMP

Ontario Ministry of Transportation

Pavements and Foundations Section

Materials Engineering and Research Office, Room 223, 2/F

145 Sir William Hearst Avenue

Toronto, ON M3M 0B6

Attn: David Staseff, P.Eng.

exp Services Inc.

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Ministry of Transportation

Western Region – Geotechnical Section

Foundation Investigation Report

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Prepared By:

Silvana Micic, Ph.D., P.Eng.

Nimesh Tamrakar, M.Eng.

Reviewed By:

TaeChul Kim, M.E.Sc., P.Eng.

Stan E. Gonsalves, M.Eng., P.Eng.

exp Services Inc.

56 Queen St, East, Suite 301

Brampton, ON L6V 4M8

Canada



Silvana Micic, Ph.D., P.Eng.
Senior Geotechnical Engineer



Stan E. Gonsalves, M.Eng., P.Eng.
Principal Engineer
Designated MTO Foundation Contact

Date Submitted:

11/29/2017

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1 FOUNDATION INVESTIGATION REPORT

1.1 Introduction

This report presents the results of a geotechnical investigation carried out by **exp** Services Inc. (**exp**) for the proposed new salt storage structure located at the MTO Jarvis Patrol Yard, located in Haldimand County, Southern Ontario. The work was undertaken under Agreement # 3015-E-0017, Assignment No. 6 (GWP 3075-16-00). The terms of reference (TOR) were as presented in the Ministry of Transportation (MTO) email received on July 27, 2017.

The purpose of this investigation is to establish existing subsurface conditions at the proposed location of the patrol yard structure within construction limits defined by MTO. The site specific geotechnical investigation consisted of field investigation including visual inspection, drilling, soil sampling, and laboratory testing. Factual results of the investigation and laboratory testing are included in this report. The report has been prepared specifically and solely for the project described in the report.

1.2 Site Description and Geological Setting

1.2.1 Site Description

The Jarvis Patrol Yard is located on Old Hwy 3, approximately 1.3 km west of the Hwy 3 and Hwy 6 junction in Jarvis, Haldimand County, Southern Ontario (see Key Map on Drawing 1, Appendix B). The site is bound by West Concession 7 Walpole to the north, Old Hwy 3 to the east, and by farm land to the south and west.

A paved roadway and parking area lead from the site entrance on Old Hwy 3 to an approximately 7x9 m steel shed, which is located approximately 60 m west of entrance gate, and to an approximately 18x32 m gambrel style building, which is located immediately west of the proposed structure.

The topography of the site is considered flat lying with borehole elevations ranging from 210.0 to 210.3 m. The ground surface of the proposed building site consists of gravel near the south end and transitions to tall grass to the north. The area beyond the north boundary of the proposed building consists of bush with mature trees. Photographs of the site are included in Appendix A.

1.2.2 Geological Setting

The Map P.2715 (Physiography of Southern Ontario, Third Edition, 1984) Bedrock Geology of Ontario, Southern Sheet, 1991) of the Ministry of Natural Resources indicates that the project area is located at the boundary of Sand Plain and Clay Plain. The Map 2556 (Quaternary Geology of Ontario, Southern Sheet, 1991) of the Ministry of Northern Development and Mines, indicates that the surface conditions consist of glaciolaustrine deposits including silt and clay, minor sand; basin and quiet water deposits. The Map 2544 (Bedrock Geology of Ontario, Southern Sheet, 1991) of the Ministry of Northern

Development and Mines, indicates that the bedrock formation of the project area consists of limestone, dolostone and shale, middle devonian.

1.3 Investigation Procedures

1.3.1 General

The field investigation was performed between August 23 and 25, 2017. The field program consisted of drilling five (5) sampled boreholes (BH-1 to BH-5). The boreholes were strategically located at the patrol yard to provide the subsurface information for the design of the proposed salt storage structure. The borehole locations are shown on Drawing 1 in Appendix B.

The borehole locations (referenced to the MTM NAD83 coordinate system) and their ground surface elevations were surveyed by **exp** personnel, with reference to a temporary benchmark (TBM) established on site. The TBM was set on top of concrete slab on grade located at the east side of the sliding garage door entrance to the large gambrel style building. The elevation of the TBM was assigned 210.0 m, and location of the TBM is shown on Drawing 1, in Appendix B.

The boreholes were advanced using a truck mounted CME-75 drill rig, equipped with a hollow stem augers and diamond bit NW casing. All borehole drilling and sampling operations were performed by a specialist drilling contractor, Elite Drilling Services. Boreholes BH-1, BH-3, and BH-5 were augered to refusal on bedrock then cored to depths ranging from 10.7 m to 11.0 m below grade and boreholes BH-2 and BH-4 were augered to refusal on bedrock at depths of 7.6 m and 7.7 m, respectively.

During the drilling of the boreholes, soil samples were obtained using a 51 mm outside diameter (O.D.) split-spoon sampler in accordance with Standard Penetration Test (SPT) procedures (ASTM D 1586), at intervals shown on the attached borehole logs (Appendix C). The original field (uncorrected) SPT "N" values were recorded on the borehole logs as recommended in the Canadian Foundation Engineering Manual (CFEM pg. 40), and used to provide an assessment of in-situ consistency of cohesive soils or relative density of non-cohesive soils. Field vane testing was conducted in cohesive soil to measure the in-situ undrained shear strength of this soil. Field vane test was conducted in accordance with ASTM D2573-08. When a hard stratum was reached sampling of hard material was performed by diamond core drilling, using a 1.5 m long NQ double tube wireline core barrel.

Upon completion of the drilling operations, groundwater level measurements were carried out in the open holes. All boreholes remained dry upon completion of the drilling operations and the groundwater level at BH-1 was measured at 7.5 m below grade after remaining open for a period of four hours (see Section 1.5). The boreholes were decommissioned by bentonite/cement mixtures in accordance with the Ministry of the Environment Regulation 903, as amended by Regulation 128/03 (the well regulation under the Ontario Water Resources Act).

The fieldwork was supervised by a member of **exp's** engineering staff who directed the drilling and sampling operation, logged borehole data in accordance with MTO and/or ASTM standards for soils classification, and retrieved soil samples for subsequent laboratory testing and identification.

All the recovered soil samples were placed in labelled moisture-proof bags and returned to **exp's** Hamilton laboratory for additional visual, textual and olfactory examination, and sampling for laboratory testing.

1.3.2 Laboratory Testing

All samples returned to the laboratory were subjected to visual examination and classification. The laboratory testing program included the determination of natural moisture content, particle size distribution for approximately 25% of the collected soil samples. Atterberg Limits tests were carried out on select cohesive soil samples. Corrosivity package tests were performed on one soil sample. All the laboratory tests were carried out in accordance with MTO and/or ASTM standards as appropriate.

The laboratory test results are provided on the attached borehole log sheets in Appendix C. The results of the grain size analyses are presented graphically in Appendix D.

1.4 Subsurface Conditions

The detailed subsurface soil and groundwater conditions encountered in the boreholes advanced during this investigation, together with the results of the laboratory tests carried out on selected soil samples, are presented on the borehole log sheets in Appendix C. Laboratory test results are provided in Appendix D. The "Explanation of Terms Used in Report" preceding the borehole logs in Appendix C forms an integral part of and should be read in conjunction with this report.

A borehole location plan and stratigraphic section along the proposed salt storage structure are provided in Appendix B. It should be noted that the stratigraphic boundaries indicated on the borehole logs and stratigraphic section are inferred from non-continuous sampling, observations of drilling progress and results of Standard Penetration Tests. These boundaries typically represent transitions from one soil type to another and should not be regarded as exact planes of geological change. Further, subsurface conditions may vary between and beyond the borehole locations.

In general, the stratigraphic sequence at the proposed structure site consists of top granular fill, underlain by native silty clay deposits followed by bedrock. A summary of the soil and groundwater conditions encountered in the boreholes is provided below.

1.4.1 Topsoil

Topsoil was encountered at the surface of boreholes BH-1, BH-2 and BH-5 and ranged in thickness from approximately 0.2 m to 0.3 m. Topsoil thicknesses may further vary beyond the borehole locations.

1.4.2 Asphalt

Asphalt was encountered at the surface of boreholes BH-3 and BH-4 and ranged in thickness from approximately 0.1 m to 0.2 m. Asphalt thicknesses may further vary beyond the borehole locations.

1.4.3 Fill: Sand and Gravel

A sand and gravel fill layer was encountered below the layer of top soil or asphalt in all drilled boreholes except in BH-2. The thickness of this fill layer is between 0.2 m and 0.8 m extending from Elev. 210 m to 209.2 m.

This layer consists of sand and gravel with trace to some silt size particles. The material is dark grey and brown in color, and damp. The SPT “N” values within this layer ranged from 13 to 30 blows per 300 mm penetration, corresponding to compact compactness condition.

Laboratory testing performed on selected samples consisted of six (6) moisture content tests. The test results are as follows:

Moisture Content:

- 3% to 4%

The results of the moisture content tests are provided on the record of borehole sheets in Appendix C.

1.4.4 Fill: Clayey Silt

A clayey silt fill layer was encountered below the layer of sand and gravel fill in BH-4. The thickness of this fill layer is about 0.3 m extending from Elev. 209.6 m to 209.3 m. This layer consists of clay and silt with trace of sand and gravel. The material is dark brown in color, and moist.

1.4.5 Silty Clay

A layer of native silty clay was encountered below the fill/topsoil in all boreholes. The silty clay extended to depths ranging between 7.6 m to 8.0 m below the ground surface corresponding to elevations between 202.6 m and 202.4 m. The explored thickness of this layer was between 6.8 m and 7.4 m. BH-2 was terminated in this layer due to auger refusal on assumed bedrock.

