



FINAL REPORT

**Foundation Investigation
Highway 417 Overhead Sign Replacements
Ottawa, Ontario**

G.W.P. 4173-15-00

Sites: 417-0120.6, 417-0120.0, 417-0119.3, 417-0119.4, 417-0119.5

Submitted to:

WSP Canada Group Limited

300-2611 Queensview Drive

Ottawa, Ontario

K2B 8K2

Submitted by:

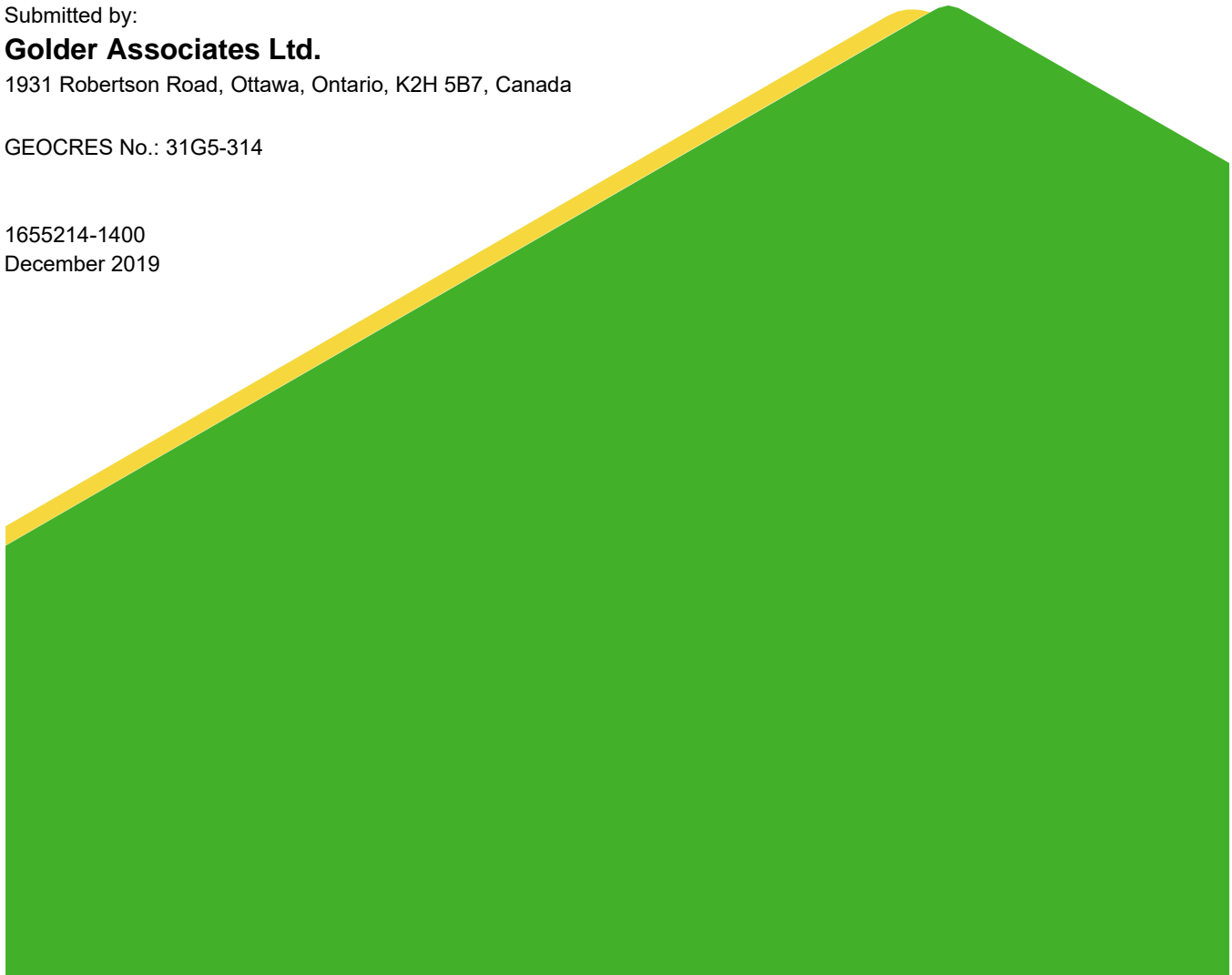
Golder Associates Ltd.

1931 Robertson Road, Ottawa, Ontario, K2H 5B7, Canada

GEOCREs No.: 31G5-314

1655214-1400

December 2019



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PART A

Foundation Investigation
Highway 417 Overhead Sign Replacements
Sites: 417-0120.6, 417-0120.0, 417-0119.3, 417-0119.4 and
417-0119.5
Ottawa, Ontario

1.0 INTRODUCTION

Golder Associates Ltd. (Golder) has been retained by WSP Canada Group Limited (WSP) on behalf of the Ministry of Transportation, Ontario (MTO) to carry out foundation investigations associated with the detailed design of numerous bridge replacements, overhead signs, noise barrier walls, temporary roadway protection systems, replacement of storm sewers (including trenchless crossings) and a high fill embankment on Highway 417 between Island Park Drive and Kent Street in Ottawa, Ontario (Assignment number 4016-E-0001).

This report presents the results of the foundation investigation carried out for the replacement of existing overhead signs and bridge mounted signs along Highway 417 between the CPR/O-Train overpass to the Kent Street overpass (Sites 417-0120.6, 417-0120.0, 417-0119.3, 417-0119.4 and 417-0119.5). The replacement of the signs is to be carried out in accordance with the current MTO Sign Support Manual, dated February 2019, and in accordance with the current Canadian Highway Bridge Design Code CAN/CSA-S6-14 (CHBDC).

The terms of reference and scope of work for the foundation investigation are outlined in the MTO's Request for Proposal, dated April 2016, and subsequent addenda. Golder's scope of work for foundation engineering services associated with the Highway 417 overhead sign replacement project is contained in Table 17.8.3 of WSP's Technical Proposal for this assignment dated June 28, 2016. The work has been carried out in accordance with Golder's Quality Control Plan for foundation engineering services for the project dated August 29, 2016.

2.0 SITE DESCRIPTION AND GEOLOGY

2.1 Site Description

The overhead signs are located along Highway 417 between the CPR/O-Train overpass and Kent Street in the City of Ottawa. The locations of the overhead sign structures are shown on the Key Plan on Drawings 1 through 5 and are detailed below.

The description and stationing for the proposed overhead signs (OHS) is based on information provided on the revised Sheet 316 of the 60% Contract Drawings provided by WSP on October 18, 2019. A copy of the revised Sheet 316 has been provided after the text of this report.

- Site 417-0120.6, the Bronson Avenue/Rochester Street overhead sign, is located at Station 27+021 in the eastbound lanes just west of Preston Street; see Drawing 1,
- Site 417-0120.0, the Bronson Avenue overhead sign, is located at Station 27+603 in the eastbound lanes about 180 m west of Bronson Avenue; see Drawing 2,
- Site 417-0119.3, the Bronson Avenue overhead sign, is located at Station 28+105 in the westbound lanes just east of Percy Street; see Drawing 3,
- Site 417-0119.4, the Kent Street overhead sign, is located at Station 28+269 in the eastbound lanes about 125 m west of Lyon Street; see Drawing 4, and
- Site 417-0119.5, the Bronson Avenue overhead sign, is located at Station 28+478 in the westbound direction just west of Kent Street; see Drawing 5.

At these locations, Highway 417 is a divided highway with three or four travel lanes in each direction separated by a concrete barrier wall.

2.2 Regional Geology

As delineated in *The Physiography of Southern Ontario*¹, this section of Highway 417 lies within the minor physiographic region known as the Ottawa Valley Clay Plain, which lies within the major physiographic region of the Ottawa-St. Lawrence Lowland.

The Ottawa Valley Clay Plain region is characterized by relatively thick deposits of sensitive marine clay, silt and silty clay that were deposited within the former Champlain Sea basin. These deposits, known as the Champlain Sea clay or Leda clay, overlie relatively thin, commonly reworked glacial till and glaciofluvial deposits, that in turn overlie bedrock².

This region is underlain by a series of sedimentary rocks, consisting of sandstones, dolostones, limestones and shales that are, in turn, underlain at depth by igneous and metamorphic bedrock of the Precambrian Shield. Regional bedrock mapping indicates that the bedrock at this site is primarily limestone of the Verulam Formation³. The limestone is described as interbedded bioclastic, sublithographic to fine crystalline with very thin to medium bedded shale interbeds up to 8 cm thick.

Highway 417 crosses two main faults striking southeast to northwest. The more prominent fault, the Gloucester fault, crosses Highway 417 at the approximate location of Preston Street⁴. The second fault crosses Highway 417 at the approximate location of Kent Street. Bedding which is normally sub-horizontal often dips steeply adjacent to and within fault zones.

The sites fall within the Western Québec (WQ) seismic zone according to the Geological Survey of Canada. The WQ zone constitutes a large area which encompasses the urban areas of Montreal, Ottawa-Hull and Cornwall. Within the WQ zone recent seismic activity has been concentrated in two subzones; one along the Ottawa River and another more active subzone along the Montreal-Maniwaki axis. The two major earthquakes that have recently occurred in the WQ zone are the 1935 Témiscaming event, which had a magnitude (i.e., a measure of the intensity of the earthquake) of 6.2, and the 1944 Cornwall-Massena event, which had a magnitude of 5.6.

3.0 INVESTIGATION PROCEDURES

The field work for this investigation was carried out on May 13, 2019 and between June 16 and July 25, 2019. The field investigation included advancing a total of ten boreholes, numbered 19-401 to 19-410, inclusive.

Two boreholes, one at each sign pedestal, were advanced at the proposed location of each overhead sign listed in Section 2. All boreholes were advanced within Highway 417, except for Borehole 19-405 which was advanced to the north of Highway 417 at the base of the highway embankment within the City of Ottawa Yard at 380 Catherine Street.

¹ Chapman, L. J. and Putnam, D. F., 1984. *The Physiography of Southern Ontario*, Ontario Geological Survey. Special Volume 2, Third Edition. Accompanied by Map P.2715, Scale 1:600,000. Ontario Ministry of Natural Resources.

² Belanger, J.R. "Urban Geology of Canada's National Capital Area", in *Urban Geology of Canadian Cities*, Geological Association of Canada Special Paper 42, Ed. P.F. Karrow and O.L. White, 1998.

³ Williams, D.A. Rae, A.M., and Wolf, R.R. 1984: Paleozoic Geology of the Ottawa Area, Southern Ontario, Ontario Geological Survey, Map P.2716. Geological Series-Preliminary Map, scale 1:50,000. Geology 1982.

⁴ MacDonald, G. and Harrison, J.E. 1976: Generalized Bedrock Geology, Ottawa-Hull, Ontario and Quebec, Geological Survey of Canada, Map 1508A, scale 1:125,000. Geology 1967.

The boreholes were advanced using a truck-mounted drill rig supplied and operated by George Downing Estate Drilling of Grenville-sur-la-rouge, Québec.

Traffic control required to close the driving lanes of Highway 417 while carrying out field operations was provided by Beacon Lite Ltd. of Ottawa Ontario.

The boreholes were advanced to depths within the overburden ranging from 4.3 to 10.4 m below the existing ground surface. Soil samples in the boreholes were obtained at vertical intervals of about 0.76 m, using a 50 mm outer diameter split-spoon sampler in accordance with Standard Penetration Test (SPT) procedure (ASTM D1586).

Boreholes 19-401 to 19-405 were further extended into the underlying bedrock using rotary diamond drilling techniques while retrieving NQ sized bedrock cores. Within these boreholes, the drilled length into the bedrock ranged from 3.1 to 4.9 m (i.e., total borehole depths ranging from about 7.7 to 13.2 m).

Monitoring wells were installed in Boreholes 19-402, 19-403, 19-405, 19-408 and 19-410 to observe the stabilised groundwater level at the sites. The monitoring wells consisted of 32 mm outside diameter PVC tubing with 1.5 to 3.0 m long screens. Table 3 summarizes the depths and the elevations of the groundwater levels measured in the monitoring wells installed at the sites. After taking the final water level readings the wells were subsequently decommissioned according to Ontario MOE Regulation 903 (O.Reg 903) by a licenced well technician.

The boreholes were backfilled with bentonite within the bedrock and bentonite mixed with soil cuttings within the overburden and capped with asphaltic concrete cold patch. The boreholes were backfilled in general accordance with the intent of Ontario MOE Regulation 903, as amended. The site conditions were restored following completion of the field work.

In addition to the borehole investigations, groundwater sampling was carried out in Borehole 19-405 by WSP for environmental testing. Further details with regards to material handling, reuse and/or disposal are provided in WSP's 2018 Phase II ESA and Earth Management Plan Reports, which are provided under separate cover.

The field work was supervised on a full-time basis by members of Golder's staff who located the boreholes in the field, directed the drilling, sampling, and in-situ testing operations, logged the boreholes and examined and cared for the samples. The soil and bedrock samples were identified in the field, placed in labelled containers, and transported to Golder's laboratory in Ottawa for further examination and testing. Index and classification tests consisting of moisture content determinations, Atterberg Limits, grain size distribution analyses and organic content testing were carried out on selected soil samples at Golder's Ottawa laboratory. Unconfined compressive strength testing was carried out on five samples of the bedrock core at Golder's Mississauga laboratory. The laboratory tests were carried out to MTO and/or ASTM Standards, as appropriate.

A total of six soil samples were submitted to Eurofins Environment Testing for chemical analysis related to potential corrosion of exposed buried steel and potential sulphate attack on buried concrete elements (corrosion and sulphate attack).

The testhole locations and elevations were surveyed by Golder using a Trimble R8 GPS unit referenced to the NAD83 CSRS CBNv6-2010.0 MTM Zone 9 geodetic datum. The borehole locations, including northing and easting coordinates, ground surface elevations, and borehole depths are summarized in Table 1.

Table 1: Summary of Borehole Locations

Borehole	Overhead Sign	Site (Highway 417 Direction)	NAD83 CSRS CBNv6-2010.0 MTM Zone 9		Ground Surface Elevation (m)	Borehole Depth (m)
			Northing (m)	Easting (m)		
19-401	OHS-1	Site 417-0120.6 (Eastbound)	5029510.2	366538.0	67.3	13.2
19-402			5029495.3	366541.9	67.0	10.8
19-403	OHS-2	Site 417-0120.0 (Eastbound)	5029679.4	367097.4	74.5	10.8
19-404			5029663.3	367103.3	74.6	7.7
19-405	OHS-3	417-0119.3 (Westbound)	5029901.7	367548.3	66.9	10.1
19-406			5029881.3	367556.4	73.6	10.4
19-407	OHS-4	Site 417-0119.4 (Eastbound)	5029955.2	367704.2	72.3	10.1
19-408			5029939.2	367712.7	72.3	10.1
19-409	OHS-5	417-0119.5 (Westbound)	5030080.3	367872.5	72.1	8.2
19-410			5030068.5	367878.7	72.4	9.8

4.0 DESCRIPTION OF SUBSURFACE CONDITIONS

4.1 General

The subsurface soil, bedrock and groundwater conditions encountered in the boreholes and the results of in-situ testing from the current investigation are given on the Record of Borehole and Drillhole sheets presented in Appendix A. The results of the laboratory testing carried out during the current investigation are presented on the Record of Borehole sheets as well as on Figures B1 to B20 in Appendix B. The borehole locations and ground surface elevations at each overhead sign are provided on Drawings 1 to 5.

Photographs of the core recovered from the bedrock are shown on Figures A1 to A10 provided in Appendix A. The results of basic chemical analysis completed on select soil samples are provided in Appendix C.

The stratigraphic boundaries shown on the Record of Borehole sheets are inferred from observations of drilling progress and noncontinuous sampling and therefore, represent transitions between soil types rather than exact planes of geological change. The subsoil conditions will vary between and beyond the borehole locations.

4.2 Overburden

In general, the subsurface conditions at the borehole locations advanced at the proposed overhead sign locations consist of asphaltic concrete pavement overlying PCC concrete, overlying fill materials, overlying native silt, silty sand to sand and gravel overlying glacial till all underlain by limestone bedrock.

The groundwater level was measured at the sites at depths ranging from 2.8 to 10.0 m, corresponding to Elevations 69.1 to 57.0 m.

A more detailed description of the overburden soil deposits, bedrock geology and groundwater conditions encountered during the field investigation is provided in the following sections.

4.3 Site 417-0120.6: OHS-1

Boreholes 19-401 and 19-402 were advanced at the proposed location of the OHS-1. A detailed description of the subsurface conditions encountered in these boreholes is provided in the following sections.

4.3.1 Pavement

Boreholes 19-401 and 19-402 were advanced through the Highway 417 pavement structure. The thickness of the asphaltic concrete pavement at the borehole locations was 0.3 and 0.2 m respectively.

Portland Cement Concrete (PCC) was encountered below the asphaltic concrete in Borehole 19-402 and is about 0.3 m in thickness.

4.3.2 Pavement Structure and Embankment Fills

Pavement structure fill consisting of gravelly sand to sand was encountered below the pavement and extends to depths of about 0.6 and 0.9 m at Boreholes 19-401 and 19-402, respectively.

Fill consisting predominantly of sand with varying amounts of silt and gravel was encountered below the pavement structure in both boreholes. The top of this layer was encountered at elevations 66.7 and 66.1 m and the layer extends to depths of about 3.1 and 2.1 m, respectively. Standard Penetration Tests (SPT) carried out within the fill material gave SPT N values ranging from 13 to 72, indicating a compact to very dense state of packing. The results of grain size distribution testing carried out on a selected sample of the fill are provided on Figure B1 in Appendix B. The measured moisture content of two samples of the fill were about 8 and 11 percent.

A sandy clayey silt fill was encountered below the sand fill in Boreholes 19-401 and 19-402 at elevations of 64.3 and 64.9 m, respectively. The clayey silt fill contains cobbles and boulders, ash, wood and organic matter. The clayey silt fill extends to depths below the existing ground surface of about 6.1 and 5.3 m. The SPT N values ranged from 2 to 16, indicating a firm to very stiff consistency. The measured moisture content of three samples of the fill ranged from about 20 to 29 percent. Results of grain size distribution testing carried out on three samples of this material are provided on Figure B2 in Appendix B. The results of Atterberg Limits testing carried out on two samples of this material indicates liquid limits of 29 and 30, plastic limits of 13 and 14, and plasticity indices of 16. The Atterberg Limits test results are provided on Figure B3 in Appendix B and indicate a clayey silt (CL) of low plasticity.

Fill consisting of gravel and sand with varying amounts of silt was encountered below the clayey silt fill in Borehole 19-401. This layer was encountered at Elevation 61.2 m and is about 2.2 m in thickness. Cobbles, ash and organic matter were encountered in this layer. The SPT N values ranged from 15 to greater than 50 but more typically 15 to 22, indicating a compact state of packing.

4.3.3 Clayey Silt

Clayey silt was encountered below the fill material in Borehole 19-402. This deposit was encountered at Elevation 61.7 m and is about 1.2 m in thickness. The SPT N values were 4 and 3 indicating a stiff consistency. The measured moisture content of a single sample of the clayey silt was 25 percent. Results of grain size distribution testing carried out a single sample of this material are provided on Figure B4 in Appendix B. The results of Atterberg Limits testing completed on a single sample of this material indicates a liquid limit of 34, a plastic limit of 16, and a plasticity index of 18. The Atterberg Limits test results are illustrated on Figure B5 in Appendix B and indicate a clayey silt of low plasticity (CL).

4.3.4 Gravel and Sand

Gravel and sand was encountered beneath the clayey silt in Borehole 19-402. The top of this deposit was encountered at Elevation 60.5 m with a thickness of about 1.2 m. One SPT N value of 52 was recorded, indicating a very dense condition.

The moisture content of one sample tested was 9 percent. The results of grain size analysis tests carried out on a single sample of this material are provided on Figure B6 in Appendix B.

4.4 Site 417-0120.0: OHS-2

Boreholes 19-403 and 19-404 were advanced at the proposed location of the OHS-2. A detailed description of the subsurface conditions encountered in these boreholes is provided in the following sections.

4.4.1 Pavement

Boreholes 19-403 and 19-404 were advanced through the Highway 417 pavement structure. The thickness of the asphaltic concrete pavement at the borehole locations ranges was 0.3 and 0.2 m.

Portland Cement Concrete (PCC) was encountered below the asphaltic concrete pavement in Borehole 19-404 and is about 0.3 m in thickness.

4.4.2 Pavement Structure and Embankment Fills

Pavement structure fill consisting of gravelly sand was encountered below pavement that extends to depths of about 0.7 m and 0.5 m in Boreholes 19-403 and 19-404, respectively.

Fill consisting predominantly of sand with varying amounts of silt was encountered below the pavement structure fill in both borehole locations. The sand fill extends to depths of about 3.8 and 2.1 m below the existing ground surface (at about Elevations 70.7 and 72.5 m), respectively. The SPT N values ranged from 3 to 54, but more typically 14 to 36, indicating a compact to dense state of packing. The measured moisture content of two samples of the fill were about 4 and 5 percent. The results of grain size distribution testing carried out on two selected samples of the sand fill are provided on Figure B7 in Appendix B.

Gravel and sand fill with varying amounts of silt was encountered below the sand fill in both boreholes that extends to depths below the existing ground surface of about 6.3 and 4.3 m (Elevations about 68.3 m and 70.3 m) respectively. Debris including brick, concrete, glass, wood and organic matter was encountered gravel and sand fill in Borehole 19-404 and organic matter was encountered in Borehole 19-403. The SPT N values ranged from 8 to greater than 50, indicating a loose to very dense state of packing. The moisture content of one sample of this material was measured at 9 percent. The results of grain size analysis tests carried out on a single sample of the sand and gravel fill are provided on Figure B8 in Appendix B.

4.4.3 Sand

Sand was encountered below the fill materials in Borehole 19-403. This deposit was encountered at Elevation 68.3 m and is about 0.6 m in thickness. One SPT N value of 45 was recorded, indicating a dense state of packing.

4.5 Site 417-0119.3: OHS-3

Boreholes 19-405 and 19-406 were advanced at the proposed location of OHS-3. Borehole 19-405 was advanced to the north of Highway 417 at the base of the highway embankment within the City of Ottawa Yard at 380 Catherine Street, while Borehole 19-406 was advanced through the Highway 417 pavement structure.

In addition to the borehole investigations groundwater sampling was carried out in Borehole 19-405 by WSP for environmental testing. Further details with regards to material handling, reuse and/or disposal are provided in WSP's 2018 Phase II ESA and Earth Management Plan Reports, which are provided under separate cover.

A detailed description of the subsurface conditions encountered in these boreholes is provided in the following sections.

4.5.1 Pavement

Asphaltic concrete pavement was encountered at the ground surface at both borehole locations. The thickness of the asphaltic concrete pavement at Borehole 19-405 was 0.1 m (City Yard) and 0.3 m at Borehole 19-406 (Highway 417).

4.5.2 Pavement Structure and Embankment Fills

Pavement structure fill consisting predominantly of gravel and sand was encountered below the asphaltic concrete pavement in both boreholes. The thickness of the pavement structure fill was 0.3 and 0.4 in Boreholes 19-405 and 19-406 respectively.

Embankment fill consisting of sand with varying amounts of silt and gravel, was encountered below the pavement structure fill in Borehole 19-406. This layer was encountered at Elevation 72.9 m and is about 7.7 m in thickness. The SPT N values ranged from 1 to 52, but were more typically 7 to 35, indicating a loose to dense state of packing. The measured moisture content of the samples tested ranged from 4 to 12 percent. The results of grain size analysis testing carried out on three samples of this material are provided on Figure B9 in Appendix B.

Sand fill was encountered below the pavement structure fill in Borehole 19-405. This layer was encountered at Elevation 66.5 m and is about 2.5 m in thickness. The SPT N values ranged from 6 to 36, but were more typically 6 to 7, indicating a loose state of packing.

4.5.3 Buried Topsoil

Buried topsoil was encountered below the embankment fill in Borehole 19-406. This layer was encountered at Elevation 65.2 m and is about 0.3 m in thickness.

4.5.4 Organic Silt and Sand

Organic silt was encountered below the fill materials in Borehole 19-405. This layer was encountered at Elevation 64.0 m and is about 0.6 m in thickness. The SPT N value was 4 indicating a loose state of packing. The measured moisture content of the sample tested was 47 percent. The results of organic content testing on a single sample indicated an organic content of 4%.

4.5.5 Sand and Gravel

Sand and gravel was encountered below the organic silt and sand in Borehole 19-405. This deposit was encountered at Elevation 63.4 m and is about 0.6 m in thickness.

4.5.6 Silt

Silt was encountered below the sand and gravel in Borehole 19-405. This deposit was encountered at Elevation 62.8 m and is about 2.0 m in thickness. The SPT N values were 16 and 17, indicating a compact state of packing. The measured moisture content of one sample tested was 20 percent. The results of grain size analysis testing carried out on a single sample of this material are provided on Figure B10 in Appendix B.

4.5.7 Silty Sand

Silty sand was encountered below the buried topsoil in Borehole 19-406. This deposit was encountered at Elevation 64.9 m and is about 1.4 m in thickness. An SPT N value of 4 indicates a loose state of packing. The measured moisture content of one sample tested was 34 percent. The results of grain size analysis testing carried out on a single sample of this material are provided on Figure B11 in Appendix B.

4.5.8 Glacial Till

Glacial till was encountered below the silt in Borehole 19-405 and the silty sand in Borehole 19-406. The glacial till generally consists of a heterogeneous mixture of cobbles within a soil matrix of silt, sand and gravel. The till is classified as sand and gravel to sandy silt with some gravel and clay. The thickness of the till layer at these locations was 0.9 and 0.3 m in Boreholes 19-405 and 19-406, respectively.

One SPT N value in the till of 7 indicates a loose state of packing. The moisture content of the two samples of till tested were 10 and 13 percent. The results of grain size analysis tests carried out on two samples of this material are provided on Figure B12 in Appendix B.

4.6 Site 417-0119.4: OHS-4

Boreholes 19-407 and 19-408 were advanced at the proposed location of OHS-4. A detailed description of the subsurface conditions encountered in these boreholes is provided in the following sections.

4.6.1 Pavement

Boreholes 19-407 and 19-408 were advanced through the Highway 417 pavement structure. The thickness of the asphaltic concrete pavement at the borehole locations was 0.3 and 0.1 m.

PCC was encountered below the asphaltic concrete pavement in Borehole 19-408 and is about 0.3 m in thickness.

4.6.2 Pavement Structure and Embankment Fills

Pavement structure fill consisting of sand and gravel with varying amounts of silt was encountered below the pavement and extends to depths of about 0.8 and 0.9 m. The measured moisture content of the sample tested was 2 percent. The results of grain size distribution testing carried out on a single sample of the pavement structure fill are provided on Figure B13 in Appendix B.

Sand fill with varying amounts of silt and gravel was encountered below the pavement structure fill in both boreholes locations. The thickness of the sand fill layer ranges from 6.7 to 7.5 m in Boreholes 19-407 and 19-408 respectively. The SPT N values in the sand fill layer ranged from 2 to 57, but were more typically 10 to 34, indicating a compact to dense state of packing. The measured moisture content of three samples of the sand fill ranged from about 5 to 7 percent. The results of grain size distribution testing carried out on three samples of the fill are provided on Figure B14 in Appendix B.

Silty clay fill was encountered below the sand fill in Borehole 19-407. This layer was encountered at Elevation 64.8 m and is about 0.7 m in thickness. The SPT N value was 7, indicating a stiff consistency.

