



## FOUNDATION INVESTIGATION REPORT

*Temporary East Access Road, East of the Credit River, QEW Widening from West of Mississauga Road to West of Hurontario Street, City of Mississauga  
Ministry of Transportation, Ontario, G.W.P. 2002-13-00*

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## 1.0 INTRODUCTION

Golder Associates Ltd. (Golder) has been retained by Morrison Hershfield Limited (MH) on behalf of the Ministry of Transportation, Ontario (MTO) to provide foundation engineering services in support of the detail design for the widening of the Queen Elizabeth Way (QEW) from west of Mississauga Road to west of Hurontario Street in the City of Mississauga, in the Regional Municipality of Peel, Ontario.

The purpose of this investigation is to establish the subsurface soil, bedrock and groundwater conditions at the location of the proposed temporary East Access Road for the construction of the proposed twinning of the Credit River bridge, by borehole drilling and laboratory testing on selected soil and bedrock core samples.

The Terms of Reference (TOR) and the scope of work for the foundation investigation are outlined in MTO's Request for Proposal, dated July 2016, and the approved Change Request letters, which forms part of the Consultant's Assignment Number (Number 2015-E-0033) for this project. The work has been carried out in accordance with Golder's Supplementary Specialty Plan for foundation engineering services for this project, dated February 3, 2017.

## 2.0 SITE DESCRIPTION

Based on a preliminary design drawing provided by MH on July 26, 2018, the alignment of the temporary East Access Road will be situated north of the proposed footprint for the twinning of the Credit River bridge (west bound), and extend from Stavebank Road to the east limit of the proposed East Pier (see Drawing 1), adjacent to the Credit River. The current ground surface along the proposed East Access Road is covered with vegetation and trees. In most of the proposed access road footprint, the existing ground surface is covered with sparse vegetation, wood chips and stumps resulting from advanced tree clearing operations in preparation for the widening of the QEW and associated structures. A marsh/swampy area, adjacent to the Credit River, is located directly northwest of west limit of the temporary East Access Road. There are currently buried oil pipelines (Trans-Northern Pipeline) and high voltage electrical transmission overhead lines directly within / across the footprint of the proposed East Access Road and the utilities are to be relocated prior to construction of the access road.

Overall, the existing ground surface on the tableland in the area of the proposed temporary East Access Road gradually slopes down to the crest of the river bank at an inclination ranging from about 5 horizontal to 1 vertical (5H:1V) to 10H:1V, from about Elevation 97 m west of Stavebank Road to about Elevation 88 m at the valley crest. The valley from the tableland to the edge of the river slopes steeply at an inclination of about 1.4H:1V to 3H:1V down to about Elevation 76 m on edge of the East Bank. The Credit River water level was measured to be about Elevation 75 m (September 1986). There is currently a low-lying area situated within the tableland, just north of the proposed East Access Road, which naturally drains down to the river along the western portion of the current East Access Road alignment. According to the design drawings provided by MH, a proposed new Stormwater Management Pond (SWMP) will eventually be located within the footprint of the temporary East Access Road and current low-lying area, and the temporary access road and surrounding topography will be modified to meet the final design grade for the permanent SWMP and associated features.

## 3.0 INVESTIGATION PROCEDURES

Field work for the foundation investigation was carried out between October 2017 and July 2018, during which time a total of 10 relevant boreholes were carried out as part of the project as follows:

- Boreholes AR-1 and AR-2, advanced on July 30, 2018 as close as possible to the temporary East Access Road alignment taking into consideration access restrictions and requirement for holes to be a minimum 10 m away from the buried oil pipelines owned by Trans-Northern Pipeline Inc. (TNPI).

- Boreholes CRB-4, CRB-5A and CRB-5, advanced between February 13 and 18, 2018 at the east pier for the Credit River bridge and associated east access road;
- Boreholes CRB-6 and CRB-7, advanced between October 17 to 23, 2017 at the east abutment, east access road and east approach for the Credit River bridge;
- Boreholes SWME-1, SWME-3 and SWME-4, which were advanced on July 27 and 31, 2018 for the SWM Dry Pond and east access road.

The locations of the relevant boreholes are shown on Drawing 1. Additional boreholes near the proposed East Access Road that were completed for other foundation components of the QEW bridge widening project are also shown on the drawing for reference only.

The borehole investigation was carried out using track-mounted CME 75 drill rig, supplied and operated by Davis Drilling Ltd. of Milton, Ontario, a CME 55 drill rig supplied and operated by Geo-Environmental Drilling Ltd. of Milton, Ontario and a CME 850 drill rig supplied and operated by Aardvark Drilling Inc. of Guelph, Ontario. The boreholes were advanced using 160 mm to 210 mm outside diameter hollow-stem augers through the overburden, and HW casing and an HQ size core barrel through the bedrock. Soil and/or bedrock samples were typically obtained at 0.75 m and 1.5 m intervals of depth, using a 50 mm outer diameter split-spoon sampler driven by an automatic hammer in accordance with Standard Penetration Test (SPT) procedures (ASTM D1586-08)<sup>1</sup>.

Boreholes were advanced through the overburden and/or bedrock to depths ranging from 5.4 m to 17.2 m below existing ground surface. Bedrock was confirmed by coring for lengths between 3.3 m and 9.5 m in Boreholes AR-2, SWME-4, CRB-4, CRB-5, CRB-5A, CRB-6 and CRB-7.

The groundwater conditions and water levels in the open boreholes were observed during and immediately following drilling operations. A standpipe piezometer was installed in Boreholes SWME-3, CRB-5A and CRB-6 to permit monitoring of the groundwater level at the borehole locations. The standpipe piezometers consist of 50 mm diameter PVC pipe, with a slotted screen within a sand filter pack sealed within the overburden / bedrock interface or upper portion of the bedrock. Above the sand filter pack and piezometer screen, the annulus surrounding the piezometer pipe was backfilled to about 0.5 m below the ground surface with bentonite pellets and finished to ground surface with concrete to set in the protective casing for the standpipe piezometer. All remaining boreholes were backfilled to ground surface with bentonite upon completion, in accordance with Ontario Regulation 903 (as amended).

The field work was observed by members of Golder's engineering and technical staff, who located the boreholes, arranged for the clearance of underground services, observed the drilling, sampling and in-situ testing operations, logged the boreholes and examined the soil and bedrock samples. The samples were identified in the field, placed in appropriate containers, labelled and transported to Golder's Mississauga geotechnical laboratory where the samples underwent further visual examination and laboratory testing. All of the laboratory tests were carried out to MTO and/or ASTM Standards, as appropriate. Classification testing (water content, Atterberg limits and grain size distribution) was carried out on selected soil samples. Uniaxial compression (UC) strength tests (including core bulk density and Young's Modulus determination) were carried out on selected specimens of the bedrock core samples by Geomechanica Inc. on behalf of Golder.

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<sup>1</sup> ASTM D1586-08a – Standard Test Method for Standard Penetration Tests and Split Barrel Sampling of the soil.

The as-drilled borehole locations and the ground surface elevations were obtained using a GPS (Trimble Geo 7X), having an accuracy of 0.1 m in both the vertical and horizontal directions. The locations given on the Record of Borehole/Drillhole sheets and shown on Drawing 1 are positioned relative to MTM NAD 83 (Zone 10) northing and easting coordinates and the ground surface elevations are referenced to Geodetic datum. The borehole locations, ground surface elevations and drilled depths are summarized below.

Borehole No.	Location (MTM NAD 83)		Ground Surface Elevation (m)	Borehole Depth (m)
	Northing (m) (Latitude, °)	Easting (m) (Longitude, °)		
AR-1	4,824,236.4 (43.558012)	295,944.3 (-79.609616)	95.7	9.2
AR-2	4,824,172.2 (43.557434)	295,921.4 (-79.609899)	88.4	11.6 (including 7.0 m bedrock core)
CRB-4	4,824,135.1 (43.557099)	295,902.0 (-79.610138)	79.1	15.3 (including 8.1 m bedrock core)
CRB-5	4,824,128.9 (43.557044)	295,914.2 (-79.609986)	79.2	15.5 (including 8.3 m bedrock core)
CRB-5A	4,824,130.9 (43.557062)	295,910.6 (-79.610032)	79.3	17.2 (including 9.5 m bedrock core)
CRB-6	4,824,196.7 (43.557650)	295,929.5 (-79.609801)	91.7	13.3 (including 8.2 m bedrock core)
CRB-7	4,824,189.6 (43.557590)	295,951.1 (-79.609531)	94.7	16.0 (including 7.5 m bedrock core)
SWME-1	4,824,195.5 (43.557643)	295,896.6 (-79.610206)	89.5	5.5
SWME-3	4,824,227.3 (43.557930)	295,901.0 (-79.610152)	91.9	5.4
SWME-4	4,824,255.4 (43.558183)	295,917.6 (-79.609946)	95.5	13.3 (including 3.3 m of bedrock core)

## 4.0 SITE GEOLOGY AND SUBSURFACE CONDITIONS

### 4.1 Regional Geology

The project area is located within the Iroquois Plain physiographic region, as delineated in *The Physiography of Southern Ontario* (Chapman and Putman, 1984)<sup>2</sup>.

<sup>2</sup> Chapman, L.J. and Putman, D.F., 1984, *The Physiography of Southern Ontario*, Ontario Geological Society, Special Volume 2, Third Edition. Accompanied by Map p. 2715, Scale 1:600,000.)

The glacial Iroquois Plain stretches along the northern shoreline of Lake Ontario, extending from the Niagara Escarpment in the west to the Scarborough Bluffs in the east. The Iroquois Plain soils consist of glaciolacustrine sediments deposited in Lake Iroquois, primarily sands, silts and gravels, with a shallow cover of till remaining over the bedrock.

The bedrock of the Georgian Bay Formation that underlies the study area consists mainly of blue-grey shale, containing siltstone, sandstone and limestone interbeds. Outcrops of this formation are commonly found along water courses on the west side of Toronto and in Mississauga, notably in the Humber River, Mimico Creek, Etobicoke Creek and Credit River valleys.

## 4.2 Subsurface Conditions

The detailed subsurface soil, bedrock and groundwater conditions as encountered in the boreholes, the piezometer installation details and water level readings and the results of the laboratory tests carried out on selected soil and bedrock core samples are presented on the Records of Boreholes and Drillholes provided in Appendix A. Photographs of the recovered bedrock core samples are presented on Figures A-1 to A-8 in Appendix A. The results of the in-situ field tests (i.e. SPT "N"-values) as presented on the borehole records and in Section 4.2 are uncorrected. Lists of abbreviations and symbols and lithological and geotechnical rock description terminology are also included in Appendix A to assist in the interpretation of the borehole and drillhole records. The detail results of the geotechnical laboratory testing on soil and bedrock core samples obtained during the investigation are presented in Appendix B.

The stratigraphic boundaries shown on the borehole records and the stratigraphic profile on Drawing 1 are inferred from non-continuous sampling, observations of drilling progress and the results of Standard Penetration Tests. These boundaries, therefore, represent transitions between soil types and soil/bedrock rather than exact planes of geological change. Furthermore, subsurface conditions will vary between and beyond the borehole locations; however, the factual data presented in the borehole and drillhole records govern any interpretation of the site conditions. It should be noted that the interpreted stratigraphy shown on Drawing 1 is a simplification of the subsurface conditions.

In general, the subsurface conditions in the area of the proposed temporary East Access Road consist of a layer of topsoil, underlain by fill comprising of sandy silt to silty sand, sand and clayey silt. The fill is underlain by deposits of silt, sandy silt to sand, clayey silt with sand to silty clay and organic clay which is further underlain by a till deposit and residual soil. The native soil deposits are underlain by shale bedrock. A more detailed description of the subsurface conditions encountered in the boreholes is provided in the following sections.

### 4.2.1 Topsoil

A layer of topsoil ranging in thickness from about 180 mm to 700 mm was encountered at the ground surface in Boreholes AR-1, AR-2, CRB-7 and SWME-4. SPT "N"-values measured within the topsoil layer range between 3 blows and 9 blows per 0.3 m of penetration, suggesting a soft to stiff consistency.

### 4.2.2 Fill

A 0.3 m to 4.3 m thick layer of fill consisting of clayey silt with sand / sandy silt to silty sand / sand and gravel was encountered from ground surface in Boreholes SWME-1, SWME-3, CRB-4, CRB-5, CRB-5A and CRB-6, and underlying the topsoil in Boreholes SWME-4, AR-1 and CRB-7. The fill was described as containing variable amounts of organics, brick fragments, and shale and limestone fragments. The depth and elevation of the top and

base of the fill layer, the thickness and the predominant fill type at each borehole location (from east to west) is presented below:

Borehole No.	Top of Layer		Bottom of Layer		Thickness (m)	Fill Type
	Depth (m)	Elevation (m)	Depth (m)	Elevation (m)		
SWME-4	0.2	95.3	0.7	94.8	0.5	Silt and Sand
AR-1	0.7	95.0	1.4	94.3	0.7	Sand
SWME-3	0.0	91.9	1.7	90.2	1.7	Sandy Silt to Silty Sand
CRB-6	0.0	91.7	1.7	90.0	1.7	Silty Sand
CRB-7	0.2	94.5	4.5	90.2	4.3	Silt and Sand
SWME-1	0.0	89.5	0.7	88.8	0.7	Sand and Gravel
	0.7	88.8	1.4	88.1	0.7	Silt and Sand
	1.4	88.1	1.7	87.8	0.3	Clayey Silt
CRB-4	0.0	79.1	3.7	75.4	3.7	Clayey Silt with Sand
CRB-5	0.0	79.2	0.7	78.5	0.7	Silty Sand
	0.7	78.5	2.4	76.8	1.7	Clayey Silt with Sand
CRB-5A	0.0	79.3	4.0	75.3	4.0	Clayey Silt with Sand

SPT “N”-values measured within the non-cohesive fill layers range between 4 blows and 21 blows per 0.3 m of penetration, suggesting a loose to compact state of compactness. One SPT “N”-value of 54 blows per 0.3 m of penetration was recorded in Borehole CRB-7 near the base of the fill and the value is likely attributed to the brick fragments that were present within the split-spoon sampler. SPT “N”-values measured within the cohesive fill layers range between 6 blows and 31 blows per 0.3 m of penetration, suggesting a firm to hard consistency.

The results of grain size distribution tests completed on three selected samples of the non-cohesive fill are shown on Figure B-1 in Appendix B.

The results of grain size distribution tests completed on two selected samples of the cohesive fill are shown on Figure B-2 in Appendix B. An Atterberg limits test was carried out on a selected sample of the cohesive fill and measured a liquid limit of about 24 per cent, a plastic limit of about 14 per cent, and a plasticity index of about 10 per cent. The test result, which is plotted on a plasticity chart on Figure B-3 in Appendix B, indicates that the cohesive fill can be classified as a clayey silt of low plasticity.

The natural water content measured on samples of the non-cohesive fill ranges between 4 per cent and 21 per cent. The natural water content measured on samples of the cohesive fill ranges between 6 per cent and 17 per cent.

### 4.2.3 Sandy Silt to Sand

Underlying the fill in Boreholes SWME-1, SWME-3, SWME-4, AR-1, CRB5, CRB-5A and CRB-7, a non-cohesive deposit ranging in composition from sandy silt to silt and sand to silty sand to sand, trace to some clay, trace gravel, was encountered. The depth and elevation of the surface and base of the non-cohesive layer at each borehole location (from east to west), the thickness and the soil type are presented below:

Borehole No.	Top of Layer		Bottom of Layer		Thickness (m)	Soil Type
	Depth (m)	Elevation (m)	Depth (m)	Elevation (m)		
SWME-4	0.7	94.8	3.7	91.8	3.0	Silt and Sand
AR-1	1.4	94.3	5.3	90.4	3.9	Sand to Silt and Sand
SWME-3	1.7	90.2	2.2	89.7	0.5	Sandy Silt
CRB-7	4.5	90.2	6.5	88.2	2.0	Sandy Silt
SWME-1	1.7	87.8	3.0	86.5	1.3	Sand
CRB-5	2.4	76.8	4.7	74.5	2.3	Silty Sand to Silt and Sand
	5.7	73.5	7.2	72.0	1.5	Silty Sand
CRB-5A	4.0	75.3	4.5	74.8	0.5	Silty Sand
	6.4	72.9	7.2	72.1	0.8	

SPT “N”-values measured within the sandy silt to sand deposit range from 0 blows to 63 blows per 0.3 m of penetration, indicating a very loose to very dense compactness condition, but was typically loose to compact.

The results of grain size distribution tests completed on nine selected samples of the sandy silt to sand deposit are shown on Figure B-4 in Appendix B. An Atterberg limits test was attempted on a sample of the sandy silt from Borehole CRB-7; however, it was classified as non-plastic.

The natural water content measured on samples of the sandy silt / silt and sand / silty sand / sand layers ranges between 4 per cent and 28 per cent.

### 4.2.4 Silt

Underlying the sandy silt deposit in Borehole SWME-3, the clayey silt in Borehole SWME-4 (discussed in Section 4.2.5) and the sand in Borehole AR-1 a deposit of silt, trace to some sand and trace to some clay, was encountered at depths between about 2.2 m and 5.6 m below ground surface (between Elevation 90.4 m and 89.7 m). The thickness of the silt layer ranges from about 1 m to 2 m and the deposit extends to depths between about 3.2 m and 7.6 m below ground surface (between Elevation 88.7 m and 87.9 m).

SPT “N”-values measured within the silt deposit are 16 blows, 19 blows and 56 blows per 0.3 m of penetration, indicating a compact to very dense compactness condition.

The results of the grain size distribution test completed on three selected samples of the silt deposit are shown on Figure B-5 in Appendix B.

The natural water content measured on samples of the silt deposit range from 14 per cent to 17 per cent.

#### 4.2.5 Clayey Silt with Sand to Silty Clay

Underlying the fill in Boreholes CRB-4 and CRB-6, the granular deposits in Borehole SWME-1 and SWME-4, and the silt deposit in Boreholes SWME-3, AR-1 and SWME-4, a deposit consisting of clayey silt with sand to silty clay was encountered. The depth and elevation of the top and bottom of this cohesive deposit at each borehole location (from east to west) and the corresponding thickness and soil type are summarized below.

Borehole No.	Top of Layer		Bottom of Layer		Thickness (m)	Soil Type
	Depth (m)	Elevation (m)	Depth (m)	Elevation (m)		
SWME-4	3.7	91.8	5.6	89.9	1.9	Clayey Silt
	7.6	87.9	8.1	87.4	0.5	Silty Clay
AR-1	7.2	88.5	8.7	87.0	1.5	Clayey Silt
SWME-3	3.2	88.7	3.7	88.2	0.5	Clayey Silt
CRB-6	1.7	90.0	4.4	87.3	2.7	Sandy Clayey Silt
SWME-1	3.0	86.5	3.7	85.8	0.7	Silty Clay
CRB-4	3.7	75.4	6.2	73.0	2.5	Sandy Clayey Silt

SPT “N”-values measured within the cohesive deposit typically range between 2 blows and 13 blows per 0.3 m of penetration, suggesting a very soft to stiff consistency.

The results of the grain size distribution test completed on six selected samples of the sandy clayey silt to silty clay deposit are shown on Figure B-6 in Appendix B.

Atterberg limits tests were carried out on six samples of the cohesive deposit and measured liquid limits ranging from 22 per cent to 42 per cent, plastic limits ranging from 14 per cent to 21 per cent, and plasticity indices ranging from 8 per cent to 21 per cent. These test results, which are plotted on a plasticity chart on Figure B-7 in Appendix B, indicate that the deposit can be classified as a clayey silt of low plasticity to silty clay of intermediate plasticity.

The natural water content measured on samples of the cohesive deposit range from about 14 per cent to 34 per cent.

#### 4.2.6 Organic Clayey Silt with Sand

Underlying the silty sand deposit in Boreholes CRB-5 and CRB-5A, and underlying the cohesive deposit in Borehole CRB-4, a deposit of organic clayey silt with sand, trace gravel, containing sand lenses, wood and shell fragments

was encountered at depths of between about 4.5 m and 6.2 m (between Elevations 74.8 m and 73.0 m) below ground surface. The thickness of the deposit ranges from about 0.8 m to 1.9 m and the deposit extends to depths of between 5.7 m and 7.0 m below ground surface (between Elevations 73.5 m and 72.1 m).

The SPT “N” values measured within the organic deposit range from 1 blow to 7 blows per 0.3 m of penetration, suggesting a very soft to firm consistency.

Three grain size distribution tests were carried out on three selected samples of the organic clayey silt deposit and the results are shown on Figure B-8 in Appendix B. Atterberg limits tests were carried out on three samples of this organic clayey silt deposit and measured liquid limits ranging from about 38 per cent to 46 per cent, plastic limits ranging from about 26 per cent to 36 per cent, and plasticity indices ranging from about 6 per cent to 17 per cent. These test results, which are plotted on the plasticity chart on Figure B-9 in Appendix B, indicate that the deposit consists of organic clayey silt of intermediate plasticity.

Organic content tests completed on two samples from this deposit measured 6 per cent and 7 per cent. The water content measured on samples from the organic deposit range from 41 per cent to 47 per cent.

#### **4.2.7 Silt and Sand / Clayey Silt to Sandy Silty Clay (Till)**

Underlying the topsoil in Borehole AR-2 and underlying the cohesive deposit in Boreholes SWME-3 and SWME-4 and underlying the non-cohesive deposit in Borehole CRB-7, a till deposit comprised of silt and sand / clayey silt to sandy silty clay was encountered at depths between about 0.6 m and 8.1 m below ground surface (between Elevation 88.2 m and 87.4 m). The thickness of the till deposit ranges from about 0.6 m to 3.2 m and the deposit extends to depths between about 3.8 m and 9.0 m below ground surface (between Elevation 87.6 m and 84.6 m). The predominantly cohesive till deposit contains trace to some sand and trace to some gravel and in Borehole AR-2, was interlayered with a 1.1 m thick sand and silt till zone at a depth of 1.1 m below ground surface.

SPT “N”-values measured within the cohesive till deposit are between 10 blows and 14 blows per 0.3 m of penetration, suggesting a stiff consistency. Two SPT “N”-values measured within the non-cohesive till were 6 blows and 14 blows per 0.3 m of penetration indicating a loose to compact state of compactness.

Grain size distribution tests carried out on three selected samples of the non-cohesive and cohesive till deposit are shown on Figure B-10 in Appendix B.

Atterberg limits tests were carried out on four samples of the cohesive till deposit and measured liquid limits ranging from about of 23 per cent to 38 per cent, plastic limits ranging from about 14 per cent to 20 per cent, and plasticity indices ranging from about 8 per cent to 18 per cent. These test results, which are plotted on a plasticity chart on Figure B-11 in Appendix B, indicate that the deposit is comprised of clayey silt of low plasticity to a silty clay of intermediate plasticity.

The natural water content measured on samples of the cohesive till deposit range from 12 per cent to 18 per cent and the natural water content measured on a sample of the non-cohesive till deposit was 15 per cent.

#### **4.2.8 Clayey Silt (Residual Soil)**

Underlying the cohesive deposit in Boreholes SWME-1, AR-1 and CRB-6, and the till deposit in Boreholes AR-2, SWME-3 and CRB-7 a 0.2 m to 1.0 m thick deposit of residual soil comprised of clayey silt, some sand to sandy, some gravel, and containing trace to some shale fragments was encountered at depths ranging between about 3.7 m and 8.7 m below ground surface (between Elevations 87.6 m and 84.6 m). The cohesive residual soil deposit is interpreted to be derived from weathering of the underlying shale bedrock and extends to the bedrock surface.

SPT “N”-values measured within the residual soil deposit are 28 blows per 0.3 m of penetration and over 50 blows for 0.13 m of penetration, suggesting a very stiff to hard consistency.

The result of a grain size distribution test completed on one selected sample of the residual soil is shown on Figure B-12 in Appendix B. Atterberg limits tests were carried out on three samples of the residual soil and measured liquid limits of about 23 per cent, plastic limits ranging from about 15 per cent to 16 per cent, and corresponding plasticity indices ranging from about 7 per cent to 8 per cent. These test results, which are plotted on a plasticity chart on Figure B-13 in Appendix B, indicate that the deposit can be classified as a clayey silt of low plasticity.

The natural water content measured on samples of the residual soil ranges between 9 per cent and 14 per cent.

#### 4.2.9 Shale Bedrock

Bedrock was encountered and inferred by split-spoon sampling in Boreholes SWME-1, SWME-3 and AR-1 and confirmed by bedrock coring in Borehole SWME-4, AR-2, CRB-4, CRB-5, CRB-5A, CRB-6 and CRB-7. The depth to bedrock below ground surface and the corresponding bedrock surface elevations at each borehole location (from east to west) are summarized below.

Borehole	Depth to Bedrock Surface (m)	Bedrock Surface Elevation (m)	Comments
SWME-4	9.0	86.5	1.0 m penetration by augering and split-spoon sampling followed by 3.3 m of bedrock coring.
AR-1	8.9	86.8	0.3 m penetration by augering and split-spoon sampling
SWME-3	4.5	87.4	0.9 m penetration by augering and split-spoon sampling
CRB-6	4.8	86.9	Bedrock cored 8.2 m
CRB-7	8.1	86.6	Bedrock cored 7.5 m
SWME-1	4.7	84.8	0.8 m penetration by augering and split-spoon sampling
AR-2	4.6	83.8	Bedrock cored 7.0 m
CRB-4	7.0	72.1	Bedrock cored 8.1 m
CRB-5	7.2	72.0	Bedrock cored 8.3 m
CRB-5A	7.2	72.1	Bedrock cored 9.5 m

In general, the inferred / confirmed bedrock surface as encountered in the boreholes advanced in the area of the proposed temporary East Access Road varies from about Elevation 72.0 m to 87.4 m.

Based on a review of the bedrock core samples, the bedrock consists of shale of the Georgian Bay Formation. In general, the bedrock samples are described as highly weathered to fresh, thinly bedded, fine grained, faintly to non-porous, weak, grey, with medium strong to strong limestone interbeds at varying intervals, as presented in the drillhole records in Appendix A, and shown on the photographs of the recovered core samples on Figures A-1 to A-8 in Appendix A. Typically, the upper portion of the bedrock surface is weathered and transitions to slightly weathered to fresh at depth. The degree of weathering of the bedrock samples (e.g. slightly weathered –W2), and

the strength classification of the intact rock mass based on field identification (e.g. weak – R2) are described in accordance with the International Society for Rock Mechanics (ISRM<sup>3</sup>) standard classification system.

The Rock Quality Designation (RQD) measured on the core samples ranges between 0 per cent to 100 per cent, with core run near (typically the upper 1 m) bedrock surface ranging from about 0 per cent to 25 per cent (indicating a rock mass of very poor to poor quality) and core run at depth (typically below about 1 m below bedrock surface) ranging from about 50 per cent to 100 per cent (indicating a rock mass of fair to excellent quality), as classified per Table 3.10 of CFEM (2006)<sup>4</sup>. The Total Core Recovery (TCR) and Solid Core Recovery (SCR) of samples recovered range between 10 and 100 per cent and between 0 per cent and 97 per cent, respectively.