The composition of this layer is silt and clay, and trace sand and gravel. The material is brown in color and moist above the 4.6 m depth, while below that depth it became grey in colour and very moist. The plasticity of this cohesive soil was measured to be low to high, but typically moderate. The SPT “N” values within this layer ranged from 6 to 100 blows per 0.3 m penetration, typically 8 to 21 blows per 0.3 m penetration, suggesting stiff to very stiff material in consistency. In addition, one (1) in-situ shear vane test was performed and field result was about 110 kPa.

Laboratory testing performed on selected sample consisted of thirty-one (31) moisture content tests, nine (9) grain size distribution tests and nine (9) Atterberg Limit tests. The test results are as follow:

Moisture Content:

- 16% to 34%

Grain Size Distribution:

- 0% to 4% gravel;
- 0% to 7% sand;
- 27% to % 77silt; and
- 22% to 72% clay

Atterberg limits

- Liquid Limit: 33% to 56%
- Plasticity Index: 15% to 38%

The results of the moisture content, gain size distribution and Atterberg Limit tests are provided on the record of borehole sheets in Appendix C. The result of the grain size distribution test and Atterberg Limit tests performed by exp are also provided on Figure 1,2,4 and 5, respectively, in Appendix D.

1.4.6 Sandy Silty Clay Till

A layer of native sandy silty clay till was encountered below the silty clay in BH-3, BH-4 and BH-5. The till extended to depths ranging between 7.7 m to 7.8 m below the ground surface with elevations ranging between 202.3 m to 202.4 m. The explored thickness of this layer was between 0.1 m and 0.2 m. BH-4 was terminated in this layer due to auger refusal on assumed bedrock.

The composition of this till layer is sand, silt and clay with some gravel. The material is grey in color, moist and low plasticity. The SPT "N" values within this layer were 100 blows per 0.3 m penetration, suggesting hard in consistency.

Laboratory testing performed on selected sample consisted of three (3) moisture content tests, one (1) grain size distribution test and one (1) Atterberg Limit test. The test results are as follow:

Moisture Content:

- 9% to 12%

Grain Size Distribution:

- 16% gravel;
- 24% sand;
- 33% silt; and
- 27% clay

Atterberg limits

- Liquid Limit: 27%
- Plasticity Index: 13%

The results of the moisture content, gain size distribution and Atterberg Limit tests are provided on the record of borehole sheets in Appendix C. The result of the grain size distribution test and Atterberg Limit tests performed by exp are also provided on Figure 3 and 6, respectively, in Appendix D.

1.4.7 Bedrock

The presence of bedrock was found to be approximately between 7.6 m to 8 m below the ground surface. The bedrock was inferred from split spoon refusal in BH-2 and BH-4, or confirmed using coring depth of 3.0 m in BH-1, BH-3 and BH-5. The elevation of the inferred or actual bedrock surface below this site ranges from Elev. 202.4 m to 202.6 m. The inferred or actual bedrock surface depth and elevation encountered at these borehole locations are listed in Table 1.1.

Based on the bedrock cores recovered, the bedrock consists of limestone. In general, the bedrock samples are described as grey in colour and fine grained with nodular appearance, weathered. The Rock Quality Designation (RQD) measured on the core samples typically ranged from approximately 37% to 85%, indicating a rock mass of poor to good quality. Photographs of rock cores are included in Appendix E.

Table 1.1 Depth and elevation of bedrock or possible bedrock surface

Borehole	Depth Below Ground Surface (m)	Elevation (m)	Comments
BH-1	8.0	202.4	Bedrock Cored
BH-2	7.6	202.5	Inferred/ Spoon Refusal
BH-3	7.7	202.3	Bedrock Cored
BH-4	7.7	202.4	Inferred/ Spoon Refusal
BH-5	7.8	202.4	Bedrock Cored

1.5 Groundwater Conditions

Information regarding groundwater levels at the site was obtained by measuring the water levels in the open boreholes upon completion of drilling. Backfilling of Borehole BH-1 was delayed in obtaining a supplemental groundwater level measurement. All boreholes remained dry upon completion of the drilling operations. The subsequent groundwater level reading obtained at BH-1 after a period of four hours following completion was 7.5 m below grade. The water levels are not considered to have stabilized during the short term of the investigation.

1.6 Chemical Analyses

One soil sample was selected for chemical analyses and was sent via courier, in a secure cooler under chain of custody, to AGAT Laboratories., a CALA-certified and accredited laboratory in Mississauga, Ontario. The analytical laboratory results are presented in Appendix D, and are summarized in Table 1.2, below.

Table 1.2. Corrosivity chemical analysis

Sample Identification	pH (unitless)	Soluble Chloride (ppm)	Soluble Sulphate (ppm)	Resistivity (ohm-cm)	Conductivity (mS/cm)
BH5-SS2 Silty Clay	8.9	41	129	2,440	0.409

2 CLOSURE

A subsurface investigation is a limited sampling of a site; the subsurface conditions have been established only at the test hole locations. Should conditions at the site be encountered which differ from those reported at the test locations, we require that we be notified immediately in order to assess this additional information and our recommendations, as appropriate. It may then be necessary to perform additional investigation and analysis.

Contractors bidding on or undertaking any proposed work at this site should, relative to the subsurface conditions, decide on their own investigations, if deemed necessary, as well as their own interpretations of the factual results provided herein, so they may draw their own conclusions as to how the subsurface conditions may affect them. .

This Foundation Investigation and Design Report has been prepared by Silvana Micic, Ph.D., P.Eng. and Nimesh Tamrakar, M.Eng. and reviewed by TaeChul Kim, M.E.Sc., P.Eng. and Stan E. Gonsalves, M.Eng., P.Eng., Designated MTO Foundation Contact. The field investigation was conducted by Dilsher Bhangal, M.Eng.

Yours truly,

exp Services Inc.



Nimesh Tamrakar, M.Eng.
Technical Specialist



Silvana Micic, Ph.D, P.Eng.
Senior Geotechnical Engineer



TaeChul Kim, M.E.Sc., P.Eng.
Senior Geotechnical/Foundation Engineer



Stan E. Gonsalves, M.Eng., P.Eng.
Principal Engineer
Designated MTO Foundation Contact



Encl.

Appendix A – Photographs



Photo 1: Jarvis Patrol Yard - the proposed new structure area, facing north



Photo 2: Jarvis Patrol Yard-existing Gambrel style shed, facing west



Photo 3: Jarvis Patrol Yard, facing south



Photo 4: Jarvis Patrol Yard, facing east



Photo 5: Facing north from location of BH-4 (Note the existing shed)



Photo 6: Facing west from location of BH-3

Appendix B – Drawings

HALDIMAND COUNTY W CONCESSION 7 WALPOLE

METRIC

DIMENSIONS ARE IN METERS AND/OR MILLIMETERS UNLESS OTHERWISE SHOWN. STATIONS ARE IN KILOMETERS + METERS

Agreement No. 3015-E-0017
Assignment No. 6
GWP 3075-16-00



NEW PATROL YARD STRUCTURE AT MTO JARVIS PATROL YARD, HALDIMAND COUNTY BOREHOLE LOCATION PLAN AND SOIL STRATA

SHEET

exp Services Inc.

KEY PLAN



LEGEND

- Borehole
- Standard Penetration Test (Blows/0.3 m)
- 73% Rock Quality Designation (RQD)
- Temporary Bench Mark (EL. 210.0m)

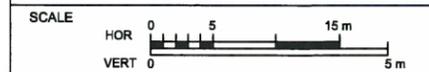
SOIL STRATA SYMBOLS

- ASPHALT
- GRANULAR FILL
- SILTY CLAY
- SANDY SILTY CLAY TILL
- BEDROCK

BH No.	APPROX. ELEV.	MTM CO-ORDINATES	
		NORTH	EAST
BH1	210.3	4748025.2	570948.8
BH2	210.1	4747996.7	570958.3
BH3	210.0	4748026.9	570957.4
BH4	210.1	4748015.6	570957.2
BH5	210.2	4747998.9	570965.3

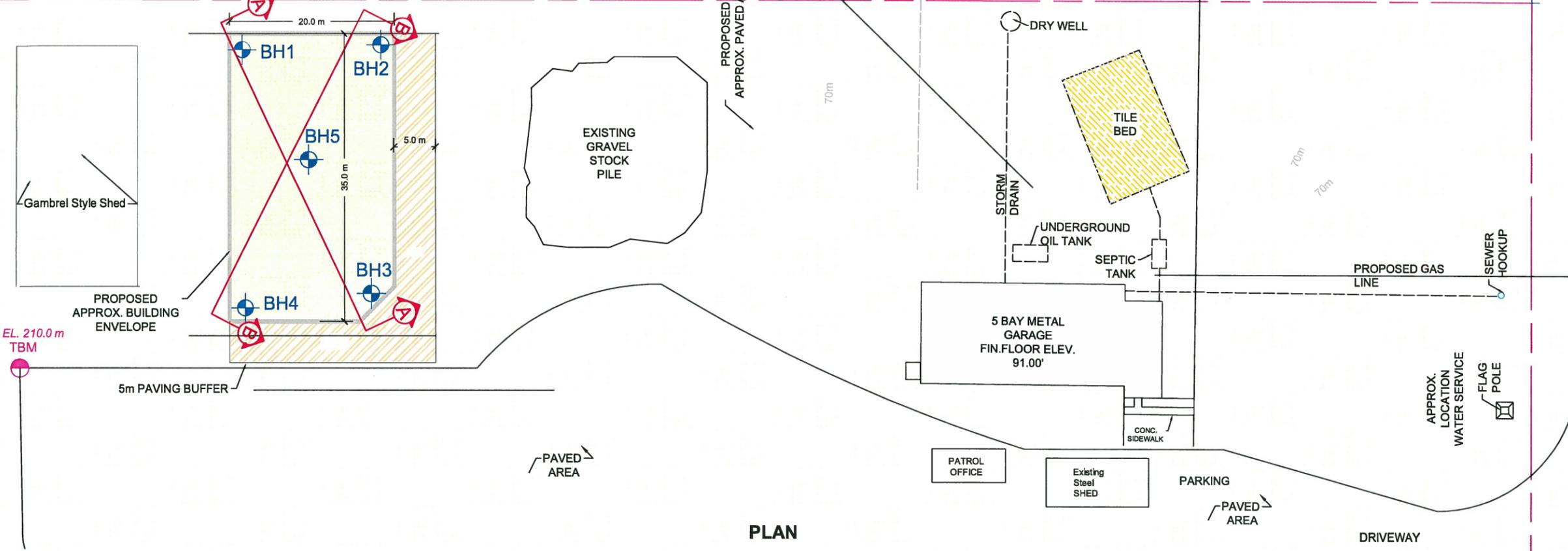
NOTE

This drawing is for subsurface information only. The proposed structure details/works are shown for illustration purposes only and may not be consistent with the final design configuration as shown elsewhere in the Contracts Documents.
The complete foundation investigation and design report for this project and other related documents may be examined at the Materials Engineering and Research Office, Downsview. Information contained in the report and related documents are specifically excluded in accordance with the conditions of Section GC 2.01 of OPS Gen. Cond.