4.6.3 Sandy Silt

Sandy silt was encountered below the fill material in Borehole 19-407. The top of this deposit was encountered at elevation 64.1 m and the deposit is about 0.8 m in thickness. One SPT N of 40 indicates a dense state of packing.

The moisture content of one sample tested was 19 percent. The results of a grain size analysis test carried out on a single sample of this material are provided on Figure B15 in Appendix B.

4.6.4 Glacial Till

A non-cohesive glacial till deposit consisting of a heterogeneous mixture of silt and sand with varying amounts of gravel, cobbles and boulders was encountered beneath the sandy silt in Borehole 19-407 and below the fill materials in Borehole 19-408. This deposit was encountered at elevations of 63.3 and 63.9 m respectively. The till was not fully penetrated but was proven to extend to depths of 10.1 m below pavement surface.

The SPT N values ranged from 13 to 88, indicating a compact to very dense state of packing. The higher blow counts (i.e., greater than 50) noted on the Record of Boreholes in the till may have been influenced by the underlying bedrock surface or the presence of cobbles or boulders within the till, rather than the state of packing of the soil matrix.

The moisture content of the two samples tested were 8 and 24 percent. The results of grain size analysis tests carried out on two samples of the till are provided on Figure B16 in Appendix B.

4.7 Site 417-0119.5: OHS-5

Boreholes 19-409 and 19-410 were advanced at the proposed location of OHS-5. A detailed description of the subsurface conditions encountered in these boreholes is provided in the following sections.

4.7.1 Pavement

Boreholes 19-409 and 19-410 were advanced through the Highway 417 pavement structure. The thickness of the asphaltic concrete pavement at both borehole locations was 0.3 m.

4.7.2 Pavement Structure and Embankment Fills

Pavement structure fill consisting of sand and gravel with varying amounts of silt was encountered below the pavement at both borehole locations extending to depths of about 2.0 and 2.1 m. The SPT N values ranged from 51 to 88, indicating a very dense state of packing. The measured moisture content of one sample of the pavement structure fill was 4 percent. The results of grain size distribution testing carried out on a single sample of this material are provided on Figure B17 in Appendix B.

Sand fill with varying amounts silt and gravel was encountered below the pavement structure fill at both borehole locations. This layer was encountered at Elevations 70.1 and 70.3 m and is about 3.2 m in thickness in Boreholes 19-409 and 19-410, respectively. The SPT N values ranged from 9 to 44, indicating a loose to dense state of packing. The measured moisture content of two samples of the fill was 7 percent. The results of grain size distribution testing carried out on two samples of the sand fill are provided on Figure B18 in Appendix B.

4.7.3 Silt and Sand

Silt and sand was encountered below the fill in both boreholes. The top of this deposit was encountered at Elevations 66.9 and 67.1 m and the thickness of the deposit is 0.7 and 1.1 m in Boreholes 19-409 and 19-410, respectively. The SPT N values were 12 and 28, indicating a compact state of packing.

The moisture content of the two samples tested were 22 and 23 percent. The results of grain size analysis tests carried out on two samples of the silt and sand are provided on Figure B19 in Appendix B.

4.7.4 Clay

Clay, grey in colour, was encountered below the silt and sand layer in both boreholes at Elevations 66.2 and 66.0 m respectively. The layer was not fully penetrated but was proven to extend to depths of about 8.2 and 9.8 m below the ground surface. The SPT N values in the clay layer ranged from 1 to 8. The results of in-situ vane testing in the clay layer gave undrained shear strength values ranging from about 42 to 85 kilopascals, indicating a firm to stiff consistency. Based on the ratio of the measured in-situ natural shear strength to the remolded shear strength ranging from 6 to 7, the clay is classified as sensitive.

The results of grain size distribution testing carried out on three samples of the clay are provided on Figure B20 in Appendix B. The results of Atterberg Limits testing completed on three samples of this material indicated liquid limits ranging from 66 to 88, plastic limits ranging from 22 to 27, and plasticity indexes ranging from 43 and to 66. Atterberg Limits analysis results are illustrated on Figure B21 in Appendix B and indicate a clay (CH) of high plasticity. The moisture content of the samples tested ranged from 58 to 71 percent and is generally below the liquid limit.

4.8 Bedrock

The overburden materials are underlain by limestone bedrock with shale partings and interbeds.

Bedrock core samples were obtained in Boreholes 19-401 to 19-405 using NQ sized equipment. Photographs of the bedrock core are provided on Figures A1 to A10 in Appendix A.

Table 2 summarizes the depth to and the elevation of the bedrock surface as encountered at the borehole locations from the current investigation.

Table 2: Summary of Bedrock Surface Depths and Elevations

Borehole	Overhead Sign	Ground Surface Elevation (m)	Depth to the Bedrock Surface (m)	Bedrock Surface Elevation (m)
19-401	OHS-1	67.3	8.3	59.0
19-402		67.0	7.7	59.3
19-403	OHS-2	74.5	6.9	67.6
19-404		74.6	4.3	70.3
19-405	OHS-3	66.9	7.0	59.9

In general, the bedrock encountered was slightly weathered to fresh and thin to medium bedded. A thin layer of weathered bedrock was encountered within Borehole 19-403. Thin shale interbeds were also present in the bedrock cores. Rock Quality Designation (RQD) values measured on recovered bedrock core samples typically ranged from about 8 to 100 percent, but more generally ranged from about 65 to 100 percent indicating fair to excellent rock quality.

Results of unconfined compressive strength (UCS) testing carried out on five bedrock core samples are summarized on Figure B22 in Appendix B. The samples tested had UCS values ranging from 65 to 81 MPa, indicating a strong bedrock.

4.9 Groundwater Conditions

Monitoring wells were installed in Boreholes 19-402, 19-403, 19-405, 19-408 and 19-410 (one at each OHS location) to observe the stabilized groundwater level at the sites.

Table 3 summarizes the depths and the elevations of the groundwater levels measured in the monitoring wells installed at the site.

Table 3: Summary of Groundwater Conditions

Borehole	Overhead Sign	Screened Interval	Depth (m)	Elevation (m)	Date of Reading
19-402	OHS-1	Bedrock	10.0	57.0	July 31, 2019
19-403	OHS-2	Bedrock	5.4	69.1	August 20, 2019
19-405	OHS-3	Fill/ Sand and Gravel/Silt	2.8	64.1	June 19, 2019
19-408	OHS-4	Glacial Till	6.4	65.9	July 23, 2019
19-410	OHS-5	Clay	Monitoring well dry at the bottom of well at Elevation 63.0 m		August 19, 2019

It is expected that the groundwater level will be subject to fluctuations both seasonally and as a result of precipitation events.

4.10 Steel Corrosion and Sulphate Attack, Chemical Analysis

Six soil samples were submitted to Eurofins Environment Testing for chemical analysis related to the potential corrosion of exposed buried steel and potential sulphate attack on buried concrete elements (corrosion and sulphate attack). The test results are provided in Appendix C and are summarized in Table 4.

Table 4: Steel Corrosion and Sulphate Attack, Chemical Analysis

Borehole	Sample	Sample Depth (m)	Sample Type	Chloride (%)	Sulphate (%)	Electrical Conductivity (mS/cm)	pH	Resistivity (ohm-cm)
19-401	SS5	3.8 – 4.4	Fill	0.114	0.02	0.35	8.3	2,860
19-404	SS3	1.5 – 2.1	Fill	0.037	0.02	0.18	9.2	5,560
19-405	SS8	5.3 – 5.9	Silt	0.032	< 0.01	0.56	8.3	1,790
19-406	SS6	2.3 – 2.9	Fill	0.058	< 0.01	0.15	8.5	6,670
19-407	SS3	1.5 – 2.1	Till	0.022	0.01	0.18	9.1	5,560
19-410	SS5	3.8 – 4.4	Fill	0.038	< 0.01	0.17	8.5	5,880

5.0 CLOSURE

This report was prepared by Mr. Kenton Power, P.Eng. It was reviewed by Mr. Bill Cavers, P.Eng., a Senior Geotechnical Engineer and Associate of Golder. Mr. Fintan Heffernan, P.Eng. a Senior Consultant with Golder and the Designated MTO Foundations Contact for this project, carried out an independent quality control review of this report.

Golder Associates Ltd.



Kenton C. Power, P.Eng., M.A.Sc.
Geotechnical Engineer

A handwritten signature in blue ink, appearing to read "Bill Cavers".

William Cavers, P.Eng.
Associate, Senior Geotechnical Engineer

A handwritten signature in blue ink, appearing to read "F. J. Heffernan".

Fintan J. Heffernan, P.Eng.
Designated MTO Foundations Contact



KCP/WC/FJH/hwd

<https://golderassociates.sharepoint.com/sites/18579g/foundations/6-reports/1400-overhead-signs/3-final/1655214-1400-001-r-rev0-final-ohs-2019-12-02.docx>

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ASTM International:

- ASTM D1586 Standard Test Method for Standard Penetration Test (SPT) and Split-Barrel Sampling of Soils

Ontario Provisional Standard Drawing:

- OPSD 3090.101 Foundation, Frost Penetration Depths for Southern Ontario

Ontario Provincial Standard Specification:

- OPSS 903 Construction Specification for Deep Foundations
- OPSS 915 Construction Specification for Sign Support Structures

Ontario Water Resources Act:

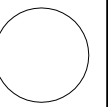
- Ontario Regulation 903 Wells

Ministry of Transportation, Ontario

- Ministry of Transportation Ontario. Sign Support Manual. Provincial Highways Management Division, Highway Standards Branch, Bridge Office. February 2019.

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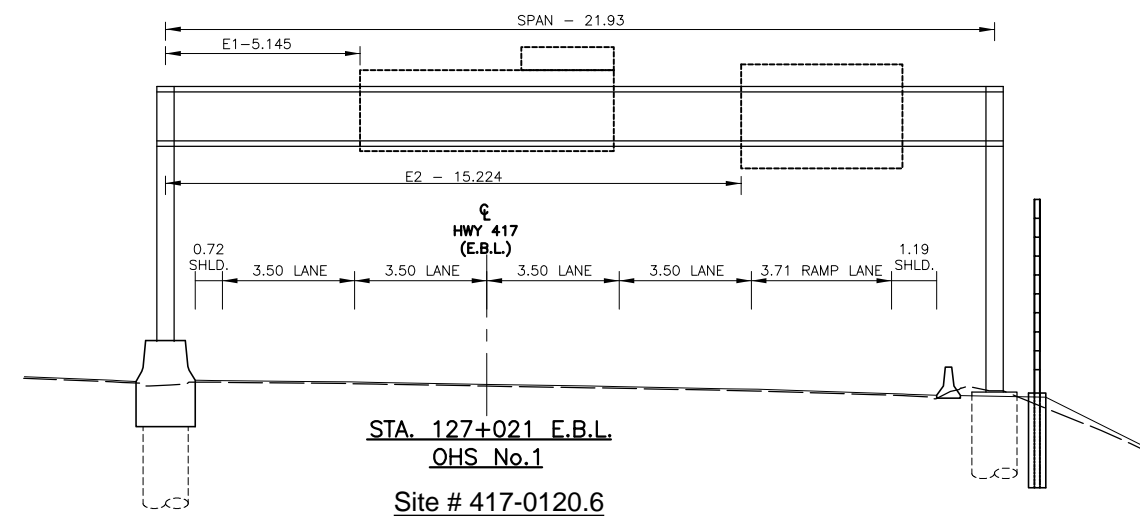
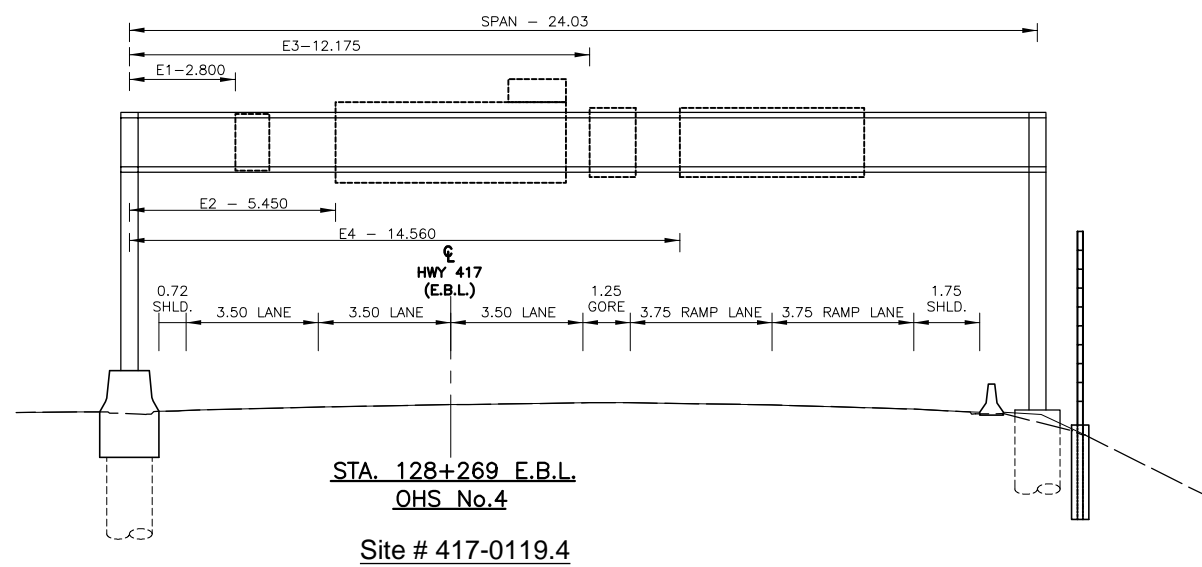
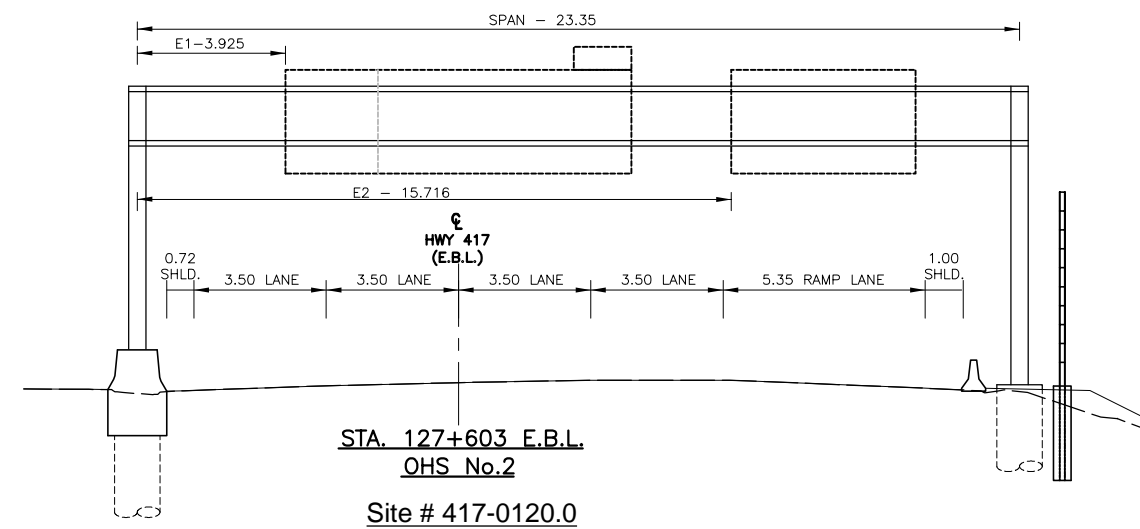
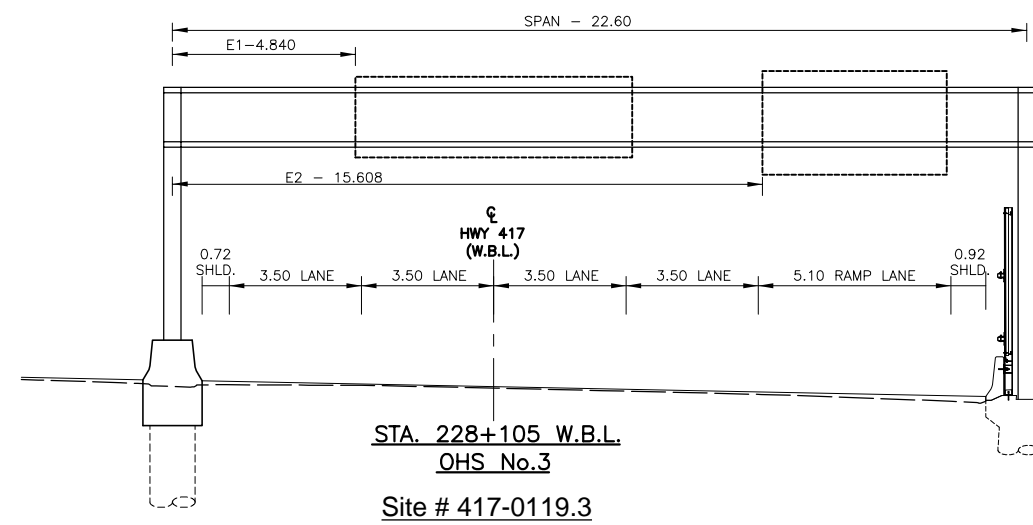
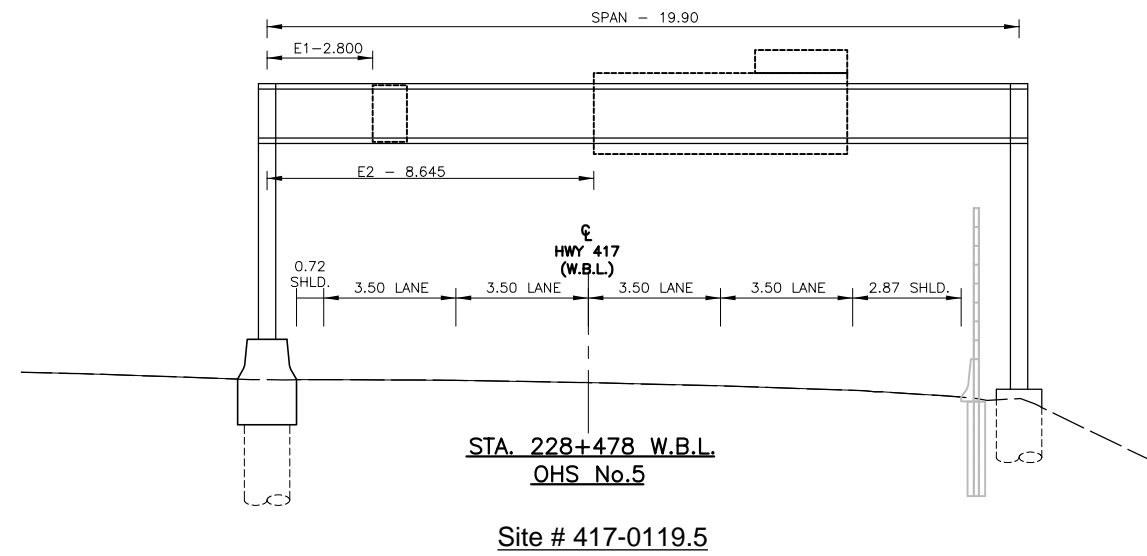
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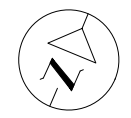
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BOREHOLE CO-ORDINATES NAD83 (CSRS)/MTM ZONE 9

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19-402	67.0	5029495.3	366541.9
19-403	74.5	5029679.4	367097.4
19-404	74.6	5029663.3	367103.3
19-405	66.9	5029901.7	367548.3
19-406	73.6	5029881.3	367556.4
19-407	72.3	5029955.2	367704.2
19-408	72.3	5029939.2	367712.7
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19-410	72.4	5030068.5	367878.7

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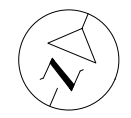
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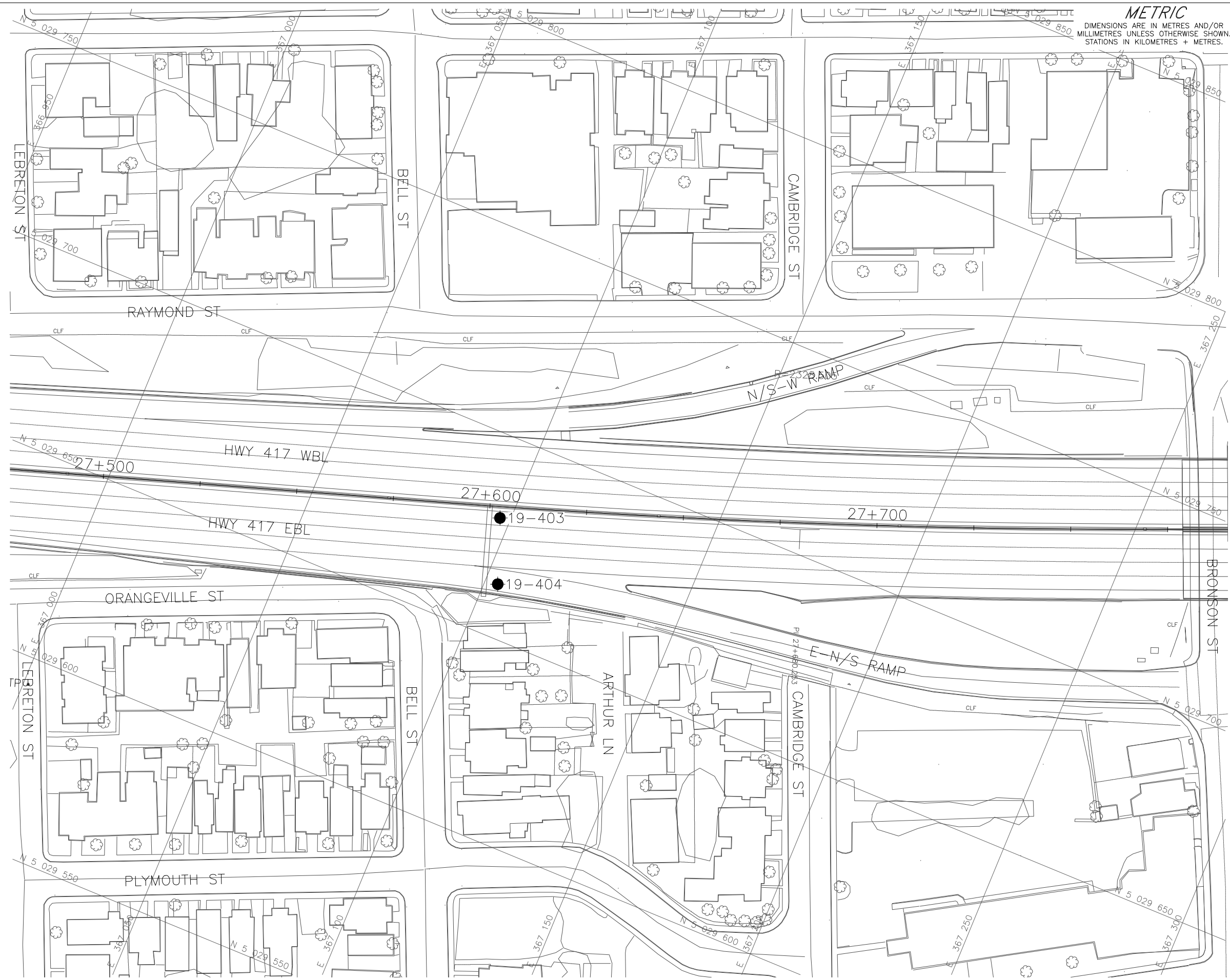
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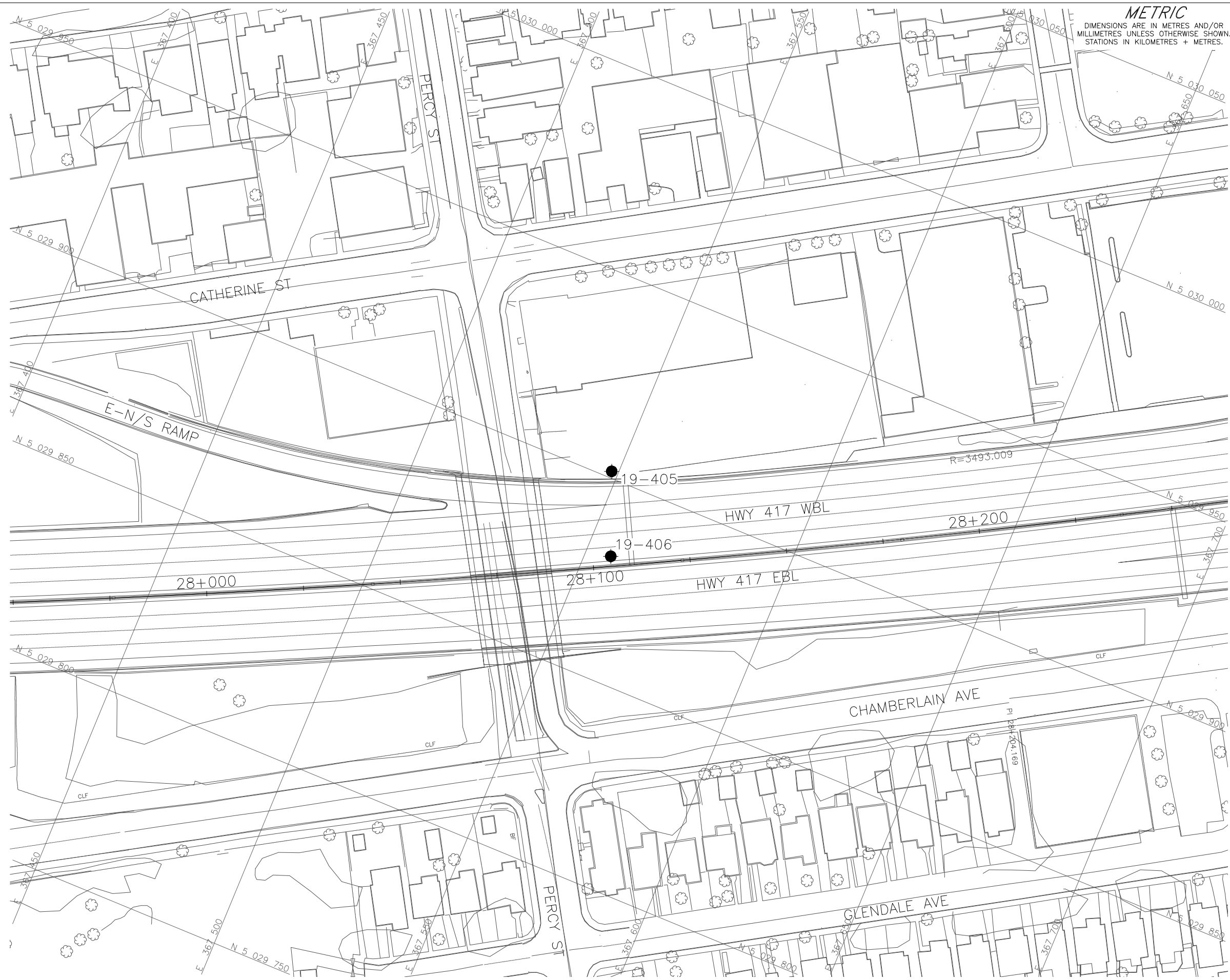
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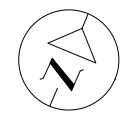
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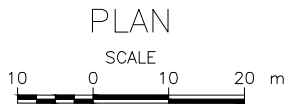
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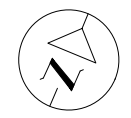
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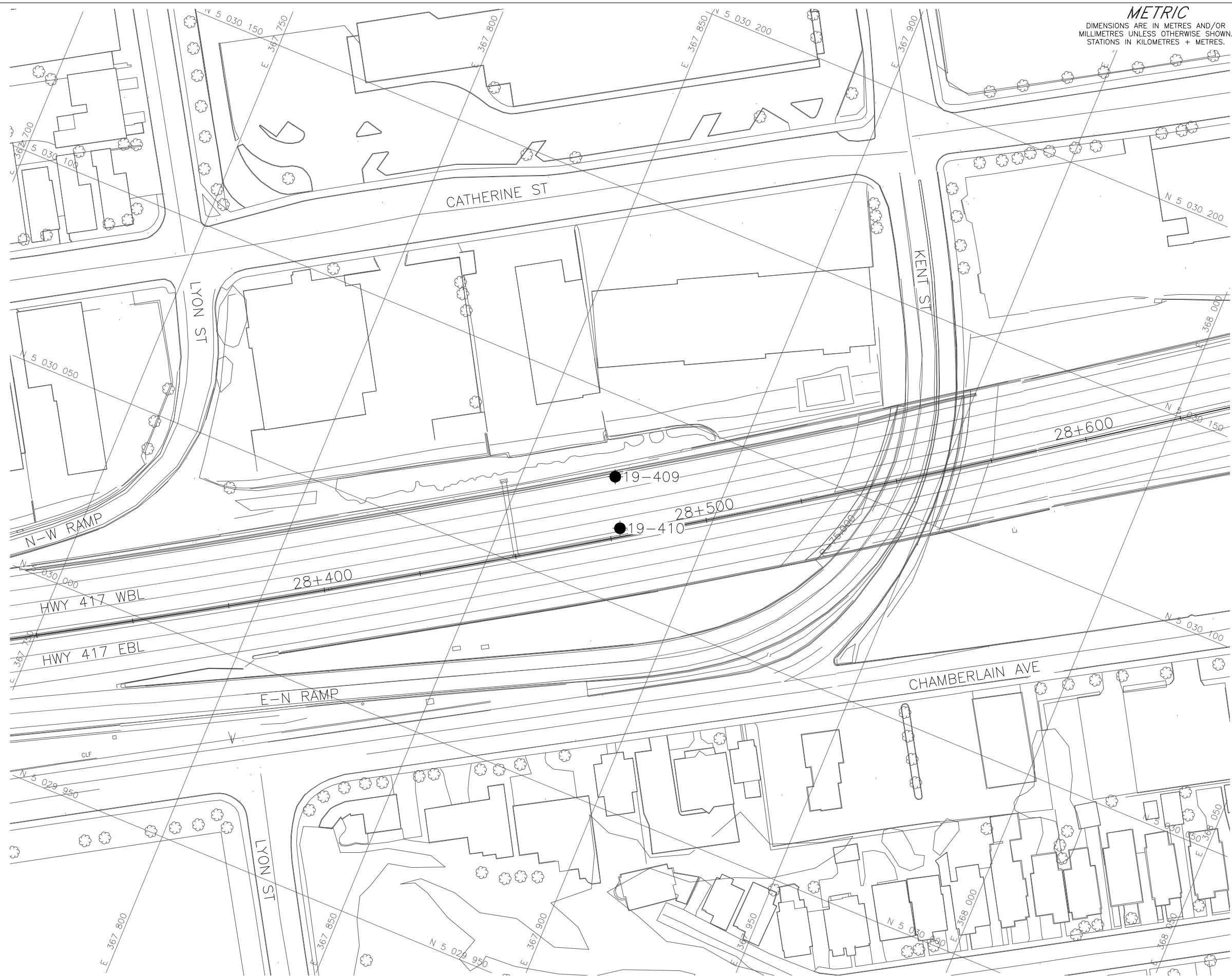