Uniaxial compression (UC) tests (ASTM D7012)<sup>5</sup> were carried out on selected core samples of the shale bedrock and the uniaxial compressive strength (UCS), bulk density and tangent Young's modulus of the intact samples are summarized below and the details are presented in the Rock Laboratory Test Result report(s) from Geomechanica in Appendix B.

Borehole Number	Sample Depth Interval (m)	Sample Elevation Interval (m)	Uniaxial Compressive Strength (UCS) (MPa)	Bulk Density (g/cm <sup>3</sup> )	Tangent Young's Modulus (GPa)
SWME-4 (Run #1)	10.4 – 10.5	85.1 to 85.0	13.5	2.59	not tested
AR-2 (Run #2)	5.9 – 6.1	82.5 to 82.3	9.1	2.57	not tested
AR-2 (Run #4)	8.6 – 8.8	79.8 to 79.6	11.5	2.59	not tested
CRB-4 (Run #5)	13.6 – 13.8	65.5 to 65.3	18.6	2.61	0.84
CRB-5 (Run #5)	13.7 – 13.9	65.5 to 65.3	15.5	2.61	0.61
CRB-5A (Run #4)	12.4 – 12.6	66.9 to 66.7	14.2	2.60	0.96
CRB-5A (Run #6)	15.4 – 15.6	63.9 to 63.7	22.7	2.64	0.93
CRB-6 (Run #1)	6.0 - 6.2	85.7 to 85.5	14.6	2.17	0.63
CRB-7 (Run#2)	9.2 – 9.4	85.5 to 85.3	15.5	2.59	0.65
CRB-7 (Run #3)	12.1 – 12.4	82.6 to 82.3	7.4	2.59	1.28

A total of fifteen diametral and fifteen axial point load tests were carried out on shale bedrock core specimens and measured axial and diametral point load strength indices ranging from 0.04 MPa to 2.14 MPa, with an average value of 0.49 MPa. The average point load test index for axial and diametral orientations was 0.66 m MPa and 0.41 MPa, respectively. The results are summarized in Table B-1 in Appendix B.

<sup>3</sup> International Society for Rock Mechanics Commission on Test Methods, 1985. Int. J. Rock Mech. Min. Sci. & Geomech. Abstr. Vol 22, No. 2, pp. 51-60.

<sup>4</sup> Canadian Geotechnical Society, 2006. Canadian Foundation Engineering Manual (CFEM), 4<sup>th</sup> Edition. The Canadian Geotechnical Society, BiTech Published Ltd., British Columbia.

<sup>5</sup> ASTM D7012 – Standard Test Method for Compressive Strength and Elastic Moduli of Intact Rock Core Specimens

Based on the laboratory UCS tests and also considering the point load strength indices, in accordance with Table 3.5 in CFEM (2006)<sup>4</sup>, the shale bedrock is generally classified as weak ( $R2, 5 \text{ MPa} < \text{UCS} < 25 \text{ MPa}$ ).

#### 4.2.10 Groundwater Conditions

The overburden samples obtained from the boreholes were generally moist. Boreholes SWME-1, CRB-6, CRB-7 and AR-2 were observed to be open and dry upon completion of drilling and prior to rock coring. Upon completion of drilling overburden in Boreholes SWME-4, AR-1, CRB-4, CRB-5 and CRB-5A the water level in the open boreholes was measured at depths of between 3.7 m and 7.6 m below ground surface (corresponding to Elevations 87.9 m, 92.0 m and 92.0 m about 75.0 m at Boreholes CRB-4, CRB-5 and CRB-5A), upon completion of overburden drilling and prior to rock coring. The depths to the water level observed in the boreholes upon completion of drilling and prior to rock coring is presented below. It is noted that these observations are not necessarily representative of the stabilized groundwater level at the site.

Borehole No.	Ground Surface Elevation (m)	Water Level Depth (m)	Water Elevation (m)	Comment
SWME-4	95.5	7.6	87.9	Upon completion of overburden drilling and prior to rock coring.
AR-1	95.7	3.7	92.0	Upon completion of drilling.
SWME-3	91.9	5.3	86.6	Upon completion of drilling.
CRB-4	79.1	3.8	75.4	Upon completion of overburden drilling and prior to rock coring.
CRB-5	79.2	4.3	74.9	
CRB-5A	79.3	3.6	75.7	

A standpipe piezometer was installed in Boreholes SWME-3, CRB-5A and CRB-6. Details of the stratum that the piezometer screen was sealed into, the recorded water levels and elevations are summarized below.

Borehole No. / Piezometer	Stratum Well Screen Sealed Into	Ground Surface Elevation (m)	Water Level Depth (m)	Water Elevation (m)	Date of Piezometer Reading
SWME-3	Clayey Silt Till, / Clayey Silt Residual Soil / Shale Bedrock	91.9	4.0	87.9	August 14, 2018
			3.8	88.1	November 6, 2018
CRB-6	Shale Bedrock	91.7	5.6	86.0	November 12, 2017
			5.0	86.7	March 12, 2018
			4.9	86.8	April 30, 2018
			4.9	86.8	November 6, 2018

Borehole No. / Piezometer	Stratum Well Screen Sealed Into	Ground Surface Elevation (m)	Water Level Depth (m)	Water Elevation (m)	Date of Piezometer Reading
CRB-5A	Silty Sand/Organic Clayey Silt/Shale Bedrock	79.3	1.6	77.7	March 12, 2018
			4.0	75.3	April 30, 2018
			4.6	74.7	November 6, 2018

It should be noted that the groundwater level in the area is subject to seasonal fluctuations and precipitation events, and should be expected to be higher during wet periods of the year. The groundwater levels may be influenced by the water level in the adjacent Credit River which was measured to be at Elevation 75 m in September 1986. The high-water level for the Credit River is reported to be at Elevation 77.7 m for the 100-year storm.

### 5.0 CLOSURE

This report was prepared by Ms. Sandra McGaghran, M.Eng., P.Eng., a Geotechnical Engineer and Associate with Golder. Mr. Kevin J. Bentley, P.Eng., an Associate and MTO Foundations Designated Contact with Golder, conducted a quality control audit of the report.



Sandra McGaghran, M.Eng., P.Eng.  
Associate, Senior Geotechnical Engineer

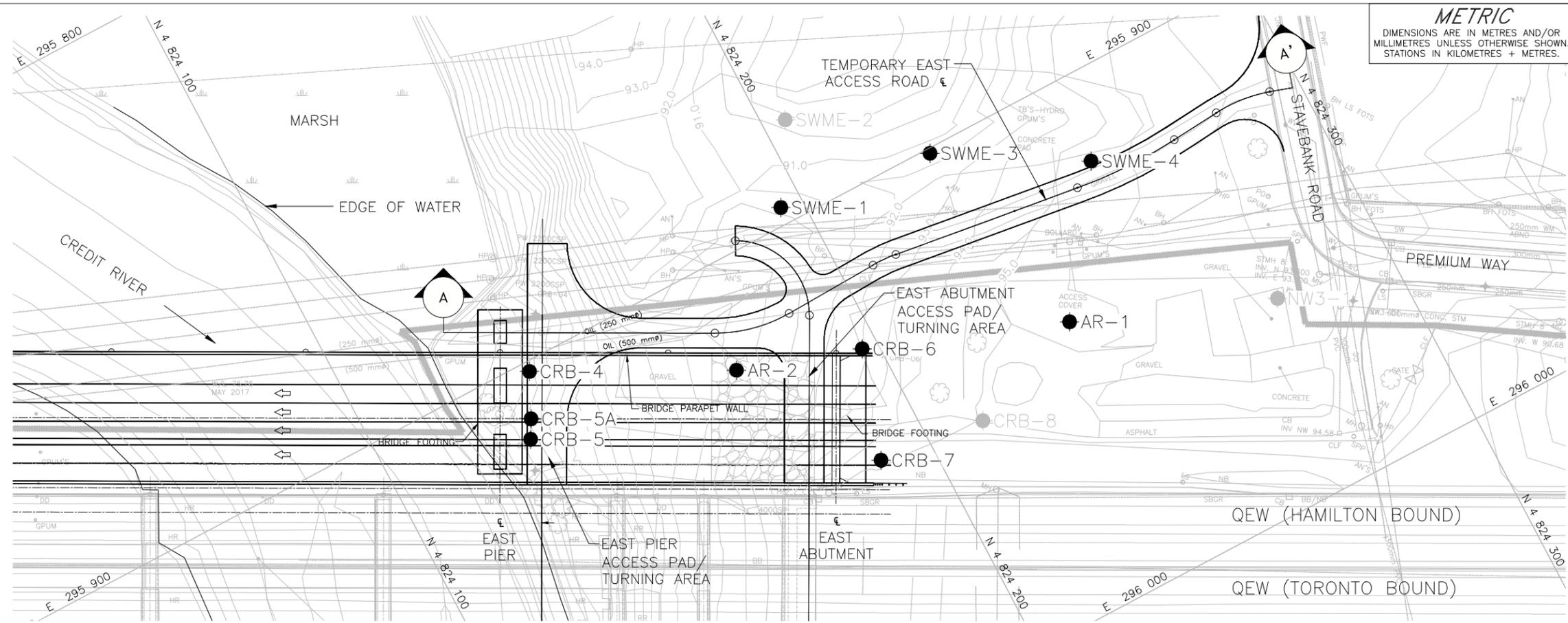


Kevin J. Bentley, P.Eng.  
Associate, MTO Foundations Designated Contact

AM//MS/SMM/KJB/rb

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[https://golderassociates.sharepoint.com/sites/11176g/shared documents/07-reporting/foundations/9 - east access road/3 - final/1662333 fidr - east access road -2019feb12.docx](https://golderassociates.sharepoint.com/sites/11176g/shared%20documents/07-reporting/foundations/9-east%20access%20road/3-final/1662333%20fidr-east%20access%20road-2019feb12.docx)



PLAN  
SCALE  
10 0 10 20 m

**METRIC**  
DIMENSIONS ARE IN METRES AND/OR MILLIMETRES UNLESS OTHERWISE SHOWN. STATIONS IN KILOMETRES + METRES.

CONT No. 2019-2016  
GWP No. 2002-13-00



QEW WIDENING-MISSISSAUGA RD TO HURONTARIO ST  
TEMPORARY EAST ACCESS ROAD  
BOREHOLE LOCATIONS AND SOIL STRATA

SHEET



KEY PLAN  
SCALE  
2 0 2 4 km

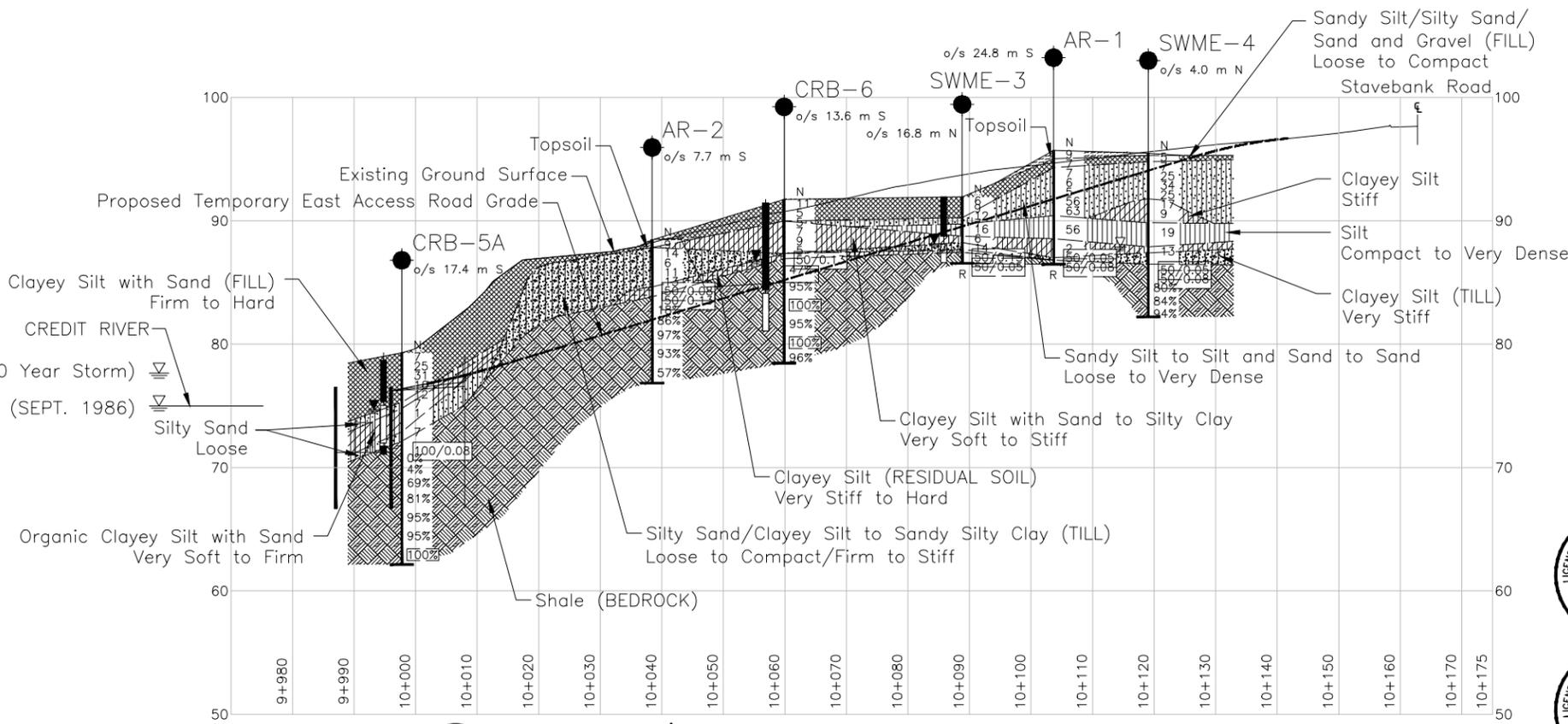
- LEGEND**
- Borehole - Current Investigation
  - ⊥ Seal
  - ⊥ Piezometer
  - N Standard Penetration Test Value
  - 16 Blows/0.3m unless otherwise stated (Std. Pen. Test, 475 j/blow)
  - 100% Rock Quality Designation (RQD)
  - R Split-Spoon Refusal
  - ⊥ WL in piezometer, measured on November 6, 2018
  - ⊥ WL upon completion of drilling

BOREHOLE CO-ORDINATES (MTM NAD 83 ZONE 10)

No.	ELEVATION	NORTHING	EASTING
AR-1	95.7	4824236.4	295944.2
AR-2	88.4	4824172.2	295921.4
CRB-4	79.1	4824135.1	295902.0
CRB-5	79.2	4824128.9	295914.2
CRB-5A	79.3	4824130.9	295910.6
CRB-6	91.7	4824196.7	295929.5
CRB-7	94.7	4824189.6	295951.1
SWME-1	89.5	4824195.5	295896.6
SWME-3	91.9	4824227.3	295901.0
SWME-4	95.5	4824255.4	295917.6

**NOTES**  
This drawing is for subsurface information only. The proposed structure details/works are shown for illustration purposes only and may not be consistent with the final design configuration as shown elsewhere in the Contracts Documents.  
The boundaries between soil strata have been established only at borehole locations. Between boreholes the boundaries are assumed from geological evidence.

**REFERENCE**  
Base plans provided in digital format by Morrison Hershfield, drawing file no. X11609340Base.dwg, received April 12, 2018.  
General Arrangement plan and profile provided in digital format by Morrison Hershfield, drawing file no. 01.GENERAL ARRANGEMENT (for Golder).dwg, received April 13, 2018.  
Utility plan provided in digital format by Morrison Hershfield, drawing file no. X-EX-UTIL-BASE.dwg, received April 17, 2018.  
Access Road plan provided in digital format by Morrison Hershfield, drawing file 1160934 - Construction Access Road.dwg, received July 26, 2018.



HORIZONTAL SCALE  
10 0 10 20 m  
VERTICAL SCALE  
5 0 5 10 m

A-A' PROFILE A-A' - TEMPORARY EAST ACCESS ROAD C

NO.	DATE	BY	REVISION

Geocres No. 30M12-437  
 HWY: QEW PROJECT NO. 1662333 DIST. CENTRAL  
 SUBM'D. AM CHKD. DPM DATE: 02/01/2019 SITE: .  
 DRAWN: DD CHKD. SMM APPD. KJB DWG. 1

**APPENDIX A**

**Record of Borehole and Drillhole  
Sheets and Bedrock Core  
Photographs**

## LIST OF SYMBOLS

Unless otherwise stated, the symbols employed in the report are as follows:

### I. GENERAL

$\pi$	3.1416
$\ln x$ ,	natural logarithm of x
$\log_{10}$	x or log x, logarithm of x to base 10
g	acceleration due to gravity
t	time
FoS	factor of safety

### II. STRESS AND STRAIN

$\gamma$	shear strain
$\Delta$	change in, e.g. in stress: $\Delta \sigma$
$\epsilon$	linear strain
$\epsilon_v$	volumetric strain
$\eta$	coefficient of viscosity
$\nu$	Poisson's ratio
$\sigma$	total stress
$\sigma'$	effective stress ( $\sigma' = \sigma - u$ )
$\sigma'_{vo}$	initial effective overburden stress
$\sigma_1, \sigma_2, \sigma_3$	principal stress (major, intermediate, minor)
$\sigma_{oct}$	mean stress or octahedral stress $= (\sigma_1 + \sigma_2 + \sigma_3)/3$
$\tau$	shear stress
u	porewater pressure
E	modulus of deformation
G	shear modulus of deformation
K	bulk modulus of compressibility

### III. SOIL PROPERTIES

#### (a) Index Properties

$\rho(\gamma)$	bulk density (bulk unit weight)*
$\rho_d(\gamma_d)$	dry density (dry unit weight)
$\rho_w(\gamma_w)$	density (unit weight) of water
$\rho_s(\gamma_s)$	density (unit weight) of solid particles
$\gamma'$	unit weight of submerged soil ( $\gamma' = \gamma - \gamma_w$ )
$D_R$	relative density (specific gravity) of solid particles ( $D_R = \rho_s / \rho_w$ ) (formerly $G_s$ )
e	void ratio
n	porosity
S	degree of saturation

#### (a) Index Properties (continued)

w	water content
$w_l$ or LL	liquid limit
$w_p$ or PL	plastic limit
$I_p$ or PI	plasticity index = $(w_l - w_p)$
$w_s$	shrinkage limit
$I_L$	liquidity index = $(w - w_p) / I_p$
$I_c$	consistency index = $(w_l - w) / I_p$
$e_{max}$	void ratio in loosest state
$e_{min}$	void ratio in densest state
$I_D$	density index = $(e_{max} - e) / (e_{max} - e_{min})$ (formerly relative density)

#### (b) Hydraulic Properties

h	hydraulic head or potential
q	rate of flow
v	velocity of flow
i	hydraulic gradient
k	hydraulic conductivity (coefficient of permeability)
j	seepage force per unit volume

#### (c) Consolidation (one-dimensional)

$C_c$	compression index (normally consolidated range)
$C_r$	recompression index (over-consolidated range)
$C_s$	swelling index
$C_{\alpha}$	secondary compression index
$m_v$	coefficient of volume change
$C_v$	coefficient of consolidation (vertical direction)
$C_h$	coefficient of consolidation (horizontal direction)
$T_v$	time factor (vertical direction)
U	degree of consolidation
$\sigma'_p$	pre-consolidation stress
OCR	over-consolidation ratio = $\sigma'_p / \sigma'_{vo}$

#### (d) Shear Strength

$\tau_p, \tau_r$	peak and residual shear strength
$\phi'$	effective angle of internal friction
$\delta$	angle of interface friction
$\mu$	coefficient of friction = $\tan \delta$
$c'$	effective cohesion
$c_u, s_u$	undrained shear strength ( $\phi = 0$ analysis)
p	mean total stress $(\sigma_1 + \sigma_3)/2$
$p'$	mean effective stress $(\sigma'_1 + \sigma'_3)/2$
q	$(\sigma_1 - \sigma_3)/2$ or $(\sigma'_1 - \sigma'_3)/2$
$q_u$	compressive strength $(\sigma_1 - \sigma_3)$
$S_t$	sensitivity

\* Density symbol is  $\rho$ . Unit weight symbol is  $\gamma$  where  $\gamma = \rho g$  (i.e. mass density multiplied by acceleration due to gravity)

Notes: 1  
2

$$\tau = c' + \sigma' \tan \phi'$$

$$\text{shear strength} = (\text{compressive strength})/2$$

## LIST OF ABBREVIATIONS

The abbreviations commonly employed on Records of Boreholes, on figures and in the text of the report are as follows:

### I. SAMPLE TYPE

AS	Auger sample
BS	Block sample
CS	Chunk sample
DS	Denison type sample
FS	Foil sample
RC	Rock core
SC	Soil core
SS	Split-spoon
ST	Slotted tube
TO	Thin-walled, open
TP	Thin-walled, piston
WS	Wash sample

### II. PENETRATION RESISTANCE

#### Standard Penetration Resistance (SPT), N:

The number of blows by a 63.5 kg. (140 lb.) hammer dropped 760 mm (30 in.) required to drive a 50 mm (2 in.) drive open sampler for a distance of 300 mm (12 in.)

#### Dynamic Cone Penetration Resistance; $N_d$ :

The number of blows by a 63.5 kg (140 lb.) hammer dropped 760 mm (30 in.) to drive uncased a 50 mm (2 in.) diameter, 60° cone attached to "A" size drill rods for a distance of 300 mm (12 in.).

**PH:** Sampler advanced by hydraulic pressure

**PM:** Sampler advanced by manual pressure

**WH:** Sampler advanced by static weight of hammer

**WR:** Sampler advanced by weight of sampler and rod

#### Piezo-Cone Penetration Test (CPT)

A electronic cone penetrometer with a 60° conical tip and a project end area of 10 cm<sup>2</sup> pushed through ground at a penetration rate of 2 cm/s. Measurements of tip resistance ( $Q_t$ ), porewater pressure (PWP) and friction along a sleeve are recorded electronically at 25 mm penetration intervals.

### V. MINOR SOIL CONSTITUENTS

Per cent by Weight	Modifier	Example
0 to 5	Trace	Trace sand
5 to 12	Trace to Some (or Little)	Trace to some sand
12 to 20	Some	Some sand
20 to 30	(ey) or (y)	Sandy
over 30	And (non-cohesive (cohesionless)) or With (cohesive)	Sand and Gravel Silty Clay with sand / Clayey Silt with sand

### III. SOIL DESCRIPTION

#### (a) Non-Cohesive (Cohesionless) Soils

Compactness	N
Condition	Blows/300 mm or Blows/ft
Very loose	0 to 4
Loose	4 to 10
Compact	10 to 30
Dense	30 to 50
Very dense	over 50

#### (b) Cohesive Soils

Consistency	$C_u, S_u$
	kPa      psf
Very soft	0 to 12      0 to 250
Soft	12 to 25      250 to 500
Firm	25 to 50      500 to 1,000
Stiff	50 to 100      1,000 to 2,000
Very stiff	100 to 200      2,000 to 4,000
Hard	over 200      over 4,000

### IV. SOIL TESTS

w	water content
$w_p$	plastic limit
$w_l$	liquid limit
C	consolidation (oedometer) test
CHEM	chemical analysis (refer to text)
CID	consolidated isotropically drained triaxial test <sup>1</sup>
CIU	consolidated isotropically undrained triaxial test with porewater pressure measurement <sup>1</sup>
$D_R$	relative density (specific gravity, $G_s$ )
DS	direct shear test
M	sieve analysis for particle size
MH	combined sieve and hydrometer (H) analysis
MPC	Modified Proctor compaction test
SPC	Standard Proctor compaction test
OC	organic content test
SO <sub>4</sub>	concentration of water-soluble sulphates
UC	unconfined compression test
UU	unconsolidated undrained triaxial test
V	field vane (LV-laboratory vane test)
$\gamma$	unit weight

**Note:** 1 Tests which are anisotropically consolidated prior to shear are shown as CAD, CAU.

# LITHOLOGICAL AND GEOTECHNICAL ROCK DESCRIPTION TERMINOLOGY

## WEATHERINGS STATE

**Fresh:** no visible sign of weathering

**Faintly weathered:** weathering limited to the surface of major discontinuities.

**Slightly weathered:** penetrative weathering developed on open discontinuity surfaces but only slight weathering of rock material.

**Moderately weathered:** weathering extends throughout the rock mass but the rock material is not friable.

**Highly weathered:** weathering extends throughout rock mass and the rock material is partly friable.

**Completely weathered:** rock is wholly decomposed and in a friable condition but the rock and structure are preserved.

## BEDDING THICKNESS

<u>Description</u>	<u>Bedding Plane Spacing</u>
Very thickly bedded	Greater than 2 m
Thickly bedded	0.6 m to 2 m
Medium bedded	0.2 m to 0.6 m
Thinly bedded	60 mm to 0.2 m
Very thinly bedded	20 mm to 60 mm
Laminated	6 mm to 20 mm
Thinly laminated	Less than 6 mm

## JOINT OR FOLIATION SPACING

<u>Description</u>	<u>Spacing</u>
Very wide	Greater than 3 m
Wide	1 m to 3 m
Moderately close	0.3 m to 1 m
Close	50 mm to 300 mm
Very close	Less than 50 mm

## GRAIN SIZE

<u>Term</u>	<u>Size*</u>
Very Coarse Grained	Greater than 60 mm
Coarse Grained	2 mm to 60 mm
Medium Grained	60 microns to 2 mm
Fine Grained	2 microns to 60 microns
Very Fine Grained	Less than 2 microns

Note: \* Grains greater than 60 microns diameter are visible to the naked eye.

## CORE CONDITION

### Total Core Recovery (TCR)

The percentage of solid drill core recovered regardless of quality or length, measured relative to the length of the total core run.

### Solid Core Recovery (SCR)

The percentage of solid drill core, regardless of length, recovered at full diameter, measured relative to the length of the total core run.

### Rock Quality Designation (RQD)

The percentage of solid drill core, greater than 100 mm length, recovered at full diameter, measured relative to the length of the total core run. RQD varied from 0% for completely broken core to 100% for core in solid sticks.

## DISCONTINUITY DATA

### Fracture Index

A count of the number of discontinuities (physical separations) in the rock core, including both naturally occurring fractures and mechanically induced breaks caused by drilling.

### Dip with Respect to Core Axis

The angle of the discontinuity relative to the axis (length) of the core. In a vertical borehole a discontinuity with a 90° angle is horizontal.

### Description and Notes

An abbreviation description of the discontinuities, whether naturally occurring separations such as fractures, bedding planes and foliation planes or mechanically induced features caused by drilling such as ground or shattered core and mechanically separated bedding or foliation surfaces. Additional information concerning the nature of fracture surfaces and infillings are also noted.