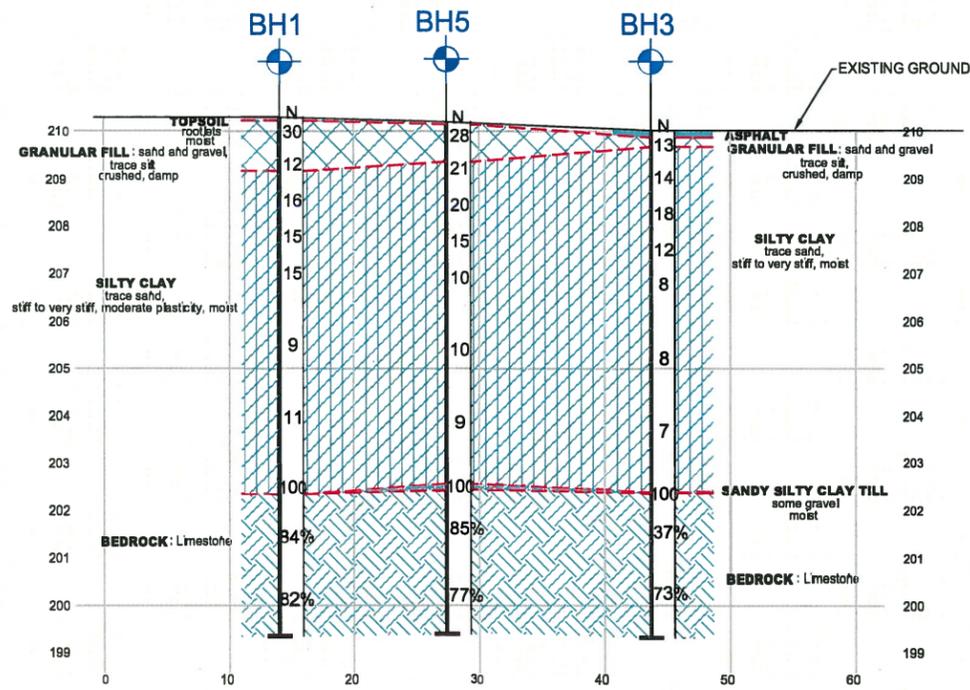


21/11/2017	-	SUBMISSION FOR MTO REVIEW
DATE	BY	DESCRIPTION
		GEOCRES NO. 4016-28
		PROJECT NO. ADM-00235197-J0
SUBMD SM	CHECKED SM	DATE
DRAWN SH	CHECKED SG	APPROVED SG
		21/11/2017
		DWG. 1

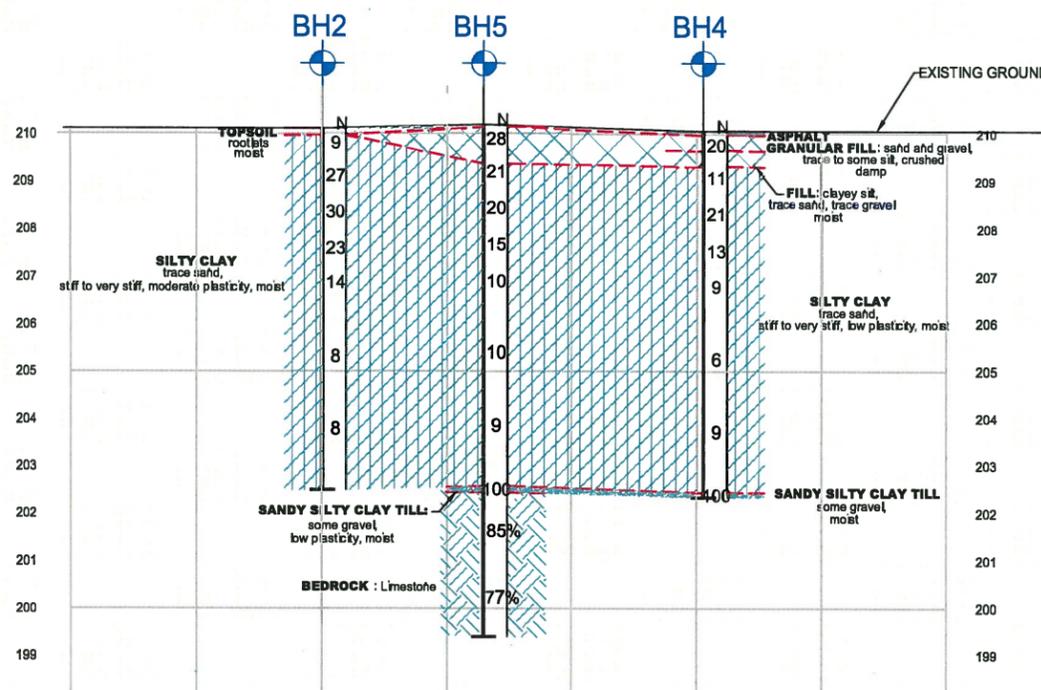
36' TO U/S OF ALL TRUSSES
5.0 M ASPHALT APRON ON EAST & SOUTH ELEVATIONS



PLAN



SECTION A-A



SECTION B-B



Appendix C – Borehole Logs

Explanation of Terms Used on Borehole Records

SOIL DESCRIPTION

Terminology describing common soil genesis:

Topsoil: mixture of soil and humus capable of supporting good vegetative growth.

Peat: fibrous fragments of visible and invisible decayed organic matter.

Fill: where fill is designated on the borehole log it is defined as indicated by the sample recovered during the boring process. The reader is cautioned that fills are heterogeneous in nature and variable in density or degree of compaction. The borehole description may therefore not be applicable as a general description of site fill materials. All fills should be expected to contain obstruction such as wood, large concrete pieces or subsurface basements, floors, tanks, etc.; none of these may have been encountered in the boreholes. Since boreholes cannot accurately define the contents of the fill, test pits are recommended to provide supplementary information. Despite the use of test pits, the heterogeneous nature of fill will leave some ambiguity as to the exact composition of the fill. Most fills contain pockets, seams, or layers of organically contaminated soil. This organic material can result in the generation of methane gas and/or significant ongoing and future settlements. Fill at this site may have been monitored for the presence of methane gas and, if so, the results are given on the borehole logs. The monitoring process does not indicate the volume of gas that can be potentially generated nor does it pinpoint the source of the gas. These readings are to advise of the presence of gas only, and a detailed study is recommended for sites where any explosive gas/methane is detected. Some fill material may be contaminated by toxic/hazardous waste that renders it unacceptable for deposition in any but designated land fill sites; unless specifically stated the fill on this site has not been tested for contaminants that may be considered toxic or hazardous. This testing and a potential hazard study can be undertaken if requested. In most residential/commercial areas undergoing reconstruction, buried oil tanks are common and are generally not detected in a conventional geotechnical site investigation.

Till: the term till on the borehole logs indicates that the material originates from a geological process associated with glaciation. Because of this geological process the till must be considered heterogeneous in composition and as such may contain pockets and/or seams of material such as sand, gravel, silt or clay. Till often contains cobbles (60 to 200 mm) or boulders (over 200 mm). Contractors may therefore encounter cobbles and boulders during excavation, even if they are not indicated by the borings. It should be appreciated that normal sampling equipment cannot differentiate the size or type of any obstruction. Because of the horizontal and vertical variability of till, the sample description may be applicable to a very limited zone; caution is therefore essential when dealing with sensitive excavations or dewatering programs in till materials.

Terminology describing soil structure:

Desiccated: having visible signs of weathering by oxidization of clay minerals, shrinkage cracks, etc.

Stratified: alternating layers of varying material or color with the layers greater than 6 mm thick.

Laminated: alternating layers of varying material or color with the layers less than 6 mm thick.

Fissured: material breaks along plane of fracture.

Varved: composed of regular alternating layers of silt and clay.

Slickensided: fracture planes appear polished or glossy, sometimes striated.

Blocky: cohesive soil that can be broken down into small angular lumps which resist further breakdown.

Lensed: inclusion of small pockets of different soil, such as small lenses of sand scattered through a mass of clay; not thickness.