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19-403	74.5	5029679.4	367097.4
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19-406	73.6	5029881.3	367556.4
19-407	72.3	5029955.2	367704.2
19-408	72.3	5029939.2	367712.7
19-409	72.1	5030080.3	367872.5
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APPENDIX A

Lists of Abbreviations and Symbols
Lithological and Geotechnical Rock Description Terminology
Records of Boreholes and Drillholes 19-401 to 19-410
Bedrock Core Photographs, Figures A1 to A10

LIST OF SYMBOLS

Unless otherwise stated, the symbols employed in the report are as follows:

I.	GENERAL	(a)	Index Properties (continued)
π	3.1416	w	water content
$\ln x$,	natural logarithm of x	w_l or LL	liquid limit
\log_{10}	x or log x, logarithm of x to base 10	w_p or PL	plastic limit
g	acceleration due to gravity	I_p or PI	plasticity index = $(w_l - w_p)$
t	time	w_s	shrinkage limit
FoS	factor of safety	I_L	liquidity index = $(w - w_p) / I_p$
		IC	consistency index = $(w_l - w) / I_p$
		e_{max}	void ratio in loosest state
		e_{min}	void ratio in densest state
		I_D	density index = $(e_{max} - e) / (e_{max} - e_{min})$ (formerly relative density)
II.	STRESS AND STRAIN	(b)	Hydraulic Properties
γ	shear strain	h	hydraulic head or potential
Δ	change in, e.g. in stress: $\Delta \sigma$	q	rate of flow
ϵ	linear strain	v	velocity of flow
ϵ_v	volumetric strain	i	hydraulic gradient
η	coefficient of viscosity	k	hydraulic conductivity (coefficient of permeability)
ν	Poisson's ratio	j	seepage force per unit volume
σ	total stress	(c)	Consolidation (one-dimensional)
σ'	effective stress ($\sigma' = \sigma - u$)	C	compression index (normally consolidated range)
σ'_{vo}	initial effective overburden stress	C_r	recompression index (over-consolidated range)
$\sigma_1, \sigma_2, \sigma_3$	principal stress (major, minor)	C_s	swelling index
σ_{oct}	mean stress or octahedral stress $= (\sigma_1 + \sigma_2 + \sigma_3) / 3$	C_α	secondary compression index
τ	shear stress	m_v	coefficient of volume change
u	porewater pressure	C_v	coefficient of consolidation (vertical direction)
E	modulus of deformation	C_h	coefficient of consolidation (horizontal direction)
G	shear modulus of deformation	T_v	time factor (vertical direction)
K	bulk modulus of compressibility	U	degree of consolidation
III.	SOIL PROPERTIES	σ'_p	pre-consolidation stress
(a)	Index Properties	OCR	over-consolidation ratio = σ'_p / σ'_{vo}
$\rho(\gamma)$	bulk density (bulk unit weight)*	(d)	Shear Strength
$\rho_d(\gamma_d)$	dry density (dry unit weight)	τ_p, τ_r	peak and residual shear strength
$\rho_w(\gamma_w)$	density (unit weight) of water	ϕ'	effective angle of internal friction
$\rho_s(\gamma_s)$	density (unit weight) of solid particles	δ	angle of interface friction
γ'	unit weight of submerged soil ($\gamma' = \gamma - \gamma_w$)	μ	coefficient of friction = $\tan \delta$
D_R	relative density (specific gravity) of solid particles ($D_R = \rho_s / \rho_w$) (formerly G_s)	c'	effective cohesion
e	void ratio	c_u, s_u	undrained shear strength ($\phi = 0$ analysis)
n	porosity	p	mean total stress $(\sigma_1 + \sigma_3) / 2$
S	degree of saturation	p'	mean effective stress $(\sigma'_1 + \sigma'_3) / 2$
		q	$(\sigma_1 - \sigma_3) / 2$ or $(\sigma'_1 - \sigma'_3) / 2$
		q_u	compressive strength $(\sigma_1 - \sigma_3)$
		S_t	sensitivity
* Density symbol is ρ . Unit weight symbol is γ where $\gamma = \rho g$ (i.e. mass density multiplied by acceleration due to gravity)		Notes:	$\tau = c' + \sigma' \tan \phi'$ shear strength = (compressive strength) / 2

LIST OF ABBREVIATIONS

The abbreviations commonly employed on Records of Boreholes, on figures and in the text of the report are as follows:

I. SAMPLE TYPE

AS	Auger sample
BS	Block sample
CS	Chunk sample
DS	Denison type sample
FS	Foil sample
RC	Rock core
SC	Soil core
SS	Split-spoon
ST	Slotted tube
TO	Thin-walled, open
TP	Thin-walled, piston
WS	Wash sample

II. PENETRATION RESISTANCE

Standard Penetration Resistance (SPT), N:

The number of blows by a 63.5 kg. (140 lb.) hammer dropped 760 mm (30 in.) required to drive a 50 mm (2 in.) drive open sampler for a distance of 300 mm (12 in.)

Dynamic Cone Penetration Resistance; N_d :

The number of blows by a 63.5 kg (140 lb.) hammer dropped 760 mm (30 in.) to drive uncased a 50 mm (2 in.) diameter, 60° cone attached to "A" size drill rods for a distance of 300 mm (12 in.).

PH: Sampler advanced by hydraulic pressure

PM: Sampler advanced by manual pressure

WH: Sampler advanced by static weight of hammer

WR: Sampler advanced by weight of sampler and rod

Piezo-Cone Penetration Test (CPT)

A electronic cone penetrometer with a 60° conical tip and a project end area of 10 cm² pushed through ground at a penetration rate of 2 cm/s. Measurements of tip resistance (Q_t), porewater pressure (PWP) and friction along a sleeve are recorded electronically at 25 mm penetration intervals.

III. SOIL DESCRIPTION

(a) Non-Cohesive (Cohesionless) Soils

Compactness	N
Condition	Blows/300 mm or Blows/ft
Very loose	0 to 4
Loose	4 to 10
Compact	10 to 30
Dense	30 to 50
Very dense	over 50

(b) Cohesive Soils

Consistency	kPa	psf
Very soft	0 to 12	0 to 250
Soft	12 to 25	250 to 500
Firm	25 to 50	500 to 1,000
Stiff	50 to 100	1,000 to 2,000
Very stiff	100 to 200	2,000 to 4,000
Hard	over 200	over 4,000

IV. SOIL TESTS

w	water content
w _p	plastic limit
w _l	liquid limit
C	consolidation (oedometer) test
CHEM	chemical analysis (refer to text)
CID	consolidated isotropically drained triaxial test ¹
CIU	consolidated isotropically undrained triaxial test with porewater pressure measurement ¹
D _R	relative density (specific gravity, G _s)
DS	direct shear test
M	sieve analysis for particle size
MH	combined sieve and hydrometer (H) analysis
MPC	Modified Proctor compaction test
SPC	Standard Proctor compaction test
OC	organic content test
SO ₄	concentration of water-soluble sulphates
UC	unconfined compression test
UU	unconsolidated undrained triaxial test
V	field vane (LV-laboratory vane test)
γ	unit weight

Note: 1 Tests which are anisotropically consolidated prior to shear are shown as CAD, CAU.

V. MINOR SOIL CONSTITUENTS

Per cent by Weight	Modifier	Example
0 to 10	Trace	Trace sand
10 to 20	Some	Some sand
20 to 35	(ey) or (y)	Sandy
over 35	And	Sand and Gravel

LITHOLOGICAL AND GEOTECHNICAL ROCK DESCRIPTION TERMINOLOGY

WEATHERINGS STATE

Fresh: no visible sign of weathering

Faintly weathered: weathering limited to the surface of major discontinuities.

Slightly weathered: penetrative weathering developed on open discontinuity surfaces but only slight weathering of rock material.

Moderately weathered: weathering extends throughout the rock mass but the rock material is not friable.

Highly weathered: weathering extends throughout rock mass and the rock material is partly friable.

Completely weathered: rock is wholly decomposed and in a friable condition but the rock and structure are preserved.

BEDDING THICKNESS

<u>Description</u>	<u>Bedding Plane Spacing</u>
Very thickly bedded	Greater than 2 m
Thickly bedded	0.6 m to 2 m
Medium bedded	0.2 m to 0.6 m
Thinly bedded	60 mm to 0.2 m
Very thinly bedded	20 mm to 60 mm
Laminated	6 mm to 20 mm
Thinly laminated	Less than 6 mm

JOINT OR FOLIATION SPACING

<u>Description</u>	<u>Spacing</u>
Very wide	Greater than 3 m
Wide	1 m to 3 m
Moderately close	0.3 m to 1 m
Close	50 mm to 300 mm
Very close	Less than 50 mm

GRAIN SIZE

<u>Term</u>	<u>Size*</u>
Very Coarse Grained	Greater than 60 mm
Coarse Grained	2 mm to 60 mm
Medium Grained	60 microns to 2 mm
Fine Grained	2 microns to 60 microns
Very Fine Grained	Less than 2 microns

Note: * Grains greater than 60 microns diameter are visible to the naked eye.

CORE CONDITION

Total Core Recovery (TCR)

The percentage of solid drill core recovered regardless of quality or length, measured relative to the length of the total core run.

Solid Core Recovery (SCR)

The percentage of solid drill core, regardless of length, recovered at full diameter, measured relative to the length of the total core run.

Rock Quality Designation (RQD)

The percentage of solid drill core, greater than 100 mm length, as measured along the centerline axis of the core, relative to the length of the total core run. RQD varies from 0% for completely broken core to 100% for core in solid segments.

DISCONTINUITY DATA

Fracture Index

A count of the number of discontinuities (physical separations) in the rock core, including both naturally occurring fractures and mechanically induced breaks caused by drilling.

Dip with Respect to Core Axis

The angle of the discontinuity relative to the axis (length) of the core. In a vertical borehole a discontinuity with a 90° angle is horizontal.

Description and Notes

An abbreviation description of the discontinuities, whether naturally occurring separations such as fractures, bedding planes and foliation planes or mechanically induced features caused by drilling such as ground or shattered core and mechanically separated bedding or foliation surfaces. Additional information concerning the nature of fracture surfaces and infillings are also noted.

Abbreviations

JN Joint	PL Planar
FLT Fault	CU Curved
SH Shear	UN Undulating
VN Vein	IR Irregular
FR Fracture	K Slickensided
SY Stylolite	PO Polished
BD Bedding	SM Smooth
FO Foliation	SR Slightly Rough
CO Contact	RO Rough
AXJ Axial Joint	VR Very Rough
KV Karstic Void	
MB Mechanical Break	

RECORD OF BOREHOLE No 19-401 SHEET 1 OF 3 **METRIC**

PROJECT 1655214-1400

G.W.P. 4173-15-00 LOCATION N 5029510.2; E 366538.0 NAD 83 MTM ZONE 9 (LAT. 45.402816; LONG. -75.711366) ORIGINATED BY KM

DIST Eastern HWY 417 BOREHOLE TYPE Power Auger, 200 mm Diam. (Hollow Stem)/Rotary Drill, NQ Core COMPILED BY ZS

DATUM Geodetic DATE June 16-17, 2019 CHECKED BY SS/KCP

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)								
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20	40	60	80						100	20	40	60	80	100	25	50
67.3	GROUND SURFACE																							
0.0	ASPHALTIC CONCRETE																							
67.0																								
0.3	(SW) Gravelly sand (FILL) Brown Moist																							
66.7																								
0.6	(SP/SW) Sand, some gravel, contains cobbles (FILL) Very dense to dense Brown Moist		1	SS		72																		
			2	SS		46																		
65.0																								
2.3	(SM/ML) Silty sand, some gravel (FILL) Compact Grey Moist		3	SS		13																		
64.3																								
3.1	(CL) Sandy clayey silt, contains wood fibers, organic matter, ash, cobbles and boulders (FILL) Stiff to very stiff Brown, mottled		4	SS		5																		
			5	SS		10																		
			6	SS		16																		
			7	SS		50/0.20																		
61.2																								
6.1	(GP/SP) Gravel and sand (FILL) Compact Grey Moist		8	SS		15																		
60.6																								
6.7	(GM/SM) Gravelly silty sand, contains cobbles, organic matter and ash (FILL) Compact Grey brown Moist		9	SS		22																		
			10	SS		50/0.20																		
59.0																								
8.3	Limestone (BEDROCK) Bedrock cored from depths 8.3 m to 13.2 m For bedrock coring details refer to Record of Drillhole 19-401		1	RC		REC 100%																		RQD = 65%
			2	RC		REC 100%																		RQD = 61%

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 +³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

PROJECT <u>1655214-1400</u>	RECORD OF BOREHOLE No 19-401	SHEET 2 OF 3	METRIC
G.W.P. <u>4173-15-00</u>	LOCATION <u>N 5029510.2; E 366538.0 NAD 83 MTM ZONE 9 (LAT. 45.402816; LONG. -75.711366)</u>	ORIGINATED BY <u>KM</u>	
DIST <u>Eastern</u> HWY <u>417</u>	BOREHOLE TYPE <u>Power Auger, 200 mm Diam. (Hollow Stem)/Rotary Drill, NQ Core</u>	COMPILED BY <u>ZS</u>	
DATUM <u>Geodetic</u>	DATE <u>June 16-17, 2019</u>	CHECKED BY <u>SS/KCP</u>	

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC NATURAL LIQUID LIMIT MOISTURE LIMIT CONTENT			UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%)					
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20	40	60	80	100	W _p	W			W _L	25	50	75	GR
	--- CONTINUED FROM PREVIOUS PAGE ---																				
	Limestone (BEDROCK)		2	RC																	RQD = 61%
	Bedrock cored from depths 8.3 m to 13.2 m		3	RC	REC 47%	57															RQD = 18%
	For bedrock coring details refer to Record of Drillhole 19-401																				
						56															
			4	RC	REC 100%	55															RQD = 93%
54.1																					
13.2	END OF BOREHOLE																				

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PROJECT 1655214-1400	RECORD OF BOREHOLE No 19-402	SHEET 1 OF 3	METRIC
G.W.P. 4173-15-00	LOCATION N 5029495.3; E 366541.9 NAD 83 MTM ZONE 9 (LAT. 45.402682; LONG. -75.711319)	ORIGINATED BY RI	
DIST Eastern HWY 417	BOREHOLE TYPE Power Auger, 200 mm Diam. (Hollow Stem)/Rotary Drill, NQ Core	COMPILED BY ZS	
DATUM Geodetic	DATE June 18-19, 2019	CHECKED BY SS/KCP	

ELEV DEPTH	SOIL PROFILE DESCRIPTION	STRAT PLOT	SAMPLES		GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
			NUMBER	TYPE			"N" VALUES	20					
67.0	GROUND SURFACE												
0.0	ASPHALTIC CONCRETE												
0.2	PORTLAND CEMENT CONCRETE												
66.5													
0.5	(SW) Gravelly sand (FILL) Grey brown		1	GS									
66.1	(SP) Sand, trace gravel (FILL) Brown												
0.9	Moist (GP/SP) Gravel and sand, some silt (FILL) Compact to dense Dark brown Moist		2	SS	14								
64.9			3	SS	36							42 40 (18)	
2.1	(CL) Sandy clayey silt, contains organic matter, moderately fissured (FILL) Firm to stiff Grey brown		4	SS	4							2 23 41 34	
61.7			5	SS	2								
5.3	(CL) CLAYEY SILT, some sand Stiff Dark brown		8	SS	4							0 19 53 28	
60.5			9	SS	3								
6.5	(GW/SW) GRAVEL and SAND, some silt Very dense Dark brown Moist		10	SS	52							47 34 (19)	
59.3			11	SS	50/0.08								
7.7	Limestone (BEDROCK) Bedrock cored from depths 7.7 m to 10.8 m For bedrock coring details refer to Record of Drillhole 19-402		1	RC	REC 100%								RQD = 95%
			2	RC	REC 100%								RQD = 98%

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 +³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

PROJECT <u>1655214-1400</u>	RECORD OF BOREHOLE No 19-402	SHEET 2 OF 3	METRIC
G.W.P. <u>4173-15-00</u>	LOCATION <u>N 5029495.3; E 366541.9 NAD 83 MTM ZONE 9 (LAT. 45.402682; LONG. -75.711319)</u>	ORIGINATED BY <u>RI</u>	
DIST <u>Eastern</u> HWY <u>417</u>	BOREHOLE TYPE <u>Power Auger, 200 mm Diam. (Hollow Stem)/Rotary Drill, NQ Core</u>	COMPILED BY <u>ZS</u>	
DATUM <u>Geodetic</u>	DATE <u>June 18-19, 2019</u>	CHECKED BY <u>SS/KCP</u>	

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC NATURAL LIQUID LIMIT MOISTURE LIMIT CONTENT			UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%)		
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20	40	60	80	100	W _p	W			W _L	25
	--- CONTINUED FROM PREVIOUS PAGE ---																	
56.3			2	RC														GR SA SI CL RQD = 98%
10.8	END OF BOREHOLE		3	RC	REC 100%													RQD = 100%
	NOTES: 1. Water level in well screen at a depth of 10.0 m below ground surface (Elev. 57.0 m), measured on July 31, 2019.																	

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+³, X³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

RECORD OF BOREHOLE No 19-403 SHEET 1 OF 3 **METRIC**

PROJECT 1655214-1400

G.W.P. 4173-15-00 LOCATION N 5029679.4; E 367097.4 NAD 83 MTM ZONE 9 (LAT. 45.404289; LONG. -75.704201) ORIGINATED BY RI

DIST Eastern HWY 417 BOREHOLE TYPE Power Auger, 200 mm Diam. (Hollow Stem)/Rotary Drill, NQ Core COMPILED BY ZS

DATUM Geodetic DATE June 16-17, 2019 CHECKED BY SS/KCP

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20					
74.5	GROUND SURFACE												
0.0	ASPHALTIC CONCRETE												
74.2													
0.3	(SW) Gravelly sand (FILL) Grey		1	GS	-								
73.8													
0.7	(SM) Sand, some silt, trace gravel, contains clayey silt seams (FILL) Dense to very dense Brown Moist		2	SS	42								3 82 (15)
			3	SS	36								
			4	SS	54								
			5	SS	36								
70.7													
3.8	(GW/SW) Gravel and sand, some silt, trace clay, contains organic matter (rootlets) (FILL) Compact to loose Dark brown to black		6	SS	15								
			7	SS	9								
			8	SS	8								46 36 13 5
68.3													
6.3	(SP) SAND, trace silt Grey		9	SS	45								
67.6													
6.9	(BEDROCK) Weathered		10	SS	100/0.05								
67.3													
7.2	Limestone (BEDROCK) Bedrock cored from depths 7.2 m to 10.8 m For bedrock coring details refer to Record of Drillhole 19-403		1	RC	REC 100%								RQD = 98%
			2	RC	REC 100%								RQD = 99%

GTA-MTO 001 N:\ACTIVE\SPATIAL_IMMTO\HWY417REHAB&WIDENING02_DATA\GINT\1655214.GPJ GAL-GTA.GDT 12/3/19 JM

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 +³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

PROJECT 1655214-1400	RECORD OF BOREHOLE No 19-404	SHEET 1 OF 2	METRIC
G.W.P. 4173-15-00	LOCATION N 5029663.3; E 367103.3 NAD 83 MTM ZONE 9 (LAT. 45.404144; LONG. -75.704126)	ORIGINATED BY RI	
DIST Eastern HWY 417	BOREHOLE TYPE Power Auger, 200 mm Diam. (Hollow Stem)/Rotary Drill, NQ Core	COMPILED BY ZS	
DATUM Geodetic	DATE June 19-20, 2019	CHECKED BY SS/KCP	

ELEV DEPTH	SOIL PROFILE DESCRIPTION	STRAT PLOT	SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
			NUMBER	TYPE	"N" VALUES			20	40	60	80	100					
74.6	GROUND SURFACE																
0.0	ASPHALTIC CONCRETE																
0.2	PORTLAND CEMENT CONCRETE																
74.1																	
0.5	(SW) Gravelly sand (FILL) Grey (SM) Sand, some silt, trace gravel (FILL) Compact to very loose Brown Moist		1	GS	-		74										
			2	SS	14												6 81 (13)
			3	SS	3		73										
72.5																	
2.1	(SM) Gravelly silty sand, contains brick, mortar, wood, concrete, organic matter and glass (FILL) Compact to very dense Brown Moist		4	SS	17		72										
			5	SS	56												
			6	SS	53/0.15		71										
70.3																	
4.3	Limestone (BEDROCK) Bedrock cored from depths 4.3 m to 7.7 m For bedrock coring details refer to Record of Drillhole 19-404		1	RC	REC 100%		70										RQD = 99%
			2	RC	REC 100%		69										RQD = 99%
			3	RC	REC 100%		68										RQD = 100%
66.9							67										
7.7	END OF BOREHOLE																

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+³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

RECORD OF BOREHOLE No 19-405 SHEET 1 OF 3 **METRIC**

PROJECT 1655214-1400

G.W.P. 4173-15-00 LOCATION N 5029901.7; E 367548.3 NAD 83 MTM ZONE 9 (LAT. 45.406249; LONG. -75.698413) ORIGINATED BY PAH

DIST Eastern HWY 417 BOREHOLE TYPE Power Auger, 200 mm Diam. (Hollow Stem)/Rotary Drill, NQ Core COMPILED BY ZS

DATUM Geodetic DATE May 13, 2019 CHECKED BY SS/KCP

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)							
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	SHEAR STRENGTH kPa									WATER CONTENT (%)						
						20	40	60	80	100	20	40	60	80	100	25	50	75	GR	SA	SI	CL	
66.9	GROUND SURFACE																						
66.7	ASPHALTIC CONCRETE		1	GRAB	-																		
66.5	(SW) Gravelly sand (FILL) Grey																						
66.5	(SP) Sand, some gravel, contains wood pieces (FILL) Loose to dense Moist		2	SS	6																		
66.5			3	SS	36																		
66.5			4	SS	7																		
64.0	(OM,SP) Organic SILT and SAND Brown and grey Moist																						
64.0			5	SS	4																		
63.4	(SW/GW) SAND and GRAVEL Grey Wet																						
63.4			6	SS	25																		
62.8	(ML) SILT, some sand, trace clay, contains clayey silt seams Compact Grey Wet																						
62.8			7	SS	17																		
62.8			8	SS	16																		
60.8	(ML) Sandy SILT, some clay, trace gravel, contains cobbles (TILL) Loose Grey Wet																						
60.8			9	SS	7																		
59.9	Limestone (BEDROCK)		10	SS	11/0.15																		
7.0	Bedrock cored from depths 7.0 m to 10.1 m For bedrock coring details refer to Record of Drillhole 19-405		1	RC	REC 97%																		RQD = 40%
7.0			2	RC	REC 99%																		RQD = 91%
7.0			3	RC	REC 100%																		RQD = 100%
57																							

GTA-MTO 001 N:\ACTIVE\SPATIAL_IMMTO\HWY417REHAB&WIDENING\02_DATA\GINT\1655214.GPJ GAL-GTA.GDT 12/3/19 JM

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 +³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

PROJECT <u>1655214-1400</u>	RECORD OF BOREHOLE No 19-405	SHEET 2 OF 3	METRIC
G.W.P. <u>4173-15-00</u>	LOCATION <u>N 5029901.7; E 367548.3 NAD 83 MTM ZONE 9 (LAT. 45.406249; LONG. -75.698413)</u>	ORIGINATED BY <u>PAH</u>	
DIST <u>Eastern</u> HWY <u>417</u>	BOREHOLE TYPE <u>Power Auger, 200 mm Diam. (Hollow Stem)/Rotary Drill, NQ Core</u>	COMPILED BY <u>ZS</u>	
DATUM <u>Geodetic</u>	DATE <u>May 13, 2019</u>	CHECKED BY <u>SS/KCP</u>	

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC NATURAL LIQUID LIMIT MOISTURE LIMIT CONTENT			UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%)	
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20	40	60	80	100	W _p	W			W _L
56.8	--- CONTINUED FROM PREVIOUS PAGE ---	/ / /	3	RC													RQD = 100%
10.1	END OF BOREHOLE NOTES: 1. Water level in well screen at a depth of 2.8 m below ground surface (Elev. 64.1 m), measured on June 19, 2019.																