### Abbreviations

JN Joint	PL Planar
FLT Fault	CU Curved
SH Shear	UN Undulating
VN Vein	IR Irregular
FR Fracture	K Slickensided
SY Stylolite	PO Polished
BD Bedding	SM Smooth
FO Foliation	SR Slightly Rough
CO Contact	RO Rough
AXJ Axial Joint	VR Very Rough
KV Karstic Void	
MB Mechanical Break	

PROJECT <u>1662333</u>	<b>RECORD OF BOREHOLE No AR-1</b>	SHEET 1 OF 1	<b>METRIC</b>
G.W.P. <u>2002-13-00</u>	LOCATION <u>N 4824236.4; E 295944.3 MTM NAD 83 ZONE 10 (LAT. 43.558012; LONG. -79.609616)</u>	ORIGINATED BY <u>ACM</u>	
DIST <u>Central</u> HWY <u>QEW</u>	BOREHOLE TYPE <u>CME 55, 114 mm I.D., Hollow Stem Augers</u>	COMPILED BY <u>CC</u>	
DATUM <u>Geodetic</u>	DATE <u>July 30, 2018</u>	CHECKED BY <u>SMM</u>	

ELEV DEPTH	SOIL PROFILE DESCRIPTION	STRAT PLOT	SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W <sub>p</sub>	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W <sub>L</sub>	UNIT WEIGHT γ kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%)
			NUMBER	TYPE	"N" VALUES			SHEAR STRENGTH kPa									
							20	40	60	80	100						
95.7	GROUND SURFACE																
0.0	TOPSOIL (700 mm)		1	SS	9												
95.0							95										
0.7	Sand, some silt to silt and sand, trace clay (FILL)		2	SS	7												
94.3	Loose Brown Moist																
1.4	SAND, some silt SILT and SAND, trace clay Loose to very dense Brown Moist - Oxidation staining from 2.3 m to 3.7 m - Wet from 3.0 m to 3.7 m		3	SS	7											0 81 16 3	
			4	SS	6												
			5	SS	5												
			6	SS	56											0 35 61 4	
			7	SS	63												
90.4																	
5.3	SILT, trace to some sand, trace to some clay Very dense Brown to grey Moist		8	SS	56											0 11 82 7	
88.5																	
7.2	CLAYEY SILT, trace sand Very soft Grey Moist to wet		9	SS	2											0 1 55 44	
87.0			10A	SS	50/0.05												
			10B	SS	50/0.05											7 29 46 18	
86.5	Sandy CLAYEY SILT, trace to some gravel, some shale fragments (RESIDUAL SOIL)		11	SS	50/0.08												
9.2	Hard Grey Moist to wet SHALE (BEDROCK) Grey END OF BOREHOLE SPLIT-SPOON REFUSAL																

GTA-MTO 001 S:\CLIENTS\MTQEW-CREDIT\_RIVER\02\_DATA\INT\QEW-CREDIT\_RIVER.GPJ GAL-GTA.GDT 1/9/19

NOTES:  
1. Water level at a depth of approximate 3.7 m below ground surface (Elev. 92.0 m) upon completion of drilling.

+<sup>3</sup>, ×<sup>3</sup>: Numbers refer to Sensitivity      ○ 3% STRAIN AT FAILURE

PROJECT <u>1662333</u>	<b>RECORD OF BOREHOLE No AR-2</b>	SHEET 1 OF 1	<b>METRIC</b>
G.W.P. <u>2002-13-00</u>	LOCATION <u>N 4824172.2; E 295921.4 MTM NAD 83 ZONE 10 (LAT. 43.557434; LONG. -79.609899)</u>	ORIGINATED BY <u>ACM</u>	
DIST <u>Central</u> HWY <u>QEW</u>	BOREHOLE TYPE <u>CME 75, 114 mm I.D. Hollow Stem Augers, HQ Casing</u>	COMPILED BY <u>CC</u>	
DATUM <u>Geodetic</u>	DATE <u>July 30, 2018</u>	CHECKED BY <u>SMM</u>	

ELEV DEPTH	SOIL PROFILE DESCRIPTION	STRAT PLOT	SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W <sub>p</sub>	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W <sub>L</sub>	UNIT WEIGHT γ kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL							
			NUMBER	TYPE	"N" VALUES			SHEAR STRENGTH kPa																
							20 40 60 80 100	○ UNCONFINED + FIELD VANE ● QUICK TRIAXIAL × REMOULDED																
88.4	GROUND SURFACE																							
0.0	TOPSOIL (600 mm)		1	SS	9																			
87.8	CLAYEY SILT, some sand, some gravel, trace rootlets, shale fragments (TILL) Stiff Brown to grey Moist	[Strat Plot]	2A	SS	14																			
0.6			2B																					
87.3	SILT and SAND, trace to some clay, trace to some gravel, clayey silt pockets, shale fragments (TILL) Loose to compact Brown Moist	[Strat Plot]	3	SS	6											6 56 31 7								
1.1			4			SS	11																	
86.2	Sandy SILTY CLAY, trace to some gravel, trace shale fragments (TILL) Stiff Brown grey with oxidation staining Moist	[Strat Plot]	5	SS	13													7 22 44 27						
2.2			6			SS	50/0.08																	
84.6	CLAYEY SILT, some sand, some shale fragments (RESIDUAL SOIL) Hard Brown grey Moist	[Strat Plot]	7	SS	50/0.13																			
3.8			1			RC	REC 100%												RQD = 18%					
83.8	SHALE (BEDROCK) Grey  Bedrock cored from a depth of 4.6 m to 11.6 m  For bedrock coring details, refer to Record of Drillhole AR-2	[Strat Plot]	2	RC	REC 100%														RQD = 86%					
4.6			3			RC	REC 100%													RQD = 97%				
			4					RC	REC 100%													RQD = 93%		
			5							RC	REC 100%													RQD = 57%
76.8	END OF BOREHOLE																							
11.6	NOTES: 1. Borehole dry prior to rock coring.																							

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 +<sup>3</sup>, ×<sup>3</sup>: Numbers refer to Sensitivity      ○ 3% STRAIN AT FAILURE



**RECORD OF BOREHOLE No CRB-4** SHEET 1 OF 2 **METRIC**

PROJECT 1662333

G.W.P. 2002-13-00 LOCATION N 4824135.1; E 295902.0 MTM NAD 83 ZONE 10 (LAT. 43.557099; LONG. -79.610138) ORIGINATED BY JL

DIST Central HWY QEW BOREHOLE TYPE CME 55, 159 mm O.D., 70 mm I.D. Hollow Stem Augers (Auto Hammer) COMPILED BY KN

DATUM Geodetic DATE February 16, 2018 CHECKED BY SMM

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W <sub>p</sub>	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W <sub>L</sub>	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)				
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	SHEAR STRENGTH kPa						WATER CONTENT (%)			
						20	40	60	80	100	10	20	30	GR	SA	SI	CL
79.1	GROUND SURFACE																
0.0	Clayey silt with sand, trace to some gravel, contains rootlets, contains shale fragments (FILL) Firm to hard Brown, becoming grey at 3.1 m Moist		1	SS	6												
			2	SS	13												
			3	SS	8												
			4	SS	23									7	41	37	15
			5	SS	31												
75.4																	
3.7	Sandy CLAYEY SILT, some gravel, contains shale fragments Stiff Moist, becoming wet at 4.6 m		6	SS	11									14	27	42	17
			7	SS	13												
73.0																	
6.2	ORGANIC CLAYEY SILT with SAND, trace gravel, contains sand lenses Soft Brown Wet		8	SS	3									2	32	56	10
72.1																	
7.0	SHALE (BEDROCK) Grey		1	RC	REC 100%												RQD = 0%
	Bedrock cored from a depth of 7.2 m to 15.3 m		9	SS	50/0.10												
	For bedrock coring details, refer to Record of Drillhole CRB-4		2	RC	REC 87%												RQD = 53%
			3	RC	REC 97%												RQD = 77%
			4	RC	REC 100%												RQD = 79%
			5	RC	REC 100%												RQD = 86%
			6	RC	REC 100%												RQD = 97%

GTA-MTO 001 S:\CLIENTS\MTQEW-CREDIT\_RIVER\02\_DATA\INTQEW-CREDIT\_RIVER.GPJ GAL-GTA.GDT 1/9/19

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 +<sup>3</sup>, ×<sup>3</sup>: Numbers refer to Sensitivity      ○ 3% STRAIN AT FAILURE

PROJECT <u>1662333</u>	<b>RECORD OF BOREHOLE No CRB-4</b>	SHEET 2 OF 2	<b>METRIC</b>
G.W.P. <u>2002-13-00</u>	LOCATION <u>N 4824135.1; E 295902.0 MTM NAD 83 ZONE 10 (LAT. 43.557099; LONG. -79.610138)</u>	ORIGINATED BY <u>JL</u>	
DIST <u>Central</u> HWY <u>QEW</u>	BOREHOLE TYPE <u>CME 55, 159 mm O.D., 70 mm I.D. Hollow Stem Augers (Auto Hammer)</u>	COMPILED BY <u>KN</u>	
DATUM <u>Geodetic</u>	DATE <u>February 16, 2018</u>	CHECKED BY <u>SMM</u>	

ELEV DEPTH	SOIL PROFILE DESCRIPTION	STRAT PLOT	SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W <sub>p</sub>	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W <sub>L</sub>	UNIT WEIGHT <b>γ</b> kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
			NUMBER	TYPE	"N" VALUES			20	40	60	80	100					
63.8	SHALE (BEDROCK)	▨	6	RC			64										
15.3	END OF BOREHOLE																
	NOTES: 1. Water level encountered during drilling at a depth of about 4.6 m (Elev. 74.5 m) below ground surface. 2. Water level measured in open borehole at a depth of about 3.8 m (Elev. 75.4 m) below ground surface prior to rock coring.																

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+<sup>3</sup>, ×<sup>3</sup>: Numbers refer to Sensitivity      ○ 3% STRAIN AT FAILURE



**RECORD OF BOREHOLE No CRB-5**      SHEET 1 OF 2      **METRIC**

PROJECT 1662333

G.W.P. 2002-13-00      LOCATION N 4824128.9; E 295914.2 MTM NAD 83 ZONE 10 (LAT. 43.557044; LONG. -79.609986)      ORIGINATED BY JL

DIST Central      HWY QEW      BOREHOLE TYPE CME 55, 203 mm O.D., 108 mm I.D. Hollow Stem Augers (Auto Hammer)      COMPILED BY KN

DATUM Geodetic      DATE February 13, 2018      CHECKED BY SMM

ELEV DEPTH	SOIL PROFILE DESCRIPTION	STRAT PLOT	SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W <sub>p</sub>	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W <sub>L</sub>	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)		
			NUMBER	TYPE	"N" VALUES			SHEAR STRENGTH kPa										WATER CONTENT (%)	
							20	40	60	80	100								
79.2	GROUND SURFACE																		
0.0	Silty sand, some gravel, contains rootlets (FILL) Loose Brown Wet		1	SS	6														
78.5	Clayey silt with sand, trace to some gravel, contains rootlets / organics. contains clayey silt pockets and shale fragments (FILL) Very stiff Brown and grey Moist/frozen		2	SS	25														
0.7			3	SS	23														
				4A	SS	6													
76.8	Silty SAND to SILT and SAND, trace gravel, trace clay, trace organics, contains clayey silt pockets and rootlets Very loose to loose Brown to grey Moist to wet		4B	SS	6														
2.4			5	SS	4														
				6	SS	0													
				7A	SS	1													
74.5	ORGANIC CLAYEY SILT with SAND, trace gravel Very soft to firm Brown Moist		7B	SS	1														
4.7			8A	SS	5														
73.5	Silty SAND, trace to some gravel, trace clay, contains clayey silt pockets, contains wood fragments Loose Grey Wet		8B	SS	4														
5.7			9	SS	4														
				10A	SS	73													
72.0	SHALE (BEDROCK) Grey Bedrock cored from a depth of 7.2 m to 15.5 m  For bedrock coring details, refer to Record of Drillhole CRB-5		10B	RC	53%														
7.2			1	RC													RQD = 0%		
				2	RC	51%												RQD = 13%	
				3	RC	100%													RQD = 99%
				4	RC	100%													RQD = 73%
				5	RC	97%													RQD = 78%
			6	RC	100%													RQD = 99%	

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 +<sup>3</sup>, ×<sup>3</sup>: Numbers refer to Sensitivity      ○ 3% STRAIN AT FAILURE

PROJECT <u>1662333</u>	<b>RECORD OF BOREHOLE No CRB-5</b>	SHEET 2 OF 2	<b>METRIC</b>
G.W.P. <u>2002-13-00</u>	LOCATION <u>N 4824128.9; E 295914.2 MTM NAD 83 ZONE 10 (LAT. 43.557044; LONG. -79.609986)</u>	ORIGINATED BY <u>JL</u>	
DIST <u>Central</u> HWY <u>QEW</u>	BOREHOLE TYPE <u>CME 55, 203 mm O.D., 108 mm I.D. Hollow Stem Augers (Auto Hammer)</u>	COMPILED BY <u>KN</u>	
DATUM <u>Geodetic</u>	DATE <u>February 13, 2018</u>	CHECKED BY <u>SMM</u>	

ELEV DEPTH	SOIL PROFILE DESCRIPTION	STRAT PLOT	SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W <sub>p</sub>	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W <sub>L</sub>	UNIT WEIGHT <b>γ</b> kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
			NUMBER	TYPE	"N" VALUES			20	40	60	80	100					
63.7	SHALE (BEDROCK) Grey		6	RC	REC 100%		64										
15.5	END OF BOREHOLE  NOTES:  1. Water level encountered during drilling at a depth of about 3.7 m (Elev. 75.5 m) below ground surface.  2. Water level measured in open borehole at a depth of about 4.3 m (Elev. 74.9 m) below ground surface prior to rock coring.																

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+<sup>3</sup>, ×<sup>3</sup>: Numbers refer to Sensitivity      ○ 3% STRAIN AT FAILURE

PROJECT: 1662333

# RECORD OF DRILLHOLE: CRB-5

SHEET 1 OF 1

LOCATION: N 4824128.9 ; E 295914.2

DRILLING DATE: February 13, 2018

DATUM: Geodetic

INCLINATION: -90° AZIMUTH: ---

DRILL RIG: CME 55 Track

DRILLING CONTRACTOR: Geo-Environmental Drilling

DEPTH SCALE METRES	DRILLING RECORD	DESCRIPTION	SYMBOLIC LOG	ELEV. (m)	RUN No.	RECOVERY		R.Q.D. %	FRACT. INDEX PER 0.25 m	DISCONTINUITY DATA				ROCK STRENGTH INDEX				WEATHERING INDEX				FEATURES	ROFT ZONES	NOTES WATER LEVELS INSTRUMENTATION		
						TOTAL CORE %	SOLID CORE %			TYPE AND SURFACE DESCRIPTION		Jr	R4	R3	R2	R1	W1	W2	W3	W4	W5				W6	
						○	○			B Angle	DIP w.r.t. CORE AXIS	Ja	Ja	Ja	Ja	Ja	Ja	Ja	Ja	Ja	Ja				Ja	
		Continued from Borehole CRB-5		72.02																						
8		Highly weathered, thinly laminated to medium bedded, brown to grey, very fine to fine grained, faintly porous, very weak SHALE (Georgian Bay Formation)		71.38	1					BD,UN,SM	CC, CI	2	4												R0	
		Slightly weathered to fresh, thinly laminated to medium bedded, grey, very fine to fine grained, faintly porous, weak SHALE (Georgian Bay Formation) with LIMESTONE interbeds		7.82	2					BD,UN,RO	PC, CI	3	3												R1	
9										JN,UN,SM	SA, CI	1	2												PLT(D) = 0.76 MPa PLT(A) = 0.37 MPa	
10		Slightly weathered to fresh, thinly to medium bedded, grey, fine grained, faintly porous, very weak to weak SHALE (Georgian Bay Formation) with LIMESTONE interbeds			3					JN,PL,SM	SA, CI	1	2												PLT(A) = 1.45 MPa	
11	HQ Core																									R1
12					4					CO,UN,SM	CL	2	1													
										CO,UN,SM	SA, CI	2	2													
										JN,IR,SM	SA, CI	2	2													
										CO,UN,SM	CC, CI	2	4													
										BD,UN,SM	CC, CI	2	4													
										BD,UN,SM	CC, CI	2	2													R0
13					5					BD,UN,SM	CL	2	2													R1
										JN,PL,SM	SA, CI	1	2													
										CO,UN,SM	CC, CI	2	4													
										BD,UN,SM	IN, CI	2	2													
										CO,UN,SM	SA, CI	2	2													PLT(D) = 0.07 MPa
										JN,IR,SM	SA, CI	2	2													
										CO,UN,SM	SA, CI	2	2													UC = 18.6 MPa
14										BD,UN,SM	IN, CI	2	6													
																										PLT(D) = 0.52 MPa PLT(A) = 0.27 MPa
15					6																					
16		END OF DRILLHOLE		63.68																						
				15.52																						

### FEATURES LEGEND



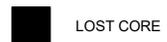
BROKEN CORE



CLAY SEAM



LIMESTONE



LOST CORE

DEPTH SCALE

1 : 50



LOGGED: JL

CHECKED: DM

GTA-RCK 054 - S:\CLIENTS\MTQ\QEW-CREDIT\_RIVER\GPJ GAL-MISS.GDT 1/9/19

PROJECT 1662333 **RECORD OF BOREHOLE No CRB-5A** SHEET 1 OF 2 **METRIC**  
 G.W.P. 2002-13-00 LOCATION N 4824130.9; E 295910.6 MTM NAD 83 ZONE 10 (LAT. 43.557062; LONG. -79.610032) ORIGINATED BY JL  
 DIST Central HWY QEW BOREHOLE TYPE CME 55, 159 mm O.D., 70 mm I.D. Hollow Stem Augers (Auto Hammer) COMPILED BY KN  
 DATUM Geodetic DATE February 15 and 16, 2018 CHECKED BY SMM

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC NATURAL LIQUID LIMIT			UNIT WEIGHT $\gamma$	REMARKS & GRAIN SIZE DISTRIBUTION (%)				
ELEV DEPTH	DESCRIPTION	NUMBER	TYPE	"N" VALUES			20	40	60	80	100			W <sub>p</sub>	W	W <sub>L</sub>	GR
79.3	GROUND SURFACE																
0.0	Clayey silt with sand, trace to some gravel, contains organics / rootlets, contains wood fragments. contains shale fragments with limestone (FILL) Firm to hard Brown to grey Moist to wet	1	SS	7													
		2	SS	25													
		3	SS	31													
		4	SS	16													
		5	SS	12													
75.3		6A	SS	7													
4.0	Silty SAND, trace rootlets and wood fragments Loose Brown Wet	6B	SS	7													
74.8																	
4.5	ORGANIC CLAYEY SILT, some sand, contains sand lenses, wood fragments and shell fragments Very soft to firm Brown Moist to wet	7	SS	1													
72.9		8A	SS	7													
6.4	Silty SAND, trace clay, contains shell fragments and rootlets Loose Grey Wet	8B	SS	7													
72.1																	
7.2	SHALE (BEDROCK) Grey	9	SS	100000													
	Bedrock cored from a depth of 7.7 m to 17.2 m	1	RC	REC 100%													RQD = 0%
	For bedrock coring details, refer to Record of Drillhole CRB-5A	2	RC	REC 13%													RQD = 4%
		3	RC	REC 100%													RQD = 69%
		4	RC	REC 100%													RQD = 81%
		5	RC	REC 100%													RQD = 95%
		6	RC	REC 100%													RQD = 95%

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 +<sup>3</sup>, ×<sup>3</sup>: Numbers refer to Sensitivity      ○ 3% STRAIN AT FAILURE

PROJECT <u>1662333</u>	<b>RECORD OF BOREHOLE No CRB-5A</b>	SHEET 2 OF 2	<b>METRIC</b>
G.W.P. <u>2002-13-00</u>	LOCATION <u>N 4824130.9; E 295910.6 MTM NAD 83 ZONE 10 (LAT. 43.557062; LONG. -79.610032)</u>	ORIGINATED BY <u>JL</u>	
DIST <u>Central</u> HWY <u>QEW</u>	BOREHOLE TYPE <u>CME 55, 159 mm O.D., 70 mm I.D. Hollow Stem Augers (Auto Hammer)</u>	COMPILED BY <u>KN</u>	
DATUM <u>Geodetic</u>	DATE <u>February 15 and 16, 2018</u>	CHECKED BY <u>SMM</u>	

ELEV DEPTH	SOIL PROFILE DESCRIPTION	STRAT PLOT	SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W <sub>p</sub>	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W <sub>L</sub>	UNIT WEIGHT $\gamma$ kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL										
			NUMBER	TYPE	"N" VALUES			20	40	60	80	100						20	40	60	80	100	10	20	30		
62.1	SHALE (BEDROCK) Grey		6	RC	REC 100%		64										RQD = 95%										
17.2	Bedrock cored from a depth of 7.7 m to 17.2 m  For bedrock coring details, refer to Record of Drillhole CRB-5A		7	RC	REC 100%		63										RQD = 100%										
	END OF BOREHOLE																										
	NOTES:  1. Water level encountered during drilling at a depth of about 4.0 m (Elev. 75.3 m) below ground surface.  2. Water level measured in open borehole at a depth of about 3.6 m (Elev. 75.7 m) below ground surface prior to rock coring.  3. Groundwater level measurements in piezometer:  <table style="margin-left: 20px;"> <tr> <td>Date</td> <td>Depth (m)</td> <td>Elev. (m)</td> </tr> <tr> <td>12/03/18</td> <td>1.6</td> <td>77.7</td> </tr> <tr> <td>30/04/18</td> <td>4.0</td> <td>75.3</td> </tr> <tr> <td>06/11/18</td> <td>4.6</td> <td>74.8</td> </tr> </table>	Date	Depth (m)	Elev. (m)	12/03/18	1.6	77.7	30/04/18	4.0	75.3	06/11/18	4.6	74.8														
Date	Depth (m)	Elev. (m)																									
12/03/18	1.6	77.7																									
30/04/18	4.0	75.3																									
06/11/18	4.6	74.8																									

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+<sup>3</sup>, ×<sup>3</sup>: Numbers refer to Sensitivity      ○ 3% STRAIN AT FAILURE





PROJECT <u>1662333</u>	<b>RECORD OF BOREHOLE No CRB-6</b>	SHEET 1 OF 2	<b>METRIC</b>
G.W.P. <u>2002-13-00</u>	LOCATION <u>N 4824196.7; E 295929.5 MTM NAD 83 ZONE 10 (LAT. 43.557650; LONG. -79.609801)</u>	ORIGINATED BY <u>JL</u>	
DIST <u>Central</u> HWY <u>QEW</u>	BOREHOLE TYPE <u>CME 850, 210 mm O.D. Hollow Stem Augers, HQ Casing (Auto Hammer)</u>	COMPILED BY <u>MPL</u>	
DATUM <u>Geodetic</u>	DATE <u>October 18-20, 2017</u>	CHECKED BY <u>SMM</u>	

ELEV DEPTH	SOIL PROFILE DESCRIPTION	STRAT PLOT	SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W <sub>p</sub>	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W <sub>L</sub>	UNIT WEIGHT γ kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
			NUMBER	TYPE	"N" VALUES			SHEAR STRENGTH kPa									
							20 40 60 80 100	○ UNCONFINED + FIELD VANE ● QUICK TRIAXIAL × REMOULDED									
							20 40 60 80 100	WATER CONTENT (%)					10 20 30				
91.7	GROUND SURFACE																
0.0	Silty sand, trace to some gravel, trace clay, contains brick fragments (FILL) Loose to compact Brown Moist		1	SS	11												
			2	SS	5											7 67 24 2	
90.0			3A	SS	5												
1.7	Sandy CLAYEY SILT, trace to some gravel Firm to stiff brown Moist to wet - Mottled brown-grey below a depth of about 2.3 m		3B														
			4	SS	7												
			5	SS	9												
	- Becoming gravelly at a depth of about 3.7 m - Auger grinding at a depth of about 3.7 m		6	SS	5											10 26 44 20	
87.3																	
4.4	Sandy CLAYEY SILT, containing shale fragments (RESIDUAL SOIL) Hard Grey Moist		7	SS	50/0.13												
86.9	SHALE (BEDROCK) Grey		1	RC	REC 86%											RQD = 47%	
4.8	Bedrock cored from a depth of 5.1 m to 13.3 m  For bedrock coring details, refer to Record of Drillhole CRB-6		2	RC	REC 100%											RQD = 95%	
			3	RC	REC 100%											RQD = 100%	
			4	RC	REC 100%											RQD = 95%	
			5	RC	REC 100%											RQD = 100%	
			6	RC	REC 96%											RQD = 96%	
78.4																	
13.3	END OF BOREHOLE																

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 +<sup>3</sup>, ×<sup>3</sup>: Numbers refer to Sensitivity      ○ 3% STRAIN AT FAILURE

PROJECT <u>1662333</u>	<b>RECORD OF BOREHOLE No CRB-6</b>	SHEET 2 OF 2	<b>METRIC</b>
G.W.P. <u>2002-13-00</u>	LOCATION <u>N 4824196.7; E 295929.5 MTM NAD 83 ZONE 10 (LAT. 43.557650; LONG. -79.609801)</u>	ORIGINATED BY <u>JL</u>	
DIST <u>Central</u> HWY <u>QEW</u>	BOREHOLE TYPE <u>CME 850, 210 mm O.D. Hollow Stem Augers, HQ Casing (Auto Hammer)</u>	COMPILED BY <u>MPL</u>	
DATUM <u>Geodetic</u>	DATE <u>October 18-20, 2017</u>	CHECKED BY <u>SMM</u>	

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W <sub>p</sub>	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W <sub>L</sub>	UNIT WEIGHT <b>γ</b> kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL															
ELEV DEPTH	DESCRIPTION	STRAT PLOT NUMBER	TYPE	"N" VALUES			20	40	60	80	100						20	40	60	80	100										
--- CONTINUED FROM PREVIOUS PAGE ---																															
	NOTES: 1. Borehole dry prior to rock coring. 2. Water level measured in standpipe piezometer: <table style="margin-left: 20px; border-collapse: collapse;"> <tr> <td style="padding-right: 10px;">Date</td> <td style="padding-right: 10px;">Depth (m)</td> <td>Elev. (m)</td> </tr> <tr> <td>12/11/17</td> <td>5.6</td> <td>86.0</td> </tr> <tr> <td>12/03/18</td> <td>5.0</td> <td>86.7</td> </tr> <tr> <td>30/04/18</td> <td>4.9</td> <td>86.8</td> </tr> <tr> <td>06/11/18</td> <td>4.9</td> <td>86.8</td> </tr> </table>	Date	Depth (m)	Elev. (m)	12/11/17	5.6	86.0	12/03/18	5.0	86.7	30/04/18	4.9	86.8	06/11/18	4.9	86.8															
Date	Depth (m)	Elev. (m)																													
12/11/17	5.6	86.0																													
12/03/18	5.0	86.7																													
30/04/18	4.9	86.8																													
06/11/18	4.9	86.8																													

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+<sup>3</sup>, ×<sup>3</sup>: Numbers refer to Sensitivity      ○ 3% STRAIN AT FAILURE



**PROJECT** 1662333 **RECORD OF BOREHOLE No CRB-7** **SHEET 1 OF 2** **METRIC**  
**G.W.P.** 2002-13-00 **LOCATION** N 4824189.6; E 295951.1 MTM NAD 83 ZONE 10 (LAT. 43.557590; LONG. -79.609531) **ORIGINATED BY** JL  
**DIST** Central **HWY** QEW **BOREHOLE TYPE** CME 850, 210 mm O.D. Hollow Stem Augers, HQ Casing (Auto Hammer) **COMPILED BY** MPL  
**DATUM** Geodetic **DATE** October 23, 2017 **CHECKED BY** SMM