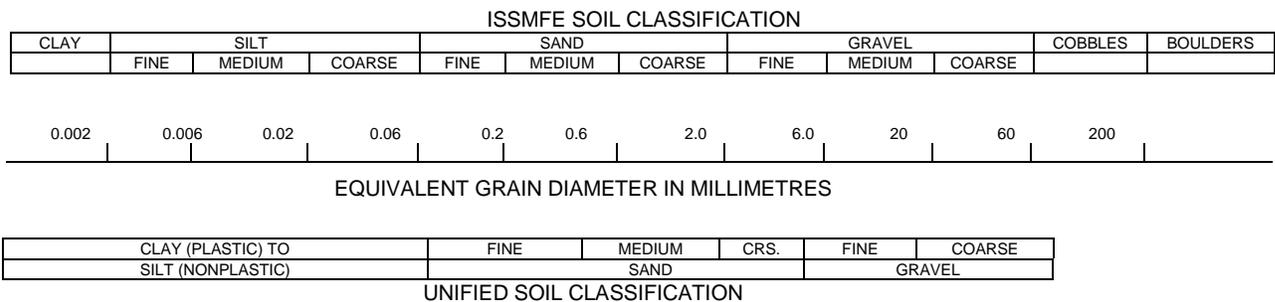
Seam: a thin, confined layer of soil having different particle size, texture, or color from materials above and below.

Homogeneous: same color and appearance throughout.

Well Graded: having wide range in grain sized and substantial amounts of all predominantly on grain size.

Uniformly Graded: predominantly on grain size.

All soil sample descriptions included in this report follow generally the ASTM D2487-11 Standard Practice for Classification of Soils for Engineering Purposes (Unified Soil Classification System) with some modification to reflect current MTO practices. The system divides soils into three major categories: (1) coarse grained, (2) fine-grained, and (3) highly organic. The soil is then subdivided based on either gradation or plasticity characteristics. The system provides a group symbol (e.g. SM) and group name (e.g. silty sand) for identification. The classification excludes particles larger than 76 mm. Please note that, with the exception of those samples where a grain size analysis has been made, all samples are classified visually in accordance with ASTM D2488-09a Standard Practice for Description and Identification of Soils (Visual-Manual Procedure). Visual classification is not sufficiently accurate to provide exact grain sizing or precise differentiation between size classification systems. Others may use different classification systems; one such system is the ISSMFE Soil Classification.



Terminology describing materials outside the USCS, (e.g. particles larger than 76 mm, visible organic matter, construction debris) is based upon the proportion of these materials present and as described below in accordance with Note 16 in ASTM D2488-09a:

Table a: Percent or Proportion of Soil, Pp

	Criteria
Trace	Particles are present but estimated to be less than 5%
Few	$5 \leq Pp \leq 10\%$
Little	$15 \leq Pp \leq 25\%$
Some	$30 \leq Pp \leq 45\%$
Mostly	$50 \leq Pp \leq 100\%$

The standard terminology to describe cohesionless soils includes the compactness as determined by the Standard Penetration Test 'N' value:

Table b: Apparent Density of Cohesionless Soil

	'N' Value (blows/0.3 m)
Very Loose	$N < 5$
Loose	$5 \leq N < 10$
Compact	$10 \leq N < 30$
Dense	$30 \leq N < 50$
Very Dense	$50 \leq N$

The standard terminology to describe cohesive soils includes consistency, which is based on undrained shear strength as measured by insitu vane tests, penetrometer tests, unconfined compression tests or similar field and laboratory analysis, Standard Penetration Test 'N' values can also be used to provide an approximate indication of the consistency and shear strength of fine grained, cohesive soils:

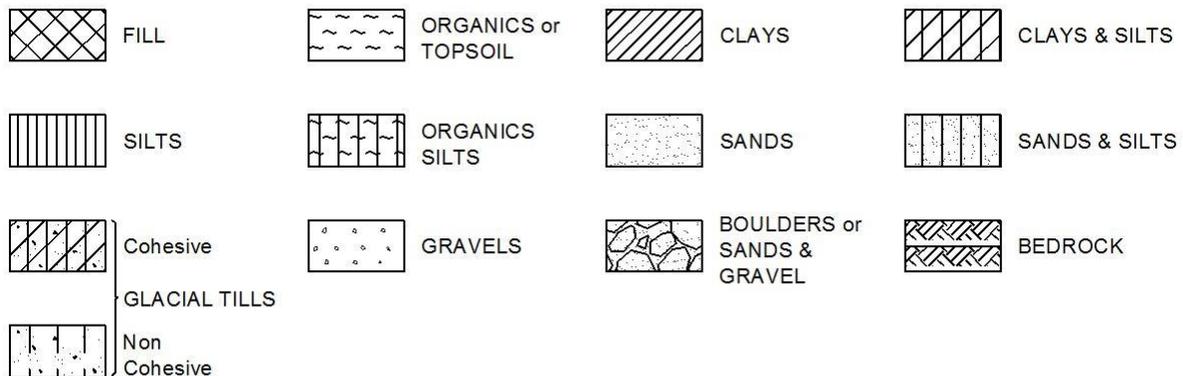
Table c: Consistency of Cohesive Soil

Consistency	Vane Shear Measurement (kPa)	'N' Value
Very Soft	<12.5	<2
Soft	12.5-25	2-4
Firm	25-50	4-8
Stiff	50-100	8-15
Very Stiff	100-200	15-30
Hard	>200	>30

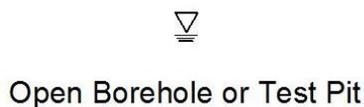
Note: 'N' Value - The Standard Penetration Test records the number of blows of a 140 pound (64kg) hammer falling 30 inches (760mm), required to drive a 2 inch (50.8mm) O.D. split spoon sampler 1 foot (305mm). For split spoon samples where full penetration is not achieved, the number of blows is reported over the sampler penetration in meters (e.g. 50/0.15).

STRATA PLOT

Strata plots symbolize the soil or bedrock description. They are combinations of the following basic symbols:



WATER LEVEL MEASUREMENT



ABBREVIATIONS AND SYMBOLS

FIELD SAMPLING

SS	Split spoon sample (obtained from the Standard Penetration Test)
WS	Wash sample
BS	Bulk sample
TW	Thin wall sample or Shelby tube
PS	Piston sample
AS	Auger sample
VT	Vane test
GS	Grab sample
HQ, NQ, etc.	Rock core samples obtained with the use of standard size diamond drilling bits

STRESS AND STRAIN

u_w	kPa	Pore water pressure
r_u	1	Pore pressure ratio
σ	kPa	Total normal stress
σ'	kPa	Effective normal stress
τ	kPa	Shear stress
$\sigma_1, \sigma_2, \sigma_3$	kPa	Principal stresses
ε	%	Linear strain
$\varepsilon_1, \varepsilon_2, \varepsilon_3$	%	Principal strains
E	kPa	Modulus of linear deformation
G	kPa	Modulus of shear deformation
μ	1	Coefficient of friction

MECHANICAL PROPERTIES OF SOIL

m_v	kPa^{-1}	Coefficient of volume change
c_c	1	Compression index
c_s	1	Swelling index
c_r	1	Recompression index
c_v	m^2/s	Coefficient of consolidation
H	m	Drainage path
T_v	1	Time factor
U	%	Degree of consolidation
σ'_{v0}	kPa	Effective overburden pressure
σ'_p	kPa	Preconsolidation pressure
τ_f	kPa	Shear strength
c'	kPa	Effective cohesion intercept
ϕ'	$-\circ$	Effective angle of internal friction
c_u	kPa	Apparent cohesion intercept
ϕ_u	$-\circ$	Apparent angle of internal friction
τ_R	kPa	Residual shear strength
τ_r	kPa	Remoulded shear strength
S_t	1	Sensitivity = c_u/τ_r

PHYSICAL PROPERTIES OF SOIL

P_s	kg/m^3	Density of solid particles
γ_s	kN/m^3	Unit weight of solid particles
ρ_w	kg/m^3	Density of water
γ_w	kN/m^3	Unit weight of water
ρ	kg/m^3	Density of soil
γ	kN/m^3	Unit weight of soil
ρ_d	kg/m^3	Density of dry soil
γ_d	kN/m^3	Unit weight of dry soil
ρ_{sat}	kg/m^3	Density of saturated soil
γ_{sat}	kN/m^3	Unit weight of saturated soil
ρ'	kg/m^3	Density of submerged soil
γ'	kN/m^3	Unit weight of submerged soil
e	1, %	Void ratio
n	1, %	Porosity
w	1, %	Water content
S_r	%	Degree of saturation
W_L	%	Liquid limit
W_P	%	Plastic limit
W_s	%	Shrinkage limit
I_P	%	Plasticity index = $(W_L - W_P)$
I_L	%	Liquidity index = $(W - W_P)/I_P$
I_C	%	Consistency index = $(W_L - W)/I_P$
e_{max}	1, %	Void ratio in loosest state
e_{min}	1, %	Void ratio in densest state
I_D	1	Density index = $(e_{max} - e)/(e_{max} - e_{min})$
D	mm	Grain diameter
D_n	mm	N percent - diameter
C_u	1	Uniformity coefficient
h	m	Hydraulic head or potential
q	m^3/s	Rate of discharge
v	m/s	Discharge velocity
i	1	Hydraulic gradient
k	m/s	Hydraulic conductivity
j	kN/m^3	Seepage force

Brampton, Ontario

RECORD OF BOREHOLE No BH-1

1 OF 1

METRIC

W.P. GWP 3075-16-00 LOCATION Old HWY 3, Jarvis, ON ORIGINATED BY DB
 DIST West HWY 3 BOREHOLE TYPE CME-55 Truck Mount, Continuous Flight Solid Stem Augers COMPILED BY JG
 DATUM Geodetic DATE 2017.08.23 - 2017.08.25 LATITUDE 42.881531 LONGITUDE -80.131222 CHECKED BY SM

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)					
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20						40	60	80	100	20
210.3	Ground Surface																	
210.4	TOPSOIL: brown, moist, rootlets GRANULAR FILL: sand and gravel, trace silt, grey, damp, crushed		1	SS	30													
209.2			2	SS	12													
1.1	SILTY CLAY: trace sand, brown, moist, stiff to very stiff, moderate plasticity		3	SS	16													0 1 56 43
	trace gravel, high plasticity below 3.1 m depth		4	SS	15													
			5	SS	15													4 7 37 52
	grey, very moist below below 4.6 m depth		6	SS	9													
			7	SS	11													
202.4	BEDROCK: limestone, grey RUN 1 (7.95 - 9.43 m): recovery 100%, RQD 84% (good) RUN 2 (9.43 - 10.95 m): recovery 100%, RQD 82% (good)		8	SS	100													
199.4	End of Borehole at 11.0 m. Notes: 1. This log is to be read with the subject report and project numbers as presented above. 2. Borehole remained dry upon completion of auger drilling. Four hours following completion, the groundwater level was measured at 7.5 m below grade. 3. Borehole open to 8.0 m below ground surface upon completion of auger drilling.																	