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+³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

PROJECT <u>1655214-1400</u>	RECORD OF BOREHOLE No 19-406	SHEET 2 OF 2	METRIC
G.W.P. <u>4173-15-00</u>	LOCATION <u>N 5029881.3; E 367556.4 NAD 83 MTM ZONE 9 (LAT. 45.406065; LONG. -75.698311)</u>	ORIGINATED BY <u>RI</u>	
DIST <u>Eastern</u> HWY <u>417</u>	BOREHOLE TYPE <u>Power Auger, 200 mm Diam. (Hollow Stem)</u>	COMPILED BY <u>ZS</u>	
DATUM <u>Geodetic</u>	DATE <u>June 20-21, 2019</u>	CHECKED BY <u>SS/KCP</u>	

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL		
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20	40	60	80						100	SHEAR STRENGTH kPa
	--- CONTINUED FROM PREVIOUS PAGE ---																	
68.7	(GP/SP) GRAVEL and SAND, some silt (TILL) Grey brown Wet END OF BOREHOLE NOTES: 1. Water level in open borehole at a depth of 8.6 m below ground surface (Elev. 73.6 m), upon completion of drilling.		16	SS	28													
63.2																		
10.4																		

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+³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

PROJECT <u>1655214-1400</u>	RECORD OF BOREHOLE No 19-407	SHEET 1 OF 2	METRIC
G.W.P. <u>4173-15-00</u>	LOCATION <u>N 5029955.2; E 367704.2 NAD 83 MTM ZONE 9 (LAT. 45.406716; LONG. -75.696414)</u>	ORIGINATED BY <u>DJG</u>	
DIST <u>Eastern</u> HWY <u>417</u>	BOREHOLE TYPE <u>Power Auger, 200 mm Diam. (Hollow Stem)</u>	COMPILED BY <u>ZS</u>	
DATUM <u>Geodetic</u>	DATE <u>June 17, 2019</u>	CHECKED BY <u>SS/KCP</u>	

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)		
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	SHEAR STRENGTH kPa									WATER CONTENT (%)	
						20	40	60	80	100				25	50	75		GR SA SI CL
72.3	GROUND SURFACE																	
0.0	ASPHALTIC CONCRETE																	
72.0																		
0.3	(SW/GW) Sand and gravel, some silt (FILL) Grey Dry		1	AS	-												40	48 (12)
71.5																		
0.8	(SP) Sand, trace silt (FILL) Compact to dense Brown Moist		2	SS	28													
			3	SS	46													
			4	SS	34												2	90 (8)
			5	SS	44													
			6	SS	37													
67.9	(SP) Sand, some gravel, contains crushed asphalt (FILL) Compact to loose Brown to dark brown Moist		7	SS	10													
			8	SS	4													
66.2	(SM) Silty sand, trace gravel, contains wood, brick, asphalt and construction debris (FILL) Very loose to compact Brown to dark brown moist		9	SS	2													
			10	SS	16													
64.8	(CI) Silty clay, trace gravel (FILL) Stiff Grey brown		11	SS	7													
64.1	(ML) Sandy SILT Dense Grey Wet		12	SS	40												0	31 67 2
63.3	(SM/ML) SAND and SILT, some gravel (TILL) Very dense Grey brown Moist		13	SS	88												13	41 (46)

GTA-MTO 001 N:\ACTIVE\SPATIAL_IMMTO\HWY417REHAB&WIDENING\02_DATA\GINT\1655214.GPJ GAL-GTA.GDT 12/3/19 JM

Continued Next Page

 +³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

PROJECT <u>1655214-1400</u>	RECORD OF BOREHOLE No 19-407	SHEET 2 OF 2	METRIC
G.W.P. <u>4173-15-00</u>	LOCATION <u>N 5029955.2; E 367704.2 NAD 83 MTM ZONE 9 (LAT. 45.406716; LONG. -75.696414)</u>	ORIGINATED BY <u>DJG</u>	
DIST <u>Eastern</u> HWY <u>417</u>	BOREHOLE TYPE <u>Power Auger, 200 mm Diam. (Hollow Stem)</u>	COMPILED BY <u>ZS</u>	
DATUM <u>Geodetic</u>	DATE <u>June 17, 2019</u>	CHECKED BY <u>SS/KCP</u>	

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC NATURAL LIQUID LIMIT MOISTURE LIMIT CONTENT			UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL	
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20	40	60	80	100	W _p	W			W _L
64.4	END OF BOREHOLE NOTES: 1. Water level in open borehole at depth of 7.8 m below ground surface (Elev. 64.5 m), upon completion of drilling.	XXXX															

GTA-MTO 001 N:\ACTIVE\SPATIAL_IMMTO\HWY417REHAB&WIDENING02_DATA\GINT\1655214.GPJ GAL-GTA.GDT 12/3/19 JM

+³, X³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

RECORD OF BOREHOLE No 19-408 SHEET 1 OF 2 **METRIC**

PROJECT 1655214-1400

G.W.P. 4173-15-00 LOCATION N 5029939.2; E 367712.7 NAD 83 MTM ZONE 9 (LAT. 45.406572; LONG. -75.696307) ORIGINATED BY KM

DIST Eastern HWY 417 BOREHOLE TYPE Power Auger, 200 mm Diam. (Hollow Stem) COMPILED BY ZS

DATUM Geodetic DATE June 19, 2019 CHECKED BY SS/KCP

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)									
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20	40	60	80						100	20	40	60	80	100	25	50	75
72.3	GROUND SURFACE																								
0.0	ASPHALT																								
71.9	PORTLAND CEMENT CONCRETE																								
0.4	(SW/GW) Sand and gravel (FILL) Grey Moist																								
71.4	(SM) Sand, some silt (FILL) Very dense to loose Brown		1	SS	42																				
0.9			2	SS	54																				1 83 (16)
			3	SS	57																				
			4	SS	34																				
			5	SS	45																				
			6	SS	9																				
			7	SS	25																				2 90 (8)
66.2	(SM) Gravelly silty sand, contains ash and brick (FILL) Compact Brown-black Moist		8	SS	28																				
65.4	(SM/ML) Sand and silt, contains organic matter, wood, ceramic, plastic and glass (FILL) Loose to compact Dark brown to black		9	SS	5																				
63.9	(SP/ML) SAND and SILT, some gravel, contains cobbles and boulders (TILL) Compact Grey		10	SS	12																				
8.4			11	SS	13																				12 46 (42)
			12	SS	50/0.03																				
			13	SS	50/0.03																				

GTA-MTO 001 N:\ACTIVE\SPATIAL_IMMTO\HWY417REHAB&WIDENING02_DATA\GINT\1655214.GPJ GAL-GTA.GDT 12/3/19 JM

Continued Next Page

 +³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

PROJECT <u>1655214-1400</u>	RECORD OF BOREHOLE No 19-408	SHEET 2 OF 2	METRIC
G.W.P. <u>4173-15-00</u>	LOCATION <u>N 5029939.2; E 367712.7 NAD 83 MTM ZONE 9 (LAT. 45.406572; LONG. -75.696307)</u>	ORIGINATED BY <u>KM</u>	
DIST <u>Eastern</u> HWY <u>417</u>	BOREHOLE TYPE <u>Power Auger, 200 mm Diam. (Hollow Stem)</u>	COMPILED BY <u>ZS</u>	
DATUM <u>Geodetic</u>	DATE <u>June 19, 2019</u>	CHECKED BY <u>SS/KCP</u>	

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20	40	60	80					
	--- CONTINUED FROM PREVIOUS PAGE ---															
66.2 10.1	END OF BOREHOLE NOTES: 1. Water level in well screen at a depth of 6.4 m below ground surface (Elev. 65.9 m), measured on July 23, 2019.	XXXX														

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+³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

PROJECT <u>1655214-1400</u>	RECORD OF BOREHOLE No 19-409	SHEET 1 OF 1	METRIC
G.W.P. <u>4173-15-00</u>	LOCATION <u>N 5030080.3; E 367872.5 NAD 83 MTM ZONE 9 (LAT. 45.407827; LONG. -75.694249)</u>	ORIGINATED BY <u>DJG</u>	
DIST <u>Eastern</u> HWY <u>417</u>	BOREHOLE TYPE <u>Power Auger, 200 mm Diam. (Hollow Stem)</u>	COMPILED BY <u>ZS</u>	
DATUM <u>Geodetic</u>	DATE <u>July 25, 2019</u>	CHECKED BY <u>SS/KCP</u>	

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)							
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	SHEAR STRENGTH kPa									WATER CONTENT (%)						
						20	40	60	80	100	20	40	60	80	100	25	50	75	GR	SA	SI	CL	
72.1	GROUND SURFACE																						
0.0	ASPHALTIC CONCRETE																						
71.8																							
0.3	(SW/GW) Gravelly sand (FILL) Very dense Grey		1	GS	-																		
			2	SS	81																		
			3	SS	55																		
70.1																							
2.0	(SM) Sand, some silt, trace gravel (FILL) Compact Brown Dry to moist		4	SS	15																		
			5	SS	22																		
			6	SS	27																		
			7	SS	16																		
66.9																							
5.2	(ML/SM) SILT and SAND Compact Grey brown		8	SS	12																		
66.2																							
5.9	(CH) CLAY Firm to stiff Grey		9	SS	4																		
			10	SS	2																		
63.9																							
8.2	END OF BOREHOLE																						
	NOTES: 1. Water level in open borehole at a depth of 4.9 m below ground surface (Elev. 67.2 m), upon completion of drilling.																						

GTA-MTO 001 N:\ACTIVE\SPATIAL_IMMTO\HWY417REHAB&WIDENING\02_DATA\GINT\1655214.GPJ GAL-GTA.GDT 12/3/19 JM

+³, X³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

PROJECT <u>1655214-1400</u>	RECORD OF BOREHOLE No 19-410	SHEET 1 OF 2	METRIC
G.W.P. <u>4173-15-00</u>	LOCATION <u>N 5030068.5; E 367878.7 NAD 83 MTM ZONE 9 (LAT. 45.407720; LONG. -75.694171)</u>	ORIGINATED BY <u>KM</u>	
DIST <u>Eastern</u> HWY <u>417</u>	BOREHOLE TYPE <u>Power Auger, 200 mm Diam. (Hollow Stem)</u>	COMPILED BY <u>ZS</u>	
DATUM <u>Geodetic</u>	DATE <u>June 20, 2029</u>	CHECKED BY <u>SS/KCP</u>	

ELEV DEPTH	SOIL PROFILE DESCRIPTION	STRAT PLOT	SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)											
			NUMBER	TYPE	"N" VALUES			20	40						60	80	100	20	40	60	80	100	25	50	75
72.4	GROUND SURFACE																								
0.0	ASPHALTIC CONCRETE																								
72.1																									
71.9	(SW/GW) Gravelly sand (FILL) Grey Moist						72																		
0.5	(SM) Silty sand, trace gravel (FILL) Grey Moist																								
71.2			1	SS	88																				3 74 (23)
1.2	(SM/GW) Gravelly sand, some silt (FILL) Very dense Grey						71																		
70.3			2	SS	51																				
2.1	(SM) Sand, some silt, contains ash (FILL) Dense Brown						70																		
70.3			3	SS	43																				
68.6			4	SS	33		69																		
3.8	(ML/SM) Silt and sand (FILL) Dense to loose Brown Moist						68																		
68.6			5	SS	44																				
67.1			6	SS	9																				
5.3	(SM/ML) SAND and SILT Compact Grey brown						67																		
67.1			7	SS	28																				
66.0			8	SS	8		66																		
6.4	(CH) CLAY Stiff Grey						65																		
66.0			9	SS	2																				
66.0			10	SS	1		64																		
62.7																									
9.8			11	SS	2		63																		
62.7																									

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 +³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

PROJECT <u>1655214-1400</u>	RECORD OF BOREHOLE No 19-410	SHEET 2 OF 2	METRIC
G.W.P. <u>4173-15-00</u>	LOCATION <u>N 5030068.5; E 367878.7 NAD 83 MTM ZONE 9 (LAT. 45.407720; LONG. -75.694171)</u>	ORIGINATED BY <u>KM</u>	
DIST <u>Eastern</u> HWY <u>417</u>	BOREHOLE TYPE <u>Power Auger, 200 mm Diam. (Hollow Stem)</u>	COMPILED BY <u>ZS</u>	
DATUM <u>Geodetic</u>	DATE <u>June 20, 2029</u>	CHECKED BY <u>SS/KCP</u>	

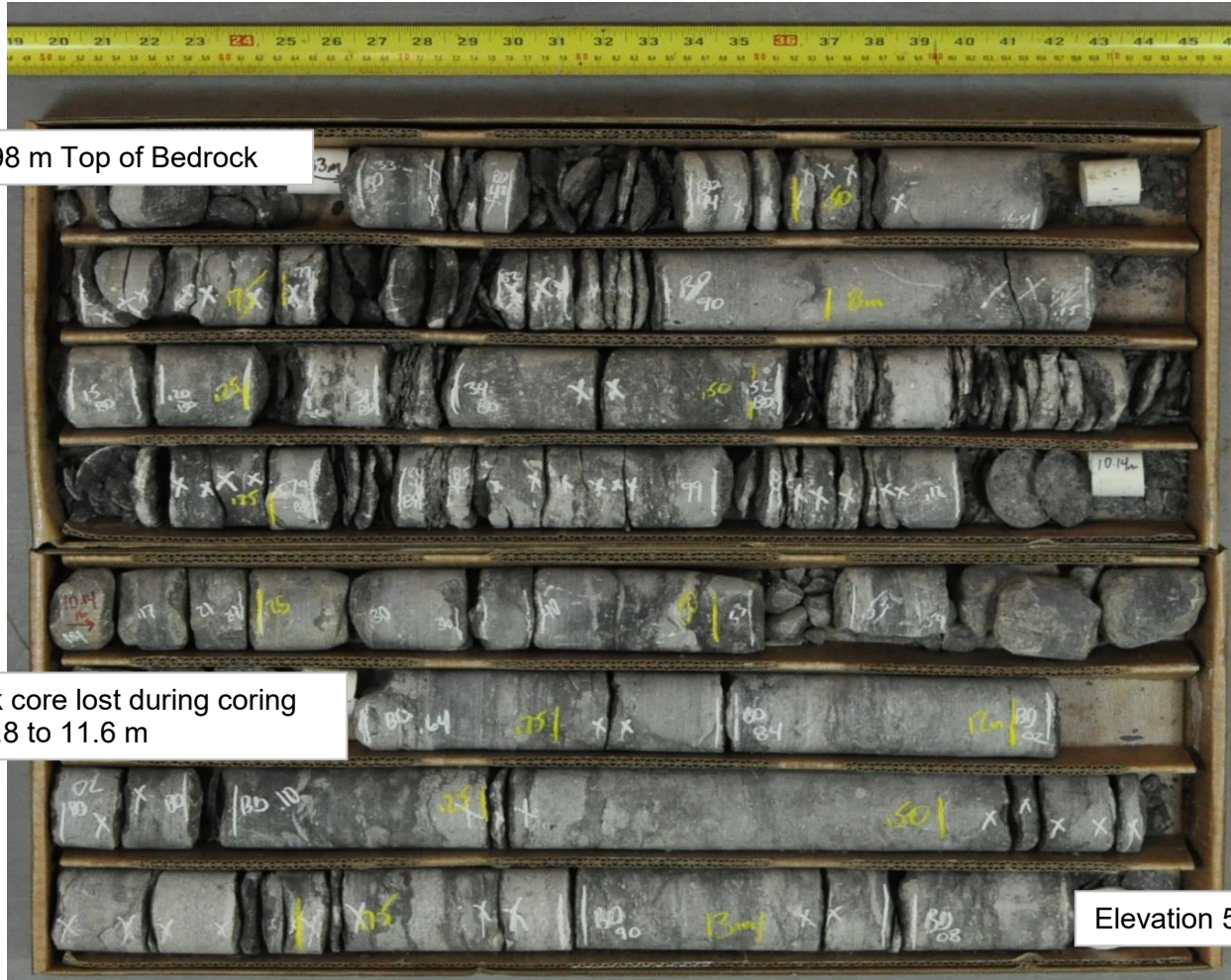
SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT NUMBER	TYPE	"N" VALUES			20	40	60	80	100					
	--- CONTINUED FROM PREVIOUS PAGE ---															
	END OF BOREHOLE NOTES: 1. Monitoring well dry at bottom of well (Elev. 63.0 m) on August 19, 2019.															

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+³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

BH 19-401 (Dry)
Cored Length : 8.3 to 13.2 m
Core Box 1 and 2 of 2

Elevation 58.98 m Top of Bedrock



Bedrock core lost during coring
 from 10.8 to 11.6 m

Elevation 54.13 m EOH

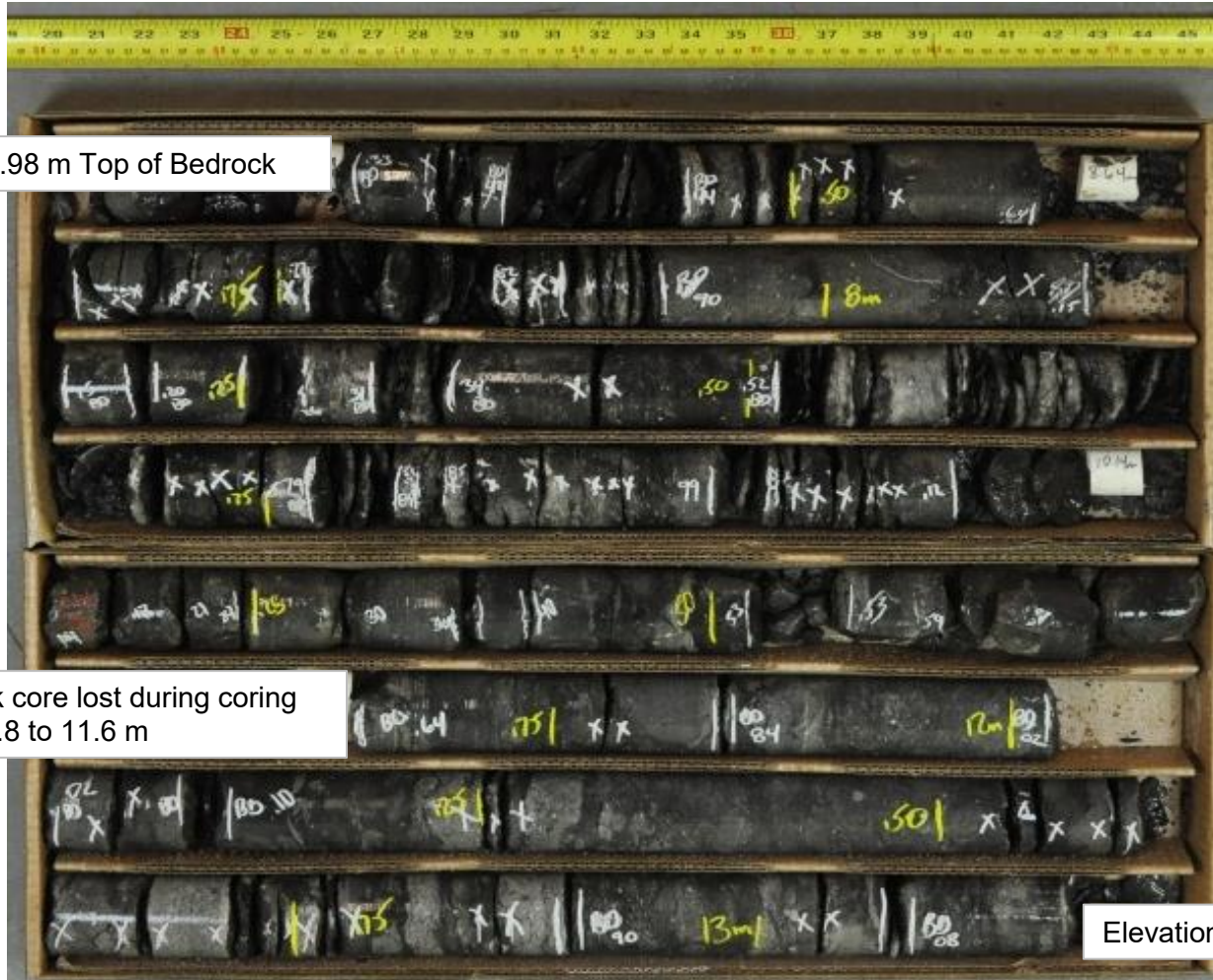


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Highway 417 Overhead Sign Replacements
Ottawa, Ontario