SOIL PROFILE		STRAT PLOT	SAMPLES		GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC NATURAL LIQUID LIMIT			UNIT WEIGHT $\gamma$	REMARKS & GRAIN SIZE DISTRIBUTION (%)
ELEV DEPTH	DESCRIPTION		NUMBER	TYPE			"N" VALUES	20 40 60 80 100	20 40 60 80 100	W <sub>p</sub>	W		
94.7	GROUND SURFACE												
0.0	TOPSOIL (180mm)												
0.2	Silt and sand, trace gravel, trace clay (FILL) Loose to compact Brown Moist		1	SS	8								
			2	SS	9								
			3	SS	12								
			4	SS	19								
	- Becoming wet at a depth of about 2.6 m		5	SS	21								
			6A	SS	54								
	- Brick fragments at a depth of about 4.0 m		6B										
90.2			7	SS	26								
4.5	Sandy SILT, trace clay Compact Brown Wet - Clayey silt layer between 4.6 m to 4.7 m - Becoming grey at a depth of about 4.9 m		8	SS	25								
			9A	SS	17								
			9B										
			9C										
88.2	- Clayey silt layer between 6.4 m and 6.5 m		10	SS	10								
6.5	CLAYEY SILT with SAND, trace gravel (TILL) Stiff to hard Grey Moist		11	SS	50/0.15								
86.9			1	RC	REC 79%								
86.6	Sandy CLAYEY SILT, containing shale fragments (RESIDUAL SOIL) Hard Grey Moist		2	RC	REC 100%								
8.1	SHALE (BEDROCK) Grey Bedrock cored from a depth of 8.5 m to 16.0 m		3	RC	REC 100%								
	For bedrock coring details, refer to Record of Drillhole CRB-7		4	RC	REC 100%								
			5	RC	REC 100%								

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 +<sup>3</sup>, ×<sup>3</sup>: Numbers refer to Sensitivity      ○ 3% STRAIN AT FAILURE

PROJECT <u>1662333</u>	<b>RECORD OF BOREHOLE No CRB-7</b>	SHEET 2 OF 2	<b>METRIC</b>
G.W.P. <u>2002-13-00</u>	LOCATION <u>N 4824189.6; E 295951.1 MTM NAD 83 ZONE 10 (LAT. 43.557590; LONG. -79.609531)</u>	ORIGINATED BY <u>JL</u>	
DIST <u>Central</u> HWY <u>QEW</u>	BOREHOLE TYPE <u>CME 850, 210 mm O.D. Hollow Stem Augers, HQ Casing (Auto Hammer)</u>	COMPILED BY <u>MPL</u>	
DATUM <u>Geodetic</u>	DATE <u>October 23, 2017</u>	CHECKED BY <u>SMM</u>	

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT    NATURAL MOISTURE CONTENT    LIQUID LIMIT			UNIT WEIGHT $\gamma$ kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%)					
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20	40	60	80	100	W <sub>p</sub>	W			W <sub>L</sub>	10	20	30	GR
78.7	SHALE (BEDROCK) Grey		5	RC	REC 100%																RQD = 100%
16.0	END OF BOREHOLE  NOTE:  1. Borehole dry prior to rock coring.		6	RC	REC 100%	79															RQD = 100%

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+<sup>3</sup>, ×<sup>3</sup>: Numbers refer to Sensitivity      ○ 3% STRAIN AT FAILURE



**PROJECT** 1662333 **RECORD OF BOREHOLE No CRB-8** SHEET 1 OF 1 **METRIC**  
**G.W.P.** 2002-13-00 **LOCATION** N 4824211.5; E 295953.7 MTM NAD 83 ZONE 10 (LAT. 43.557788; LONG. -79.609499) **ORIGINATED BY** JL  
**DIST** Central **HWY** QEW **BOREHOLE TYPE** CME 850, 210 mm O.D. Hollow Stem Augers (Auto Hammer) **COMPILED BY** MPL  
**DATUM** Geodetic **DATE** October 17, 2017 **CHECKED BY** SMM

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W <sub>p</sub>	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W <sub>L</sub>	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)							
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	SHEAR STRENGTH kPa									WATER CONTENT (%)						
						20	40	60	80	100	20	40	60	80	100	10	20	30	GR	SA	SI	CL	
94.7	GROUND SURFACE																						
8.9	TOPSOIL (80 mm)																						
	Sand, some silt, trace clay (FILL) Very loose to compact Brown Moist		1	SS	3																		
			2	SS	12																		
93.3																							
1.5	SAND, some silt, trace clay Compact to dense Brown Moist		3	SS	21																		
			4	SS	44																		
			5	SS	35																		
	- Becoming wet below a depth of about 3.1 m - Clayey silt pockets at a depth of about 3.1 m																						
91.0																							
3.7	SILT, trace to some sand, trace to some clay Slight plasticity Dense to very dense Grey Wet		6	SS	67																		
			7	SS	32																		
	- Becoming grey and brown at a depth of about 5.6 m																						
88.3																							
6.4	CLAYEY SILT, some sand Very stiff Grey Wet		8A 8B	SS	22																		
87.1																							
7.6	Sandy CLAYEY SILT with shale fragments (RESIDUAL SOIL) Hard Grey Moist		9A 9B	SS	50/0.13																		
86.7																							
8.1																							
86.2																							
8.5	- Auger grinding at a depth of about 7.6 m SHALE (BEDROCK) Grey END OF BOREHOLE - SPLIT-SPOON REFUSAL		10	SS	50/0.08																		

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NOTE:  
1. Water level measured at a depth of about 1.5 m (Elev. 93.2 m) below ground surface upon completion of drilling.

+<sup>3</sup>, ×<sup>3</sup>: Numbers refer to Sensitivity      ○ 3% STRAIN AT FAILURE

PROJECT 1662333	<b>RECORD OF BOREHOLE No NW3-1</b>	SHEET 1 OF 2	<b>METRIC</b>
G.W.P. 2002-13-00	LOCATION N 4824275.8; E 295959.8 MTM NAD 83 ZONE 10 (LAT. 43.558358; LONG. -79.609422)	ORIGINATED BY JL	
DIST Central HWY QEW	BOREHOLE TYPE CME 850, 210 mm O.D. Hollow Stem Augers	COMPILED BY MPL	
DATUM Geodetic	DATE October 16-17, 2017	CHECKED BY SMM	

ELEV DEPTH	SOIL PROFILE DESCRIPTION	STRAT PLOT	SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W <sub>p</sub>	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W <sub>L</sub>	UNIT WEIGHT γ kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%)
			NUMBER	TYPE	"N" VALUES			20	40					
96.5	GROUND SURFACE													
0.0	TOPSOIL (150mm)													
0.2	Silty sand, trace clay (FILL) Loose Brown Moist		1	SS	5		96							0 64 33 3
95.0			2	SS	5		95							
1.5	SILT and SAND to silty SAND, trace clay, trace gravel Compact to very dense Brown Moist to wet		3	SS	22		94							0 70 28 2
	- Silt pocket at a depth of about 2.6 m		4	SS	24		93							
	- Becoming wet at a depth of about 3.7 m		5	SS	22		92							
			6	SS	24		91							
			7	SS	47		90							
	- Becoming grey at a depth of about 6.3 m		8	SS	78		89							5 34 59 2
89.3	SILTY CLAY, trace to some sand, trace gravel Soft Grey Wet		9	SS	4		88							
87.8	Sandy CLAYEY SILT, trace to some gravel (TILL) Stiff Grey Moist to wet		10	SS	12		87							10 29 45 16
86.4	Sandy gravelly CLAYEY SILT, some shale fragments (RESIDUAL SOIL) Hard Grey Moist to wet - Tricone grinding at a depth of about 10.1 m		11	SS	64		86							
84.7	- Tricone grinding at a depth of about 11.6 m		12	SS	100/0.06		85							
11.8	Shale (BEDROCK) Grey		1	RC	REC 100%		84							RQD = 97%
	Bedrock cored from a depth of 11.8 m to 15.4 m		2	RC	REC 96%		83							RQD = 90%
	For bedrock coring details, refer to Record of Drillhole NW3-01		3	RC	REC 97%		82							RQD = 97%

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 +<sup>3</sup>, ×<sup>3</sup>: Numbers refer to Sensitivity      ○ 3% STRAIN AT FAILURE

PROJECT <u>1662333</u>	<b>RECORD OF BOREHOLE No NW3-1</b>	SHEET 2 OF 2	<b>METRIC</b>
G.W.P. <u>2002-13-00</u>	LOCATION <u>N 4824275.8; E 295959.8 MTM NAD 83 ZONE 10 (LAT. 43.558358; LONG. -79.609422)</u>	ORIGINATED BY <u>JL</u>	
DIST <u>Central</u> HWY <u>QEW</u>	BOREHOLE TYPE <u>CME 850, 210 mm O.D. Hollow Stem Augers</u>	COMPILED BY <u>MPL</u>	
DATUM <u>Geodetic</u>	DATE <u>October 16-17, 2017</u>	CHECKED BY <u>SMM</u>	

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC NATURAL LIQUID LIMIT MOISTURE LIMIT CONTENT			UNIT WEIGHT $\gamma$ kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20	40	60	80	100	W <sub>p</sub>	W		
81.1	--- CONTINUED FROM PREVIOUS PAGE ---		3	RC	REC 97%											
15.4	END OF BOREHOLE  NOTES: 1. Water level measured at a depth of about 4.5 m (Elev. 92.0 m) below ground surface prior to start of rock coring.  2. Water level measured at top of casing (Elev. 96.9 m) following completion of bedrock coring.															

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+<sup>3</sup>, X<sup>3</sup>: Numbers refer to Sensitivity      ○ 3% STRAIN AT FAILURE



PROJECT <u>1662333</u>	<b>RECORD OF BOREHOLE No SWME-1</b>	SHEET 1 OF 1	<b>METRIC</b>
G.W.P. <u>2002-13-00</u>	LOCATION <u>N 4824195.5; E 295896.6 MTM NAD 83 ZONE 10 (LAT. 43.557643; LONG. -79.610206)</u>	ORIGINATED BY <u>ACM</u>	
DIST <u>Central</u> HWY <u>QEW</u>	BOREHOLE TYPE <u>CME 55, 210 mm O.D., Hollow Stem Augers</u>	COMPILED BY <u>CC</u>	
DATUM <u>Geodetic</u>	DATE <u>July 31, 2018</u>	CHECKED BY <u>SMM</u>	

ELEV DEPTH	SOIL PROFILE DESCRIPTION	STRAT PLOT	SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W <sub>p</sub>	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W <sub>L</sub>	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)
			NUMBER	TYPE	"N" VALUES			SHEAR STRENGTH kPa									
							20	40	60	80	100						
							○ UNCONFINED	+ FIELD VANE			○						
							● QUICK TRIAXIAL	× REMOULDED			○						
							20	40	60	80	100	10	20	30			
89.5	GROUND SURFACE																
0.0	Sand and gravel (FILL) Loose Brown grey Moist		1	SS	7												
88.8																	
0.7	Silt and sand, trace clay, trace gravel (FILL) Very loose Brown Moist		2	SS	4											1 64 30 5	
88.1																	
1.7	Clayey silt, trace to some sand (FILL), oxidation staining Grey Moist		3	SS	7												
	SAND, some silt, trace clay, trace rootlets Very loose to loose Brown to dark brown Moist		4	SS	3											0 77 19 4	
86.5																	
3.0	- organics between depths of 2.6 m and 2.9 m		5A	SS	8												
85.8			5B														
3.7	SILTY CLAY, some sand, trace gravel, trace organics Firm to very stiff Grey brown Moist		6	SS	28												
84.8																	
4.7	CLAYEY SILT, some gravel, some shale fragments (RESIDUAL SOIL) Hard Grey Moist		7	SS	50/0.10												
84.0																	
84.0			8	SS	50/0.13												
5.5	SHALE (BEDROCK) Grey END OF BOREHOLE SPLIT-SPOON REFUSAL  NOTE: 1. Open borehole dry upon completion of drilling.																

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+<sup>3</sup>, ×<sup>3</sup>: Numbers refer to Sensitivity      ○ 3% STRAIN AT FAILURE

PROJECT <u>1662333</u>	<b>RECORD OF BOREHOLE No SWME-2</b>	SHEET 1 OF 1	<b>METRIC</b>
G.W.P. <u>2002-13-00</u>	LOCATION <u>N 4824204.6; E 295881.3 MTM NAD 83 ZONE 10 (LAT. 43.557725; LONG. -79.610395)</u>	ORIGINATED BY <u>ACM</u>	
DIST <u>Central</u> HWY <u>QEW</u>	BOREHOLE TYPE <u>CME 55, 210 mm O.D., Hollow Stem Augers</u>	COMPILED BY <u>CC</u>	
DATUM <u>Geodetic</u>	DATE <u>July 27, 2018</u>	CHECKED BY <u>SMM</u>	

ELEV DEPTH	SOIL PROFILE DESCRIPTION	STRAT PLOT	SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W <sub>p</sub>	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W <sub>L</sub>	UNIT WEIGHT γ kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
			NUMBER	TYPE	"N" VALUES			20	40	60	80	100					
87.4	GROUND SURFACE																
0.0	TOPSOIL (500 mm) Soft		1	SS	3		87										
86.9																	
0.5	CLAYEY SILT with SAND, some gravel Firm Brown Moist		2	SS	7		86										20 31 34 15
85.9	- Trace to some rootlets, organics, wood, tree fragments from 0.8 m to 1.4 m																
1.5			3	SS	46												
85.2	CLAYEY SILT, trace to some sand, some shale fragments (RESIDUAL SOIL) Hard Brown Moist		4	SS	50/0.15		85										
2.2																	
84.3	SHALE (BEDROCK) Grey		5	SS	50/0.08												
3.1	END OF BOREHOLE SPLIT-SPOON REFUSAL																
	NOTE:  1. Open borehole dry upon completion of drilling.																

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+<sup>3</sup>, ×<sup>3</sup>: Numbers refer to Sensitivity      ○ 3% STRAIN AT FAILURE

PROJECT <u>1662333</u>	<b>RECORD OF BOREHOLE No SWME-3</b>	SHEET 1 OF 1	<b>METRIC</b>
G.W.P. <u>2002-13-00</u>	LOCATION <u>N 4824227.3; E 295901.0 MTM NAD 83 ZONE 10 (LAT. 43.557930; LONG. -79.610152)</u>	ORIGINATED BY <u>ACM</u>	
DIST <u>Central</u> HWY <u>QEW</u>	BOREHOLE TYPE <u>CME 55, 210 mm O.D., Hollow Stem Augers</u>	COMPILED BY <u>CC</u>	
DATUM <u>Geodetic</u>	DATE <u>July 27, 2018</u>	CHECKED BY <u>SMM</u>	

ELEV DEPTH	SOIL PROFILE DESCRIPTION	STRAT PLOT	SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W <sub>p</sub>	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W <sub>L</sub>	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)
			NUMBER	TYPE	"N" VALUES			SHEAR STRENGTH kPa									
								20	40	60	80	100					
91.9	GROUND SURFACE																
0.0	Sandy silt to silty sand to, trace to some clay (FILL) Loose to compact Brown Moist - Some oxidation between depths of 0.6 m and 1.2 m		1	SS	6												
			2	SS	9												
			3	SS	12												
90.2																	
1.7	Sandy SILT, trace to some clay Loose Brown		4	SS	7												0 29 64 7
89.7	Moist																
2.2	SILT, some sand, trace to some clay Compact Grey Moist		5	SS	16												0 13 79 8
88.7																	
3.2	CLAYEY SILT, trace sand Firm Grey Moist		6A	SS	6												0 2 59 39
88.2			6B	SS	6												
3.7	CLAYEY SILT, trace gravel, trace sand (TILL) Firm to stiff Grey Moist to wet		7A	SS	14												
87.6			7B	SS	14												
4.5	CLAYEY SILT, some sand, some shale fragments (RESIDUAL SOIL) Grey Moist		8	SS	50/0.13												
86.5	SHALE (BEDROCK) Grey		9	SS	50/0.08												
5.4	END OF BOREHOLE SPLIT-SPOON REFUSAL																

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NOTE:

- Water level in open borehole at a depth of 5.3 m (Elev. 86.6 m) below ground surface upon completion of drilling.
- Groundwater level measurements in piezometer:
 

Date	Depth (m)	Elev. (m)
14/08/18	4.0	87.9
06/11/18	3.8	88.1

+<sup>3</sup>, ×<sup>3</sup>: Numbers refer to Sensitivity      ○ 3% STRAIN AT FAILURE

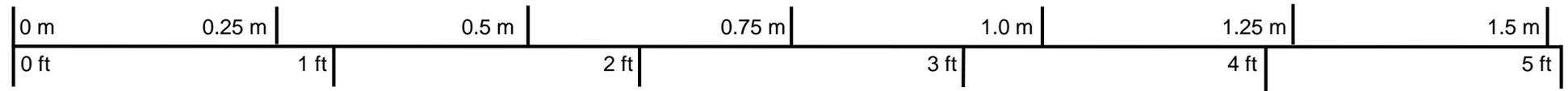
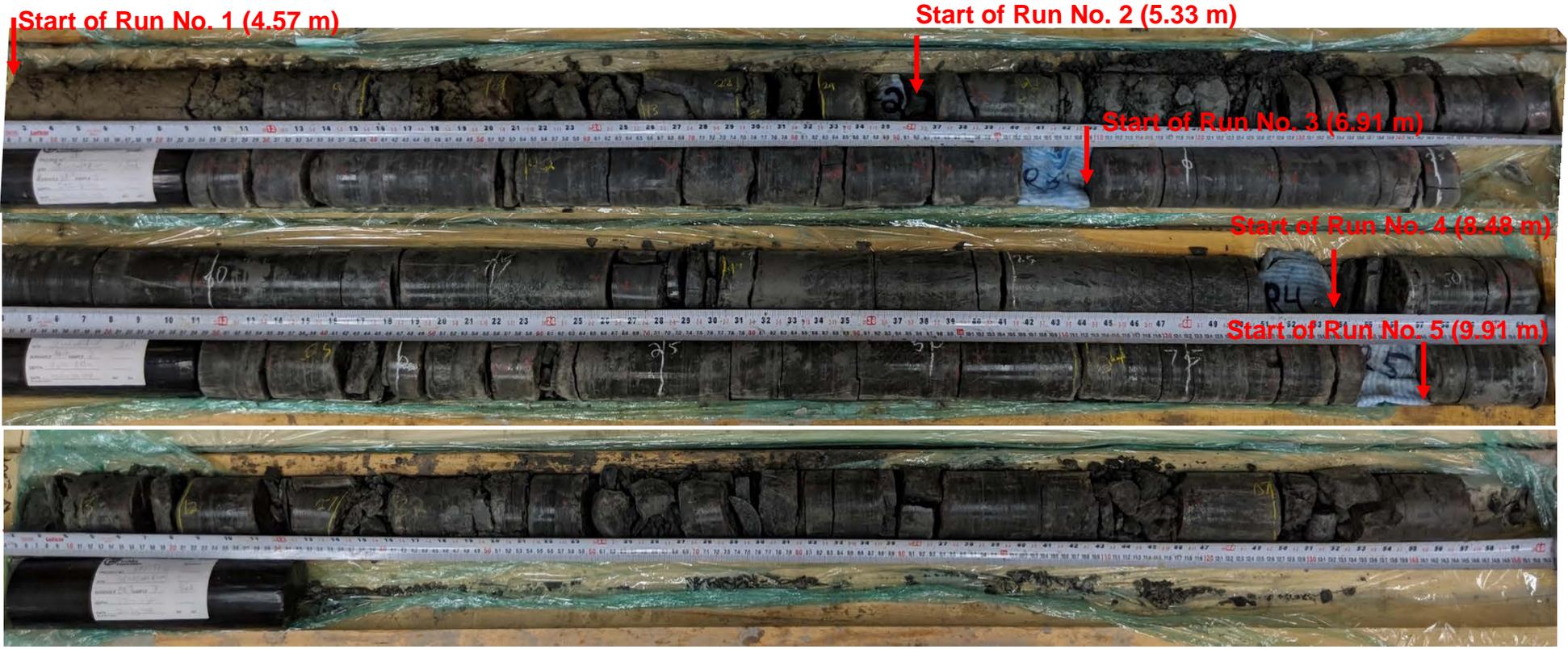
PROJECT 1662333	<b>RECORD OF BOREHOLE No SWME-4</b>	SHEET 1 OF 1	<b>METRIC</b>
G.W.P. 2002-13-00	LOCATION N 4824255.4; E 295917.6 MTM NAD 83 ZONE 10 (LAT. 43.558183; LONG. -79.609946)	ORIGINATED BY ACM	
DIST Central HWY QEW	BOREHOLE TYPE CME 55, 210 mm O.D., Hollow Stem Augers	COMPILED BY CC	
DATUM Geodetic	DATE July 27, 2018	CHECKED BY SMM	

ELEV DEPTH	SOIL PROFILE DESCRIPTION	STRAT PLOT	SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W <sub>p</sub>	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W <sub>L</sub>	UNIT WEIGHT γ kN/m <sup>3</sup>	REMARKS & GRAIN SIZE DISTRIBUTION (%)
			NUMBER	TYPE	"N" VALUES			20	40					
95.5	GROUND SURFACE													
0.0	TOPSOIL													
0.2	Silt and sand, trace to some clay, trace gravel (FILL)		1	SS	5									
94.8	Loose Brown Moist													
0.7	- Trace organics and rootlets to 0.6 m		2	SS	7									
	SILT and SAND, trace to some clay, trace gravel													
	Compact Brown to grey at 3.2 m		3	SS	25									
	Moist - Pockets of sand present between 1.6 m and 2.1 m													
	- Clayey silt interlayer between 3.0 m and 3.2 m													
			4	SS	34								1 50 42 7	
			5	SS	25									
91.8														
3.7	CLAYEY SILT, trace sand, trace gravel, some silt and sand interlayers		6	SS	17									
	Stiff Grey Moist													
			7	SS	9								1 13 60 26	
89.9														
5.6	SILT, trace to some sand, trace to some clay													
	Compact Grey Moist to wet		8	SS	19								0 11 82 7	
	- Pocket of sand from 6.1 m to 6.2 m													
87.9														
7.6	SILTY CLAY		9A	SS	13									
	Stiff Grey Moist													
87.4			9B											
8.1	CLAYEY SILT, some gravel, trace sand (TILL)													
	Very stiff Grey Moist													
86.5														
9.0	SHALE (BEDROCK)		10	SS	50/0.05									
	Grey													
	Bedrock cored from a depth of 10.0 m to 13.3 m.		11	SS	50/0.08									
	For bedrock coring details, refer to Record of Drillhole SWME-4.													
			1	RC	REC 100%								RQD = 80%	
			2	RC	REC 100%								RQD = 84%	
			3	RC	REC 100%								RQD = 94%	
82.2														
13.3	END OF BOREHOLE													
	NOTE:													
	1. Water level in open borehole at a depth of 7.6 m (Elev. 87.9) below ground surface prior to rock coring.													

GTA-MTO 001 S:\CLIENTS\MTQEQW-CREDIT\_RIVER\02\_DATA\INTQEQW-CREDIT\_RIVER\GPJ\_GAL-GTA.GDT 1/9/19

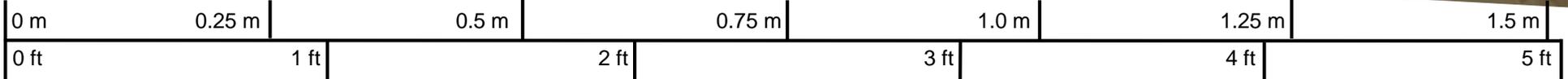
 +<sup>3</sup>, ×<sup>3</sup>: Numbers refer to Sensitivity      ○ 3% STRAIN AT FAILURE





Scale

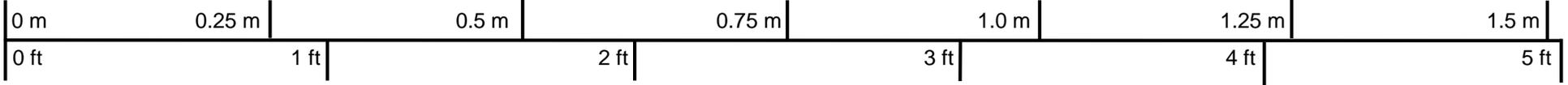
PROJECT	<b>MTO Assignment 2015-E-0033 QEW Widening Between Mississauga Road and Hurontario Street</b>					
TITLE	<b>Bedrock Core Photograph Borehole AR-2 (4.57 m to 11.60 m)</b>					
	PROJECT No. 1662333			FILE No. ----		
	DRAFT	SE	20180821	SCALE	AS SHOWN	VER. 1.
	CADD	--		<b>FIGURE A-1</b>		
	CHECK	SMM	20181116			
	REVIEW	JMAC	20181116			



Scale

PROJECT		<b>MTO Assignment 2015-E-0033 QEW Widening Between Mississauga Road and Hurontario Street</b>		
TITLE		<b>Bedrock Core Photograph Borehole CRB-4 (7.22 m to 15.31 m)</b>		
	PROJECT No. 1662333		FILE No. ----	
	DRAFT	JIL	Mar 2018	SCALE AS SHOWN
	CADD	--		VER. 1.
	CHECK	JMAC	11/14/2018	<b>FIGURE A-2</b>
REVIEW	SMM	11/14/2018		

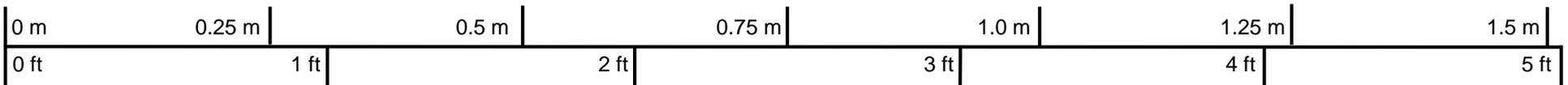
REVISION DATE: March 7, 2018 BY: JIL Project: 1662333



Scale

PROJECT		<b>MTO Assignment 2015-E-0033 QEW Widening Between Mississauga Road and Hurontario Street</b>			
TITLE		<b>Bedrock Core Photograph Borehole CRB-5 (7.18 m to 15.52 m)</b>			
	PROJECT No. 1662333		FILE No. ----		
	DRAFT	JIL	Mar 2018	SCALE	AS SHOWN
	CADD	--			VER. 1.
	CHECK	JMAC	11/14/2018	<b>FIGURE A-3</b>	
	REVIEW	SMM	11/14/2018		

REVISION DATE: March 7, 2018 BY: JIL Project: 1662333



Scale

PROJECT	<b>MTO Assignment 2015-E-0033 QEW Widening Between Mississauga Road and Hurontario Street</b>					
TITLE	<b>Bedrock Core Photograph Borehole CRB-5A (7.72 m to 17.16 m)</b>					
	PROJECT No. 1662333			FILE No. ----		
	DRAFT	JIL	Mar 2018	SCALE	AS SHOWN	VER. 1.
	CADD	--		<b>FIGURE A-4</b>		
	CHECK	JMAC	11/14/2018			
REVIEW	SMM	11/14/2018				

REVISION DATE: March 7, 2018 BY: JIL Project: 1662333

Start of Run No. 1 (5.12 m)