ONTARIO MTO ADM-00235197-J0 - SALT STORAGE DOME.GPJ ONTARIO MTO.GDT 20/9/17

+³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

RECORD OF BOREHOLE No BH-2

1 OF 1

METRIC

W.P. GWP 3075-16-00 LOCATION Old HWY 3, Jarvis, ON ORIGINATED BY DB
 DIST West HWY 3 BOREHOLE TYPE CME-55 Truck Mount, Continuous Flight Solid Stem Augers COMPILED BY JG
 DATUM Geodetic DATE 2017.08.23 - 2017.08.23 LATITUDE 42.881273 LONGITUDE -80.131108 CHECKED BY SM

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)			
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	SHEAR STRENGTH kPa									WATER CONTENT (%)		
						20	40	60	80	100	20	40	60		GR	SA	SI	CL	
210.1	Ground Surface																		
210.0	TOPSOIL: brown, moist, rootlets SILTY CLAY: brown, moist, stiff to very stiff, moderate plasticity		1	SS	9														
			2	SS	27														
			3	SS	30														
	trace sand at 2.3 m depth		4	SS	23											0	1	49	51
	grey below 3.1 m depth		5	SS	14														
			6	SS	8											0	0	27	72
	very moist, high plasticity below 4.6 m depth		7	SS	8														
202.5	End of Borehole at 7.6 m due to auger refusal on assumed bedrock. Notes: 1. This log is to be read with the subject report and project numbers as presented above. 2. Borehole remained dry upon completion of drilling. 3. Borehole open to 7.6 m below ground surface upon completion of drilling.																		

ONTARIO MTO ADM-00235197-J0 - SALT STORAGE DOME.GPJ ONTARIO MTO.GDT 20/09/17

+³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

Brampton, Ontario

RECORD OF BOREHOLE No BH-3

1 OF 1

METRIC

W.P. GWP 3075-16-00 LOCATION Old HWY 3, Jarvis, ON ORIGINATED BY DB
 DIST West HWY 3 BOREHOLE TYPE CME-55 Truck Mount, Continuous Flight Solid Stem Augers COMPILED BY JG
 DATUM Geodetic DATE 2017.08.23 - 2017.08.25 LATITUDE 42.881546 LONGITUDE -80.131116 CHECKED BY SM

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)		
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20	40	60	80						100	20
210.0	Ground Surface																	
209.0	ASPHALT (~150 mm thick)																	
209.2	GRANULAR FILL: sand and gravel, trace silt, grey, damp, crushed		1	SS	13													
0.4	SILTY CLAY: trace sand, brown, moist, stiff to very stiff		2	SS	14													
			3	SS	18													
			4	SS	12													
	very moist, high plasticity below 3.1 m depth		5	SS	8													0 1 41 58
			6	SS	8													
	grey below below 4.6 m depth																	
			7	SS	7													0 1 35 64
	firm below 6.1 m depth																	
202.4			8	SS	100													
202.6	SANDY SILTY CLAY TILL: some gravel, grey, moist																	
7.7	BEDROCK: limestone, grey																	
	RUN 1 (7.65 - 9.12 m): recovery 98%, RQD 37% (poor)																	
	RUN 2 (9.12 - 10.70 m): recovery 100%, RQD 73% (fair)																	
199.3																		
10.7	End of Borehole at 10.7 m.																	
	Notes: 1. This log is to be read with the subject report and project numbers as presented above. 2. Borehole remained dry upon completion of auger drilling. 3. Borehole open to 7.7 m below ground surface upon completion of auger drilling.																	

ONTARIO MTO ADM-00235197-J0 - SALT STORAGE DOME.GPJ ONTARIO MTO.GDT 20/09/17

+³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

Brampton, Ontario

RECORD OF BOREHOLE No BH-4

1 OF 1

METRIC

W.P. GWP 3075-16-00 LOCATION Old HWY 3, Jarvis, ON ORIGINATED BY DB
 DIST West HWY 3 BOREHOLE TYPE CME-55 Truck Mount, Continuous Flight Solid Stem Augers COMPILED BY JG
 DATUM Geodetic DATE 2017.08.23 - 2017.08.23 LATITUDE 42.881444 LONGITUDE -80.13112 CHECKED BY SM

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)			
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	SHEAR STRENGTH kPa									WATER CONTENT (%)		
						20	40	60	80	100	20	40	60		GR	SA	SI	CL	
210.1	Ground Surface																		
210.0	ASPHALT: (~90 mm thick)																		
209.6	GRANULAR FILL: sand and gravel, trace to some silt, dark grey and brown, damp, crushed		1	SS	20						o								
0.4																			
209.3	FILL: clayey silt, dark brown, moist, trace sand, trace gravel		2	SS	11														
0.8	SILTY CLAY: trace sand, brown, moist, stiff to very stiff, low plasticity																		
	very moist below 3.1 m depth		3	SS	21														0 1 77 22
			4	SS	13														0 1 54 45
			5	SS	9														
	occasional silt seam, very moist, grey below 4.6 m depth		6	SS	6														
			7	SS	9														
			8	SS	100														
202.4	SANDY SILTY CLAY TILL: some gravel, grey, moist																		
202.8	End of Borehole at 7.7 m due to auger refusal on assumed bedrock.																		
7.7																			
	Notes: 1. This log is to be read with the subject report and project numbers as presented above. 2. Borehole remained dry upon completion of drilling. 3. Borehole open to 7.7 m below ground surface upon completion drilling.																		

ONTARIO MTO ADM-00235197-J0 - SALT STORAGE DOME.GPJ ONTARIO MTO.GDT 20/09/17

+³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

Brampton, Ontario

RECORD OF BOREHOLE No BH-5

1 OF 1

METRIC

W.P. GWP 3075-16-00 LOCATION Old HWY 3, Jarvis, ON ORIGINATED BY DB
 DIST West HWY 3 BOREHOLE TYPE CME-55 Truck Mount, Continuous Flight Solid Stem Augers COMPILED BY JG
 DATUM Geodetic DATE 2017.08.23 - 2017.08.25 LATITUDE 42.881292 LONGITUDE -80.131023 CHECKED BY SM

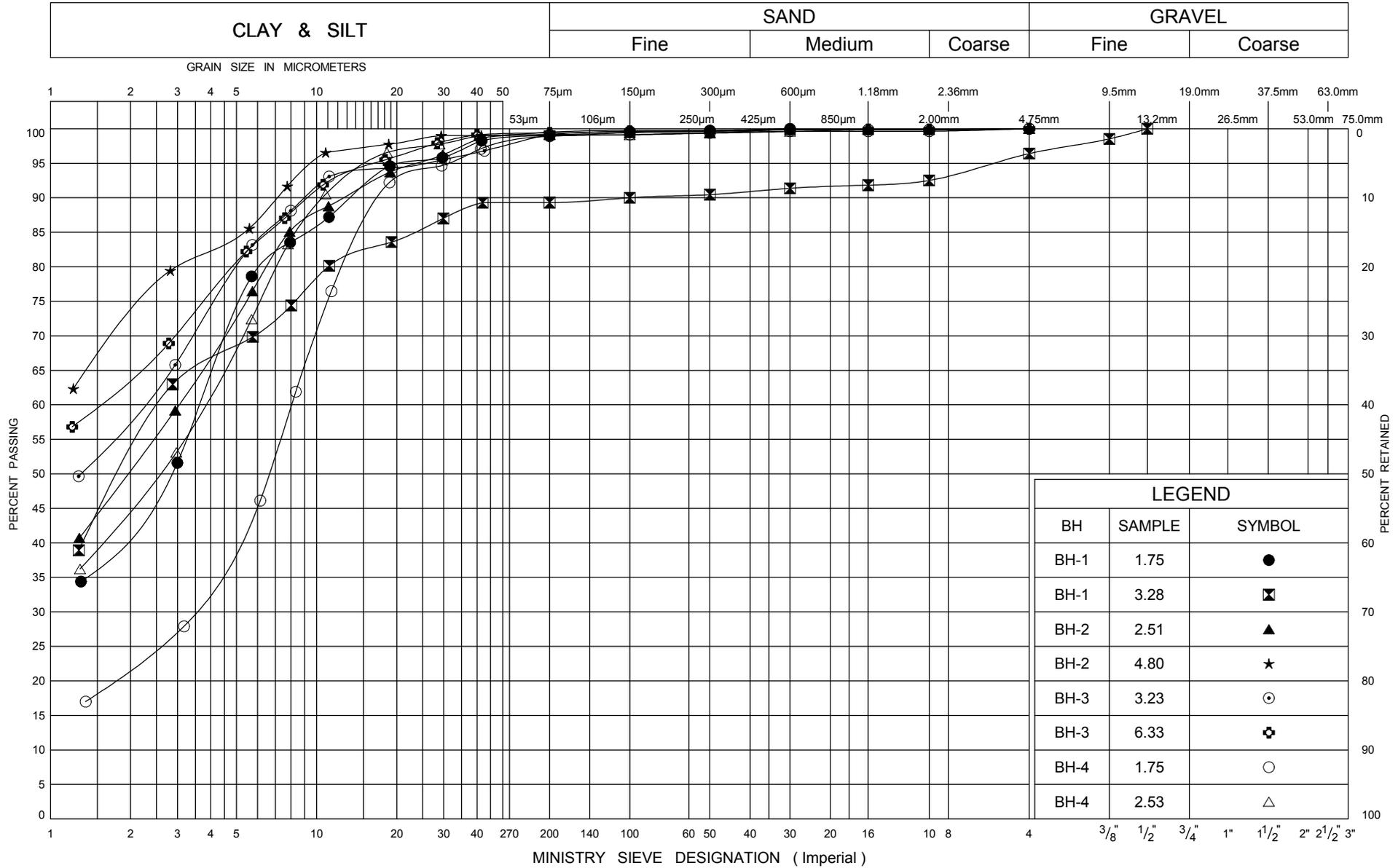
SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)							
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20						40	60	80	100	20	40	60
210.2	Ground Surface																			
210.4	TOPSOIL: brown, moist, rootlets GRANULAR FILL: sand and gravel, trace silt, grey, damp, crushed		1	SS	28															
209.4	SILTY CLAY: trace sand, trace gravel, brown, moist, stiff to very stiff, moderate plasticity grey, very moist below below 4.6 m depth		2	SS	21													1 1 40 58		
209.8			3	SS	20															
			4	SS	15															
			5	SS	10															
			6	SS	10															
202.6	SANDY SILTY CLAY TILL: some gravel, grey, moist, low plasticity BEDROCK: limestone, grey RUN 1 (7.75 - 9.27 m): recovery 100%, RQD 85% (good) RUN 2 (9.27 - 10.80 m): recovery 100%, RQD 77% (good)		7	SS	9															
202.8			8	SS	100														16 24 33 27	
199.4	End of Borehole at 10.8 m. Notes: 1. This log is to be read with the subject report and project numbers as presented above. 2. Borehole remained dry upon completion of auger drilling. 3. Borehole open to 7.8 m below ground surface upon completion of auger drilling.																			