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Figure A1

BH 19-401 (Wet)
Cored Length : 8.3 to 13.2 m
Core Box 1 and 2 of 2



Elevation 58.98 m Top of Bedrock

Bedrock core lost during coring from 10.8 to 11.6 m

Elevation 54.13 m EOH

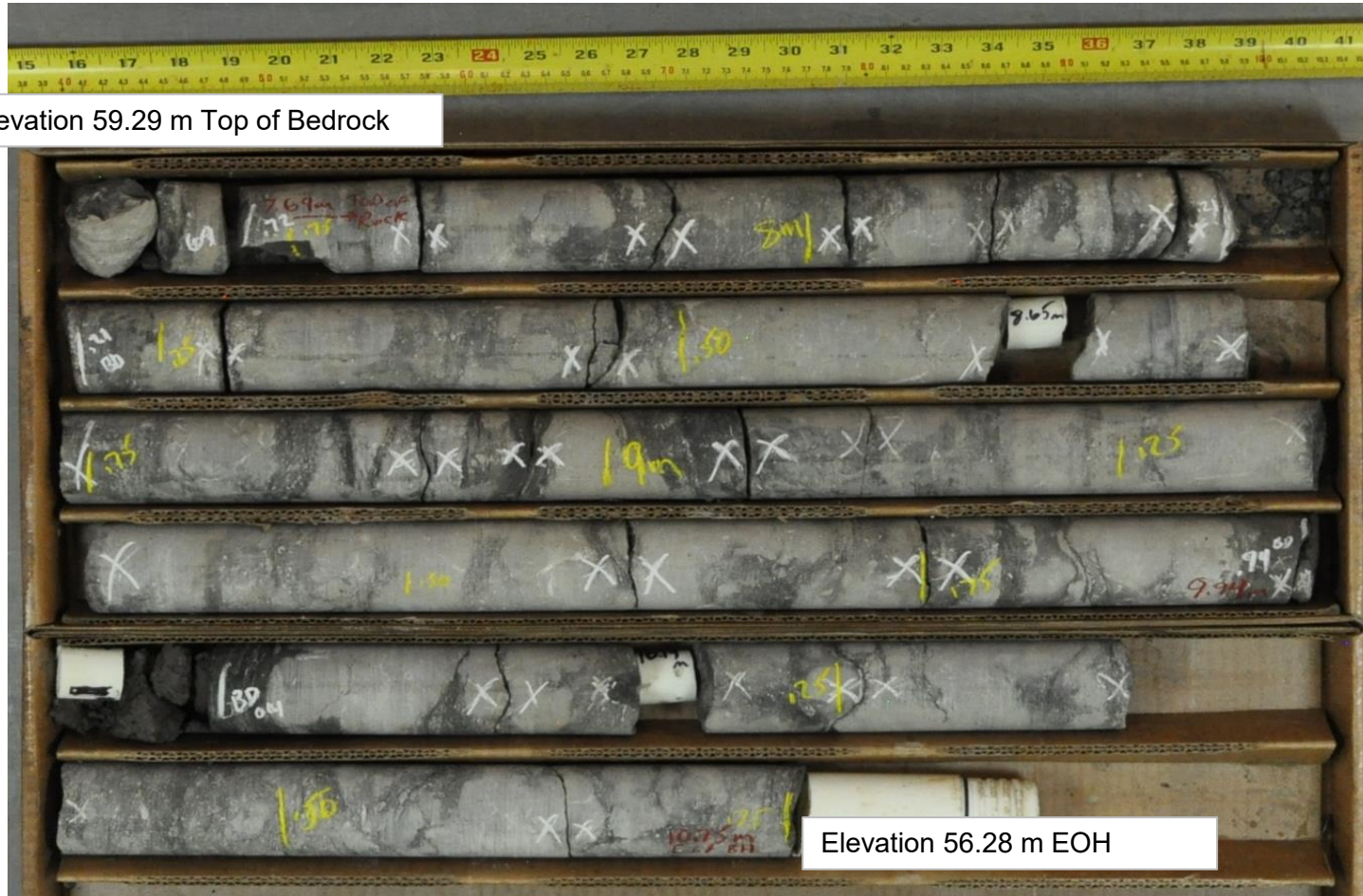


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Figure A2

BH 19-402 (Dry)
 Cored Length : 7.7 to 10.8 m
 Core Box 1 and 2 of 2

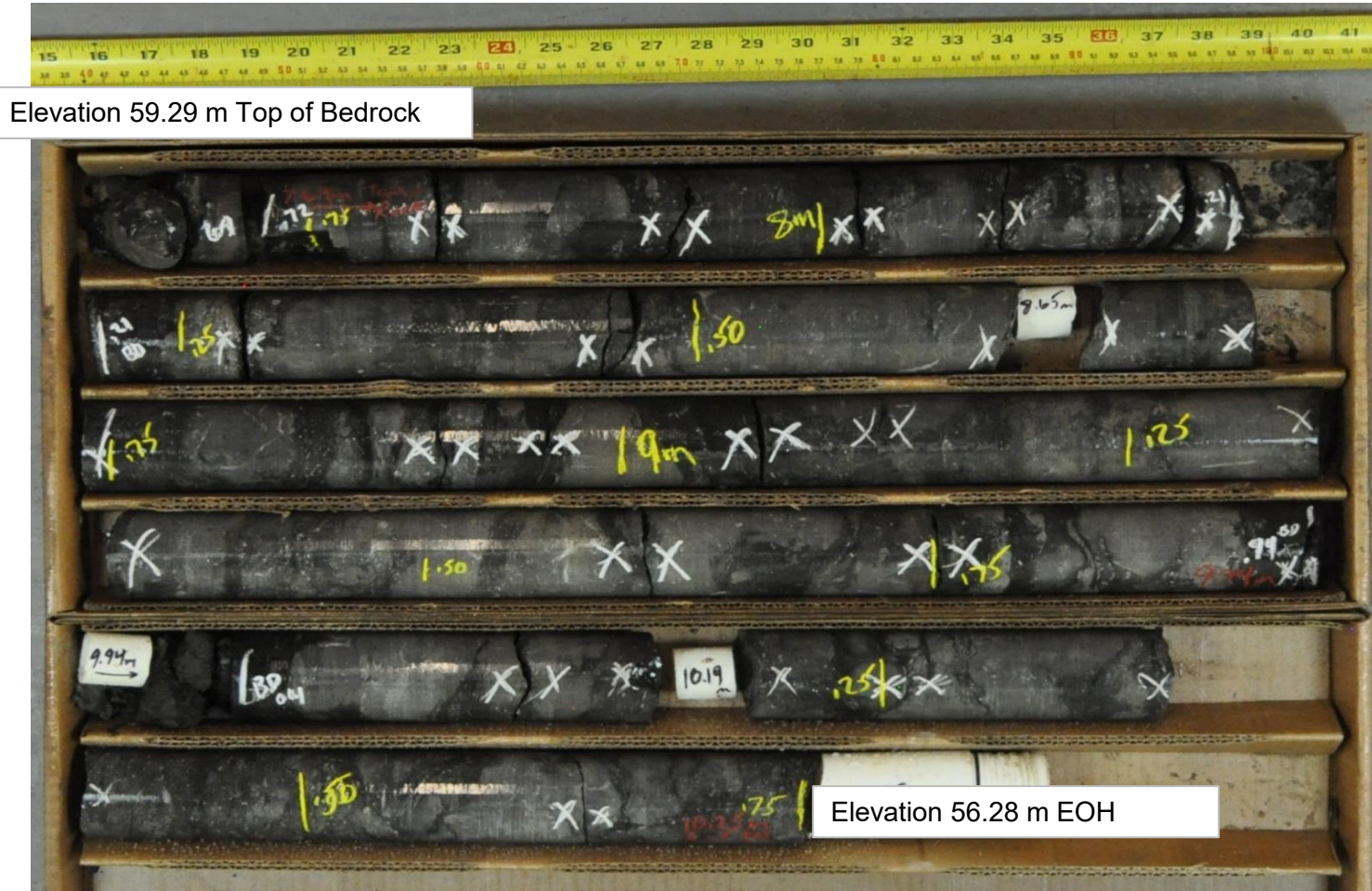


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Figure A3

BH 19-402 (Wet)
Cored Length : 7.7 to 10.8 metres
Core Box 1 and 2 of 2

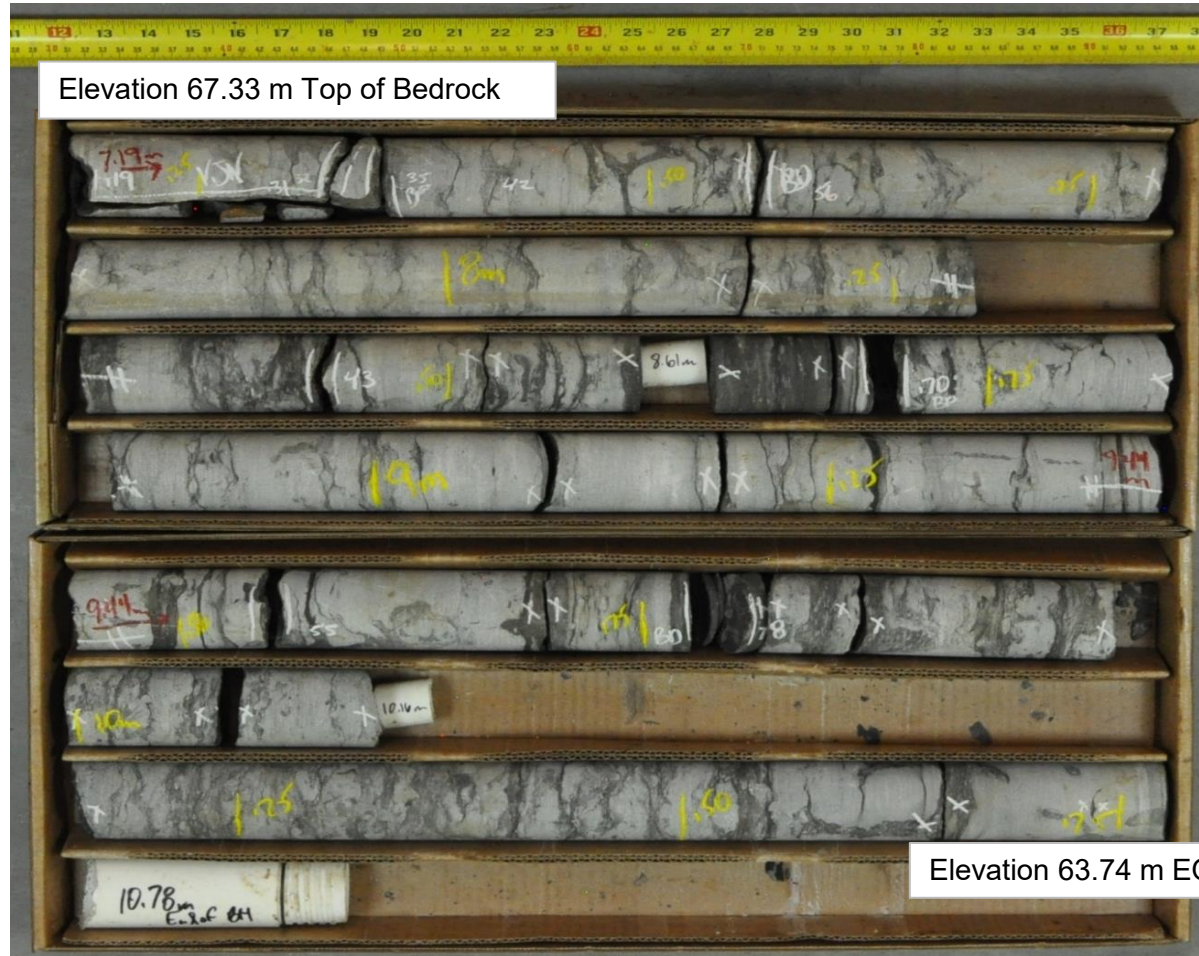


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Figure A4

**BH 19-403 (Dry)
Cored Length : 7.2 to 10.8 m
Core Box 1 and 2 of 2**



Elevation 67.33 m Top of Bedrock

Elevation 63.74 m EOH

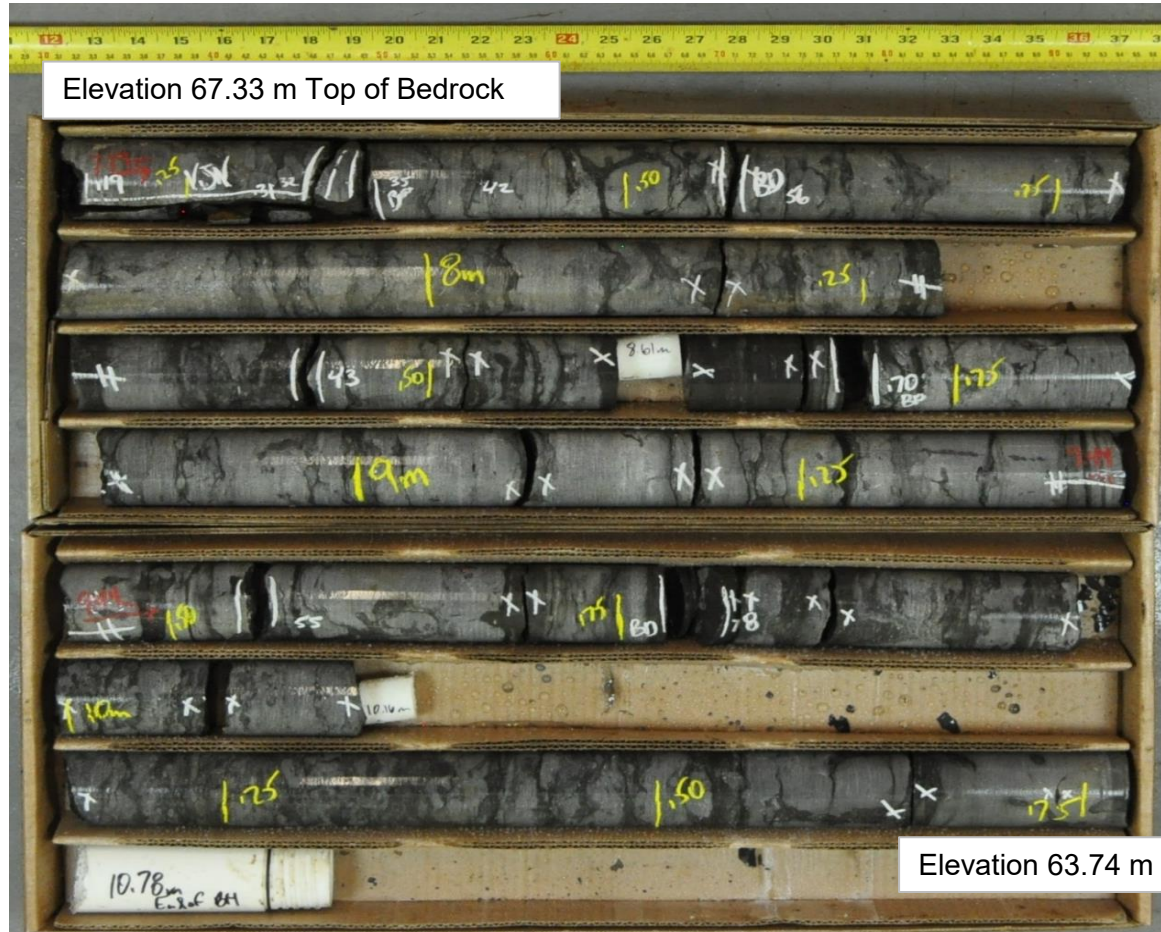


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Figure A5

BH 19-403 (Wet)
Cored Length : 7.2 to 10.8 m
Core Box 1 and 2 of 2

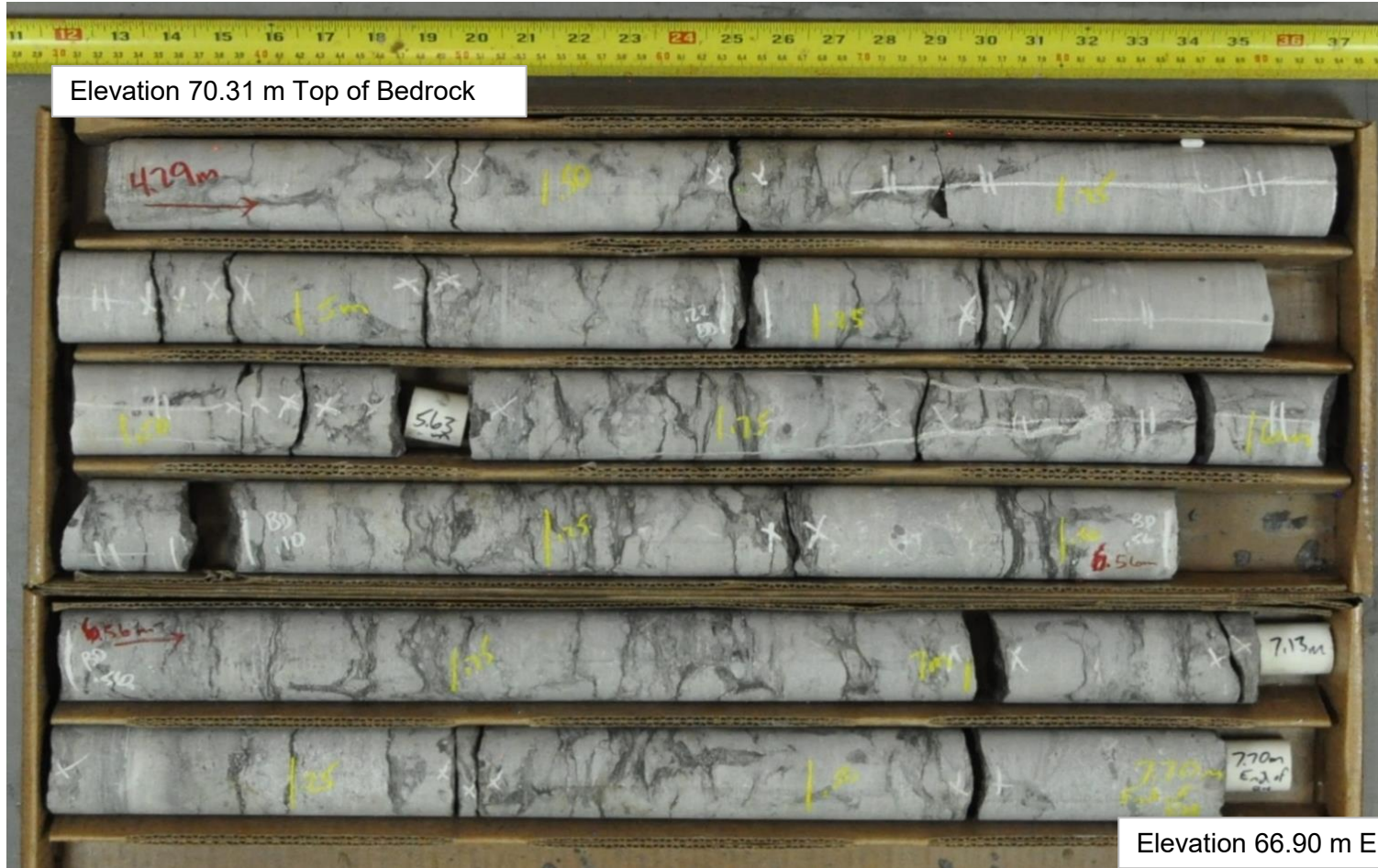


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Figure A6

BH 19-404 (Dry)
Cored Length : 4.3 to 7.7 m
Core Box 1 and 2 of 2

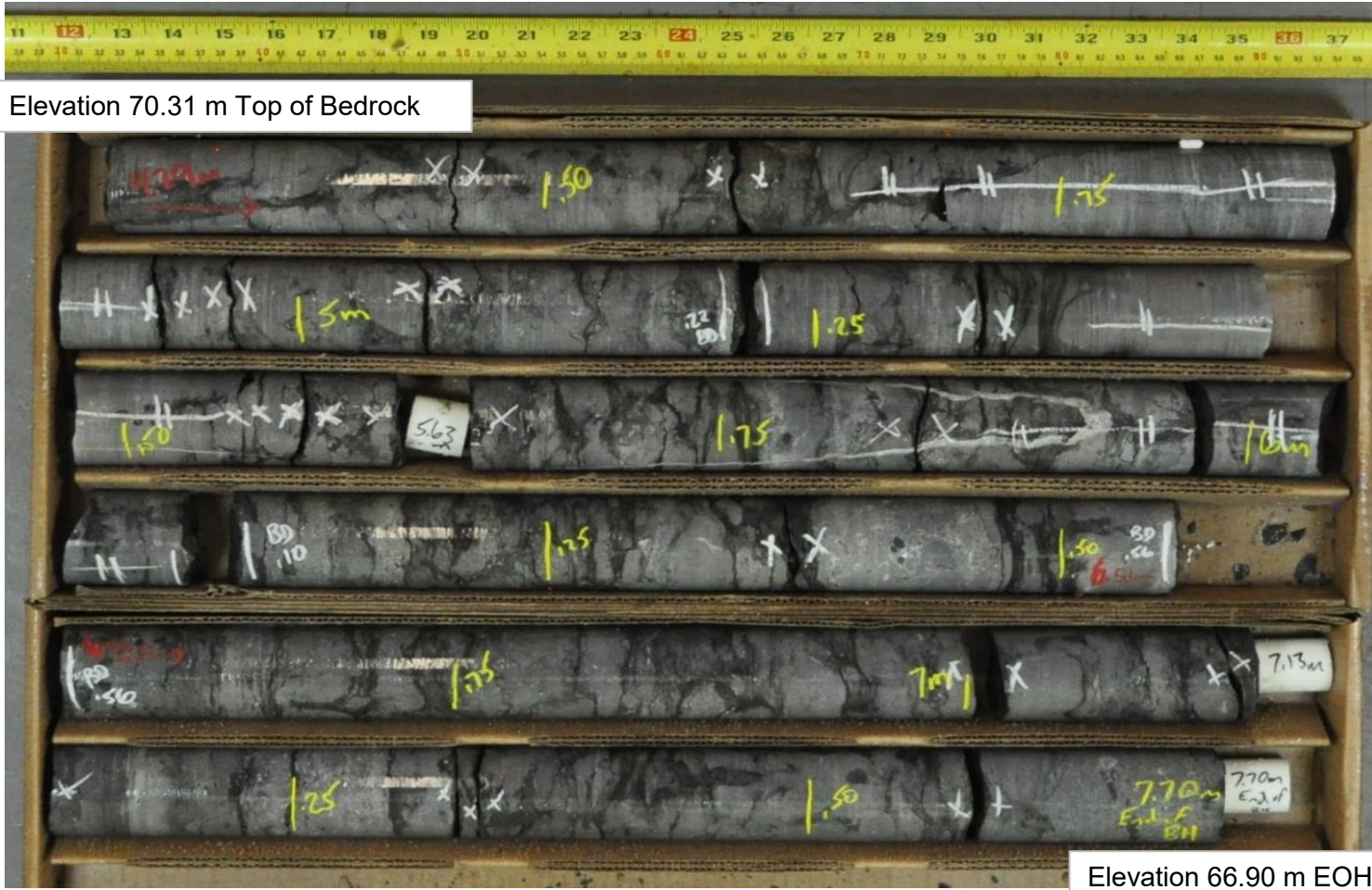


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Figure A7

BH 19-404 (Wet)
Cored Length : 4.3 to 7.7 m
Core Box 1 and 2 of 2



Elevation 70.31 m Top of Bedrock

Elevation 66.90 m EOH

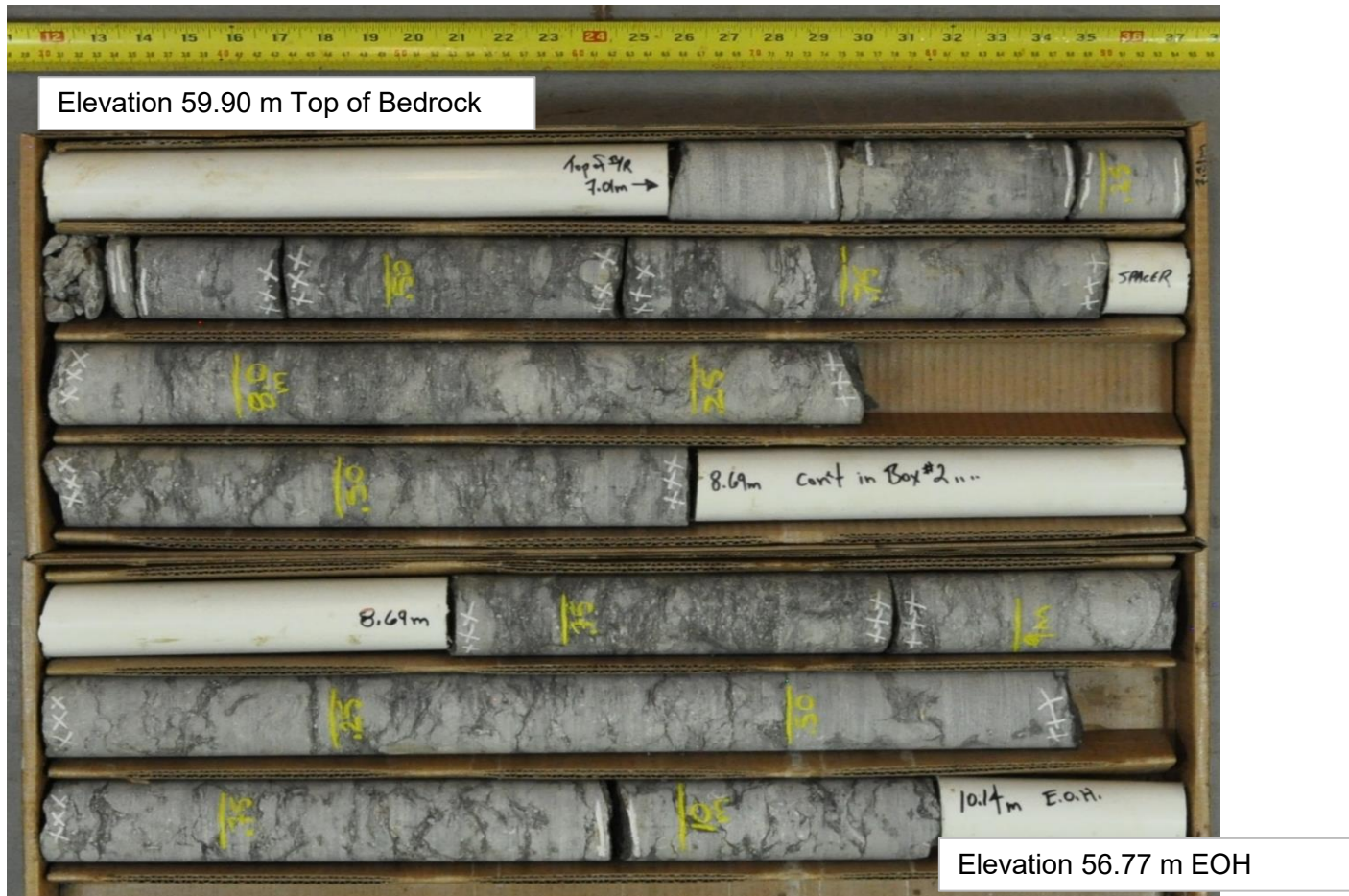


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Figure A8

BH 19-405 (Dry)
Cored Length : 7.0 to 10.1 m
Core Box 1 and 2 of 2

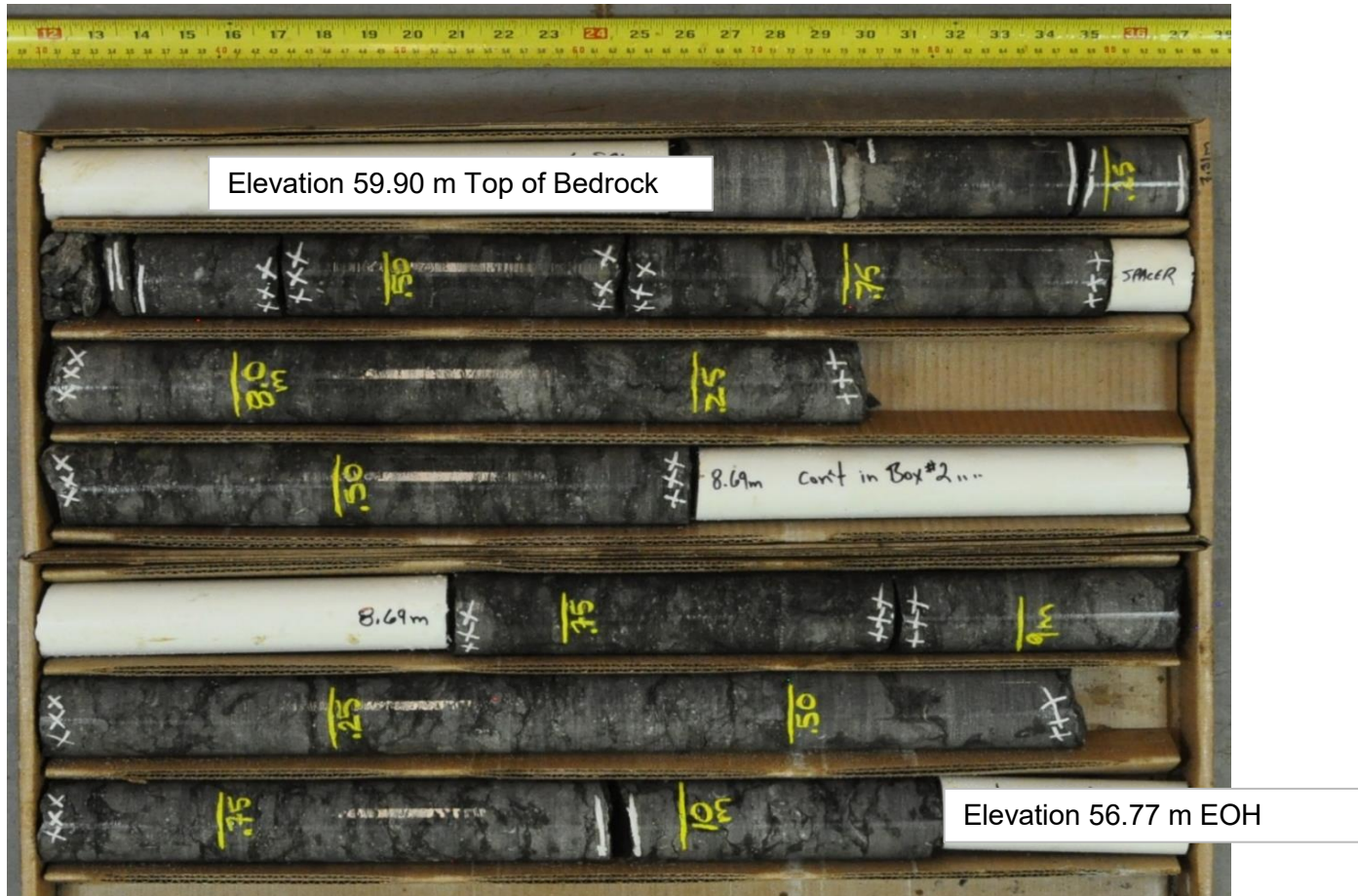


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Figure A9

BH 19-405 (Wet)
 Cored Length : 7.0 to 10.1 m
 Core Box 1 and 2 of 2



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Figure A10

APPENDIX B

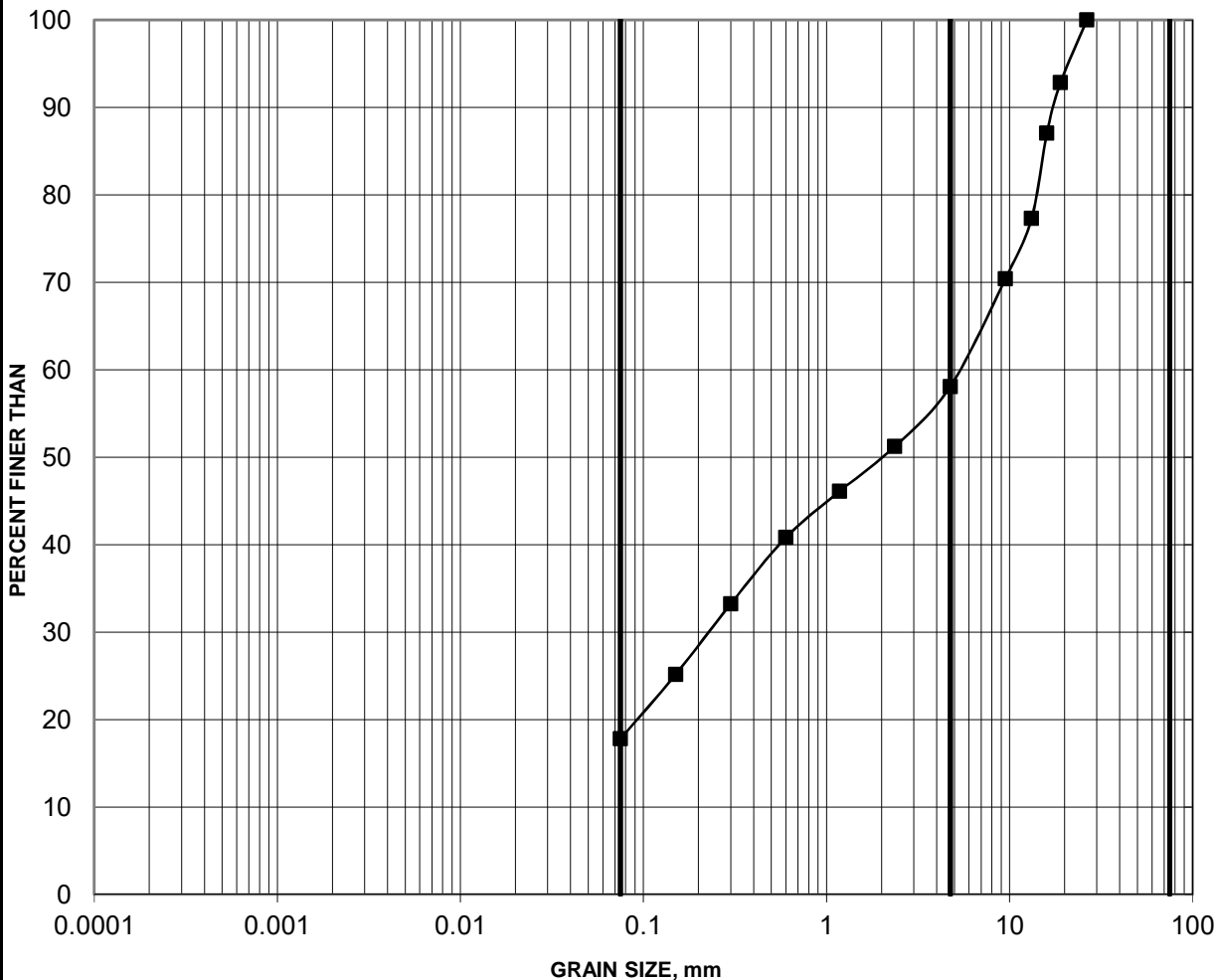
Laboratory Test Results, Current Investigation