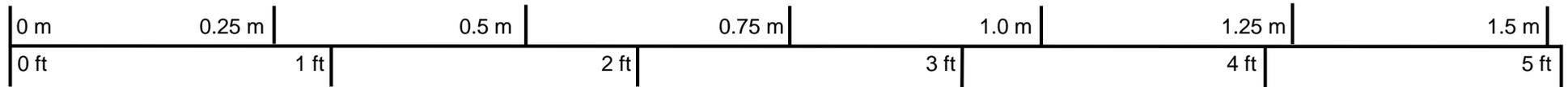
Start of Run No. 2 (6.28 m)

Start of Run No. 3 (7.8 m)

Start of Run No. 4 (9.32 m)

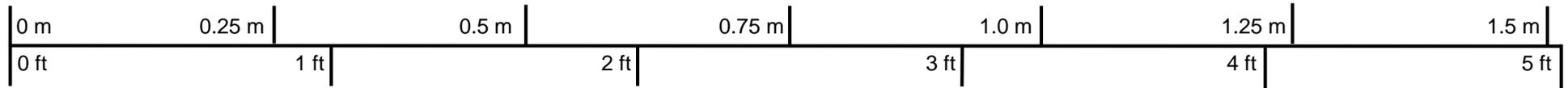
Start of Run No. 5 (10.84 m)

Start of Run No. 6 (12.36 m)



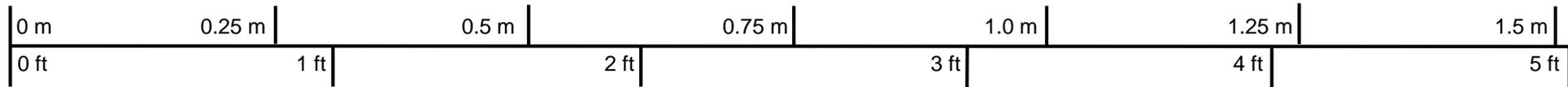
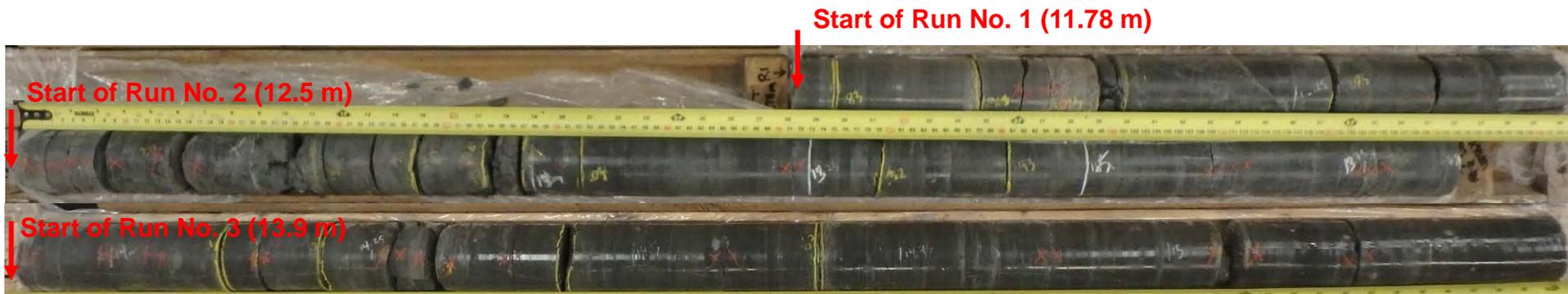
Scale

PROJECT		<b>MTO Assignment 2015-E-0033 QEW Widening Between Mississauga Road and Hurontario Street</b>				
TITLE		<b>Bedrock Core Photograph Borehole CRB-6 (5.12 m to 13.27 m)</b>				
	PROJECT No. 1662333			FILE No. ----		
	DRAFT	JIL	Mar 2018	SCALE	AS SHOWN	VER. 1.
	CADD	--		<b>FIGURE A-5</b>		
	CHECK	JMAC	11/14/2018			
REVIEW	SMM	11/14/2018				



Scale

PROJECT	<b>MTO Assignment 2015-E-0033 QEW Widening Between Mississauga Road and Hurontario Street</b>					
TITLE	<b>Bedrock Core Photograph Borehole CRB-7 (8.53 m to 16.04 m)</b>					
	PROJECT No. 1662333			FILE No. ----		
	DRAFT	JIL	Mar 2018	SCALE	AS SHOWN	VER. 1.
	CADD	--		<b>FIGURE A-6</b>		
	CHECK	JMAC	11/14/2018			
	REVIEW	SMM	11/14/2018			



Scale

PROJECT		<b>MTO Assignment 2015-E-0033 QEW Widening Between Mississauga Road and Hurontario Street</b>				
TITLE		<b>Bedrock Core Photograph Borehole NW3-1 (11.78 m to 15.42 m)</b>				
	PROJECT No. 1662333			FILE No. ----		
	DRAFT	SE	20180821	SCALE	AS SHOWN	VER. 1.
	CADD	--		<b>FIGURE A-7</b>		
	CHECK	JMAC	11/14/2018			
	REVIEW	SMM	11/14/2018			

Start of Run No. 1 (9.95 m)

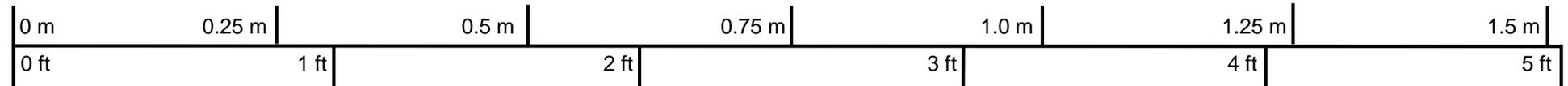
Start of Run No. 2 (11.23 m)



12.75 m

Start of Run No. 3 (12.75m)

13.26 m



Scale

PROJECT		<b>MTO Assignment 2015-E-0033 QEW Widening Between Mississauga Road and Hurontario Street</b>			
TITLE		<b>Bedrock Core Photograph Borehole SWME-4 (9.95 m to 13.26 m)</b>			
	PROJECT No. 1662333		FILE No. ----		
	DRAFT	JIL	20180307	SCALE	AS SHOWN
	CADD	--		VER.	1.
	CHECK	SMM	20181116	<b>FIGURE A-8</b>	
REVIEW	JMAC	20181116			

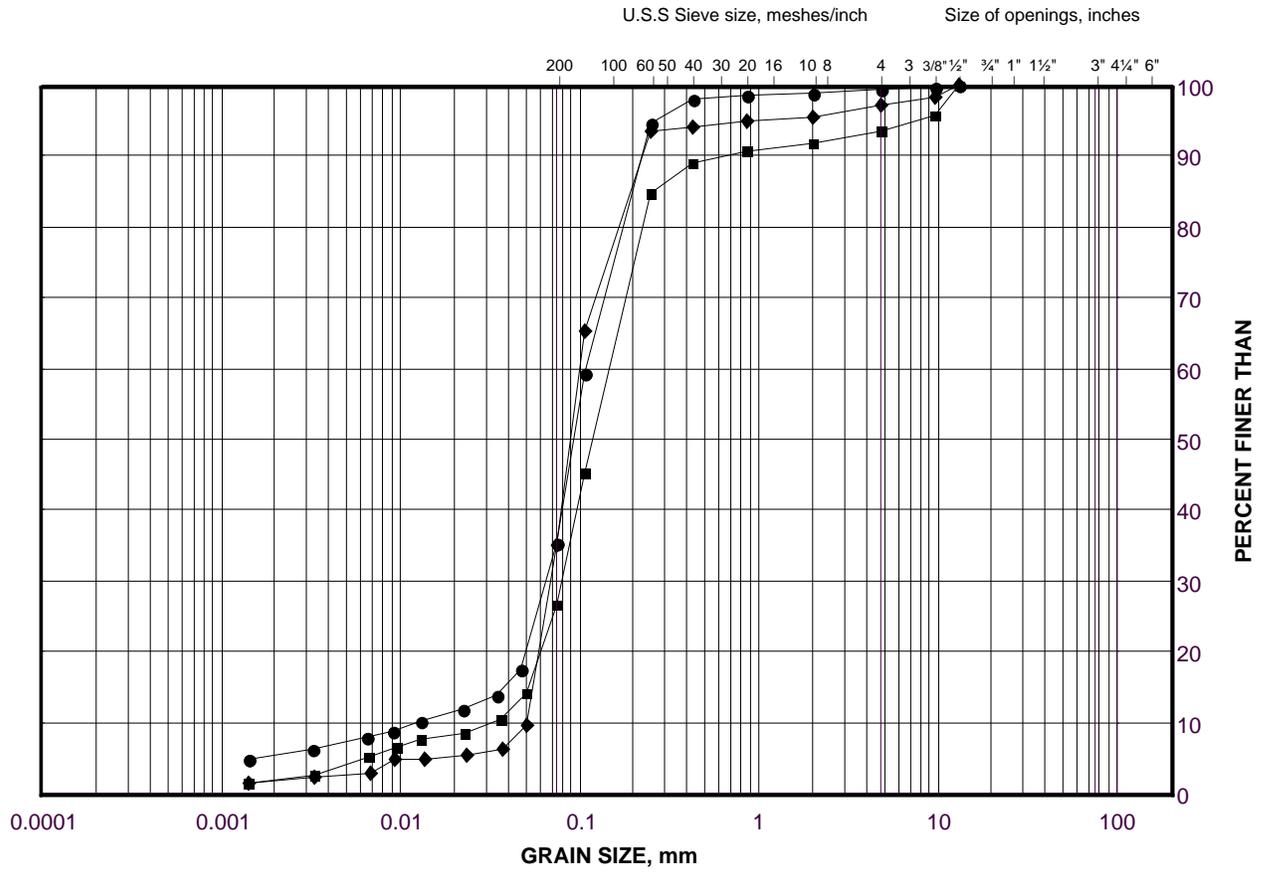
**APPENDIX B**

**Geotechnical Laboratory Test  
Results (incl. Geomechanics Test  
Results on Rock)**

# GRAIN SIZE DISTRIBUTION

Silt and Sand to Silty Sand (Fill)

FIGURE B-1



SILT AND CLAY SIZES		FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE
FINE GRAINED		SAND SIZE			GRAVEL SIZE		SIZE

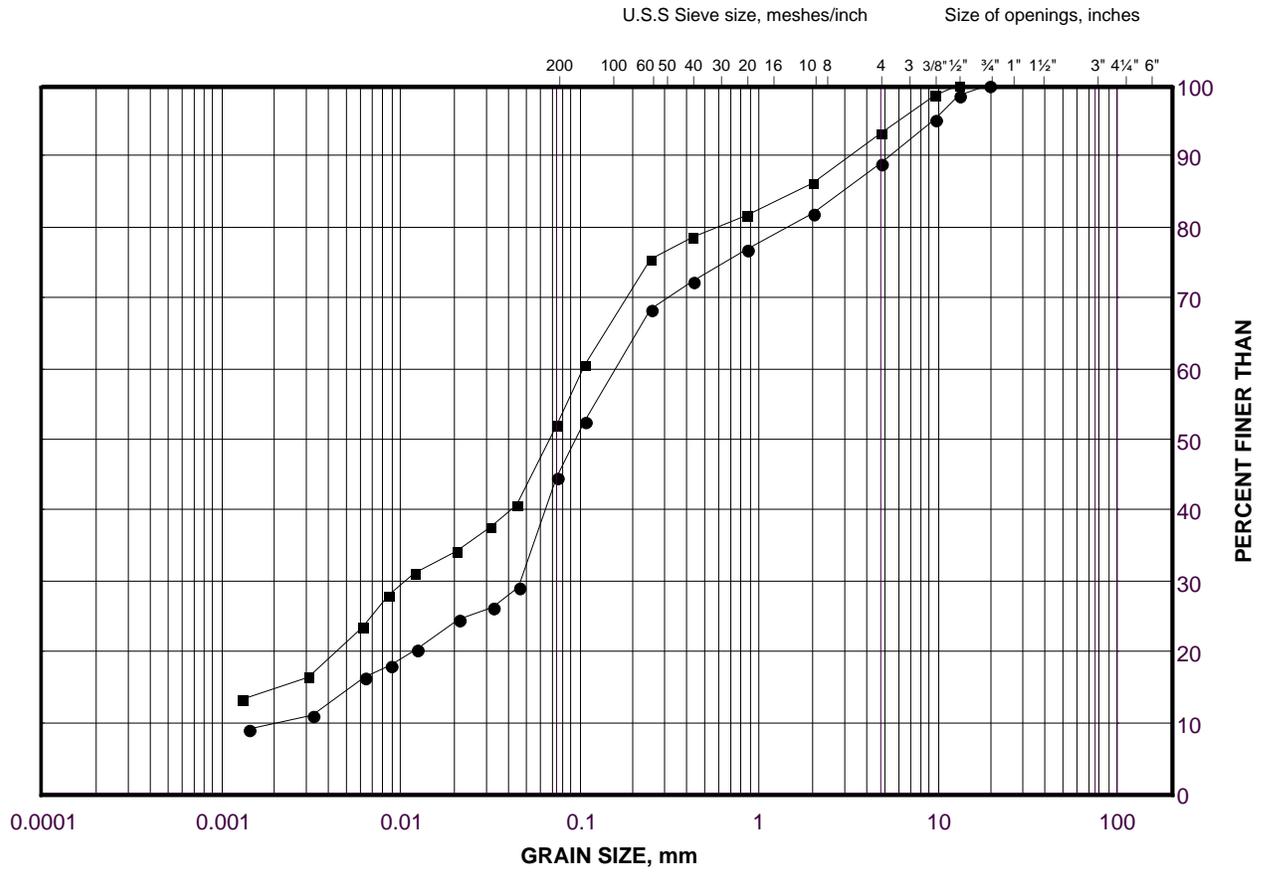
## LEGEND

SYMBOL	Borehole	SAMPLE	ELEVATION(m)
●	SWME-1	2	88.4
■	CRB-6	2	90.7
◆	CRB-7	3	92.9

# GRAIN SIZE DISTRIBUTION

Clayey Silt with Sand (Fill)

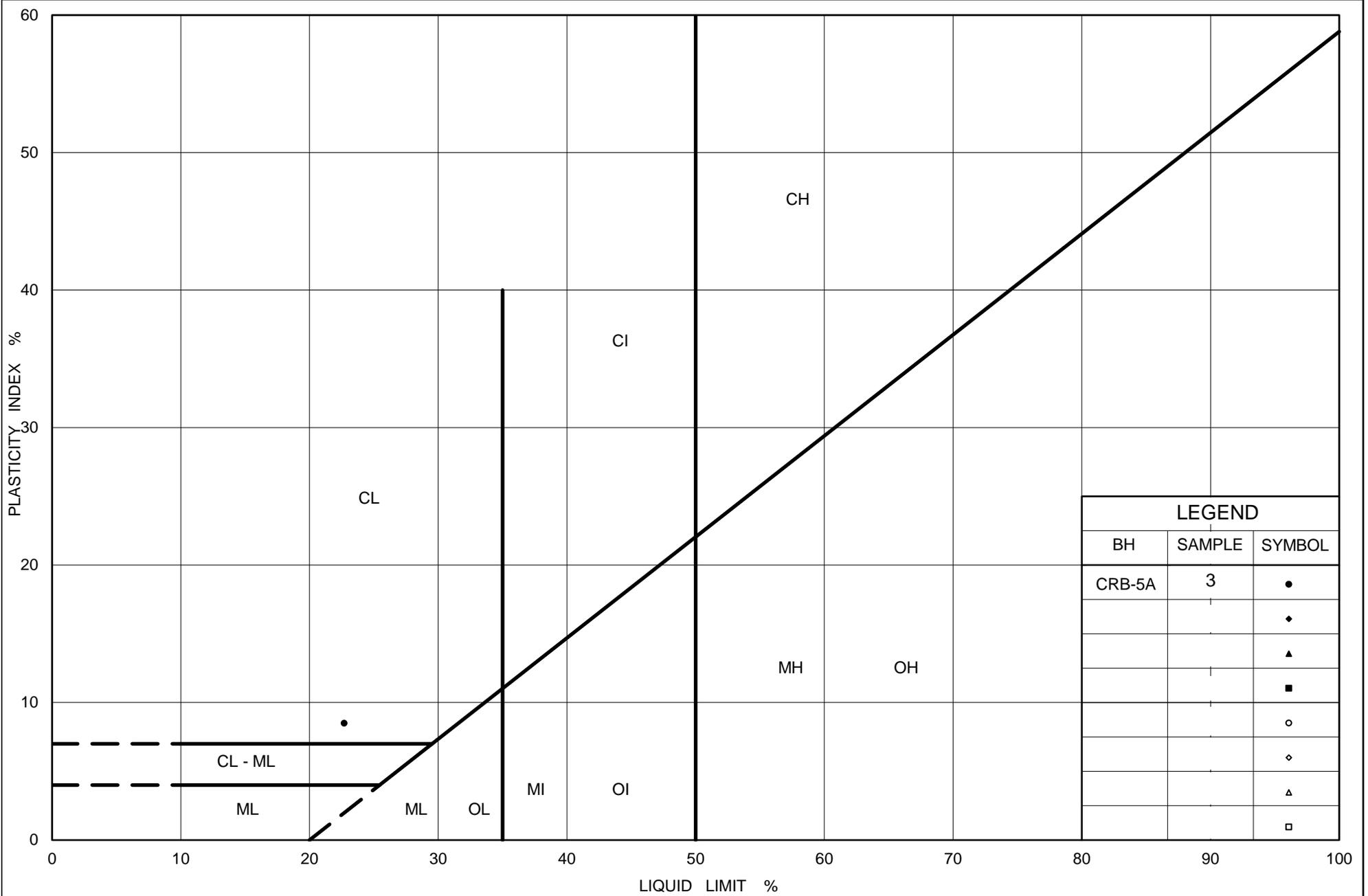
FIGURE B-2



SILT AND CLAY SIZES	FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE
FINE GRAINED	SAND SIZE			GRAVEL SIZE		SIZE

## LEGEND

SYMBOL	Borehole	SAMPLE	ELEVATION(m)
●	CRB-5A	3	77.5
■	CRB-4	4	76.5



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### PLASTICITY CHART Clayey Silt with Sand (Fill)

Figure No. B-3

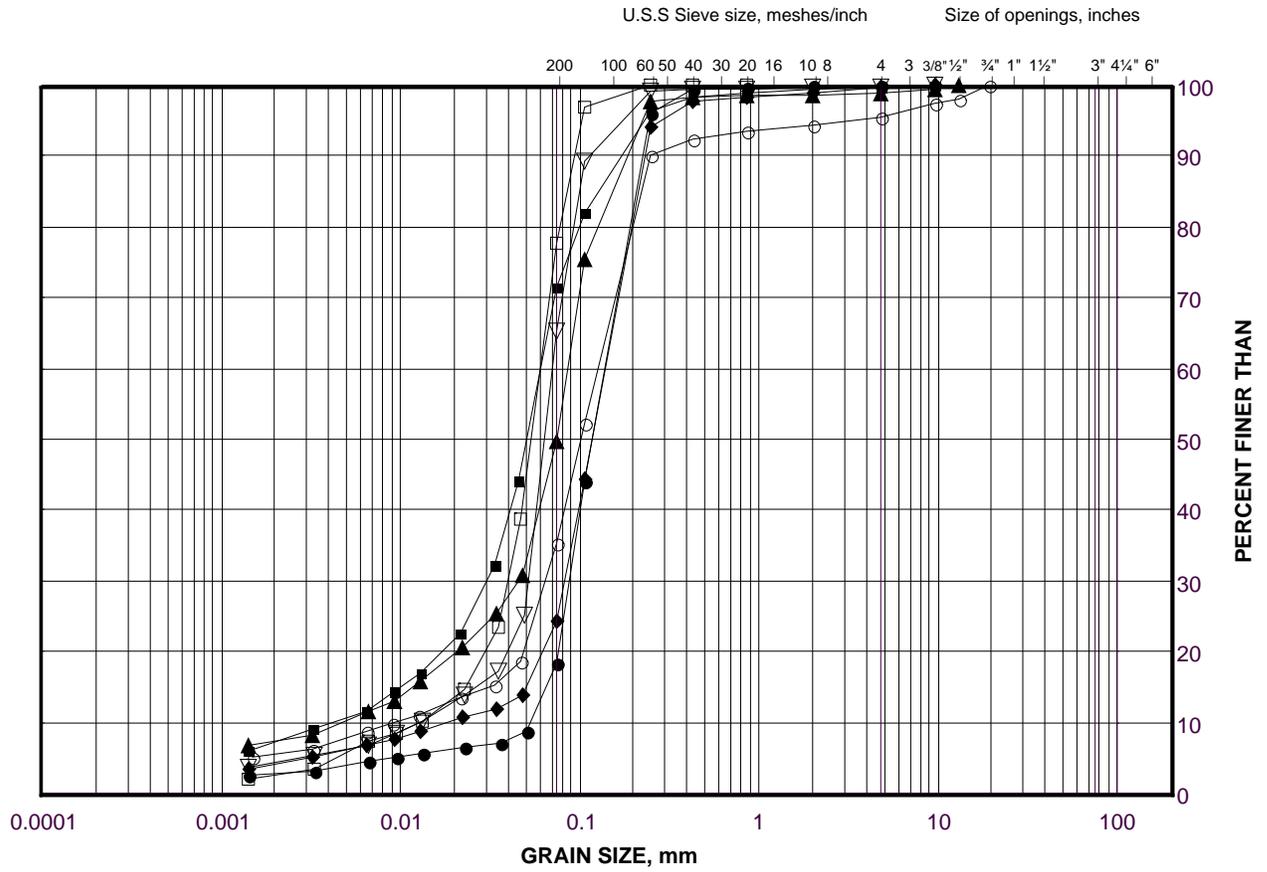
Project No. 1662333

Checked By: SMM

# GRAIN SIZE DISTRIBUTION

Sandy Silt to Sand

FIGURE B-4A



SILT AND CLAY SIZES		FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE
FINE GRAINED		SAND SIZE			GRAVEL SIZE		SIZE

## LEGEND

SYMBOL	Borehole	SAMPLE	ELEVATION(m)
●	AR-1	3	93.9
■	SWME-3	4	89.9
◆	SWME-1	4	86.9
▲	SWME-4	4	92.9
▽	AR-1	6	91.6
○	CRB-5	6	75.1
□	CRB-7	8	89.1

Project Number: 1662333

Checked By: SMM

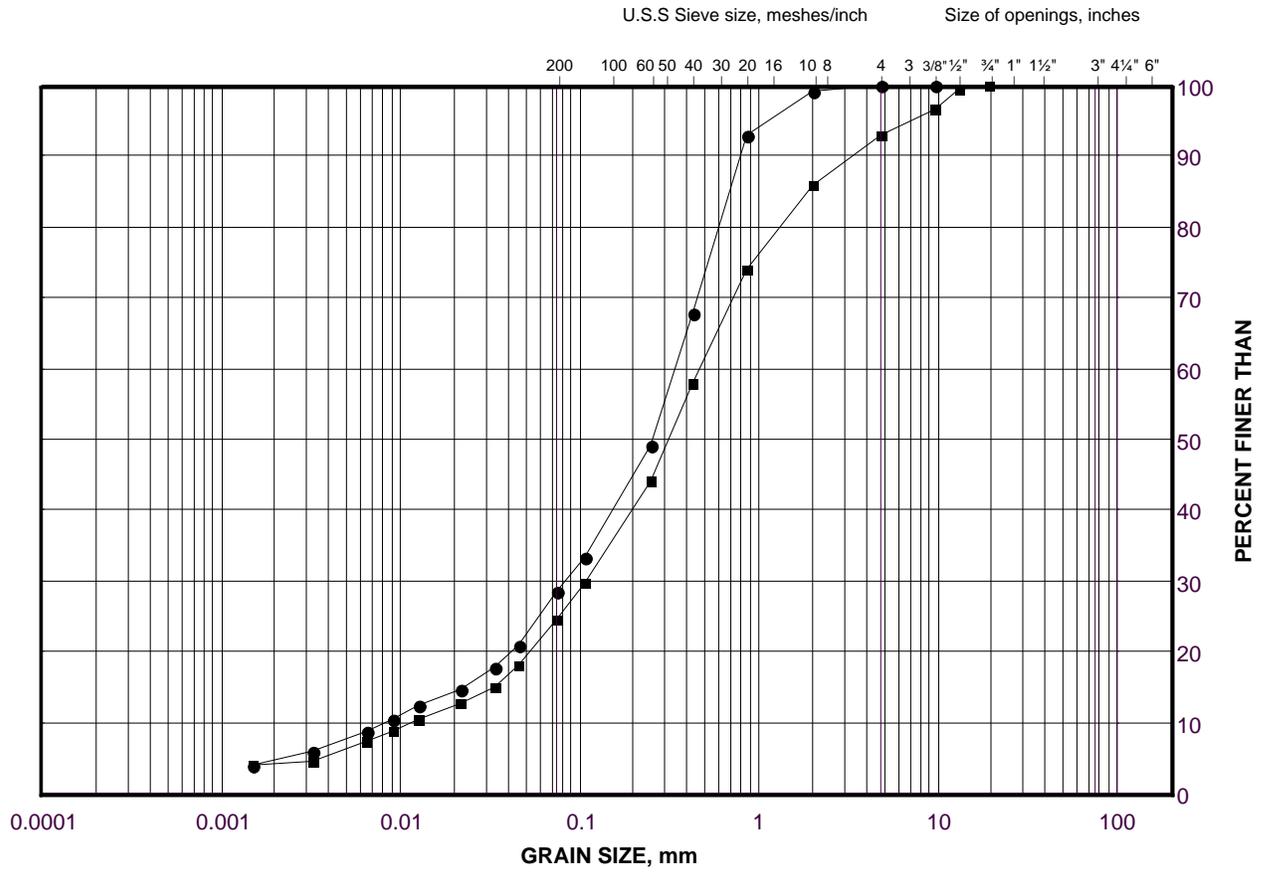
**Golder Associates**

Date: 10-Dec-18

# GRAIN SIZE DISTRIBUTION

Sandy Silt to Sand

FIGURE B-4B



SILT AND CLAY SIZES		FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE
FINE GRAINED		SAND SIZE			GRAVEL SIZE		SIZE

## LEGEND

SYMBOL	Borehole	SAMPLE	ELEVATION(m)
●	CRB-5A	8B	72.9
■	CRB-5	9	72.8

Project Number: 1662333

Checked By: SMM

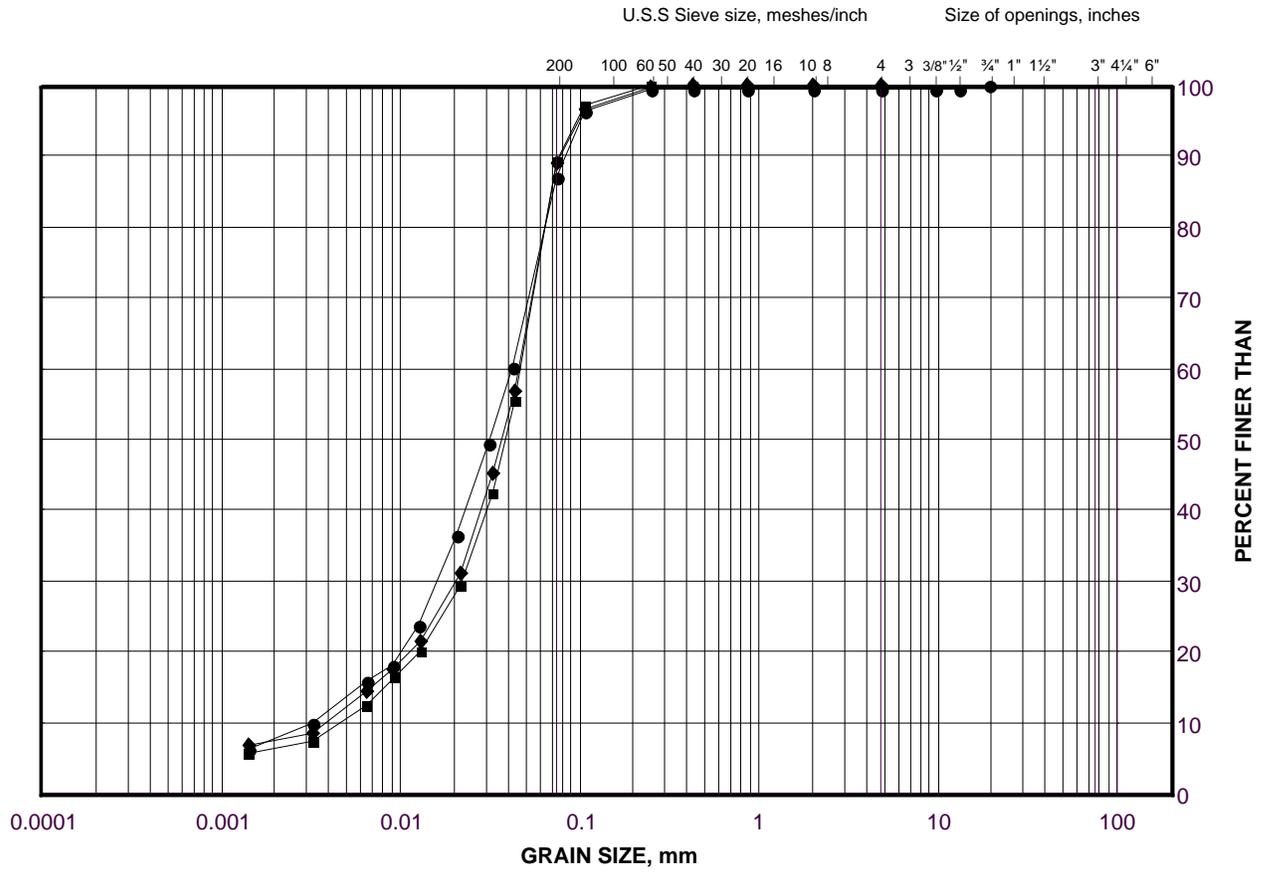
**Golder Associates**

Date: 10-Dec-18

# GRAIN SIZE DISTRIBUTION

Silt

FIGURE B-5



SILT AND CLAY SIZES		FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE
FINE GRAINED		SAND SIZE			GRAVEL SIZE		SIZE

## LEGEND

SYMBOL	Borehole	SAMPLE	ELEVATION(m)
●	SWME-3	5	89.3
■	AR-1	8	89.3
◆	SWME-4	8	89.1