ONTARIO MTO ADM-00235197-J0 - SALT STORAGE DOME.GPJ ONTARIO MTO.GDT 20/09/17

+³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

Appendix D – Laboratory Data

UNIFIED SOIL CLASSIFICATION SYSTEM



ONTARIO MOT GRAIN SIZE ADM-00235197-J0 - SALT STORAGE DOME.GPJ ONTARIO MOT.GDT 9/19/17



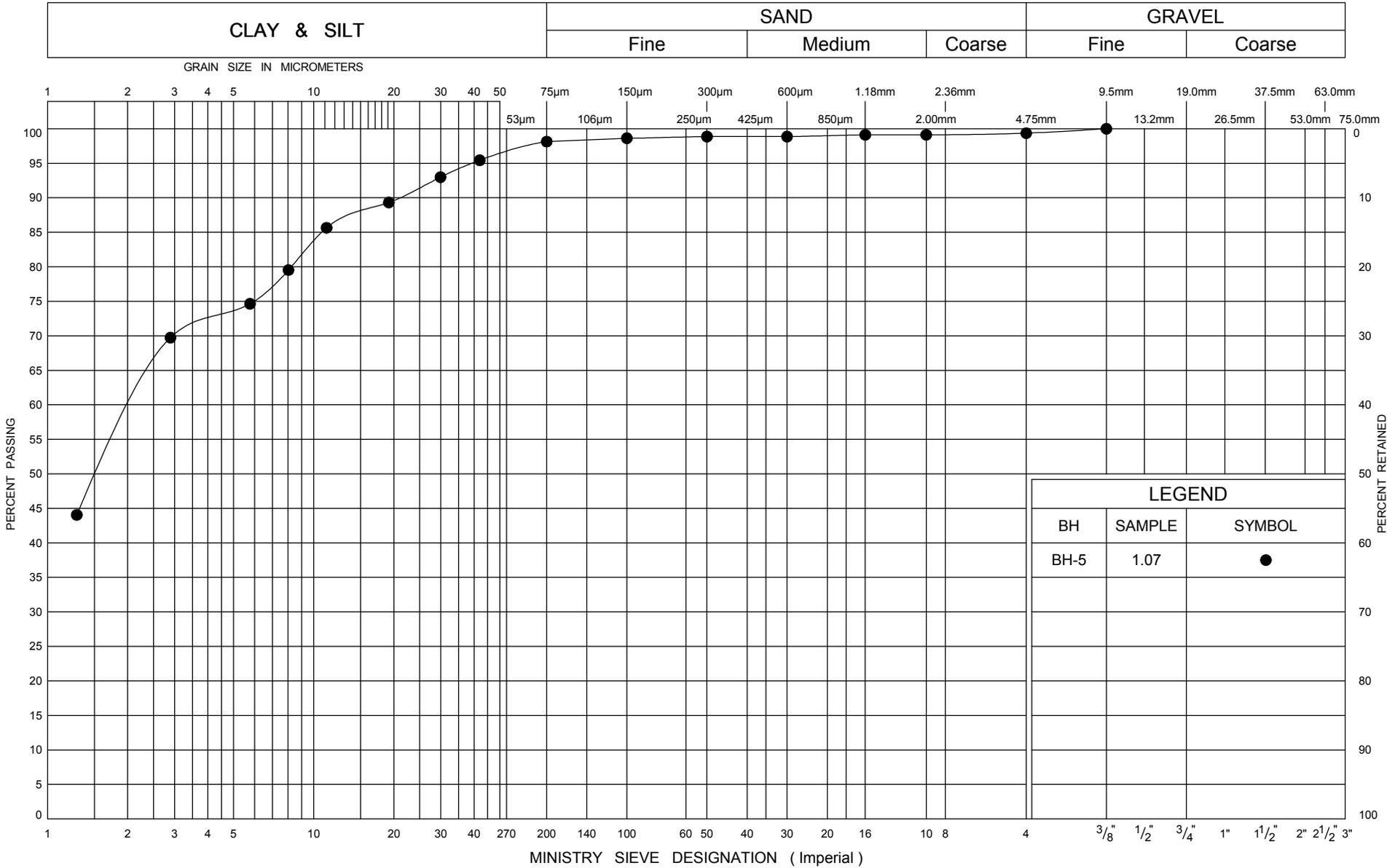
GRAIN SIZE DISTRIBUTION

FIG No 1

W P(GWP 3075-16-00)

3015-E-0017, Assignment 6

UNIFIED SOIL CLASSIFICATION SYSTEM



ONTARIO MOT GRAIN SIZE ADM-00235197-J0 - SALT STORAGE DOME.GPJ ONTARIO MOT.GDT 9/19/17



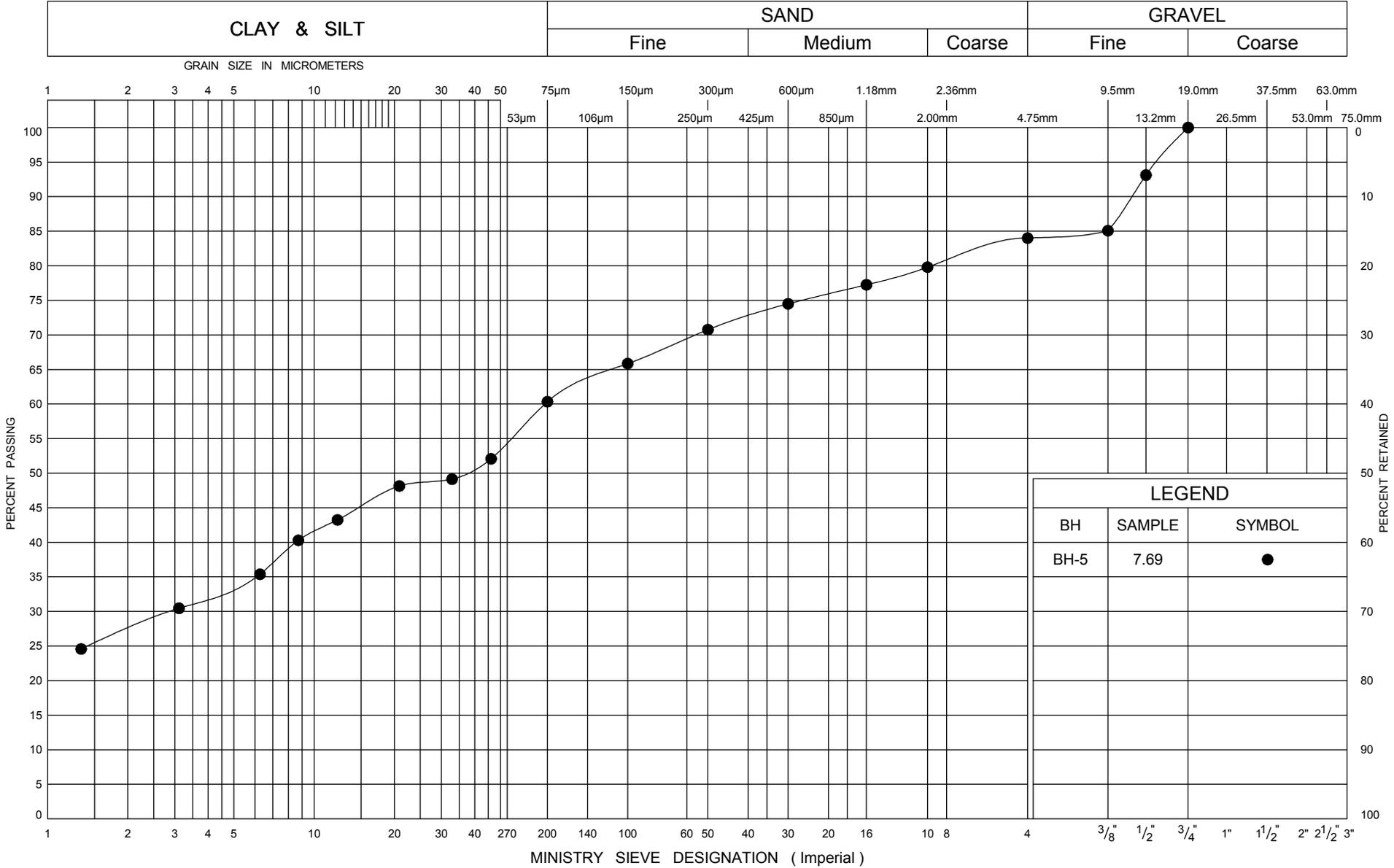
GRAIN SIZE DISTRIBUTION

FIG No 2

W P(GWP 3075-16-00)