- Figure B1 – Grain Size Distribution Test Results – Gravel and Sand (Fill)
- Figure B2 – Grain Size Distribution Test Results – Sandy Clayey Silt (Fill)
 - Figure B3 – Plasticity Chart – Sandy Clayey Silt (Fill)
- Figure B4 – Grain Size Distribution Test Results – Clayey Silt
 - Figure B5 – Plasticity Chart – Clayey Silt
- Figure B6 – Grain Size Distribution Test Results – Sand and Gravel
 - Figure B7 – Grain Size Distribution Test Results – Sand (Fill)
- Figure B8 – Grain Size Distribution Test Results – Gravel and Sand (Fill)
 - Figure B9 – Grain Size Distribution Test Results – Sand (Fill)
 - Figure B10 – Grain Size Distribution Test Results – Silt
 - Figure B11 – Grain Size Distribution Test Results – Silty Sand
 - Figure B12 – Grain Size Distribution Test Results – Glacial Till
- Figure B13 – Grain Size Distribution Test Results – Sand and Gravel (Fill)
 - Figure B14 – Grain Size Distribution Test Results – Sand (Fill)
 - Figure B15 – Grain Size Distribution Test Results – Sandy Silt
 - Figure B16 – Grain Size Distribution Test Results – Glacial Till
- Figure B17 – Grain Size Distribution Test Results – Silty Sand (Fill)
 - Figure B18 – Grain Size Distribution Test Results – Sand (Fill)
 - Figure B19 – Grain Size Distribution Test Results – Silt and Sand
 - Figure B20 – Grain Size Distribution Test Results – Clay
 - Figure B21 – Plasticity Chart – Clay
- Figure B22 – Summary of Laboratory Unconfined Compression Strength Tests

GRAIN SIZE DISTRIBUTION

FIGURE B1

GRAVEL AND SAND (FILL)



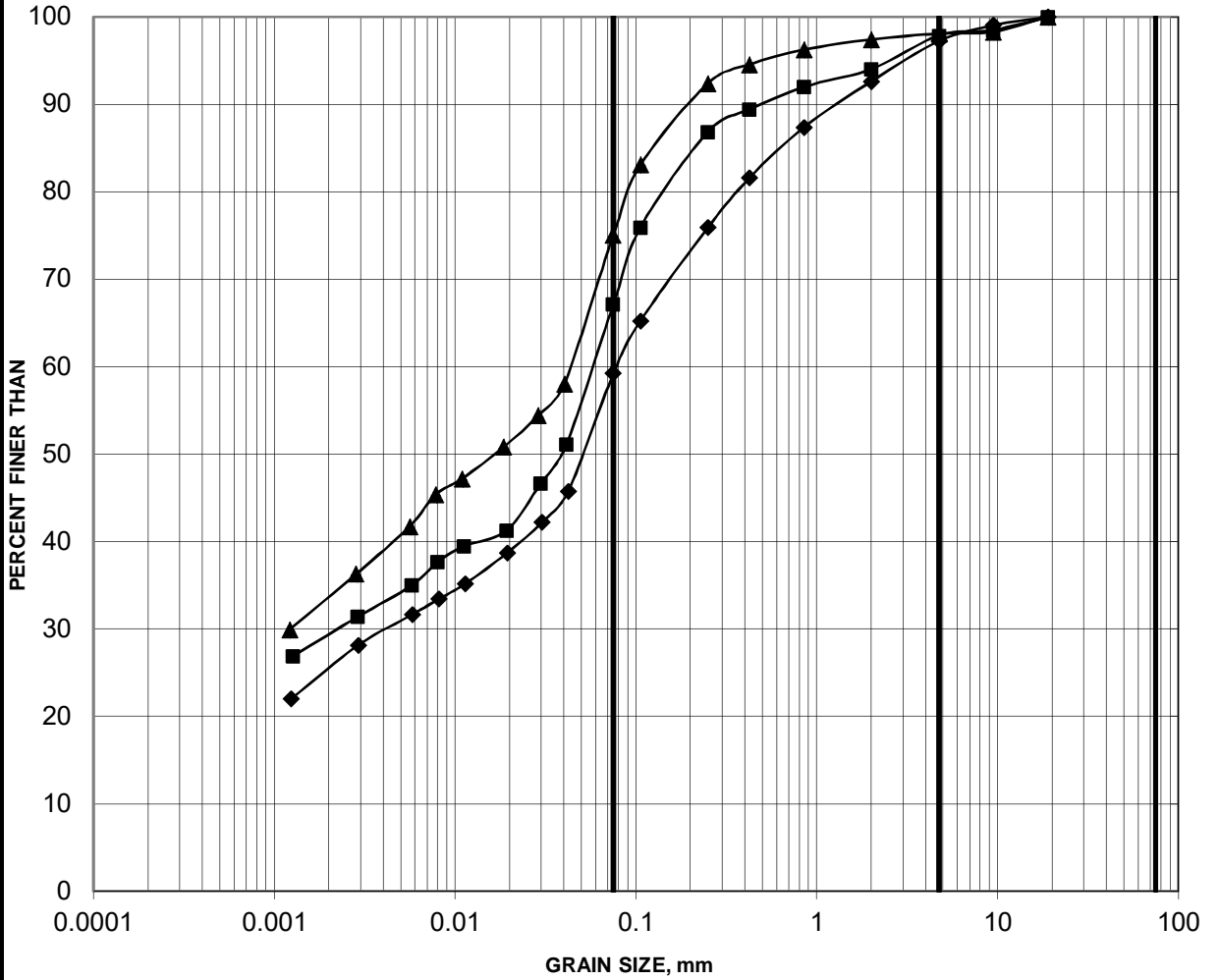
SILT AND CLAY	FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE SIZE
	SAND SIZE			GRAVEL SIZE		

Borehole	Sample	Depth (m)
■ 19-402	3	1.52-2.13

GRAIN SIZE DISTRIBUTION

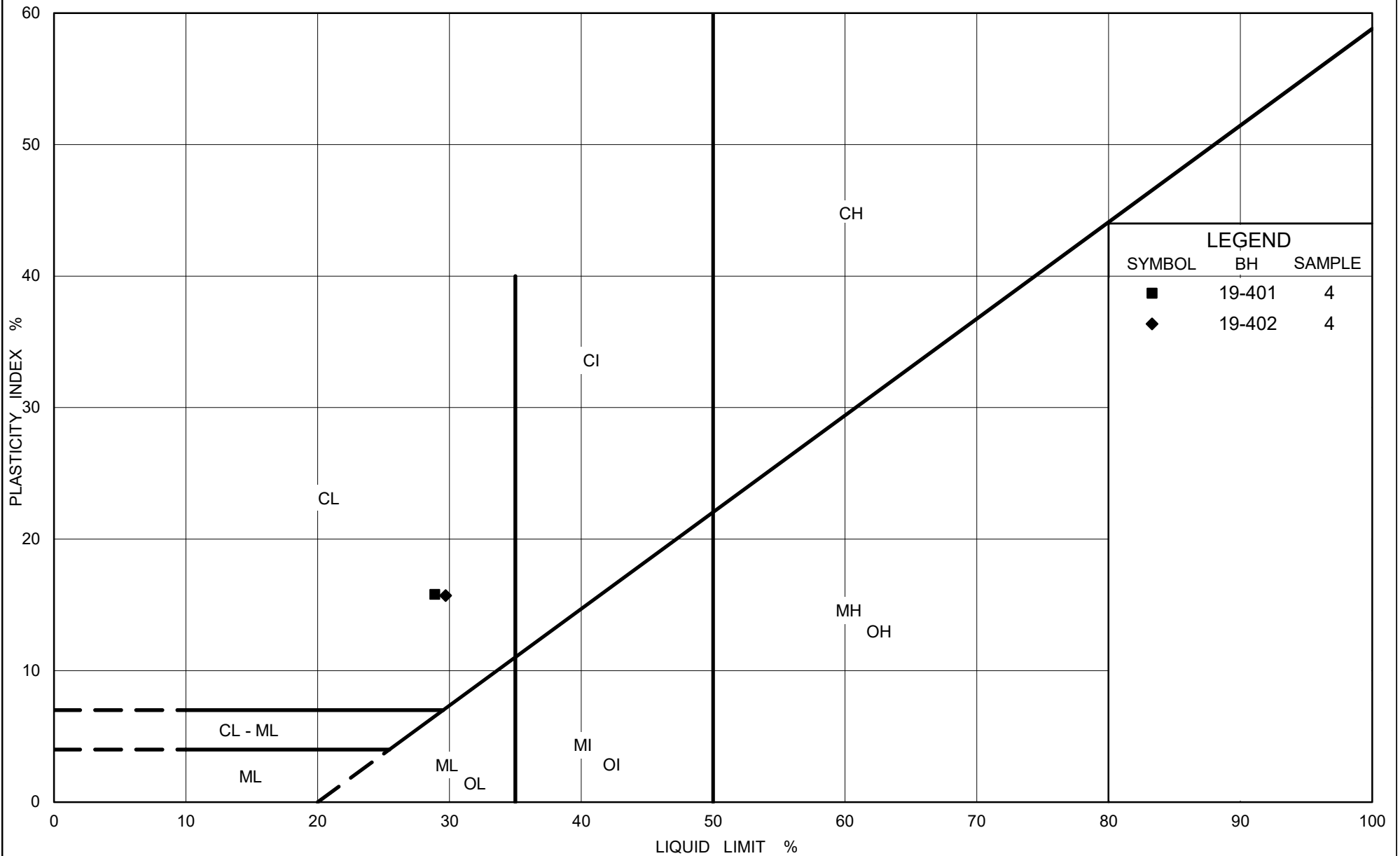
FIGURE B2

SANDY CLAYEY SILT (FILL)



SILT AND CLAY	FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE SIZE
	SAND SIZE			GRAVEL SIZE		

Borehole	Sample	Depth (m)
—■—	19-401 4	3.05-3.66
—◆—	19-401 7	5.33-5.94
—▲—	19-402 4	2.29-2.90

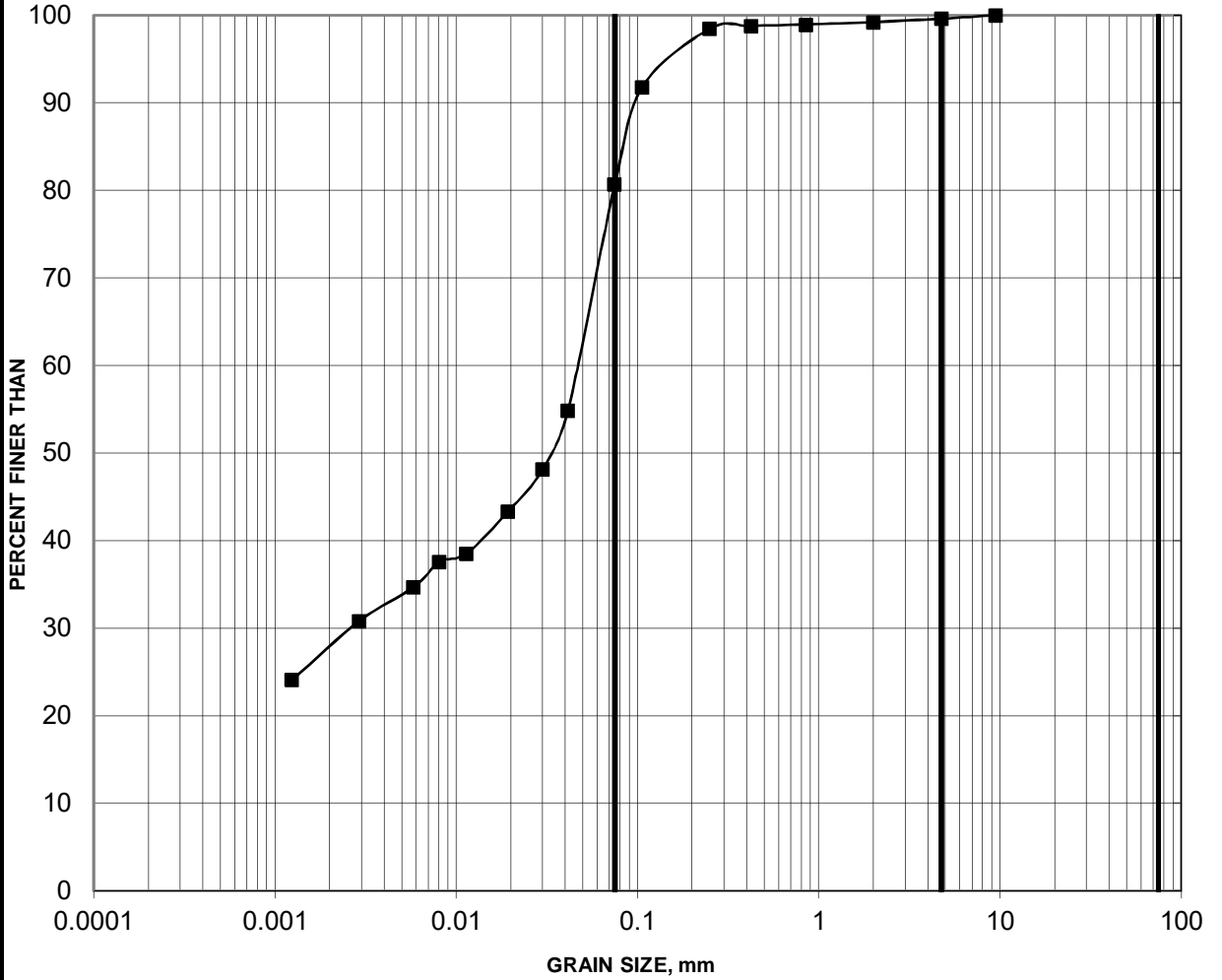


LEGEND		
SYMBOL	BH	SAMPLE
■	19-401	4
◆	19-402	4

GRAIN SIZE DISTRIBUTION

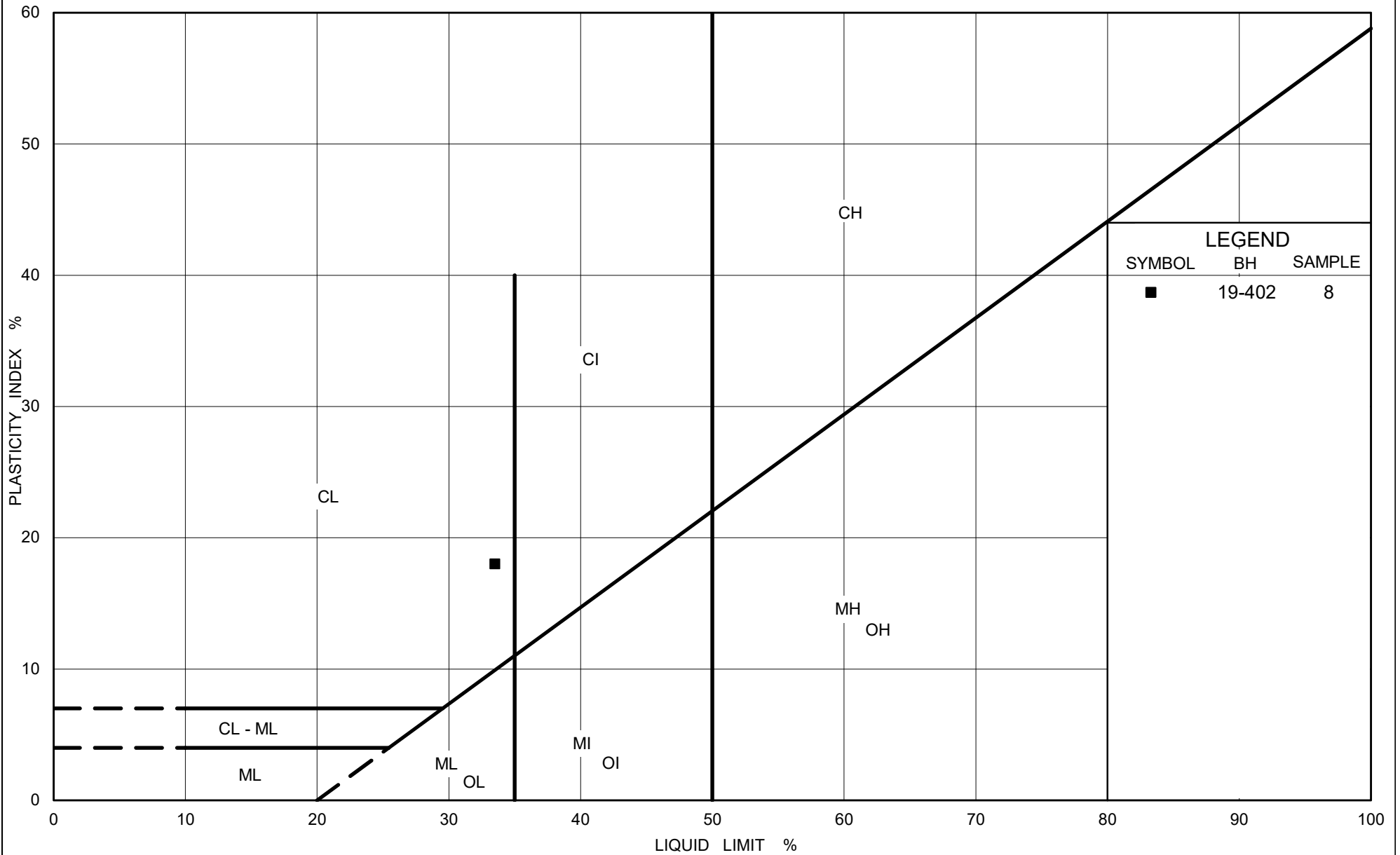
FIGURE B4

CLAYEY SILT



SILT AND CLAY	FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE SIZE
	SAND SIZE			GRAVEL SIZE		

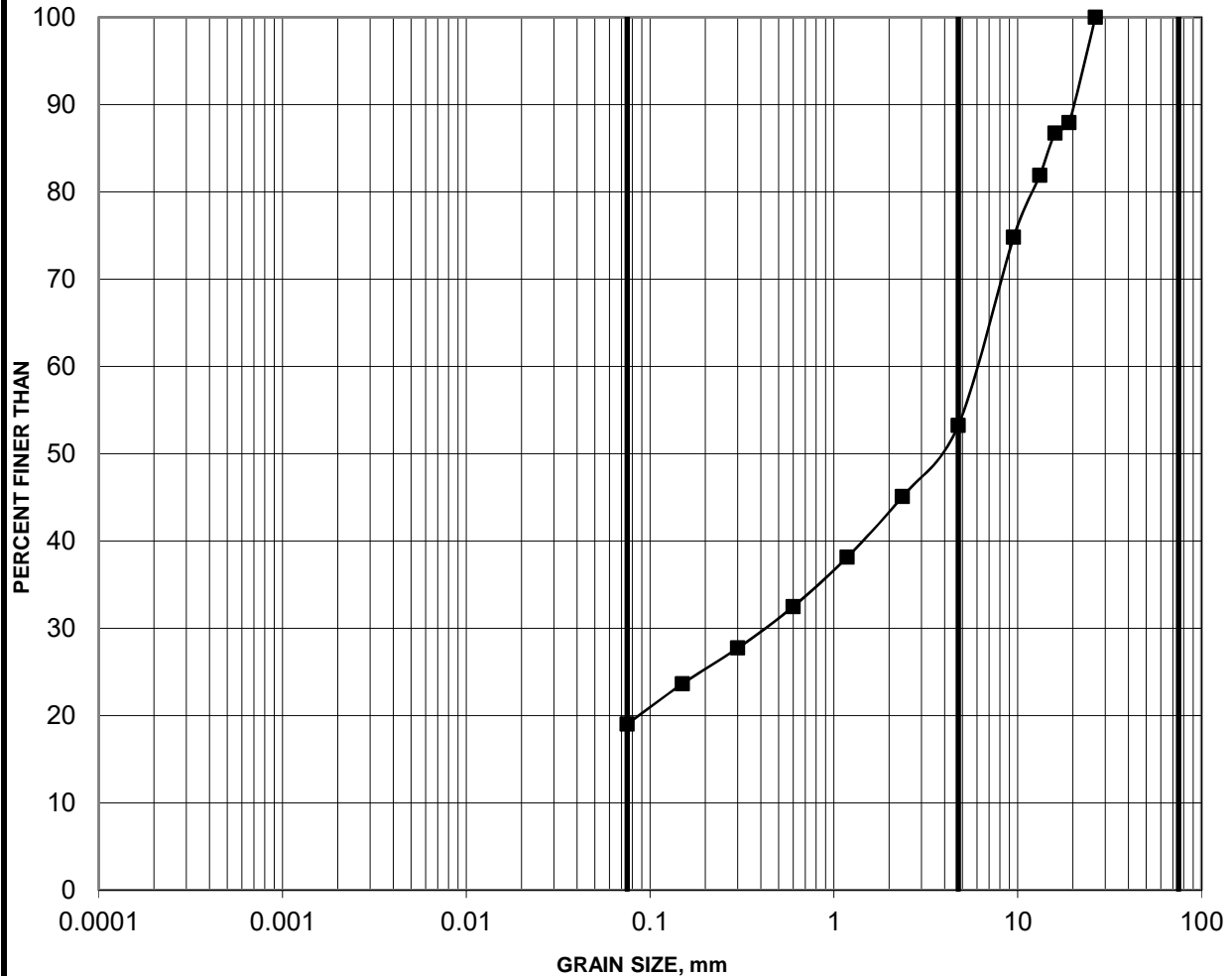
Borehole	Sample	Depth (m)
—■— 19-402	8	5.33-5.94



GRAIN SIZE DISTRIBUTION

FIGURE B6

SAND AND GRAVEL



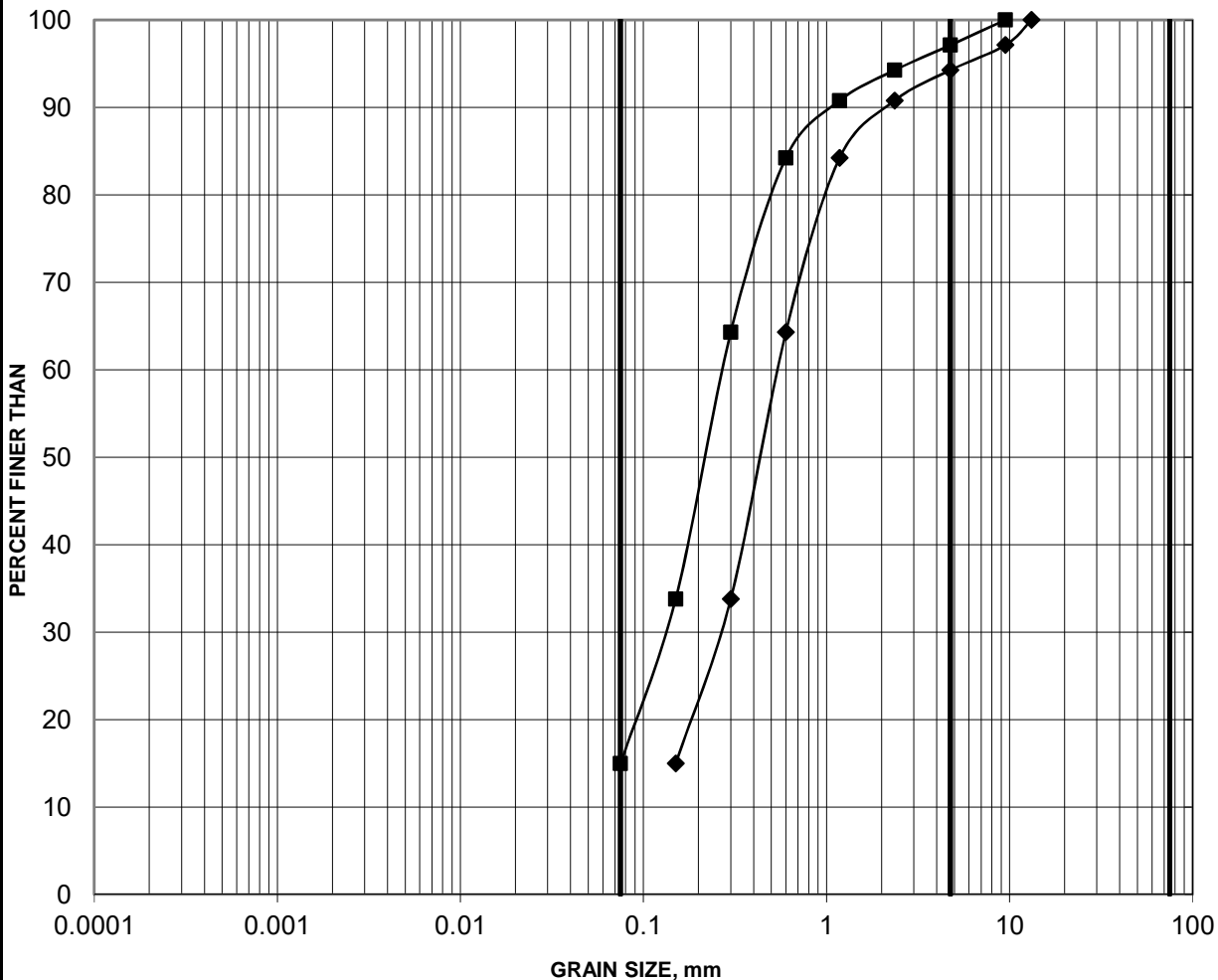
SILT AND CLAY	FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE SIZE
	SAND SIZE			GRAVEL SIZE		