Project Number: 1662333

Checked By: \_\_\_\_\_

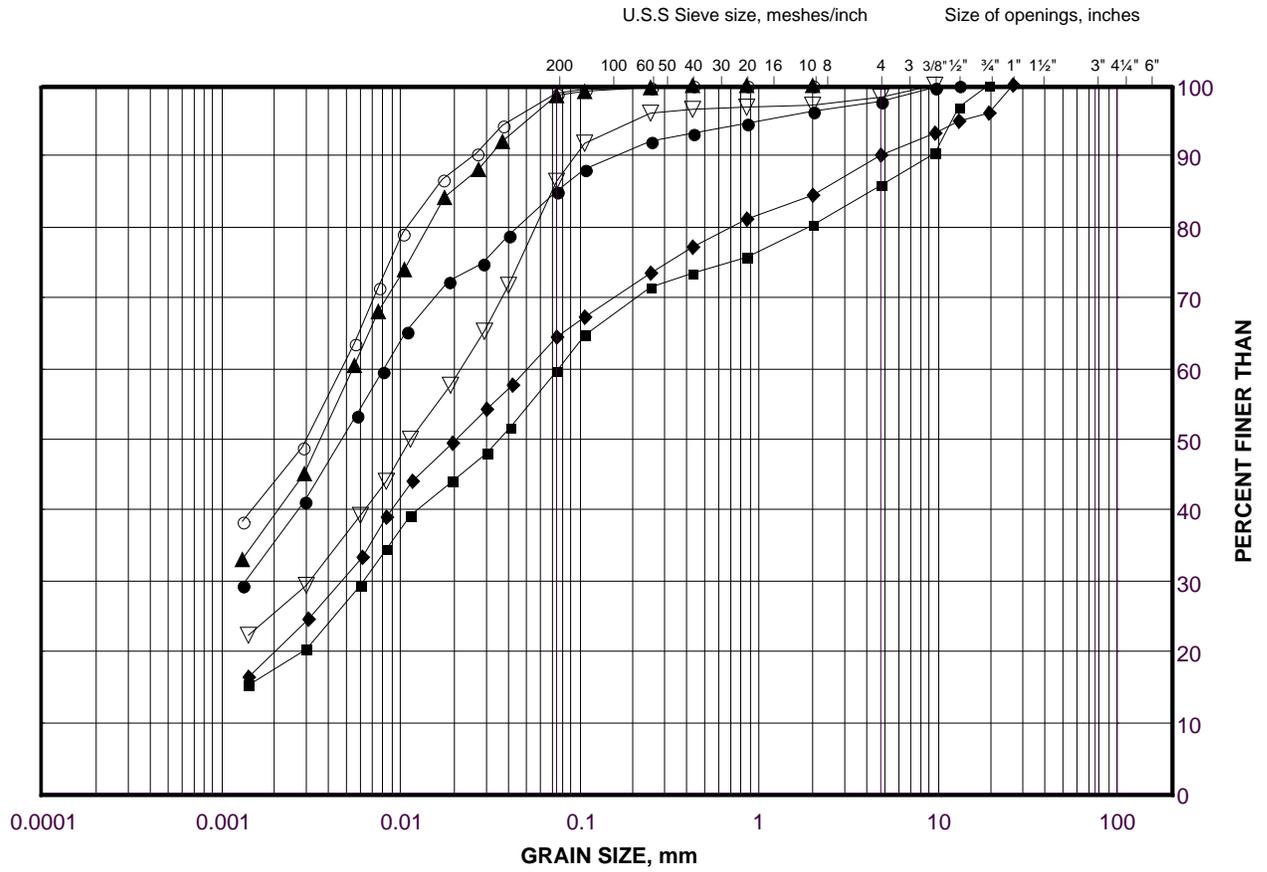
**Golder Associates**

Date: 10-Dec-18

# GRAIN SIZE DISTRIBUTION

Sandy Clayey Silt to Silty Clay

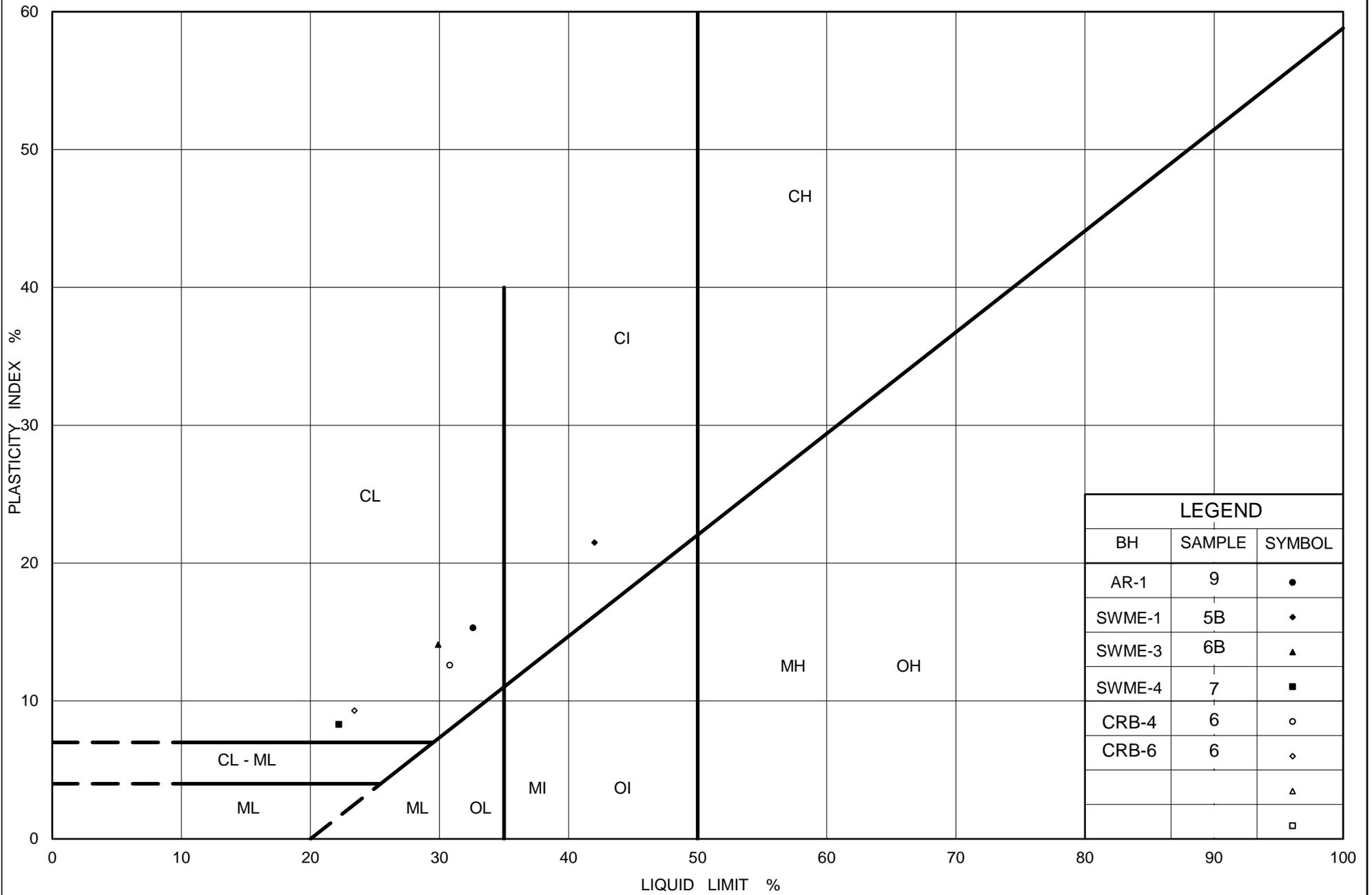
FIGURE B-6



SILT AND CLAY SIZES		FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE
FINE GRAINED		SAND SIZE			GRAVEL SIZE		SIZE

## LEGEND

SYMBOL	Borehole	SAMPLE	ELEVATION(m)
●	SWME-1	5B	85.9
■	CRB-4	6	75.0
◆	CRB-6	6	87.6
▲	SWME-3	6B	88.5
▽	SWME-4	7	90.6
○	AR-1	9	87.8



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## PLASTICITY CHART

### Sandy Clayey Silt to Silty Clay

Figure No. B-7

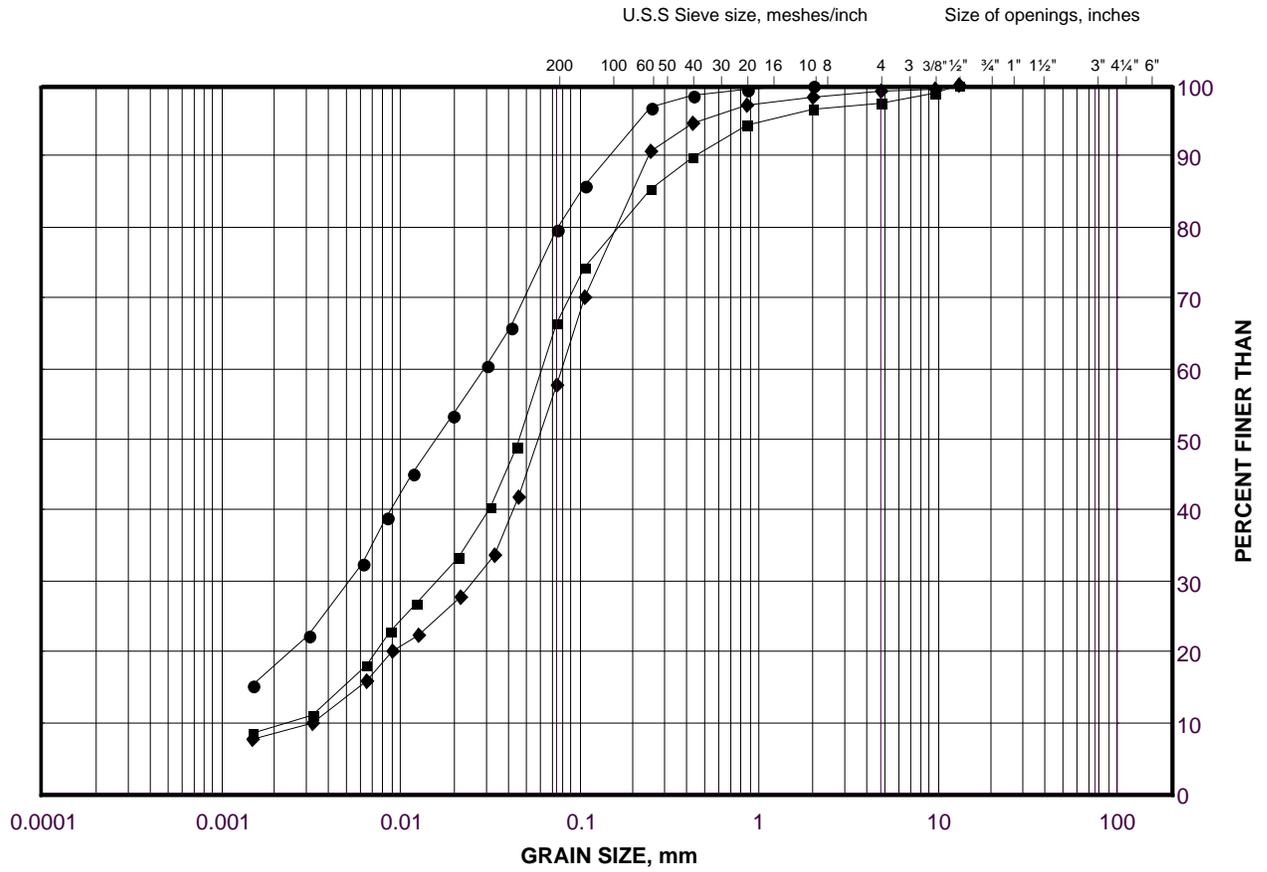
Project No. 1662333

Checked By: SMM

# GRAIN SIZE DISTRIBUTION

Organic Clayey Silt

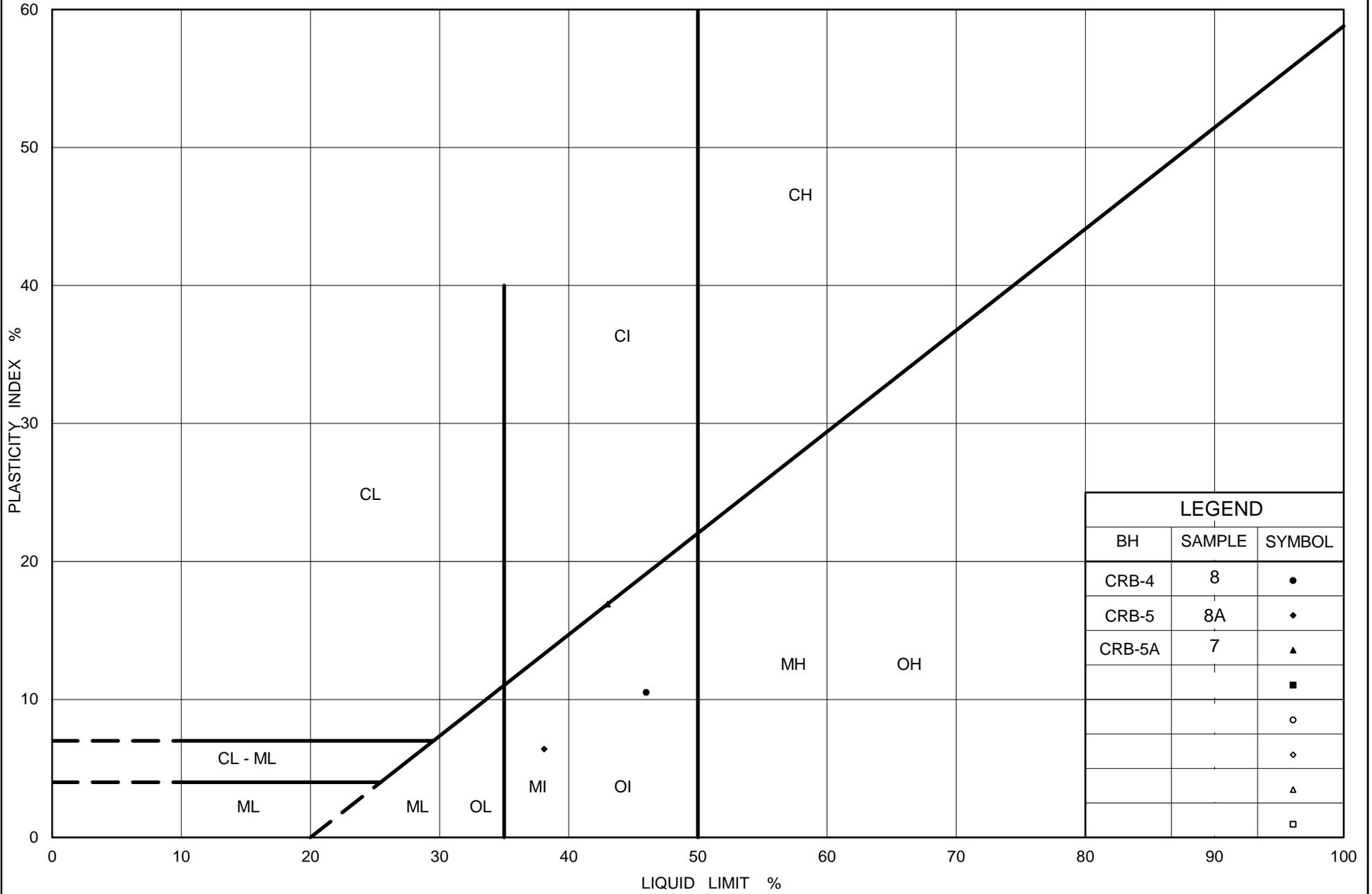
FIGURE B-8



SILT AND CLAY SIZES		FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE
FINE GRAINED		SAND SIZE			GRAVEL SIZE		SIZE

## LEGEND

SYMBOL	Borehole	SAMPLE	ELEVATION(m)
●	CRB-5A	7	74.4
■	CRB-4	8	72.8
◆	CRB-5	8A	73.7



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# PLASTICITY CHART

## Organic Clayey Silt

Figure No. B-9

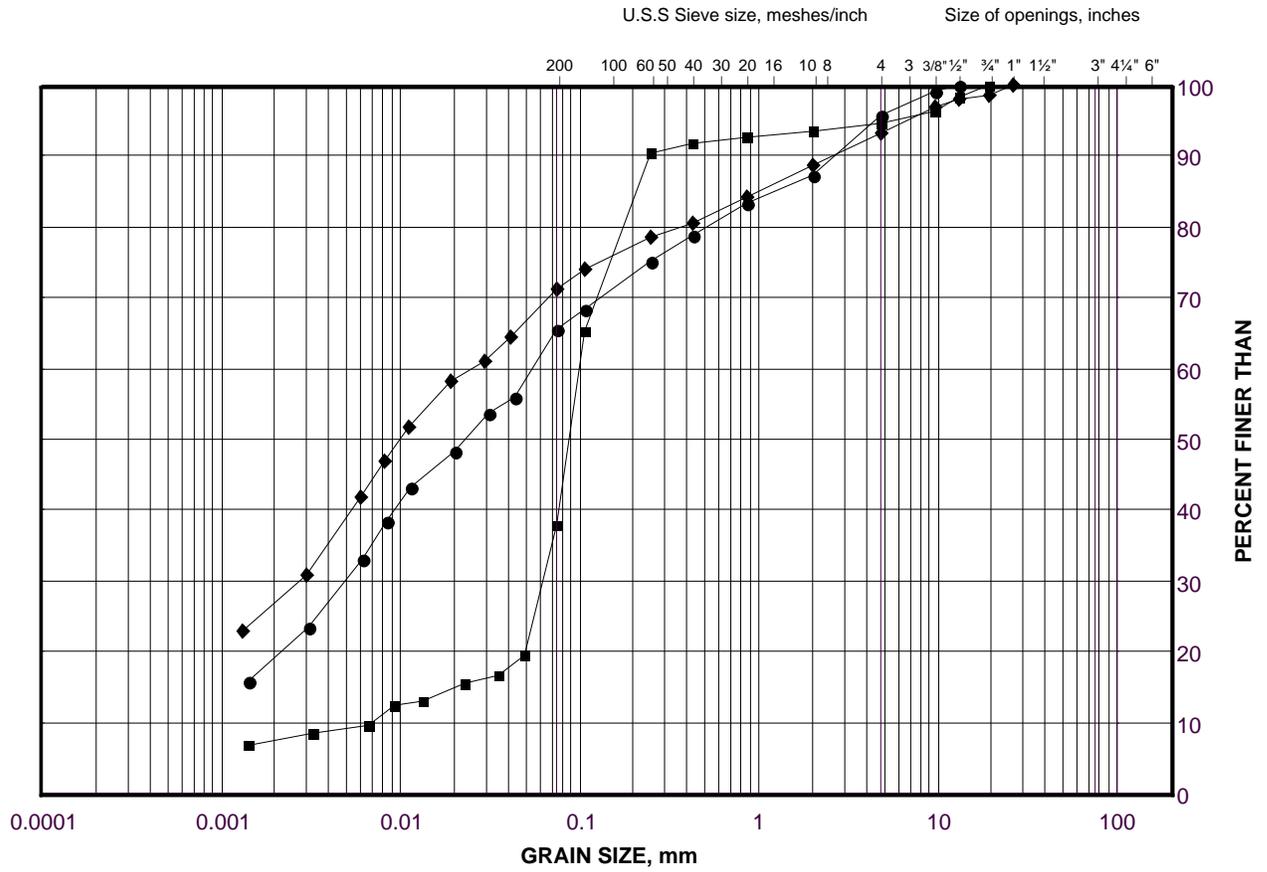
Project No. 1662333

Checked By: SMM

# GRAIN SIZE DISTRIBUTION

Silt and Sand/Clayey Silt with Sand to Sandy Silty Clay (Till)

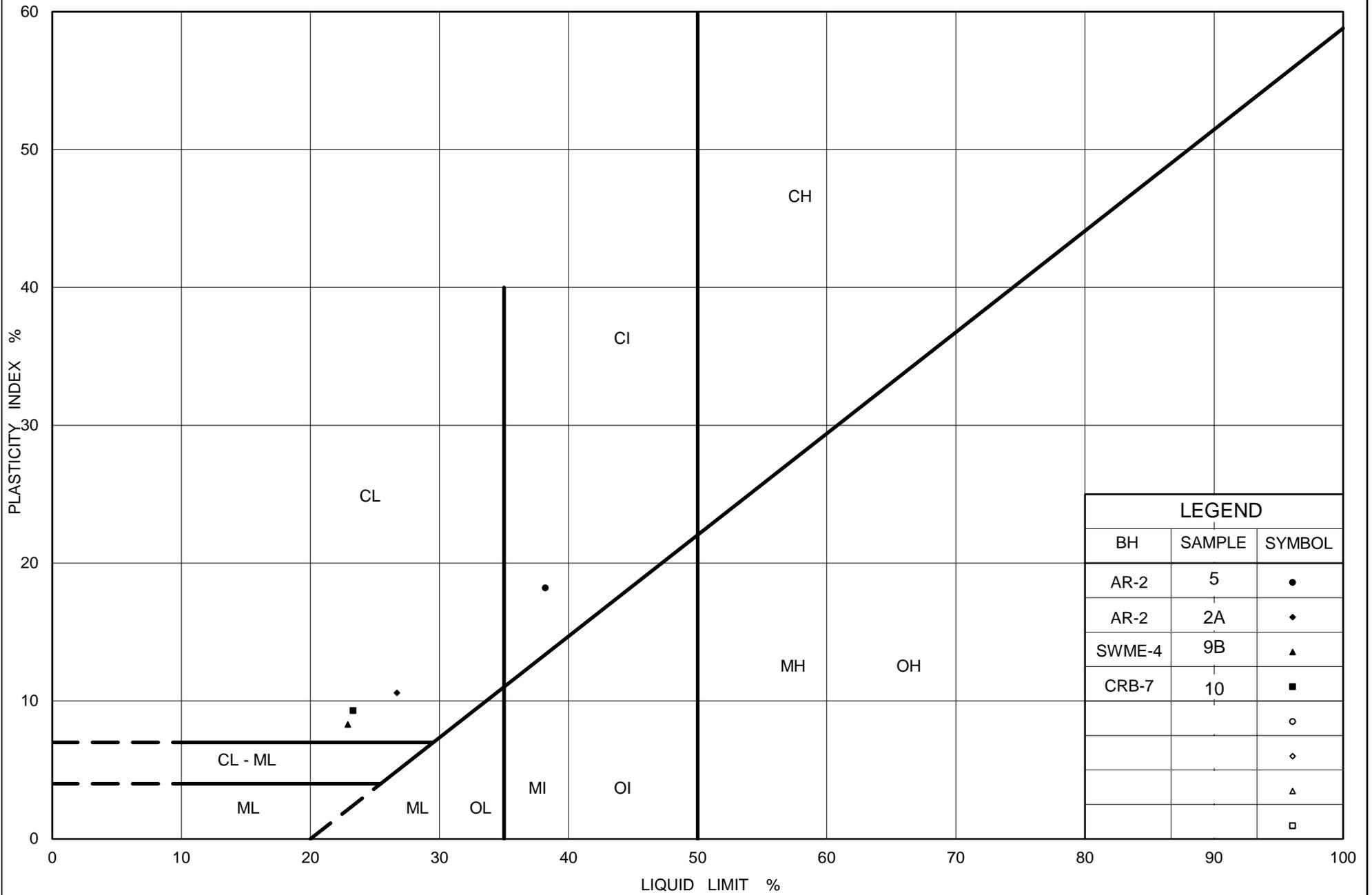
FIGURE B-10



SILT AND CLAY SIZES	FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE
FINE GRAINED	SAND SIZE			GRAVEL SIZE		SIZE

## LEGEND

SYMBOL	Borehole	SAMPLE	ELEVATION(m)
●	CRB-7	10	87.5
■	AR-2	3	86.7
◆	AR-2	5	85.1



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## PLASTICITY CHART

### Clayey Silt with Sand to Sandy Silty Clay (Till)

Figure No. B-11

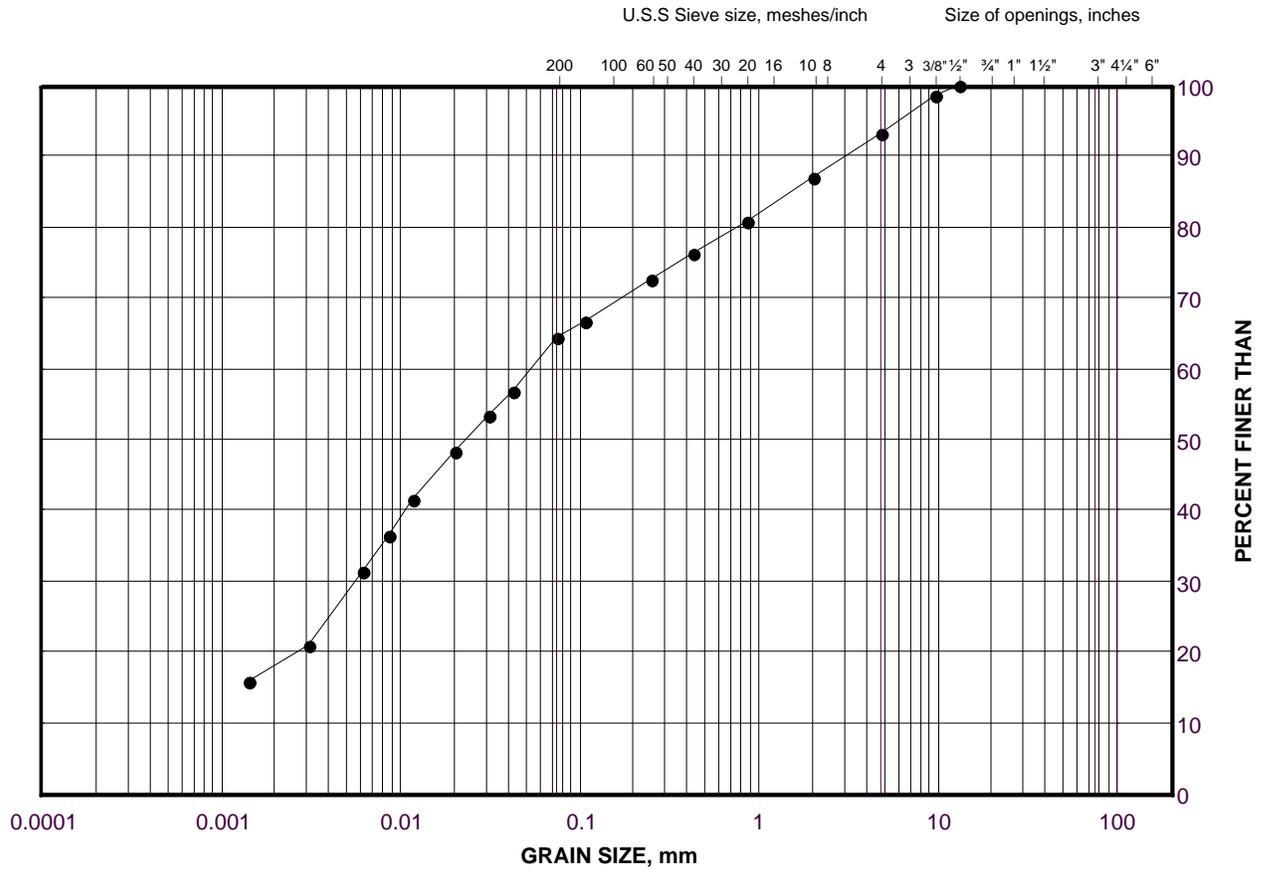
Project No. 1662333

Checked By: SMM

# GRAIN SIZE DISTRIBUTION

Sandy Clayey Silt to Clayey Silt (Residual Soil)