3015-E-0017, Assignment 6

UNIFIED SOIL CLASSIFICATION SYSTEM



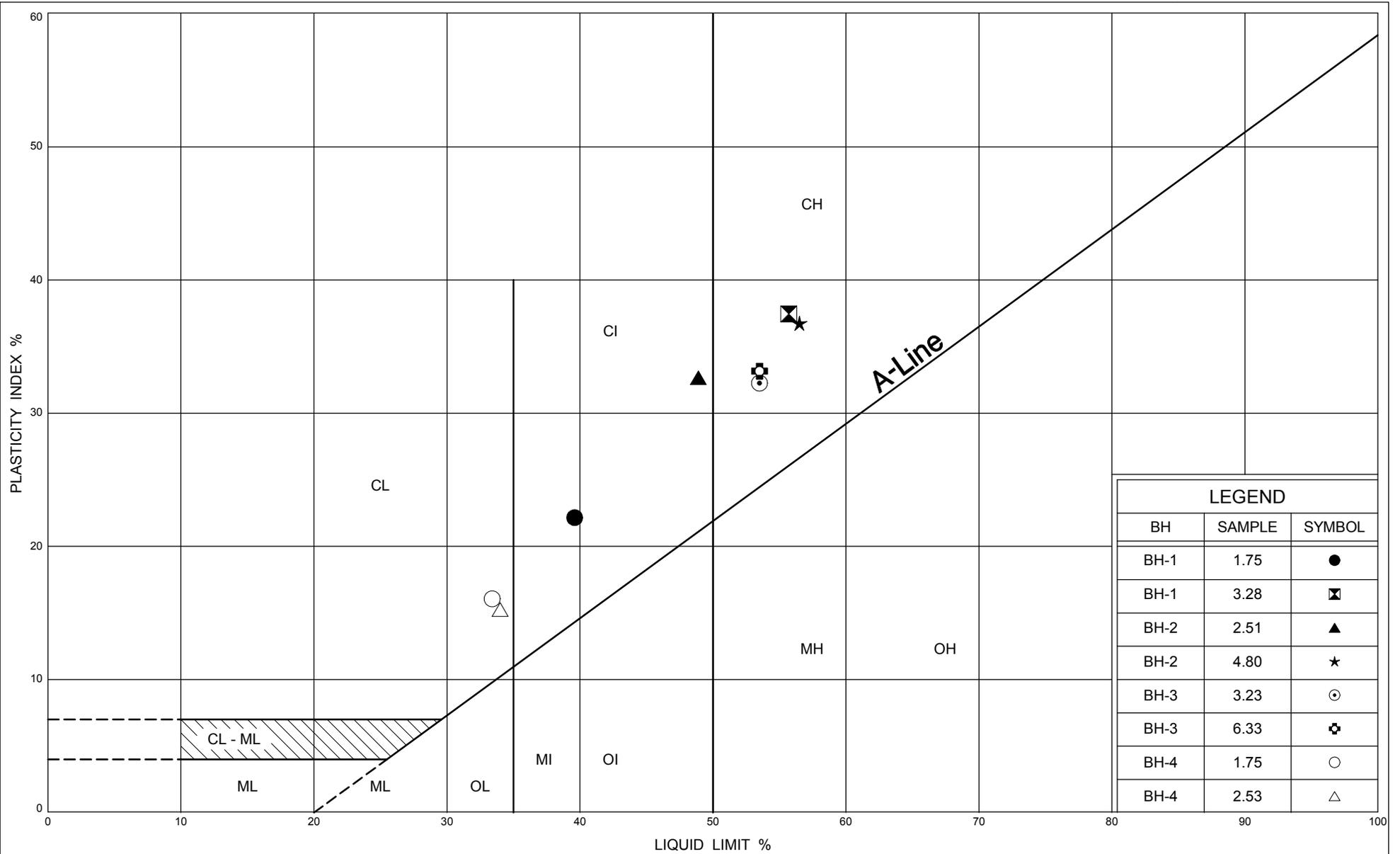
LEGEND		
BH	SAMPLE	SYMBOL
BH-5	7.69	●

ONTARIO MOT GRAIN SIZE ADM-00235197-J0 - SALT STORAGE DOME.GPJ ONTARIO MOT.GDT 9/19/17



GRAIN SIZE DISTRIBUTION

FIG No 3
 W P(GWP 3075-16-00)
 3015-E-0017, Assignment 6

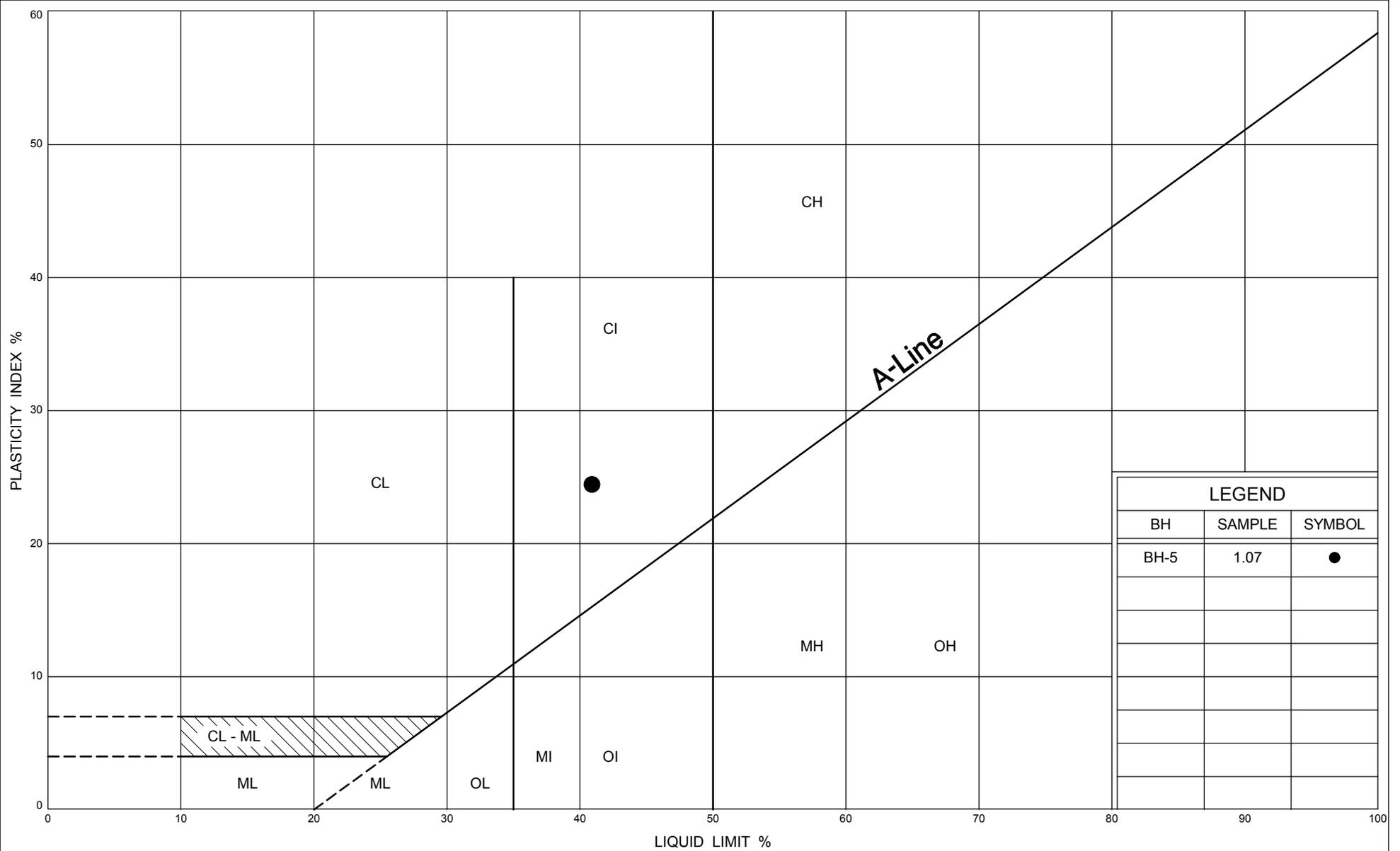


PLASTICITY CHART

FIG No 4

W P (GWP 3075-16-00)