Borehole	Sample	Depth (m)
■ 19-402	10	6.86-7.47

GRAIN SIZE DISTRIBUTION

FIGURE B7

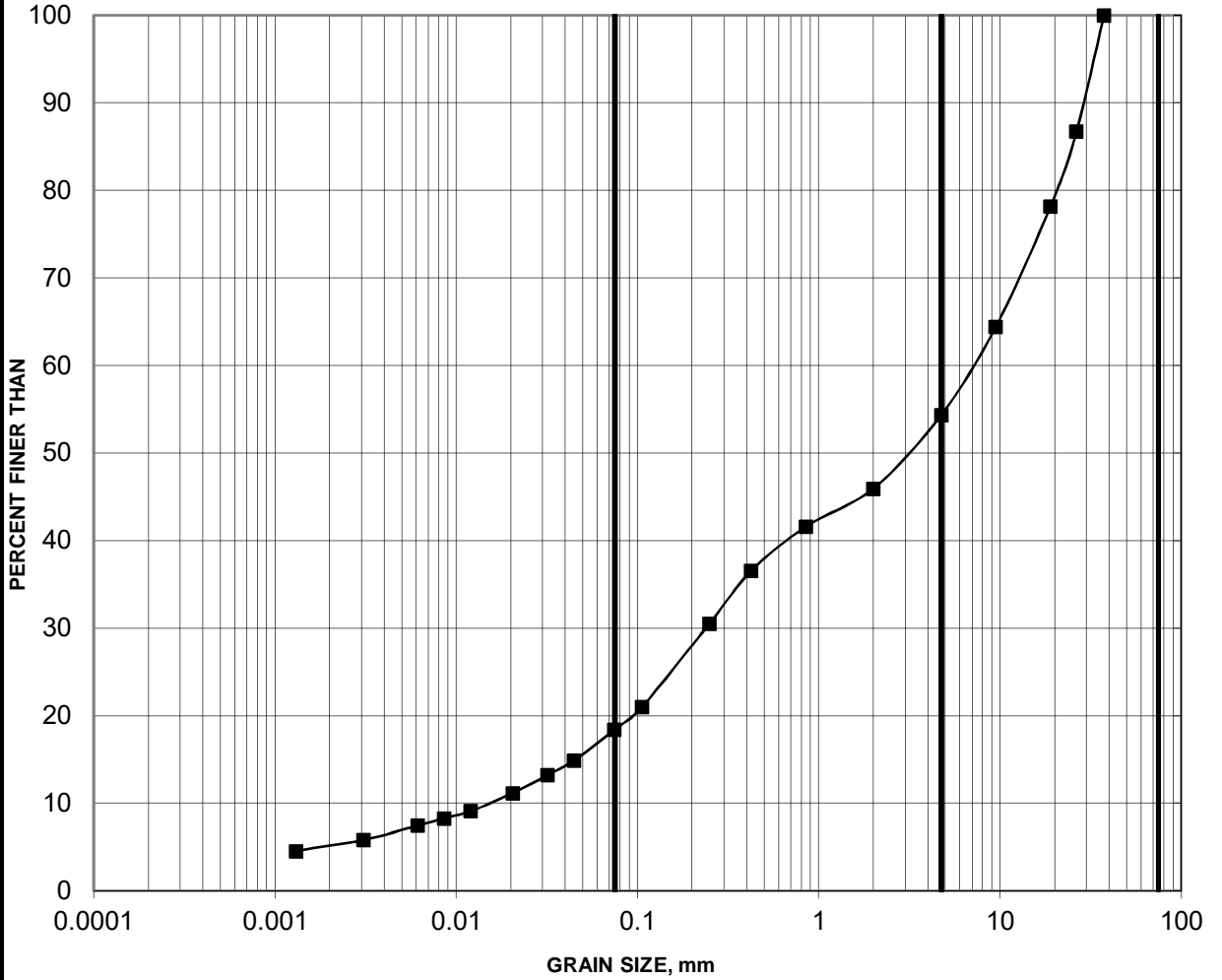
SAND (FILL)



SILT AND CLAY	FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE SIZE
	SAND SIZE			GRAVEL SIZE		

Borehole	Sample	Depth (m)
■ 19-403	2	0.76-1.37
◆ 19-404	2	0.76-1.37

GRAVEL AND SAND (FILL)



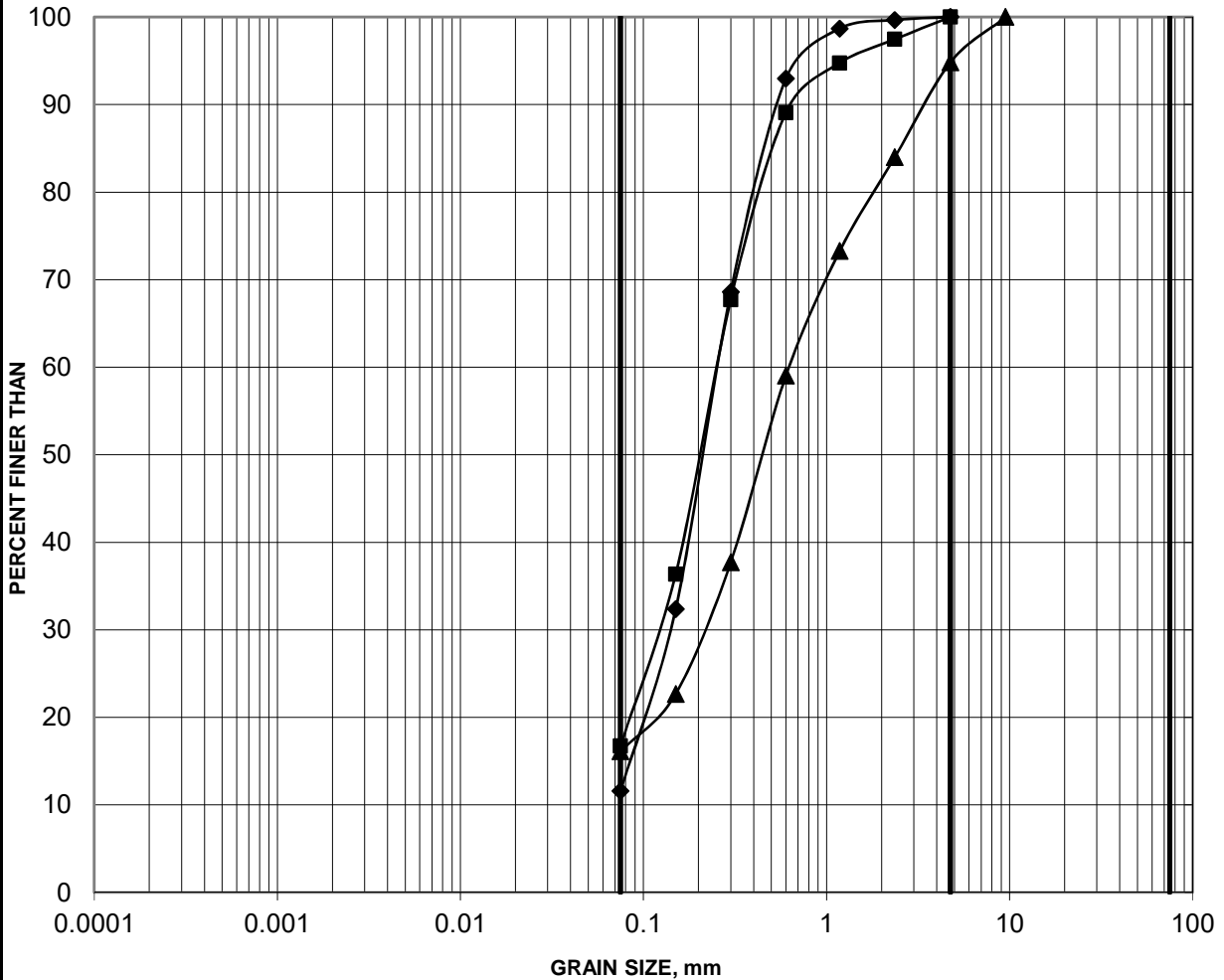
SILT AND CLAY	FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE SIZE
	SAND SIZE			GRAVEL SIZE		

Borehole	Sample	Depth (m)
■ 19-403	8	5.33-5.94

GRAIN SIZE DISTRIBUTION

FIGURE B9

SAND (FILL)

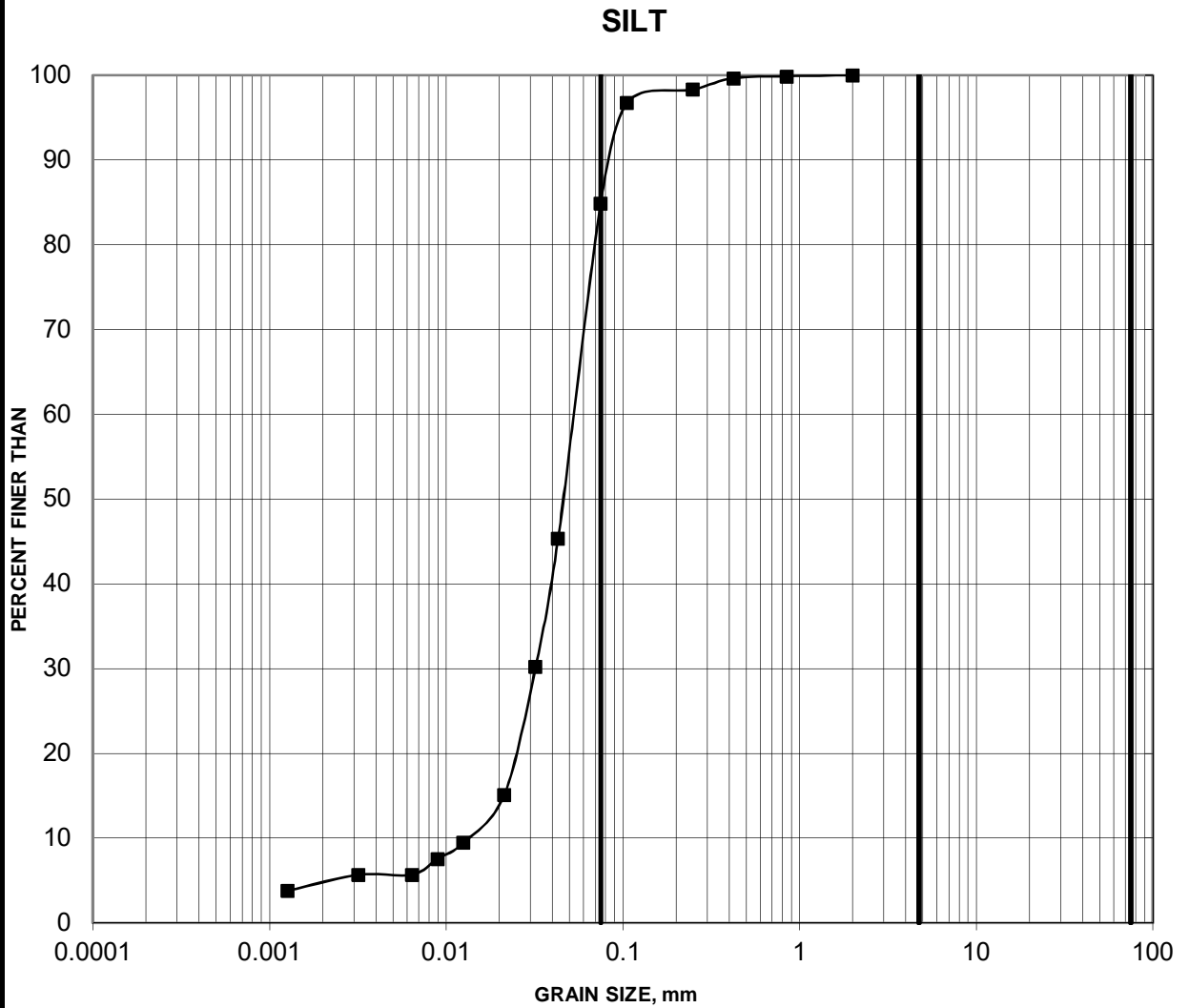


SILT AND CLAY	FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE SIZE
	SAND SIZE			GRAVEL SIZE		

Borehole	Sample	Depth (m)
—■— 19-406	4	0.76-1.37
—◆— 19-406	8	3.81-4.42
—▲— 19-406	12	6.86-7.47

GRAIN SIZE DISTRIBUTION

FIGURE B10



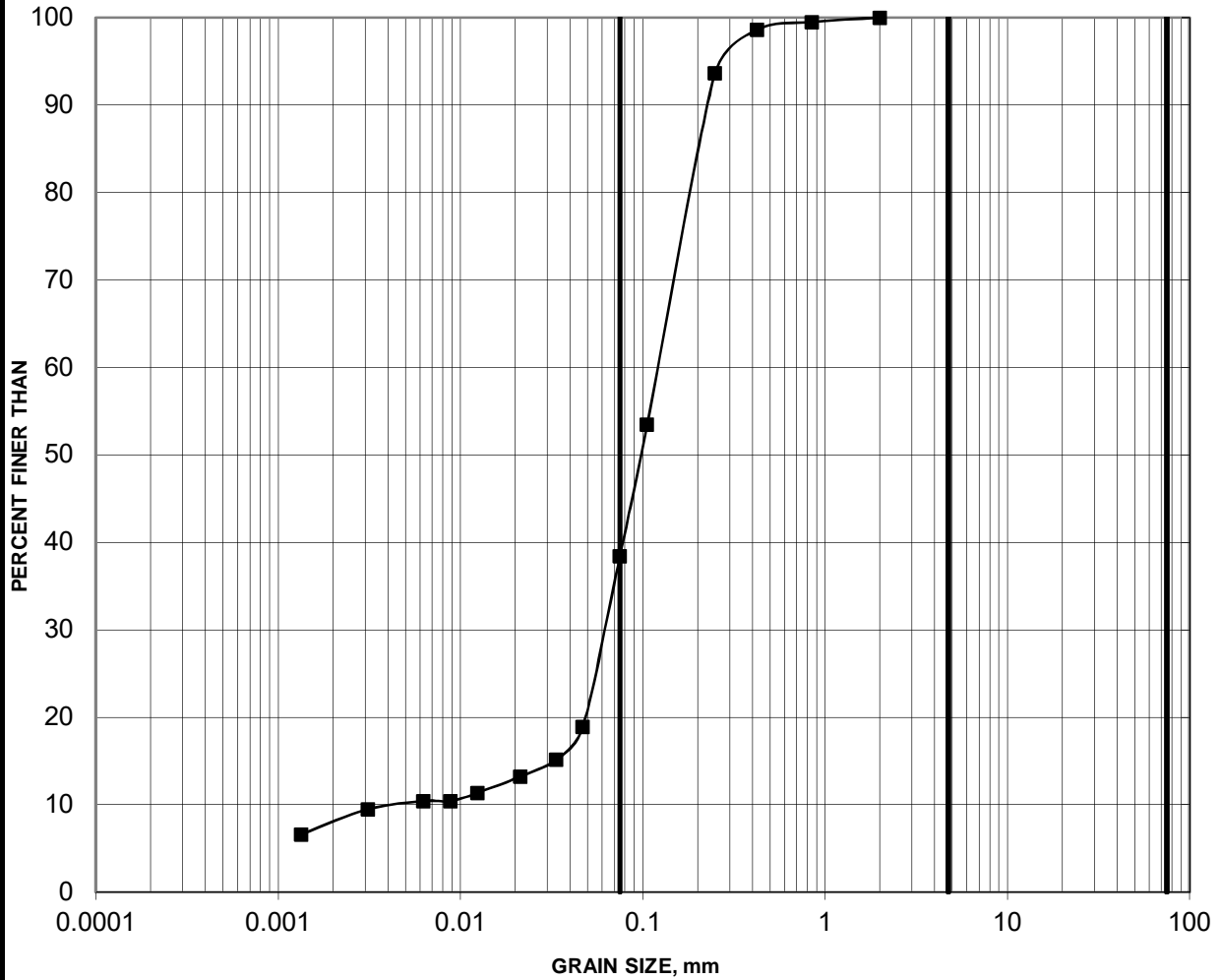
SILT AND CLAY	FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE SIZE
	SAND SIZE			GRAVEL SIZE		

Borehole	Sample	Depth (m)
19-405	7	4.57-5.18

GRAIN SIZE DISTRIBUTION

FIGURE B11

SILTY SAND



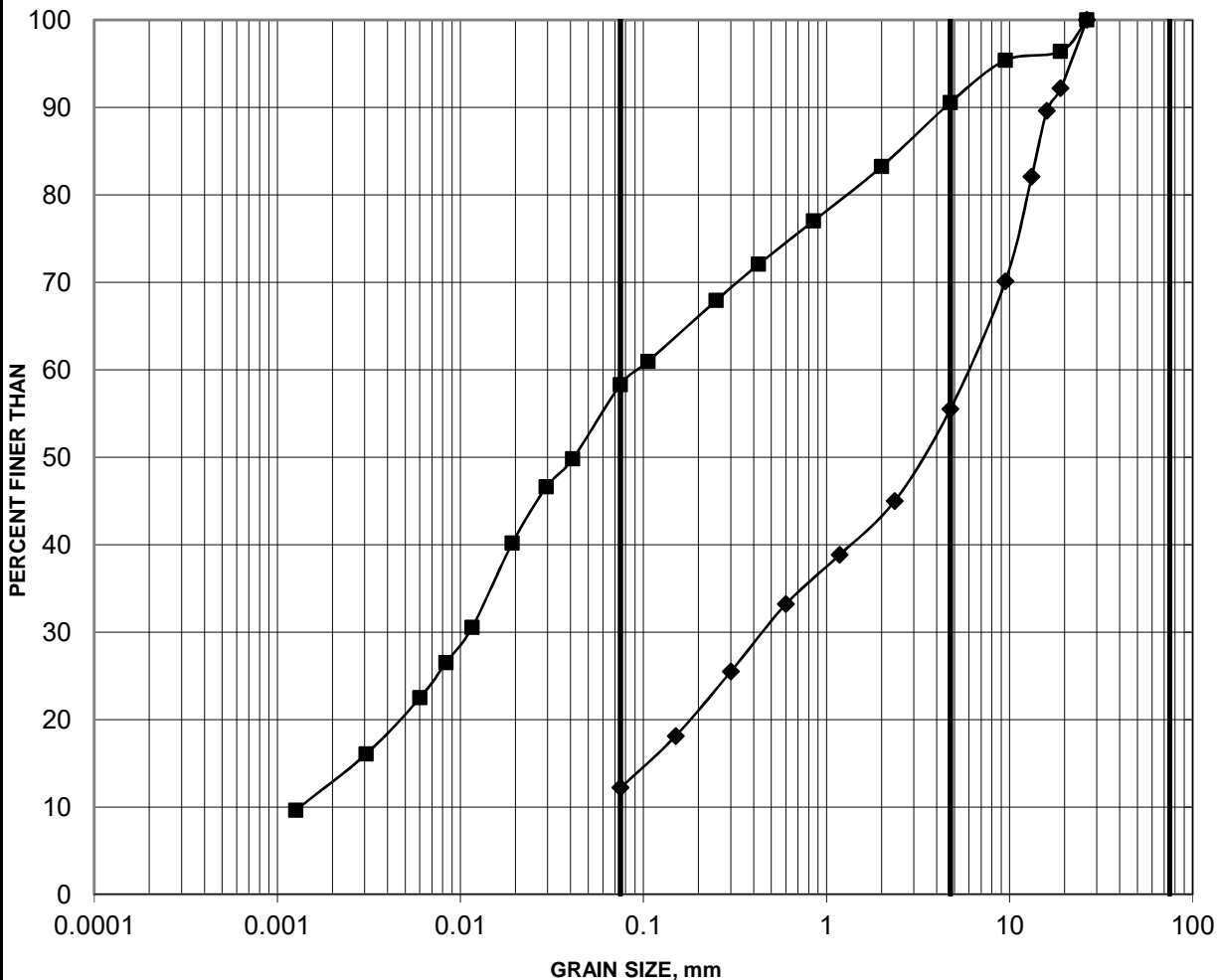
SILT AND CLAY	FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE SIZE
	SAND SIZE			GRAVEL SIZE		

Borehole	Sample	Depth (m)
19-406	15	9.14-9.75

GRAIN SIZE DISTRIBUTION

FIGURE B12

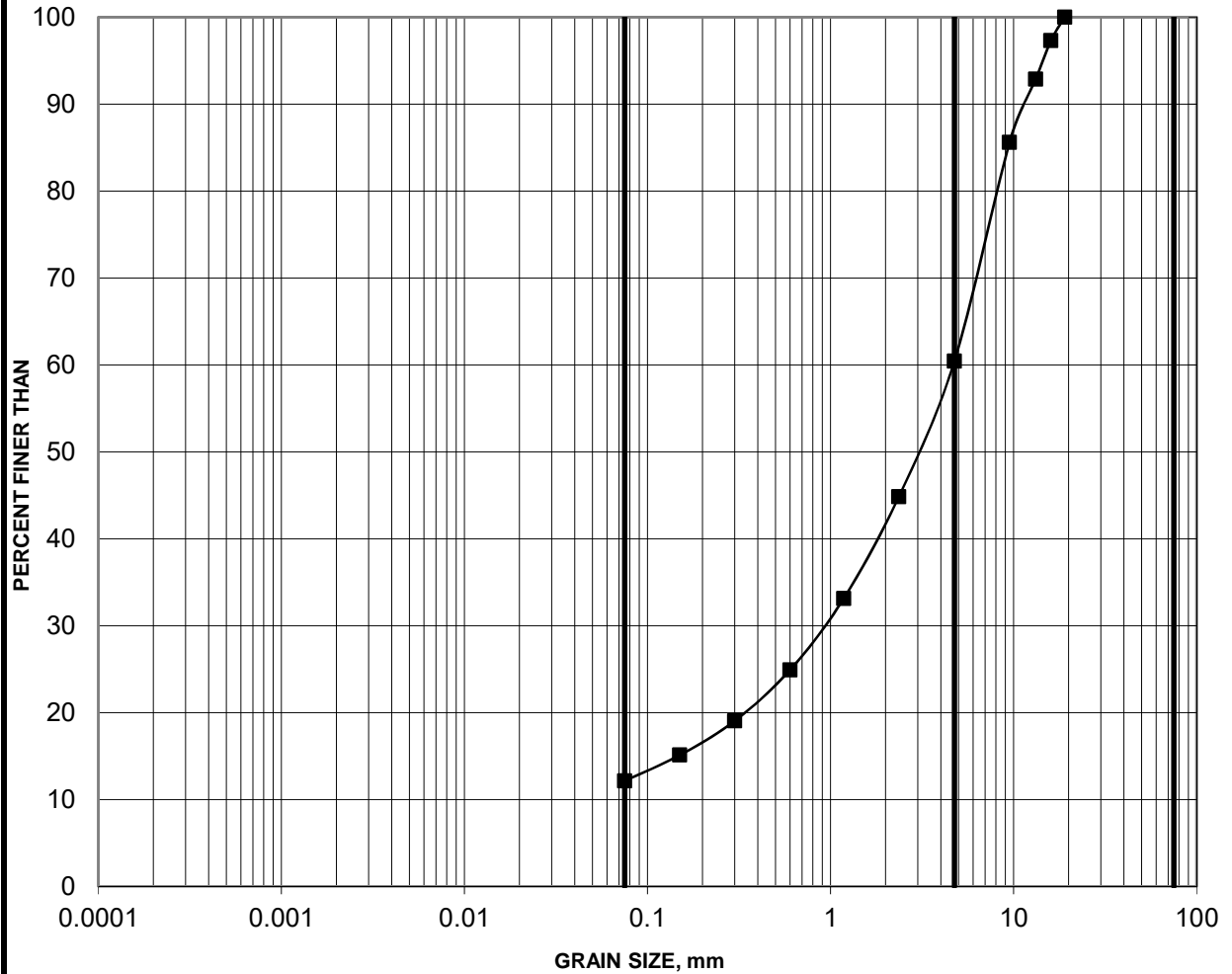
GLACIAL TILL



SILT AND CLAY	FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE SIZE
	SAND SIZE			GRAVEL SIZE		

Borehole	Sample	Depth (m)
■ 19-405	9	6.10-6.71
◆ 19-406	16B	10.06-10.36

SAND AND GRAVEL (FILL)



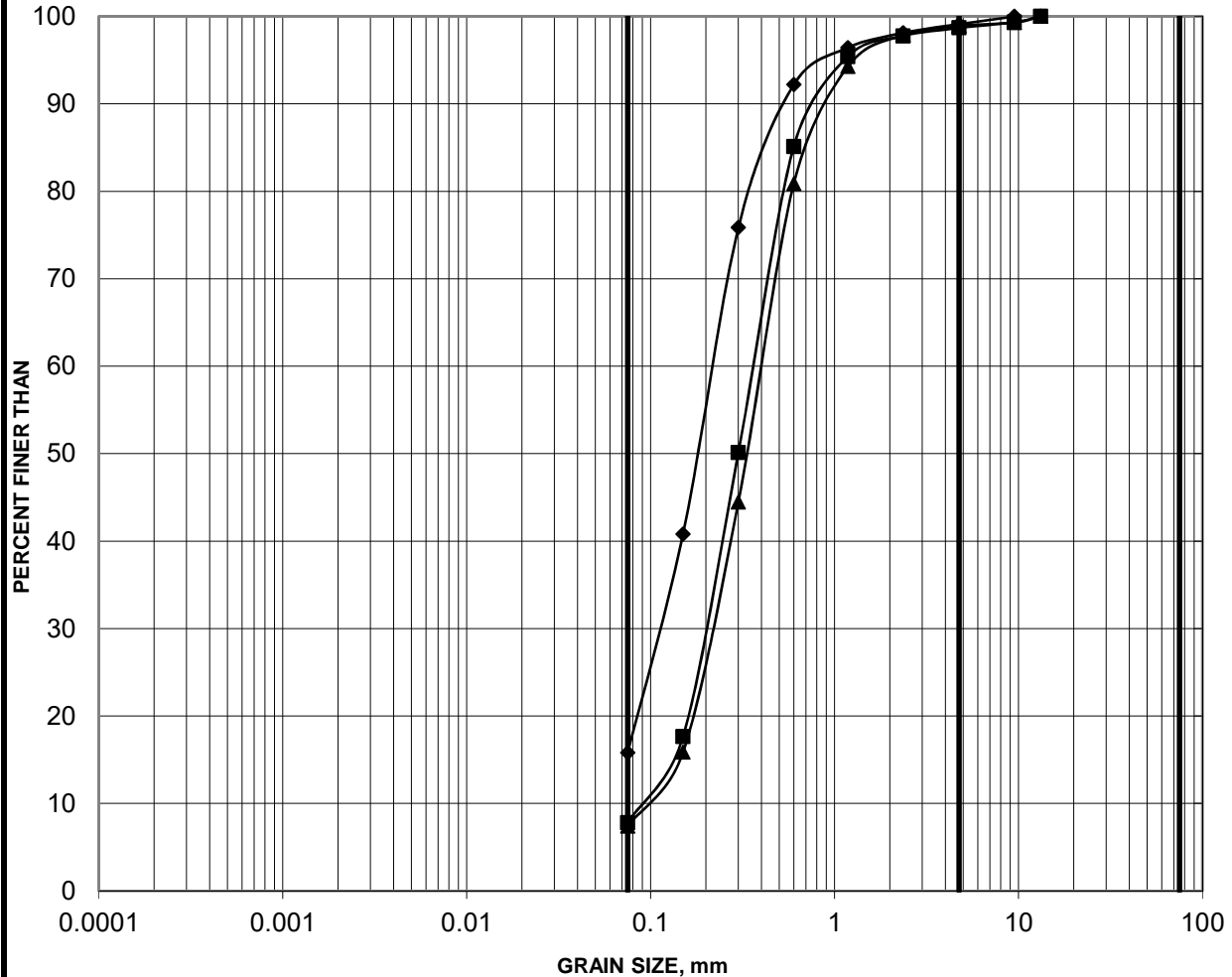
SILT AND CLAY	FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE SIZE
	SAND SIZE			GRAVEL SIZE		

Borehole	Sample	Depth (m)
■ 19-407	1	0.30-0.76

GRAIN SIZE DISTRIBUTION

FIGURE B14

SAND (FILL)