FIGURE B-12



SILT AND CLAY SIZES	FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE
FINE GRAINED	SAND SIZE			GRAVEL SIZE		SIZE

**LEGEND**

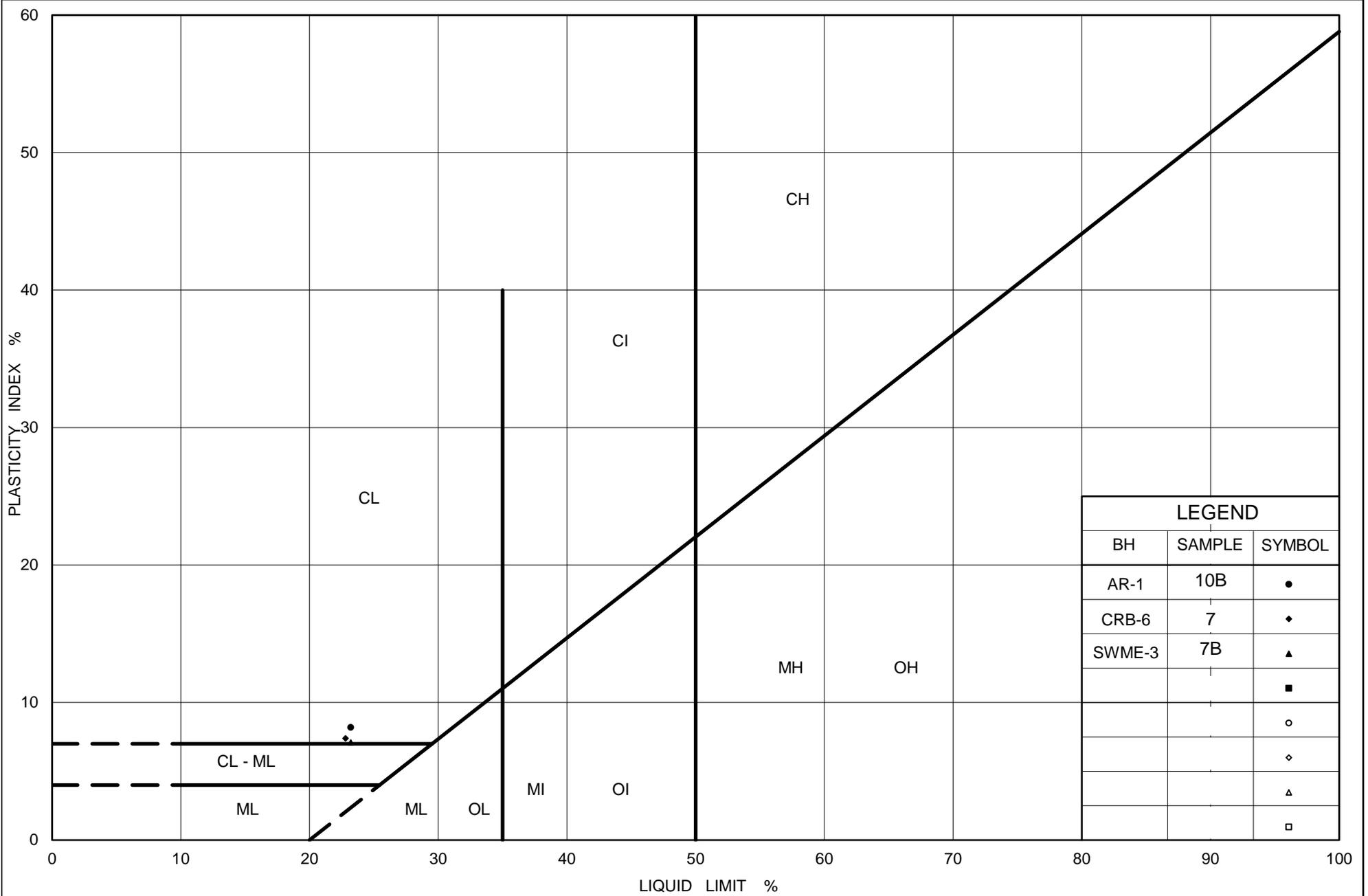
SYMBOL	Borehole	SAMPLE	ELEVATION(m)
●	AR-1	10B	87.0

Project Number: 1662333

Checked By: SMM

**Golder Associates**

Date: 10-Dec-18



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### PLASTICITY CHART

#### Sandy Clayey Silt to Clayey Silt (Residual Soil)

Figure No. B-13

Project No. 1662333

Checked By: SMM

**Table B-1: Summary of Point Load Test Results**

Borehole No.	Sample Depth (m)	Sample Elevation (m)	Orientation	Corrected Is (50 mm) (MPa)
CRB-4	13.5	65.60	Diametral	0.89
CRB-4	9.22	69.88	Diametral	0.04
CRB-4	9.22	69.88	Axial	1.02
CRB-4	9.28	69.82	Axial	2.14
CRB-4	14.93	64.17	Diametral	0.08
CRB-4	14.93	64.17	Axial	0.23
CRB-5	8.95	70.25	Diametral	0.76
CRB-5	9.03	70.17	Axial	0.37
CRB-5	14.48	64.72	Diametral	0.52
CRB-5	14.51	64.69	Axial	0.27
CRB-5	13.31	65.89	Diametral	0.07
CRB-5	9.53	69.67	Axial	1.45
CRB-5A	10.24	69.06	Diametral	0.56
CRB-5A	10.29	69.01	Axial	0.42
CRB-5A	13.84	65.46	Diametral	0.43
CRB-5A	13.89	65.41	Axial	0.07
CRB-5A	16.8	62.50	Diametral	0.82
CRB-5A	17	62.30	Axial	0.24
CRB-6	6.03	85.67	Axial	0.70
CRB-6	6.03	85.67	Diametral	0.44
CRB-6	7.34	84.36	Axial	0.65
CRB-6	7.34	84.36	Diametral	0.51

---

Borehole No.	Sample Depth (m)	Sample Elevation (m)	Orientation	Corrected Is (50 mm) (MPa)
CRB-6	9.03	82.67	Axial	0.61
CRB-6	9.03	82.67	Diametral	0.15
CRB-7	9.06	85.64	Axial	0.47
CRB-7	9.06	85.64	Diametral	0.26
CRB-7	9.46	85.24	Axial	0.56
CRB-7	9.46	85.24	Diametral	0.42
CRB-7	12.04	82.66	Axial	0.85
CRB-7	12.04	82.66	Diametral	0.32

November 22, 2017

Mr. David Marmor  
Golder Associates Ltd.  
6925 Century Avenue, Suite #100  
Mississauga, Ontario  
Canada L5N 7K2

Re: UCS + E testing  
(Golder Project No. 166233)

Dear Mr. Marmor:

On November 3, 2017 four (4) HQ-sized core samples were received by Geomechanica Inc. via courier. These samples were identified as being from boreholes drilled as part of Golder project 166233 (denoted as QEW/Credit River UCS samples). A uniaxial compressive strength (UCS) specimen was prepared and tested from each of these samples (4 tests total).

Details regarding the steps of specimen preparation and testing along with the test results and specimen photographs before and after testing are presented in the accompanying laboratory report.

Sincerely,



Giovanni Grasselli Ph.D., P. Eng.

Geomechanica Inc.  
Tel: (647) 478-9767  
Email: [giovanni.grasselli@geomechanica.com](mailto:giovanni.grasselli@geomechanica.com)

# Rock Laboratory Testing Results

**A report submitted to:**

David Marmor  
Golder Associates Ltd.  
6925 Century Avenue, Suite #100  
Mississauga, Ontario  
Canada L5N 7K2

**Prepared by:**

Bryan Tatone, PhD  
Omid Mahabadi, PhD  
Giovanni Grasselli, PhD, PEng

Geomechanica Inc  
#300-90 Adelaide St W  
Toronto ON  
M5H 3V9 Canada  
Tel: +1-647-478-9767  
info@geomechanica.com

**November 22, 2017**  
Project number: 1662333

**Abstract**

This document summarizes the results of 4 uniaxial compression tests on HQ-sized core samples for Golder Project 1662333. Results including uniaxial compressive strength (UCS) and Young's modulus along with photographs of samples before and after testing are presented.

**In this document:**

1	Overview	1
2	Results	2

## 1 Overview

This report summarizes the results of laboratory testing of 4 uniaxial compression tests on HQ-sized core samples for Golder Project 1662333. The tests were performed in Geomechanica's laboratory in Oakville, Ontario, Canada using a 1.3 MN capacity Forney compression testing machine (Figure 1). The specimens were loaded with a nearly constant axial displacement rate of 0.150 mm/min. The specimen preparation and testing procedure included the following:

1. Unwrapping of the core samples, inspecting them for damage, and re-wrapping them in electrical tape to minimize disturbance during subsequent specimen preparation.
2. Diamond cutting of core samples to obtain cylindrical specimens with an appropriate length (length:diameter = 2:1) and nearly parallel end faces.
3. Surface grinding of specimens to obtain flat (within  $\pm 0.025$  mm) and parallel end faces (within  $0.25^\circ$ ).
4. Placing each specimen into the loading frame, applying a 0.5-1.0 kN axial load, removing the electrical tape, and subsequently increasing the axial load gradually to cause rupture while continuously recording axial force and axial deformation to determine peak strength (UCS) and (tangent) Young's modulus.



Figure 1: UCS Test setup.

## 2 Results

The results of the tests are summarized in Table 1. The corresponding stress-strain curves for the uniaxial compression tests are presented in Figure 2. The Young's modulus is the tangent modulus, calculated as the slope of the best fit line through  $\pm 300$  data points on either side of the point representing 50% of the peak strength.

Table 1: Summary of laboratory test results.

Sample	Depth (m)	Bulk density $\rho$ (g/cm <sup>3</sup> )	UCS (MPa)	Young's Modulus $E$ (GPa)	Notes
CRB-3, UCS-1	11.44 - 11.66	2.61	9.4	2.10	<sup>1</sup>
CRB-6, UCS-1	6.06 - 6.17	2.17	14.6	0.63	1,2
CRB-7, UCS-1	9.21 - 9.369	2.59	15.5	0.65	1,2
CRB-7, UCS-3	12.11 - 12.36	2.59	7.4	1.28	
Mean		2.49	11.7	1.2	
Standard Deviation		0.18	3.4	0.6	

<sup>1</sup> Specimen emitted fresh pore water upon loading  
<sup>2</sup> length:diameter ratio < 2:1.

### 2.1 Specimen photographs

Photographs of the specimens before and after testing are presented in Figure 3.

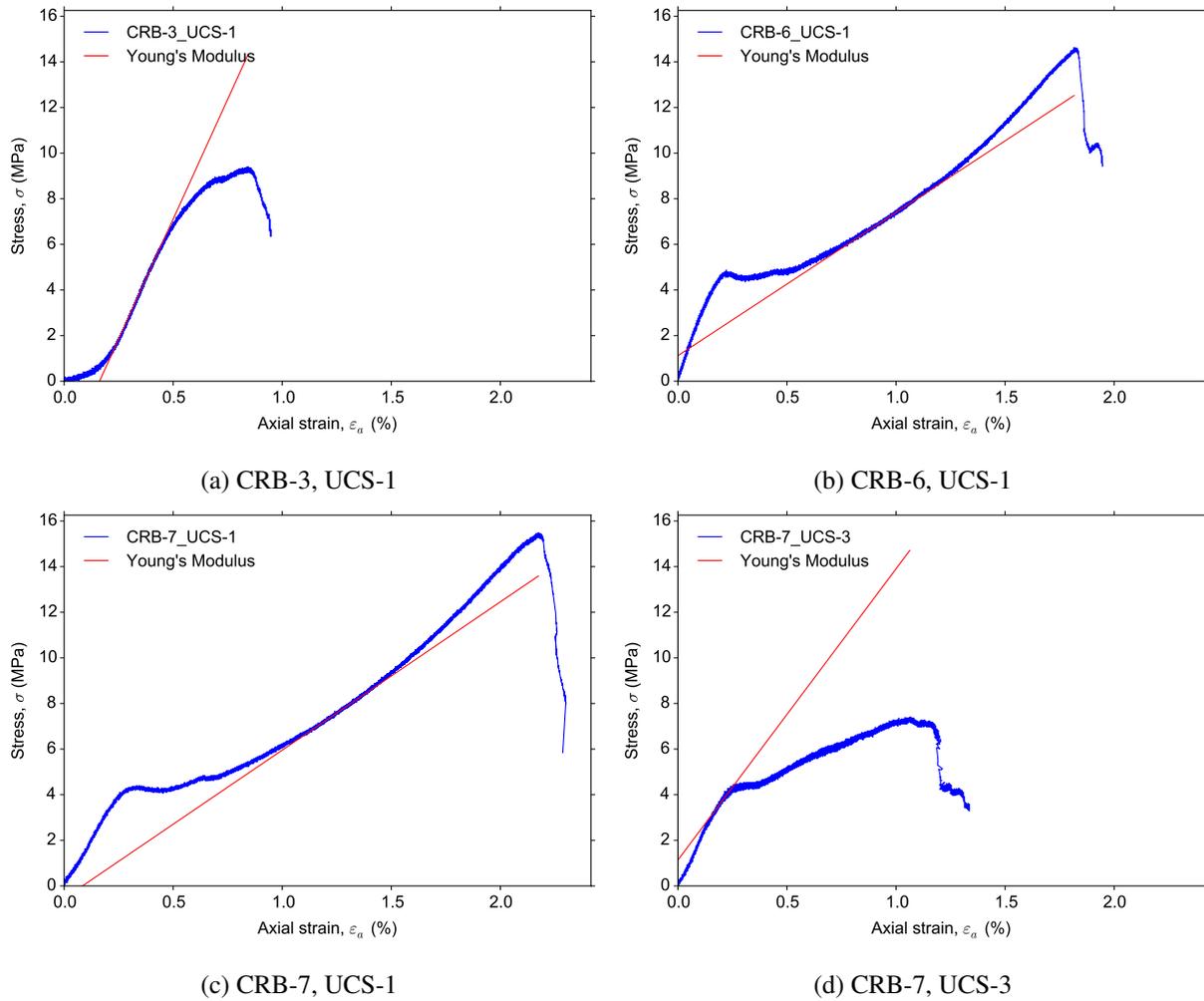


Figure 2: Measured stress-strain curves.

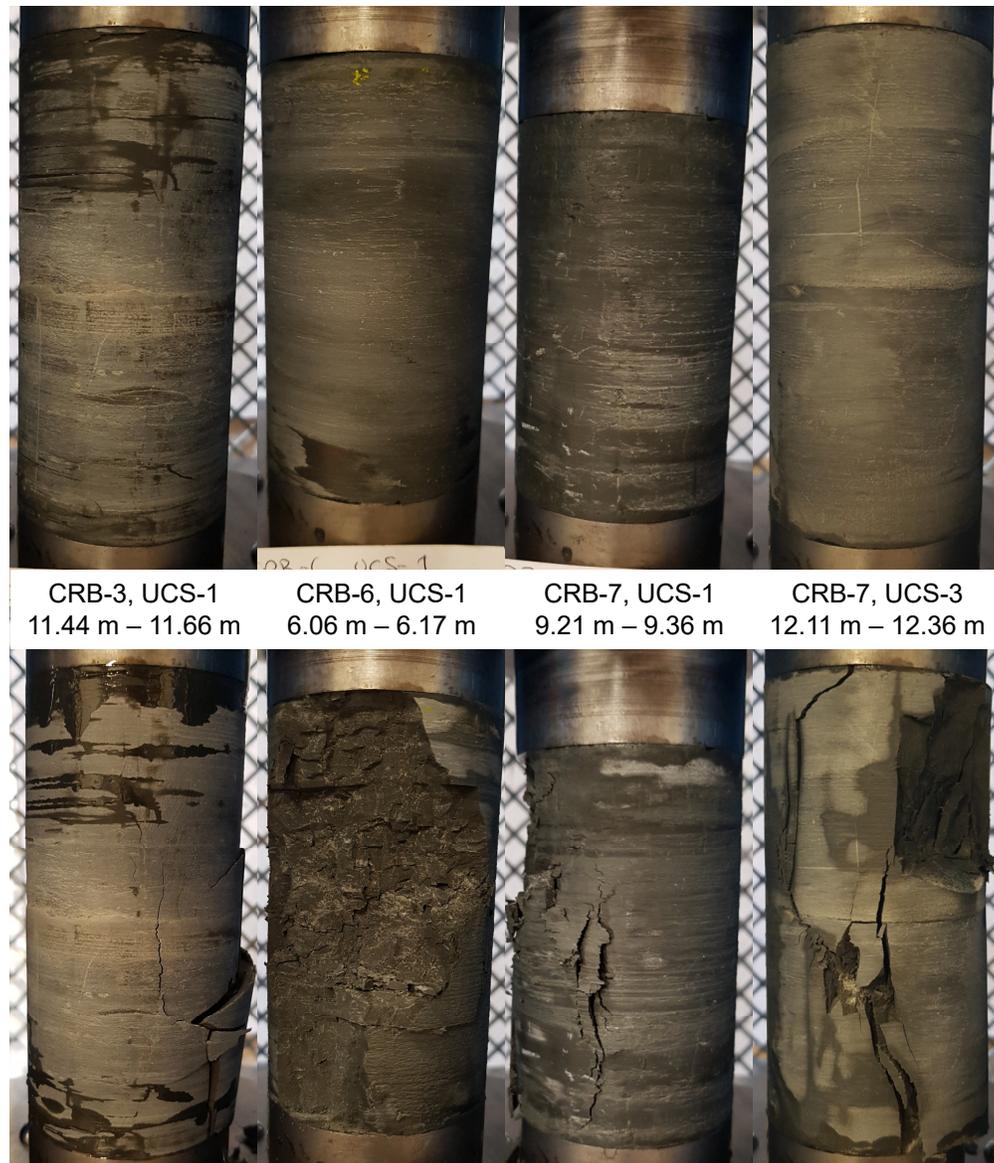


Figure 3: Photographs of specimens prior to testing.

April 09, 2018

Mr. David Marmor  
Golder Associates Ltd.  
6925 Century Avenue, Suite #100  
Mississauga, Ontario  
Canada L5N 7K2

Re: UCS + E testing  
(Golder Project No. 1662333)

Dear Mr. Marmor:

On March 27, 2018 three (3) NQ-sized and eight (8) HQ-sized core samples were received by Geomechanica Inc. via drop-off by Golder personnel. These samples were identified as being from boreholes drilled as part of Golder project. A uniaxial compressive strength (UCS) specimen was prepared and tested from each of these samples (11 tests total).

Details regarding the steps of specimen preparation and testing along with the test results and specimen photographs before and after testing are presented in the accompanying laboratory report.

Sincerely,



Bryan Tatone Ph.D., P. Eng.

Geomechanica Inc.  
Tel: (647) 478-9767  
Email: [bryan.tatone@geomechanica.com](mailto:bryan.tatone@geomechanica.com)

# Rock Laboratory Testing Results

**A report submitted to:**

David Marmor  
Golder Associates Ltd.  
6925 Century Avenue, Suite #100  
Mississauga, Ontario  
Canada L5N 7K2

**Prepared by:**

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Toronto ON  
M5H 2Y2 Canada  
Tel: +1-647-478-9767  
info@geomechanica.com

**April 9, 2018**

Project number: 1662333

**Abstract**

This document summarizes the results of 11 uniaxial compression tests on a combination of NQ and HQ core samples. Results, including uniaxial compressive strength (UCS) and Young's modulus, along with photographs of test specimens before and after testing are presented.

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## 1 Overview

This report summarizes the results of 11 uniaxial compression tests. The specimen preparation and testing procedure included the following:

1. Unwrapping of the core samples, inspecting them for damage, and re-wrapping them in electrical tape to minimize disturbance during subsequent specimen preparation.
2. Diamond cutting of core samples to obtain cylindrical specimens with an appropriate length (length:diameter = 2:1) and nearly parallel end faces.
3. Surface grinding of specimens to obtain flat (within  $\pm 0.025$  mm) and parallel end faces (within  $0.25^\circ$ ).
4. Placing each specimen into the loading frame, applying a 0.5-1.0 kN axial load, removing the electrical tape, and axial loading at a constant displacement rate to rupture while continuously recording axial force and axial deformation to determine the peak strength (UCS) and (tangent) Young's modulus ( $E$ ).

## 2 Results

The results of the tests are summarized in Table 1. The corresponding stress-strain curves for the uniaxial compression tests are presented in Figure 1 to Figure 2. The Young's modulus is the tangent modulus, calculated as the slope of the best fit line through  $\pm 300$  data points on either side of the point representing 50.0% of the peak strength.

Table 1: Summary of laboratory test results.