3015-E-0017, Assignment 6

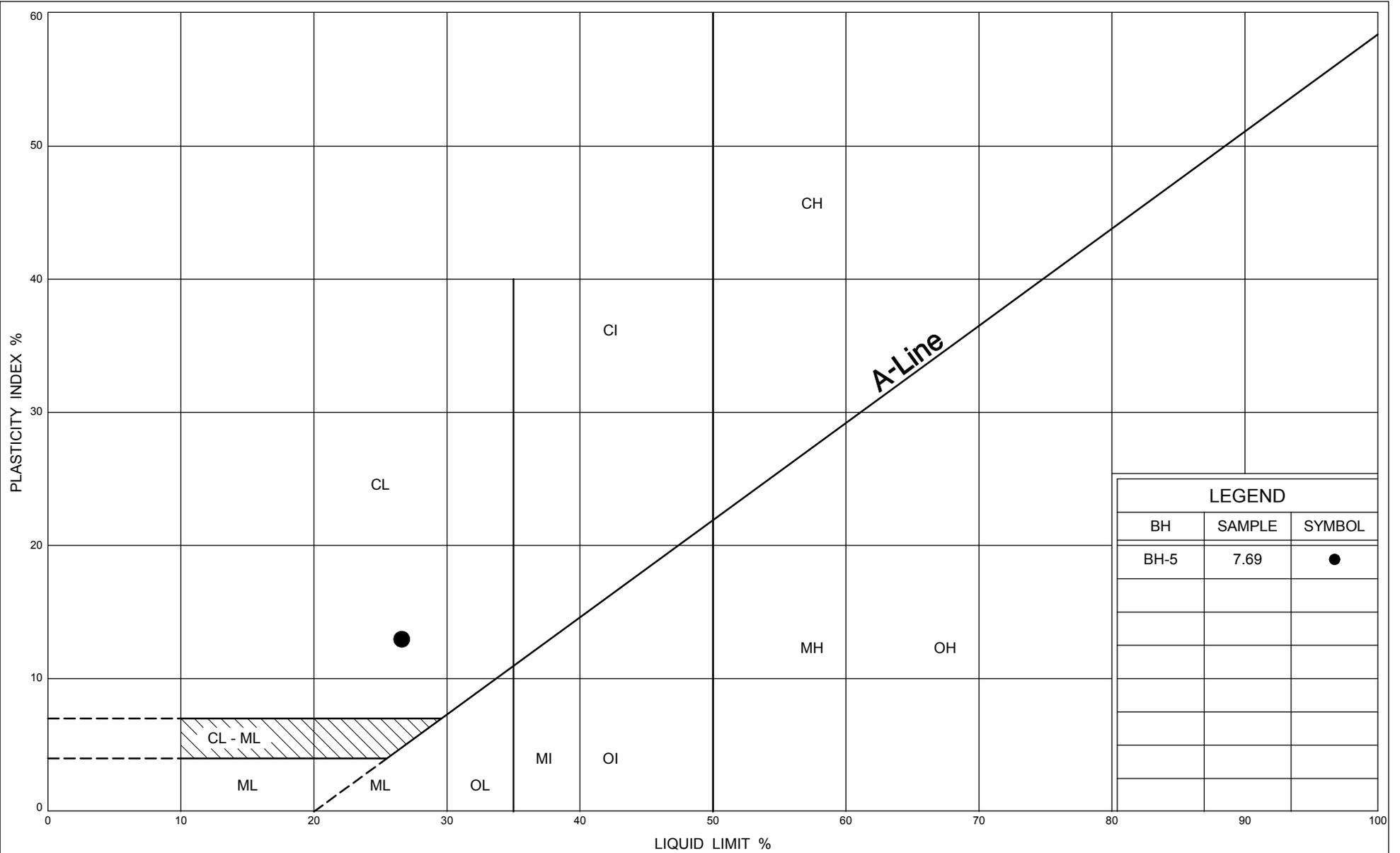


ONTARIO MOT PLASTICITY CHART ADM-00235197-J0 - SALT STORAGE DOME.GPJ ONTARIO MOT.GDT 9/19/17



PLASTICITY CHART

FIG No 5
 W P (GWP 3075-16-00)
 3015-E-0017, Assignment 6



LEGEND		
BH	SAMPLE	SYMBOL
BH-5	7.69	●

ONTARIO MOT PLASTICITY CHART ADM-00235197-J0 - SALT STORAGE DOME.GPJ ONTARIO MOT.GDT 9/19/17



PLASTICITY CHART

FIG No 6
 W P (GWP 3075-16-00)
 3015-E-0017, Assignment 6

**CLIENT NAME: EXP. SERVICES INC.
80 BANCROFT STREET
HAMILTON, ON L8E2W5
(905) 573-4000**

ATTENTION TO: Jeff Golder

PROJECT: Borehole Investigation

AGAT WORK ORDER: 17H254496

SOIL ANALYSIS REVIEWED BY: Amanjot Bhela, Inorganic Coordinator

DATE REPORTED: Sep 07, 2017

PAGES (INCLUDING COVER): 5

VERSION*: 1

Should you require any information regarding this analysis please contact your client services representative at (905) 712-5100

***NOTES**

All samples will be disposed of within 30 days following analysis. Please contact the lab if you require additional sample storage time.



Certificate of Analysis

AGAT WORK ORDER: 17H254496

PROJECT: Borehole Investigation

5835 COOPERS AVENUE
 MISSISSAUGA, ONTARIO
 CANADA L4Z 1Y2
 TEL (905)712-5100
 FAX (905)712-5122
<http://www.agatlabs.com>

CLIENT NAME: EXP. SERVICES INC.

ATTENTION TO: Jeff Golder

SAMPLING SITE:

SAMPLED BY:

Corrosivity Package

DATE RECEIVED: 2017-08-29

DATE REPORTED: 2017-09-07

SAMPLE DESCRIPTION: BH-5 SS2

SAMPLE TYPE: Soil

DATE SAMPLED: 2017-08-23

8676073

Parameter	Unit	G / S	RDL	8676073
Sulfide (S2-)	%		0.05	<0.05
Chloride (2:1)	µg/g		2	41
Sulphate (2:1)	µg/g		2	129
pH (2:1)	pH Units		NA	8.90
Electrical Conductivity (2:1)	mS/cm		0.005	0.409
Resistivity (2:1)	ohm.cm		1	2440

Comments: RDL - Reported Detection Limit; G / S - Guideline / Standard

8676073 EC, pH, Chloride, Sulphate and Redox Potential were determined on the extract obtained from the 2:1 leaching procedure (2 parts DI water: 1 part soil).

*Sulphide analyzed at AGAT 5623 McAdam

Certified By:

Amanjot Bhela

Quality Assurance

CLIENT NAME: EXP. SERVICES INC.
PROJECT: Borehole Investigation
SAMPLING SITE:

AGAT WORK ORDER: 17H254496
ATTENTION TO: Jeff Golder
SAMPLED BY:

Soil Analysis															
RPT Date: Sep 07, 2017			DUPLICATE				Method Blank	REFERENCE MATERIAL			METHOD BLANK SPIKE		MATRIX SPIKE		
PARAMETER	Batch	Sample Id	Dup #1	Dup #2	RPD	Measured Value		Acceptable Limits		Recovery	Acceptable Limits		Recovery	Acceptable Limits	
								Lower	Upper		Lower	Upper		Lower	Upper

Corrosivity Package

Sulfide (S2-)	8676073	8676073	< 0.05	< 0.05	NA	< 0.05	97%	80%	120%	NA			NA		
Chloride (2:1)	8676073	8676073	41	44	7.1%	< 2	97%	80%	120%	98%	80%	120%	102%	70%	130%
Sulphate (2:1)	8676073	8676073	129	139	7.5%	< 2	94%	80%	120%	97%	80%	120%	99%	70%	130%
pH (2:1)	8676073	8676073	8.90	8.93	0.3%	NA	101%	90%	110%	NA			NA		
Electrical Conductivity (2:1)	8676073	8676073	0.409	0.427	4.3%	< 0.005	95%	90%	110%	NA			NA		

Comments: NA signifies Not Applicable.

Duplicate Qualifier: As the measured result approaches the RL, the uncertainty associated with the value increases dramatically, thus duplicate acceptance limits apply only where the average of the two duplicates is greater than five times the RL.

Certified By:

Amanjot Bhela



Method Summary

CLIENT NAME: EXP. SERVICES INC.

AGAT WORK ORDER: 17H254496

PROJECT: Borehole Investigation

ATTENTION TO: Jeff Golder

SAMPLING SITE:

SAMPLED BY:

PARAMETER	AGAT S.O.P	LITERATURE REFERENCE	ANALYTICAL TECHNIQUE
Soil Analysis			
Sulfide (S ²⁻)	MIN-200-12025	ASTM E1915-09	GRAVIMETRIC
Chloride (2:1)	INOR-93-6004	McKeague 4.12 & SM 4110 B	ION CHROMATOGRAPH
Sulphate (2:1)	INOR-93-6004	McKeague 4.12 & SM 4110 B	ION CHROMATOGRAPH
pH (2:1)	INOR 93-6031	MSA part 3 & SM 4500-H+ B	PH METER
Electrical Conductivity (2:1)	INOR-93-6036	McKeague 4.12, SM 2510 B	EC METER
Resistivity (2:1)	INOR-93-6036	McKeague 4.12, SM 2510 B,SSA #5 Part 3	CALCULATION

Appendix E – Rock Core Photographs

Project No: ADM 00235197-J0
BH No: 1 Run No: 1 & 2
Sample Depth: 8.0 m to 11.0 m
Elevation: 202.4 m to 199.4 m
Description: Limestone
Date: August 23 to 25, 2017



Figure E1. Rock cores from BH-1

Project No: ADM 00235197-J0
BH No: 3 Run No: 1 & 2
Sample Depth: 7.7 m to 10.7 m
Elevation: 202.3 m to 199.3 m
Description: Limestone
Date: August 23 to 25, 2017



Figure E2. Rock cores from BH-3

Project No: ADM 00235197-J0
BH No: 5 Run No: 1 & 2
Sample Depth: 7.8 m to 10.8 m
Elevation: 202.4 m to 199.4 m
Description: Limestone
Date: August 23 to 25, 2017



Figure E3. Rock cores from BH-5