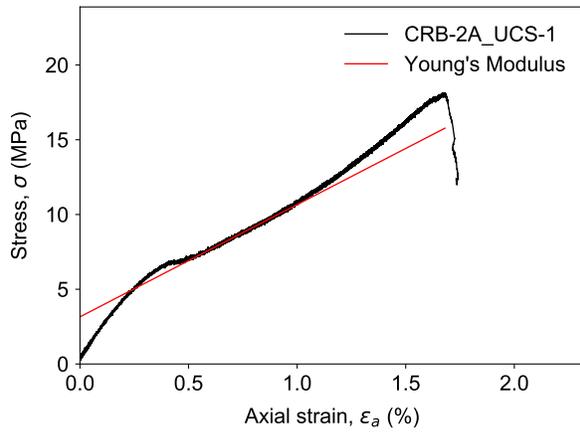
Sample	Rock (m)	Depth type	Bulk density $\rho$ (g/cm <sup>3</sup> )	UCS (MPa)	Young's Modulus $E$ (GPa)	Notes
CRB-2A, UCS-1	Shale	4.31 - 4.46	2.59	18.2	0.75	1, 2
CRB-2A, UCS-2	Shale	4.92 - 5.15	2.60	17.1	0.76	1
CRB-3C, UCS-3	Limestone	7.87 - 7.98	2.61	114.1	22.91	2, 3
CRB-2, UCS-2	Shale	7.75 - 7.92	2.58	11.2	0.83	1
CRB-2, UCS-3	Shale	11.37 - 11.52	2.61	13.0	2.19	3
CRB-3A, UCS-3	Shale	10.19 - 10.33	2.60	8.9	0.48	1, 4 - 2 limestone layers <sup>5</sup> 5-10 mm thick
CRB-3A, UCS-5	Shale	12.99 - 13.28	2.62	16.9	0.67	1
CRB-4, UCS-3	Shale	13.62 - 13.80	2.61	18.6	0.84	1
CRB-5, UCS-2	Shale	13.68 - 13.95	2.61	15.5	0.61	1
CRB-5A, UCS-2	Shale	12.43 - 12.57	2.60	14.2	0.96	1
CRB-5A, UCS-4	Shale	15.34 - 15.57	2.64	22.7	0.93	1

<sup>1</sup> Upon loading specimen emitted pore water

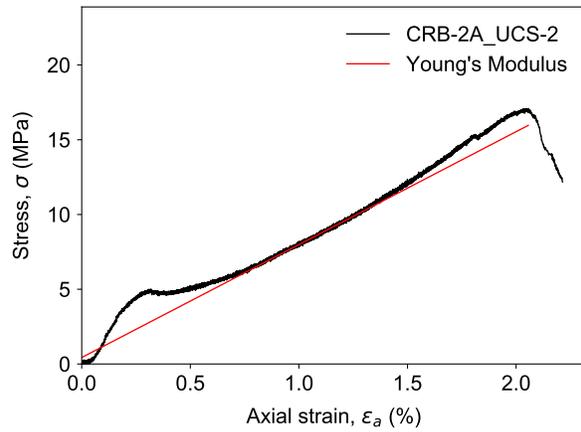
<sup>2</sup> Irregular diameter > 0.5 mm

<sup>3</sup> Length:Diameter ratio less than 2

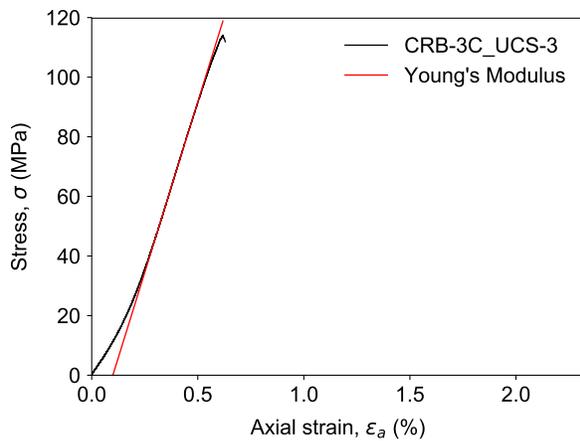
<sup>4</sup> Inter-bedded limestone and shale



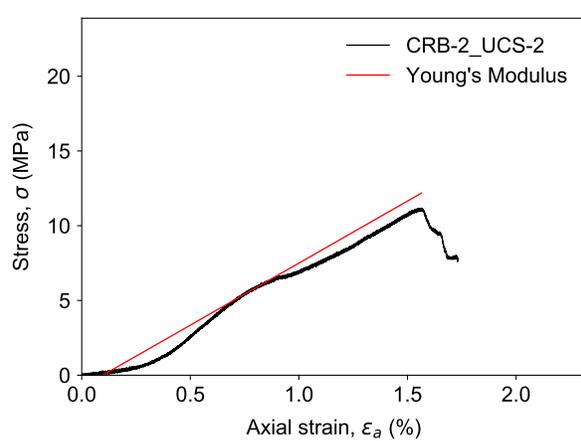
(a) CRB-2A, UCS-1



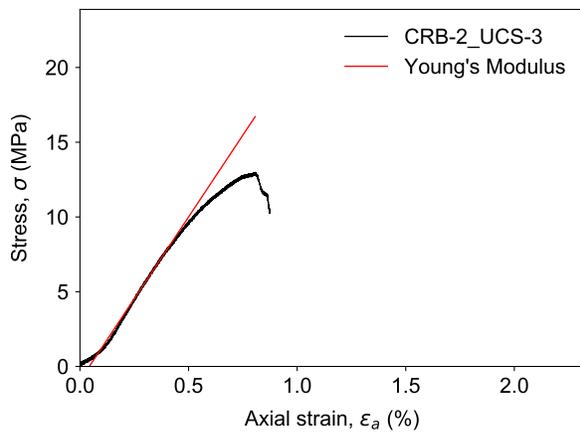
(b) CRB-2A, UCS-2



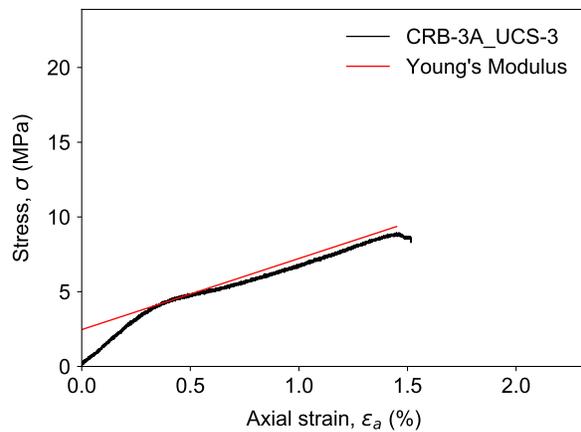
(c) CRB-3C, UCS-3



(d) CRB-2, UCS-2

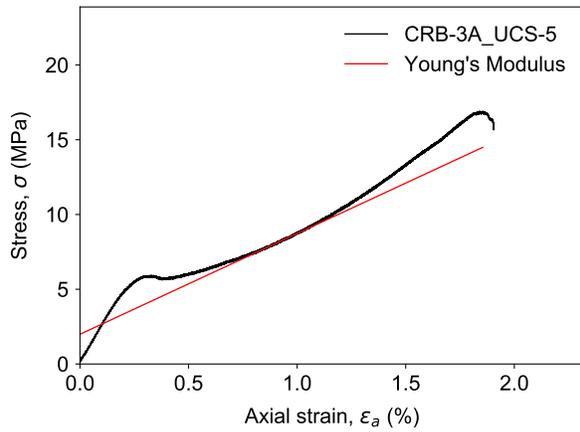


(e) CRB-2, UCS-3

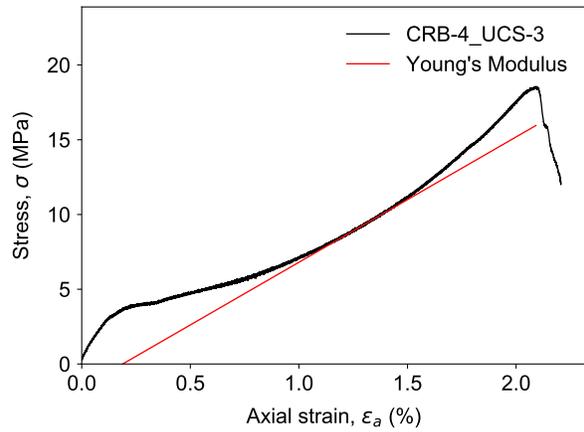


(f) CRB-3A, UCS-3

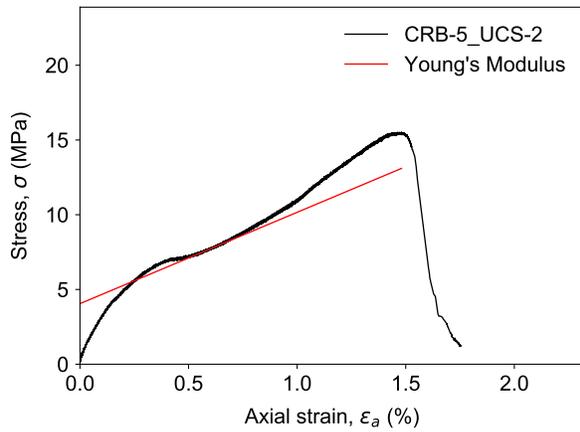
Figure 1: Measured stress-strain curves.



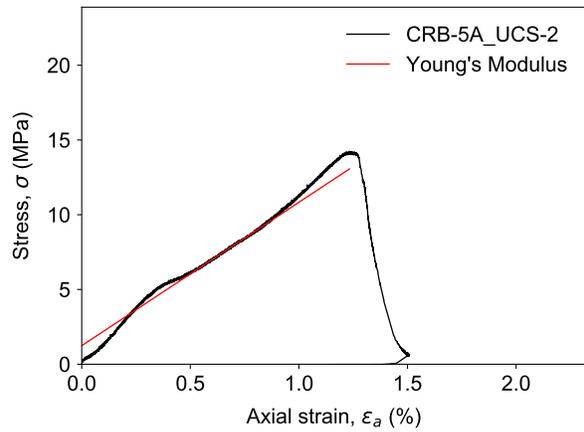
(a) CRB-3A, UCS-5



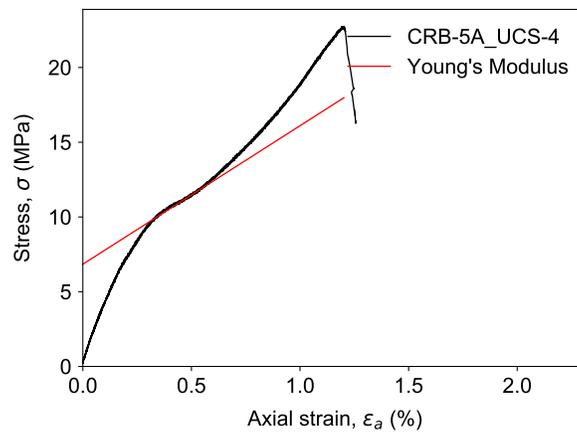
(b) CRB-4, UCS-3



(c) CRB-5, UCS-2



(d) CRB-5A, UCS-2



(e) CRB-5A, UCS-4

Figure 2: Measured stress-strain curves.

## 2.1 Specimen photographs

Photographs of the specimens before and after testing are presented in Figure 3 and Figure 4



Figure 3: Photographs of specimens prior to testing.

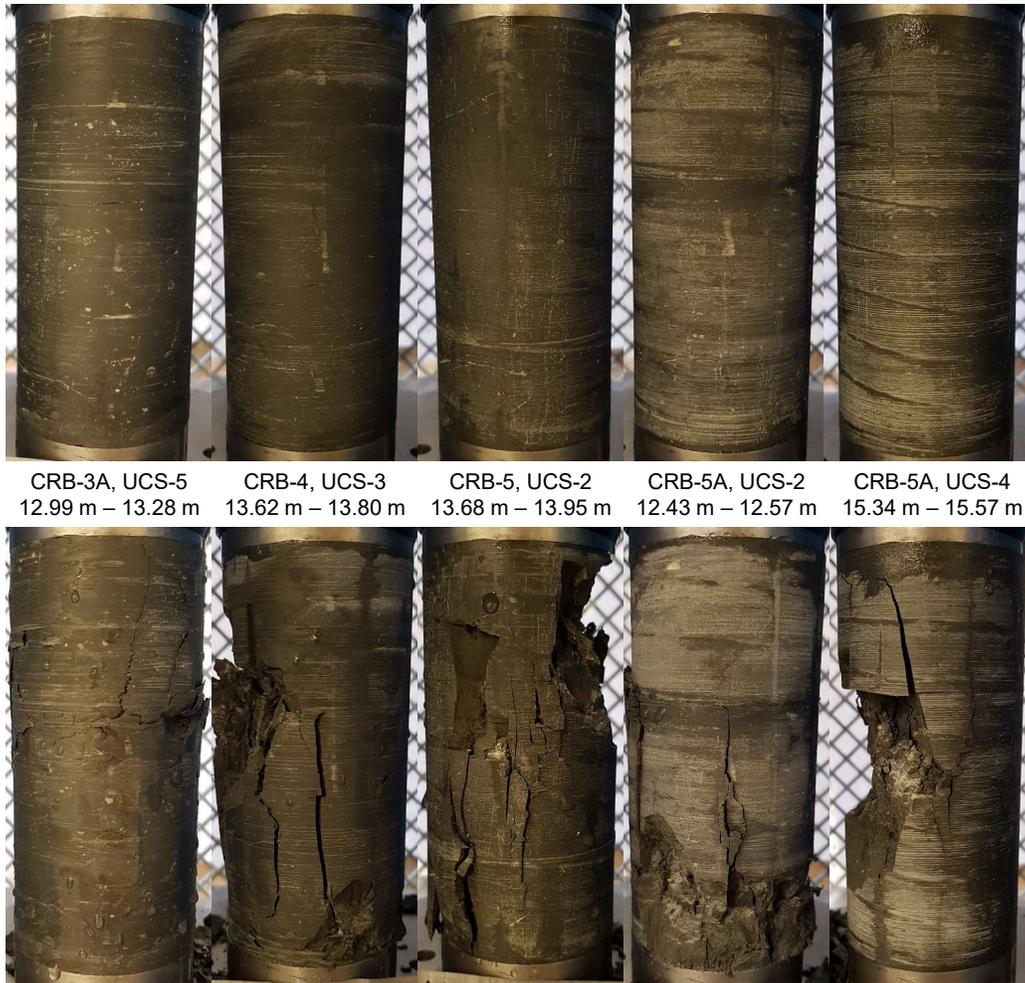


Figure 4: Photographs of failed specimens after testing.

August 27, 2018

Mr. David Marmor  
Golder Associates Ltd.  
6925 Century Avenue, Suite #100  
Mississauga, Ontario  
Canada L5N 7K2

Re: UCS only and UCS + E testing  
(Golder Project No. 1662333)

Dear Mr. Marmor:

On July 31, 2018 and August 17, 2018 seven (7) and six (6) HQ-sized core samples were received by Geomechanica Inc. via drop-off by Golder personnel, respectively. These samples were identified as being from boreholes drilled as part of Golder project 1662333. A total of 13 uniaxial compressive strength (UCS) specimens were prepared and tested from these samples. The tangent elastic modulus was measured for 5 of these 13 tests.

Details regarding the steps of specimen preparation and testing along with the test results and specimen photographs before and after testing are presented in the accompanying laboratory report.

Sincerely,



Bryan Tatone Ph.D., P. Eng.

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# Rock Laboratory Testing Results

**A report submitted to:**

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**August 27, 2018**

Project number: 1662333

**Abstract**

This document summarizes the results of rock laboratory testing of 13 uniaxial compressive strength (UCS) tests. Results, including uniaxial compressive strength (UCS) and Young's modulus (for select samples) along with photographs of samples before and after testing are presented. Additional specimen information is included in an accompanying summary spreadsheet.

**In this document:**

1	Uniaxial Compressive Strength (UCS) testing	1
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## 1 Uniaxial Compressive Strength (UCS) testing

This report summarizes the results of 13 uniaxial compressive strength (UCS) tests. The testing was performed in Geomechanica's rock testing laboratory using a 150 ton (1.3 MN) Forney loading frame equipped with pressure-compensated control valve to maintain an axial displacement rate of approximately 0.15 mm/min for shale and 0.075 mm/min for limestone samples (Figure 1). This displacement rate was selected to target specimen failure to occur within 2 - 15 minutes.

The specimen preparation and testing procedure included the following:

1. Unwrapping of the core sample, inspecting it for damage, and re-wrapping it in electrical tape to minimize exposure to moisture during subsequent specimen preparation.
2. Diamond cutting of core sample to obtain a cylindrical specimen with an appropriate length (length:diameter = 2:1) and nearly parallel end faces.
3. Diamond grinding of specimen to obtain flat (within  $\pm 0.025$  mm) and parallel end faces (within  $0.25^\circ$ ).
4. Placement of the specimen into the loading frame, applying a 1 kN axial load, and removing the electrical tape.
5. Axial loading to rupture while continuously recording axial force and axial deformation to determine the peak strength (UCS) and (tangent) Young's modulus ( $E$ ) for select samples.



Figure 1: UCS test setup.

## 1.1 Results

The results of the tests are summarized in Table 1. The corresponding stress-strain curves for the uniaxial compression tests are presented in Figure 2 and 3. Young's modulus is the tangent modulus, calculated as the slope of the best fit line through  $\pm 300$  data points on either side of the point representing 50.0% of the peak strength. Additional specimen information is included in the accompanying summary spreadsheet.

Table 1: Summary of laboratory test results.

Sample	Depth (m)	Lithology description	Bulk density $\rho$ (g/cm <sup>3</sup> )	UCS (MPa)	Young's Modulus $E$ (GPa)	Failure description
NRW3-7, SA-1	9.57 - 9.71	Georgian Bay Formation - Shale	2.596	14.4	0.68	Axial splitting <sup>1, 2</sup>
NWI-2, SA-1	5.06 - 5.31	Georgian Bay Formation - Shale	2.619	23.3	1.26	Inclined shear fracture <sup>2</sup>
NWI-3, SA-1	4.29 - 4.44	Georgian Bay Formation - Shale with several limestone lenses < 5 mm	2.601	16.8	-	Localized crushing <sup>2</sup>
NW5-4, SA-1	5.47 - 5.61	Georgian Bay Formation - Limestone	2.732	196.3	60.84	Inclined shear fracture
OHS-1, SA-1	5.26 - 5.44	Georgian Bay Formation - Shale	2.591	13.0	-	Inclined shear fracture <sup>2</sup>
OHS-2, SA-1	5.38 - 5.49	Georgian Bay Formation - Shale with 2 limestone layers $\approx 5$ mm thick	2.449	23.4	-	Hourglass failure <sup>1, 2</sup>
OHS-5, SA-1	6.13 - 6.27	Georgian Bay Formation - Shale	2.603	16.7	-	Axial splitting <sup>2</sup>
AR-2, SA-1	5.92 - 6.12	Georgian Bay Formation - Shale	2.574	9.1	-	Axial splitting <sup>2</sup>
AR-2, SA-2	8.60 - 8.82	Georgian Bay Formation - Shale	2.588	11.5	-	Axial splitting <sup>2</sup>
NW5-1, SA-1	4.29 - 4.45	Georgian Bay Formation - Shale	2.593	13.6	-	Hourglass failure <sup>2</sup>
SWME-4, SA-1	10.40 - 10.54	Georgian Bay Formation - Shale	2.586	13.5	-	Axial splitting <sup>2</sup>
HMPL-1, SA-1	4.81 - 4.96	Georgian Bay Formation - Shale	2.573	11.8	0.50	Localized crushing <sup>2</sup>
HMPL-2, SA-1	3.70 - 3.85	Georgian Bay Formation - Shale	2.594	13.7	0.88	Axial splitting <sup>2</sup>

<sup>1</sup> Specimen Length:Diameter ratio < 2 due to short sample length

<sup>2</sup> Specimen emitted pore water upon loading

## 1.2 Specimen photographs

Photographs of the specimens before and after testing are presented in Figures 4 to 6.

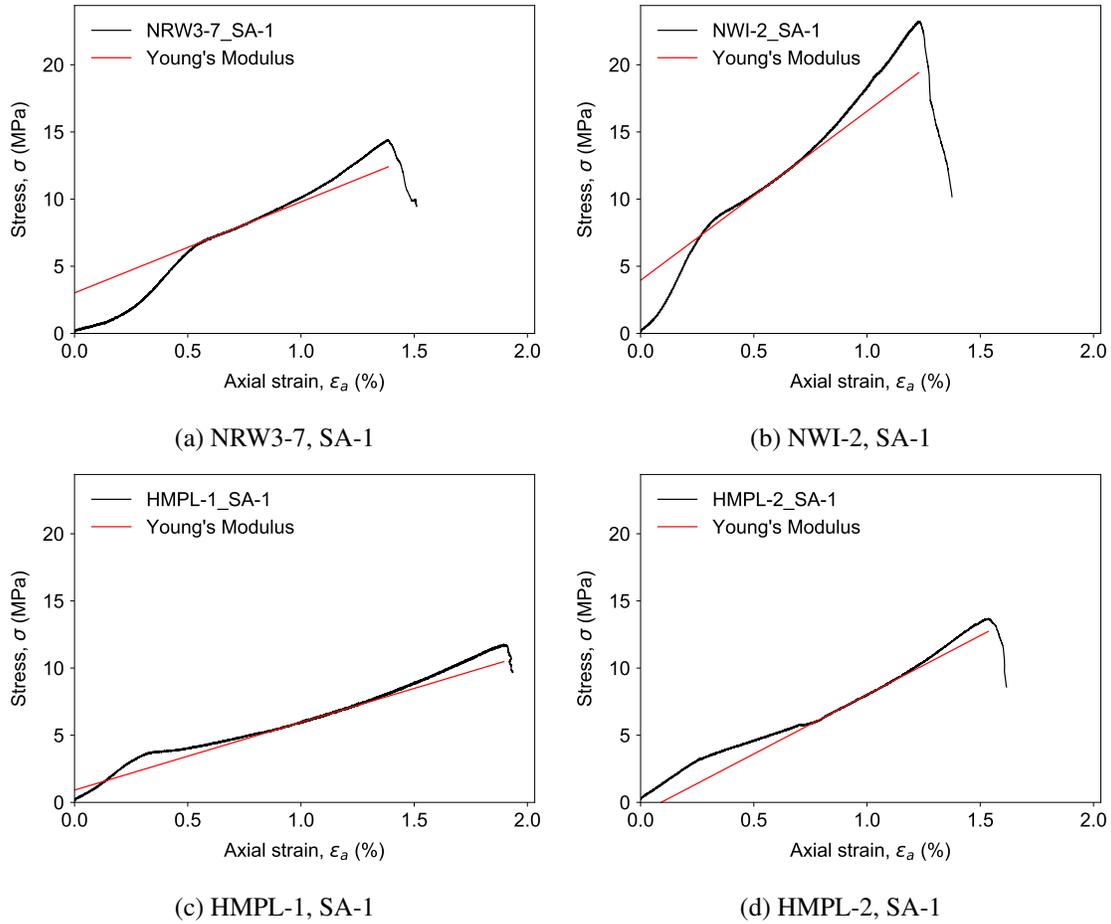


Figure 2: Measured stress-strain curves for shale samples.

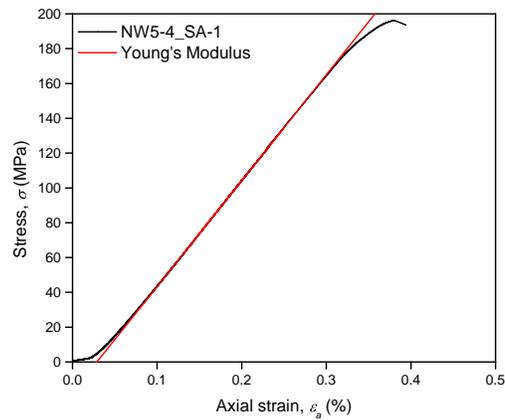


Figure 3: Measured stress-strain curves for limestone samples.

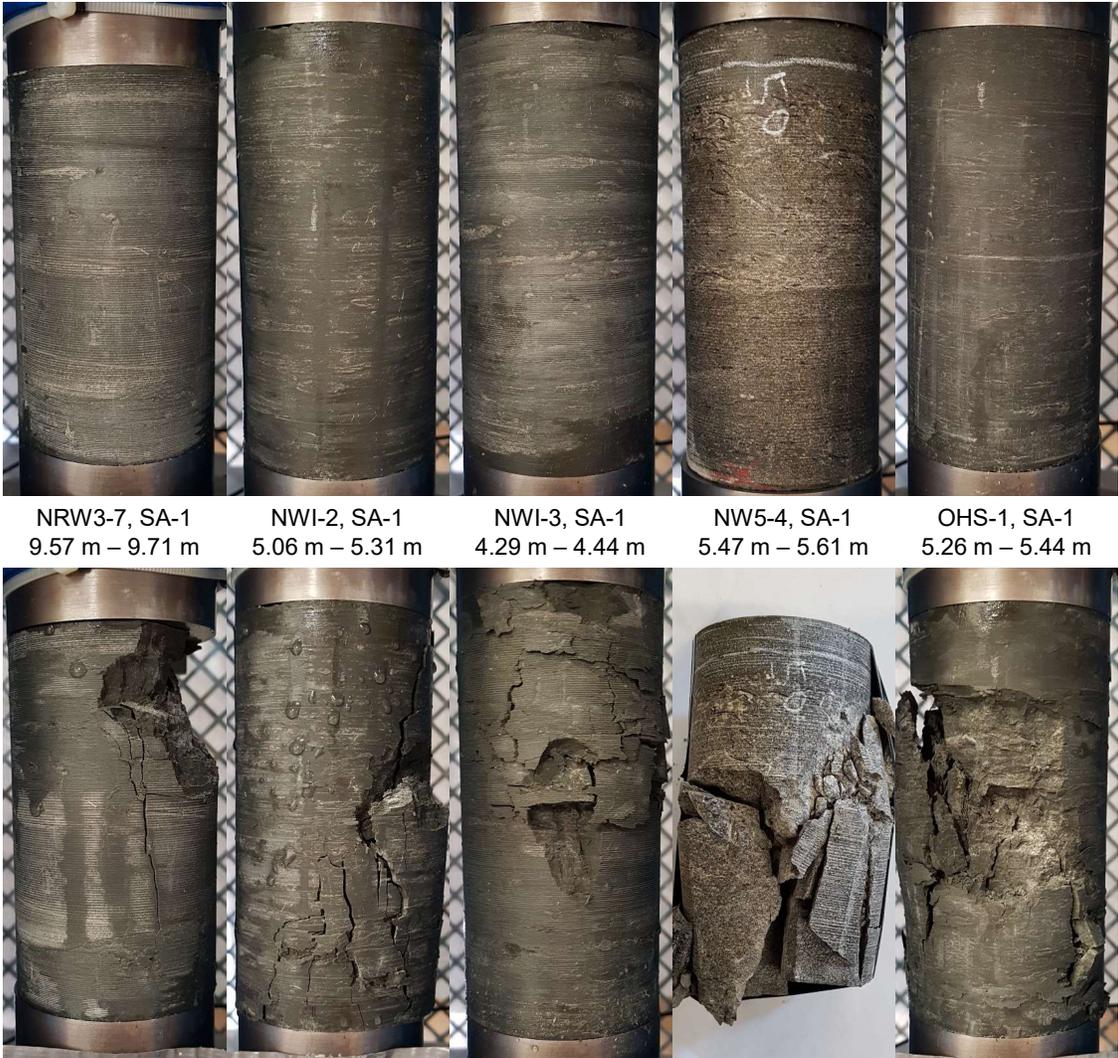


Figure 4: Photographs of specimens before and after testing.



Figure 5: Photographs of failed specimens before and after testing (continued).

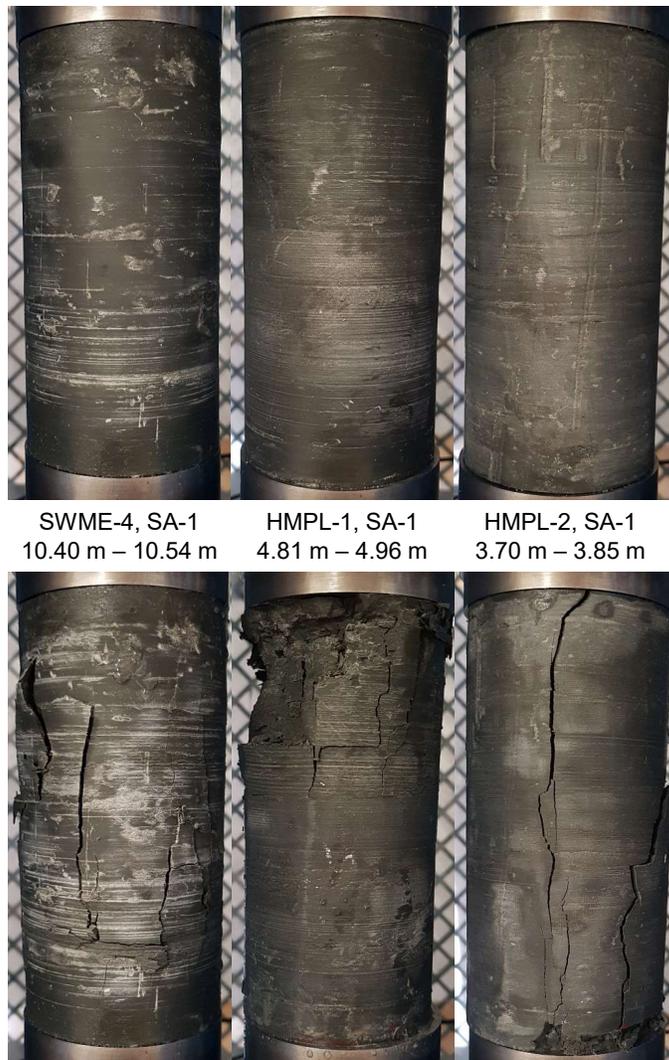


Figure 6: Photographs of failed specimens before and after testing (continued).



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