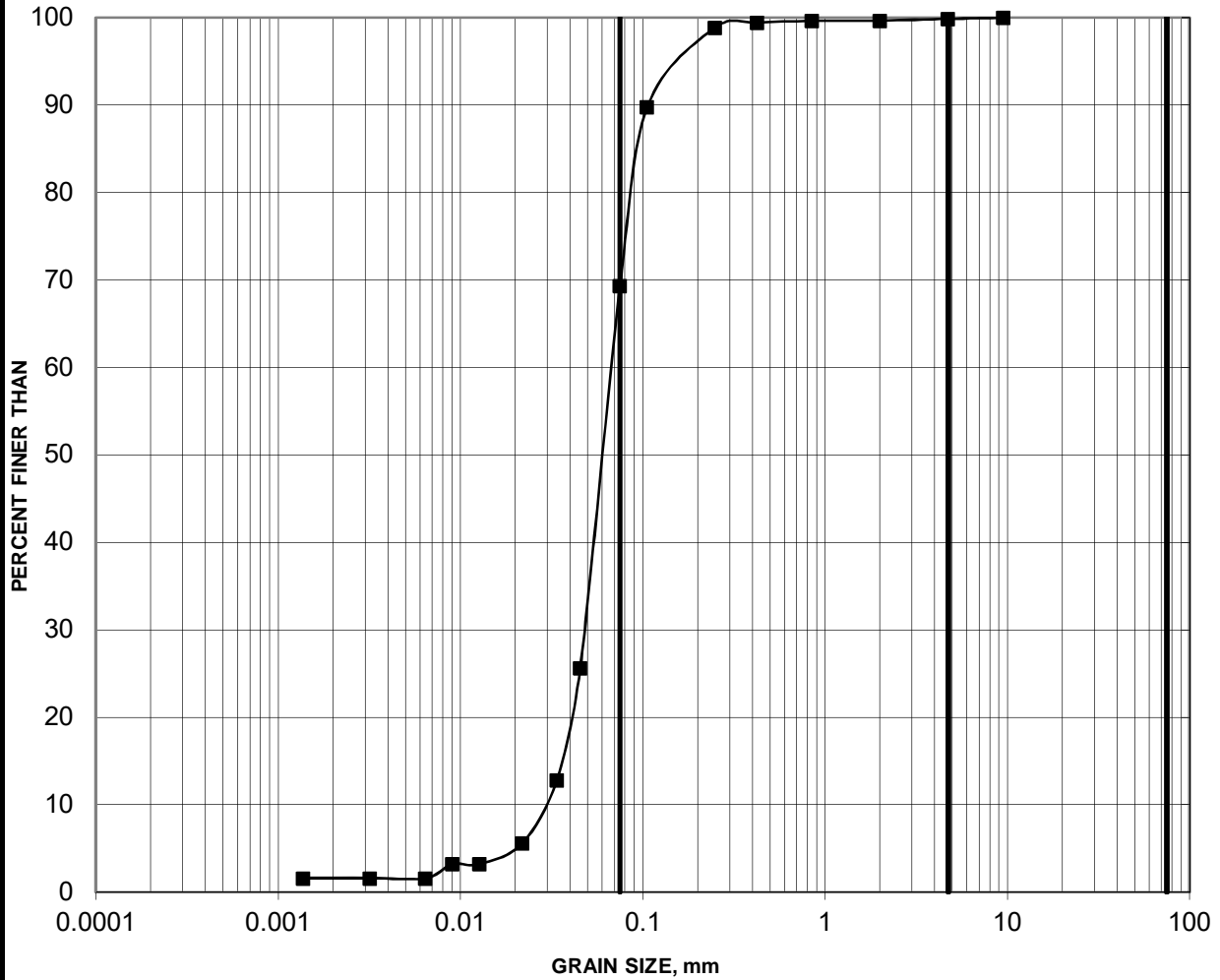
SILT AND CLAY	FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE SIZE
	SAND SIZE			GRAVEL SIZE		

Borehole	Sample	Depth (m)
■ 19-407	4	2.29-2.90
◆ 19-408	2	1.52-2.13
▲ 19-408	7	5.33-5.94

GRAIN SIZE DISTRIBUTION

FIGURE B15

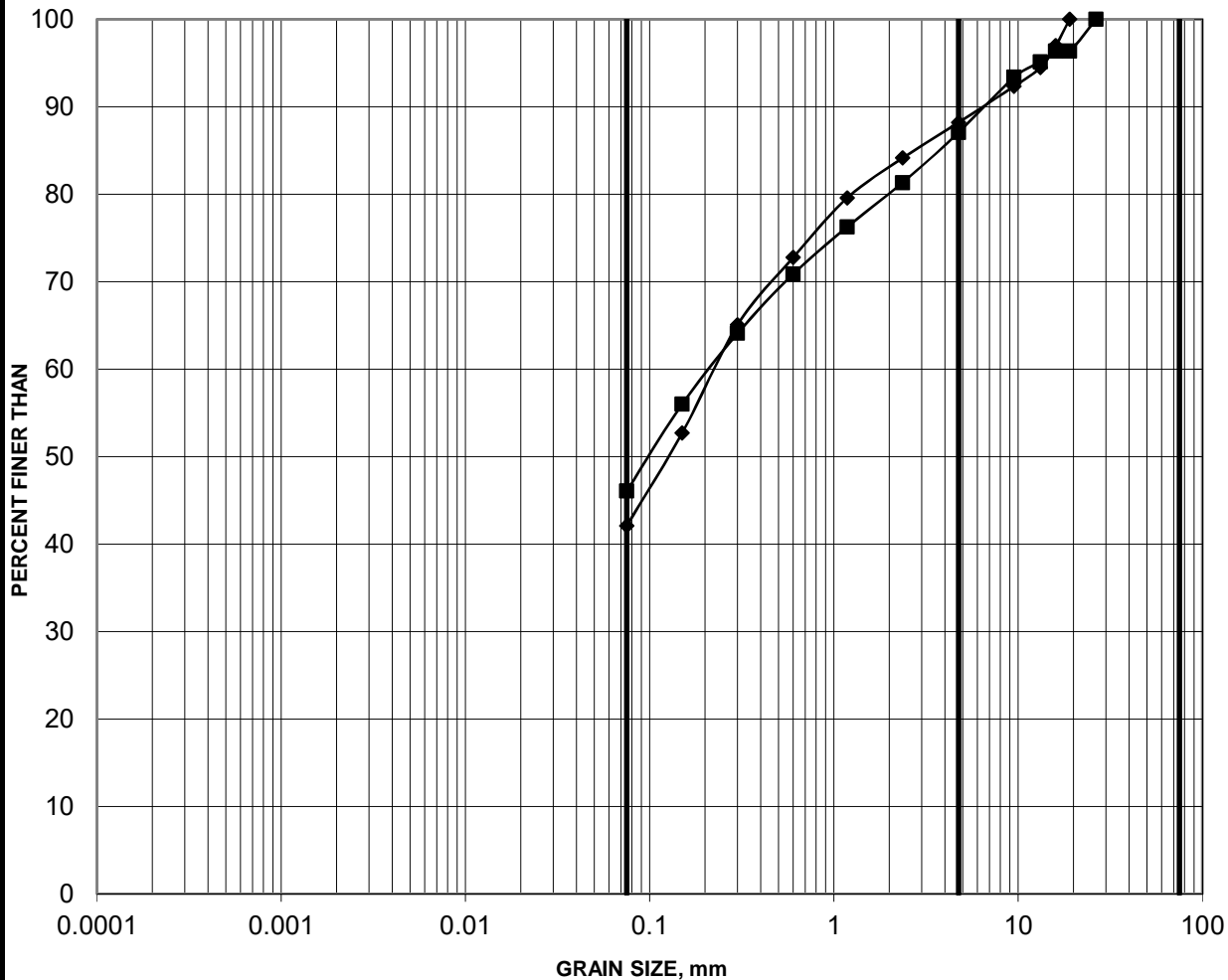
SANDY SILT



SILT AND CLAY	FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE SIZE
	SAND SIZE			GRAVEL SIZE		

Borehole	Sample	Depth (m)
19-407	12	8.38-8.99

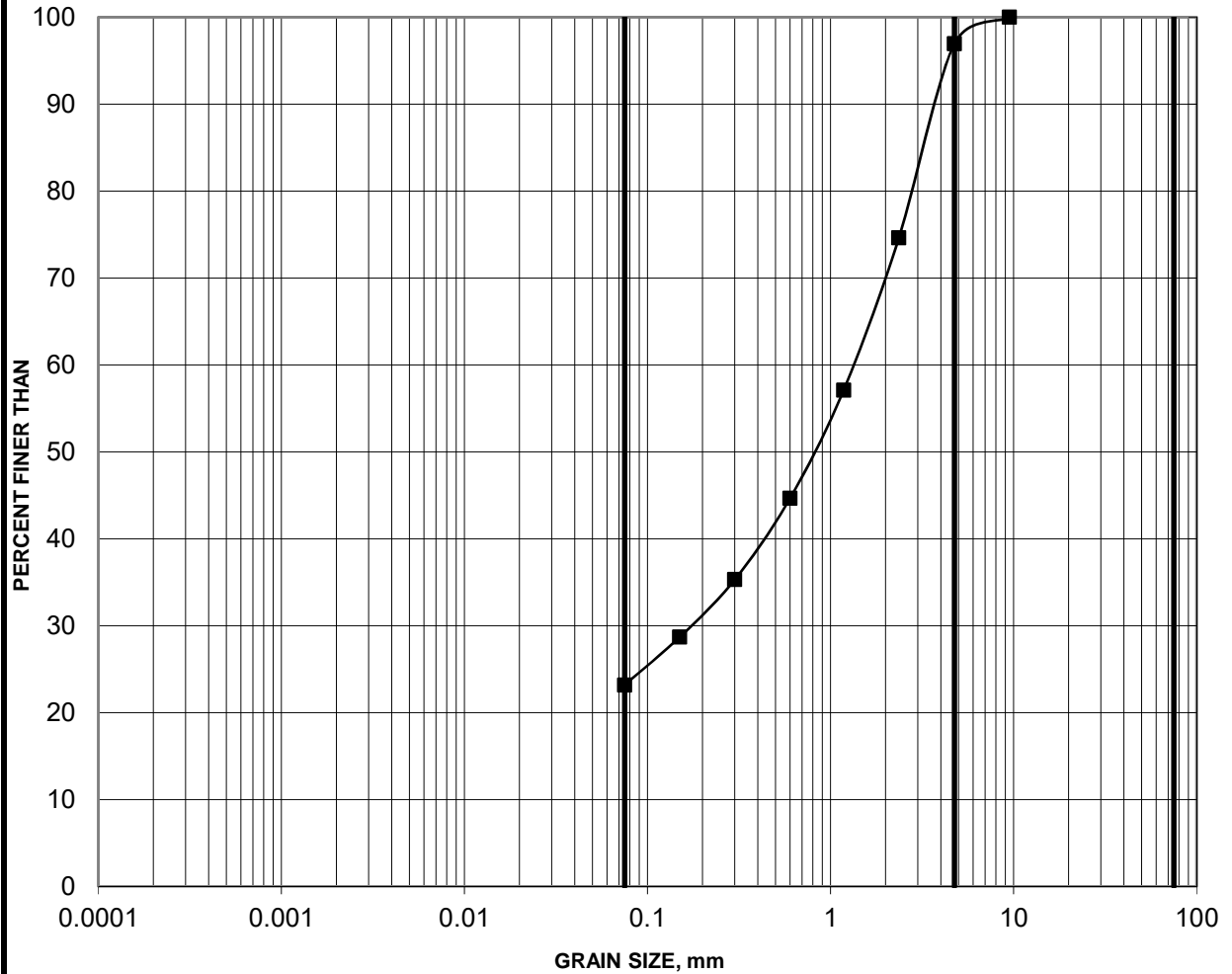
GLACIAL TILL



SILT AND CLAY	FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE SIZE
	SAND SIZE			GRAVEL SIZE		

Borehole	Sample	Depth (m)
■ 19-407	13	9.14-9.75
◆ 19-408	11	8.38-8.99

SILTY SAND (FILL)



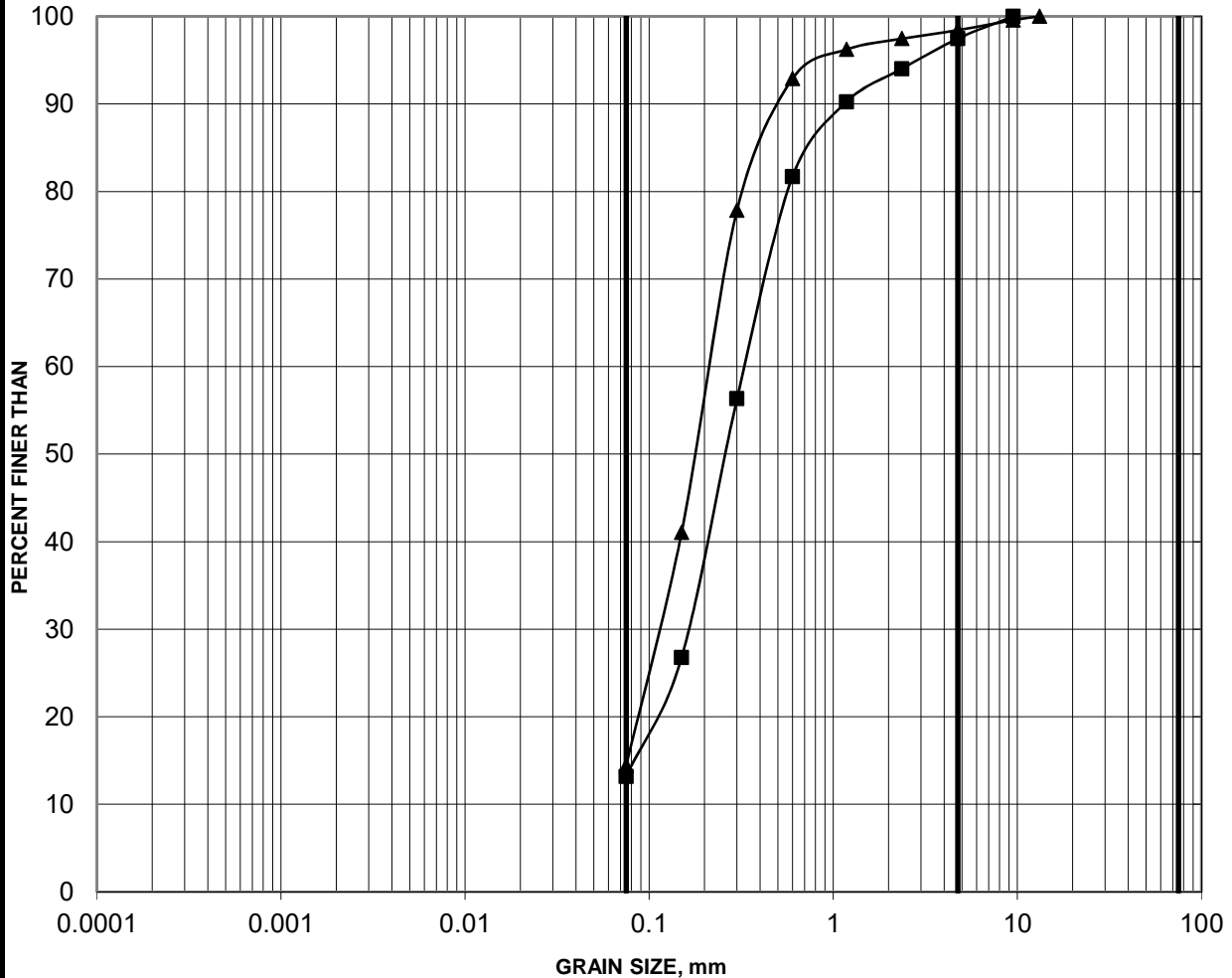
SILT AND CLAY	FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE SIZE
	SAND SIZE			GRAVEL SIZE		

Borehole	Sample	Depth (m)
■ 19-410	1	0.76-1.40

GRAIN SIZE DISTRIBUTION

FIGURE B18

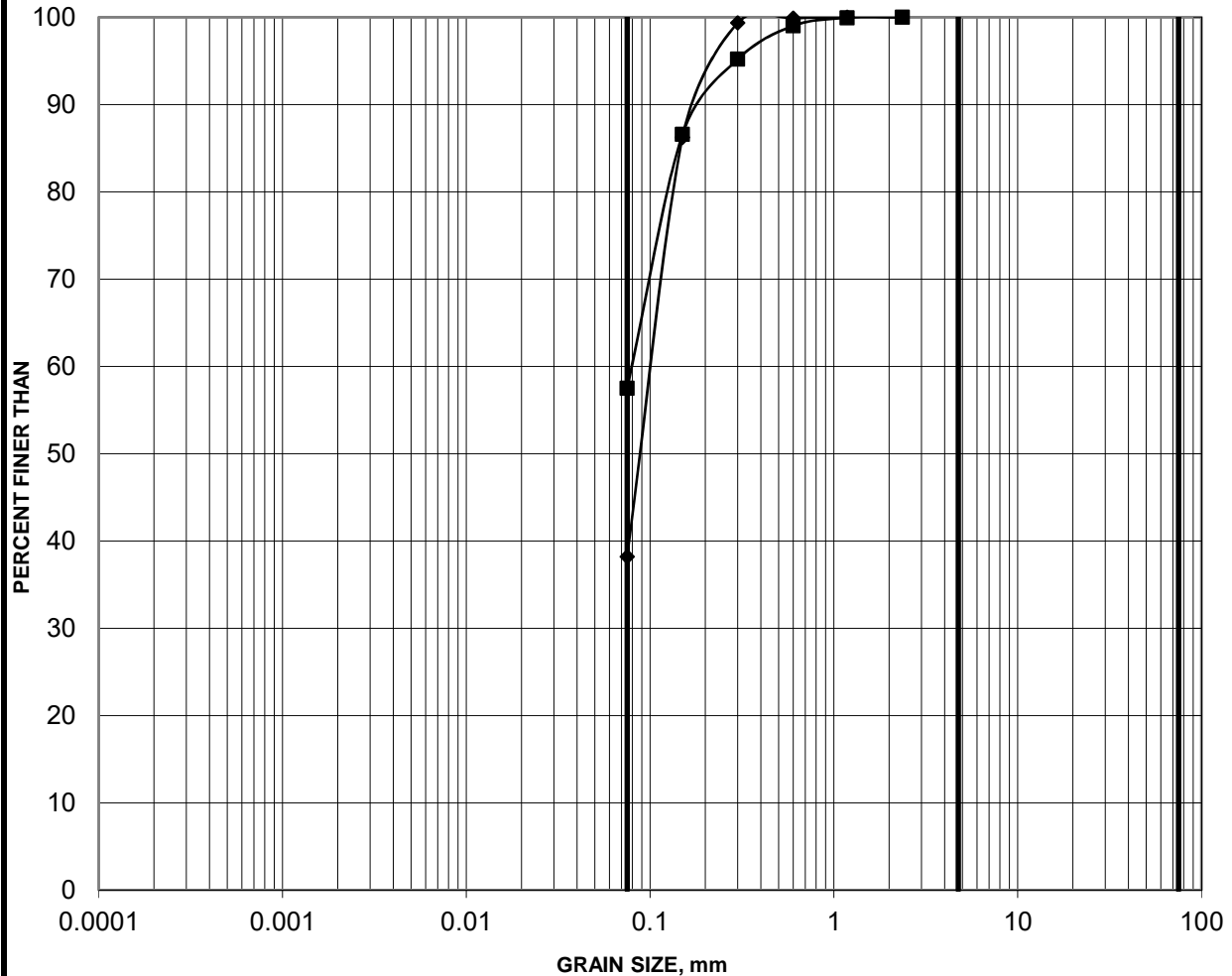
SAND (FILL)



SILT AND CLAY	FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE SIZE
	SAND SIZE			GRAVEL SIZE		

Borehole	Sample	Depth (m)
■ 19-409	4	2.29-2.90
▲ 19-410	3	2.29-2.90

SILT AND SAND

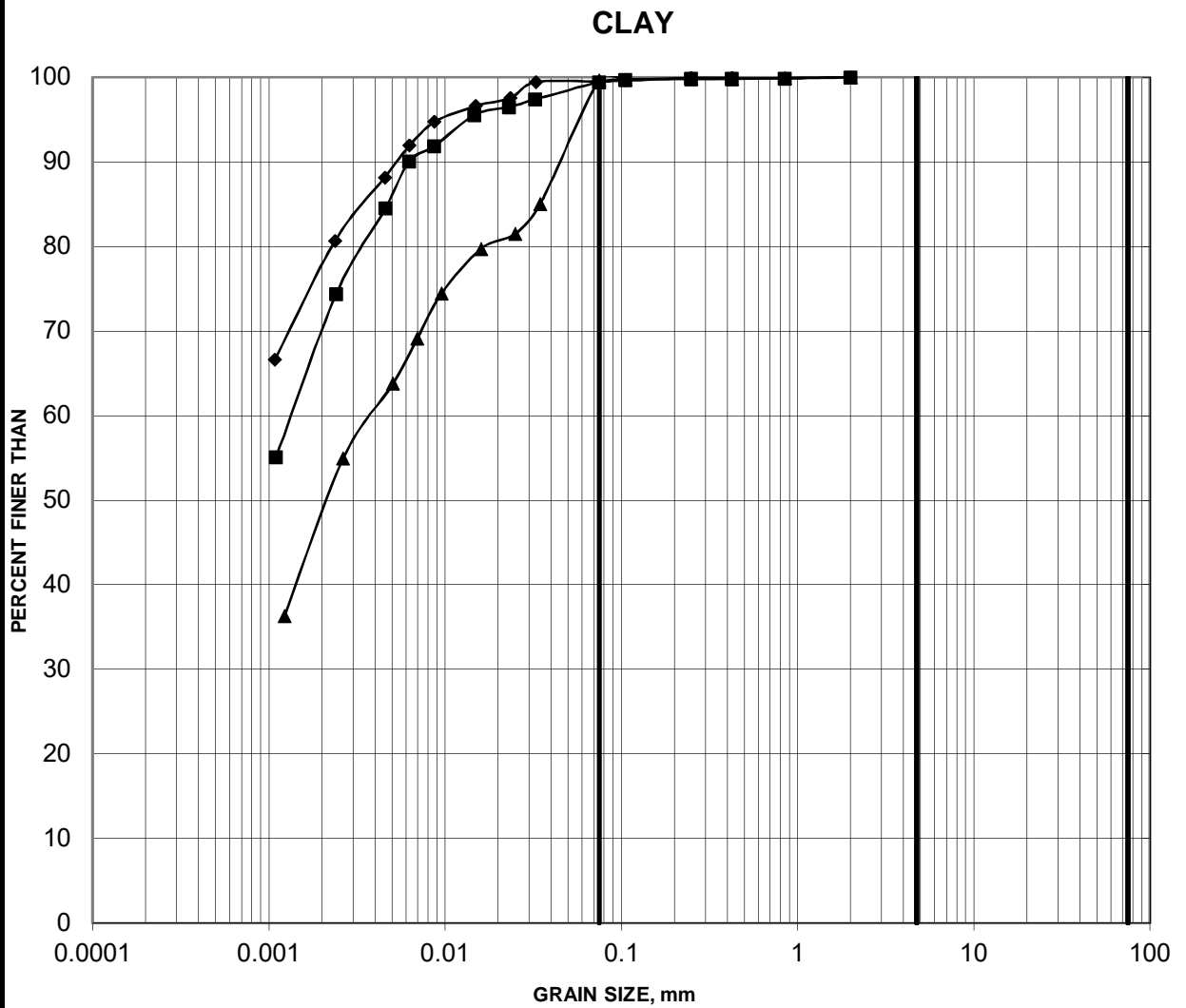


SILT AND CLAY	FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE SIZE
	SAND SIZE			GRAVEL SIZE		

Borehole	Sample	Depth (m)
■ 19-409	8	5.33-5.94
◆ 19-410	7	5.33-5.94

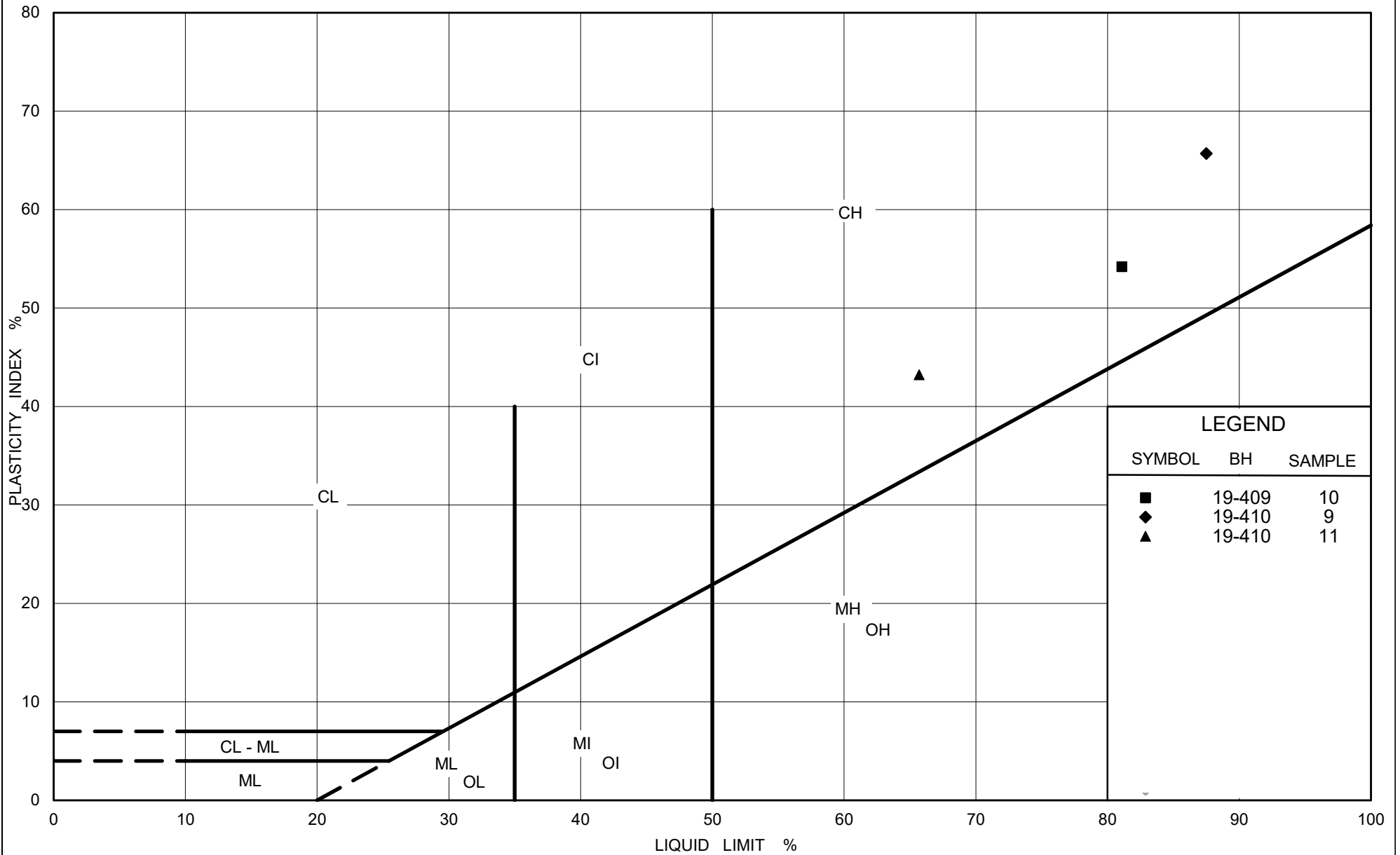
GRAIN SIZE DISTRIBUTION

FIGURE B20



SILT AND CLAY	FINE	MEDIUM	COARSE	FINE	COARSE	COBBLE SIZE
	SAND SIZE			GRAVEL SIZE		

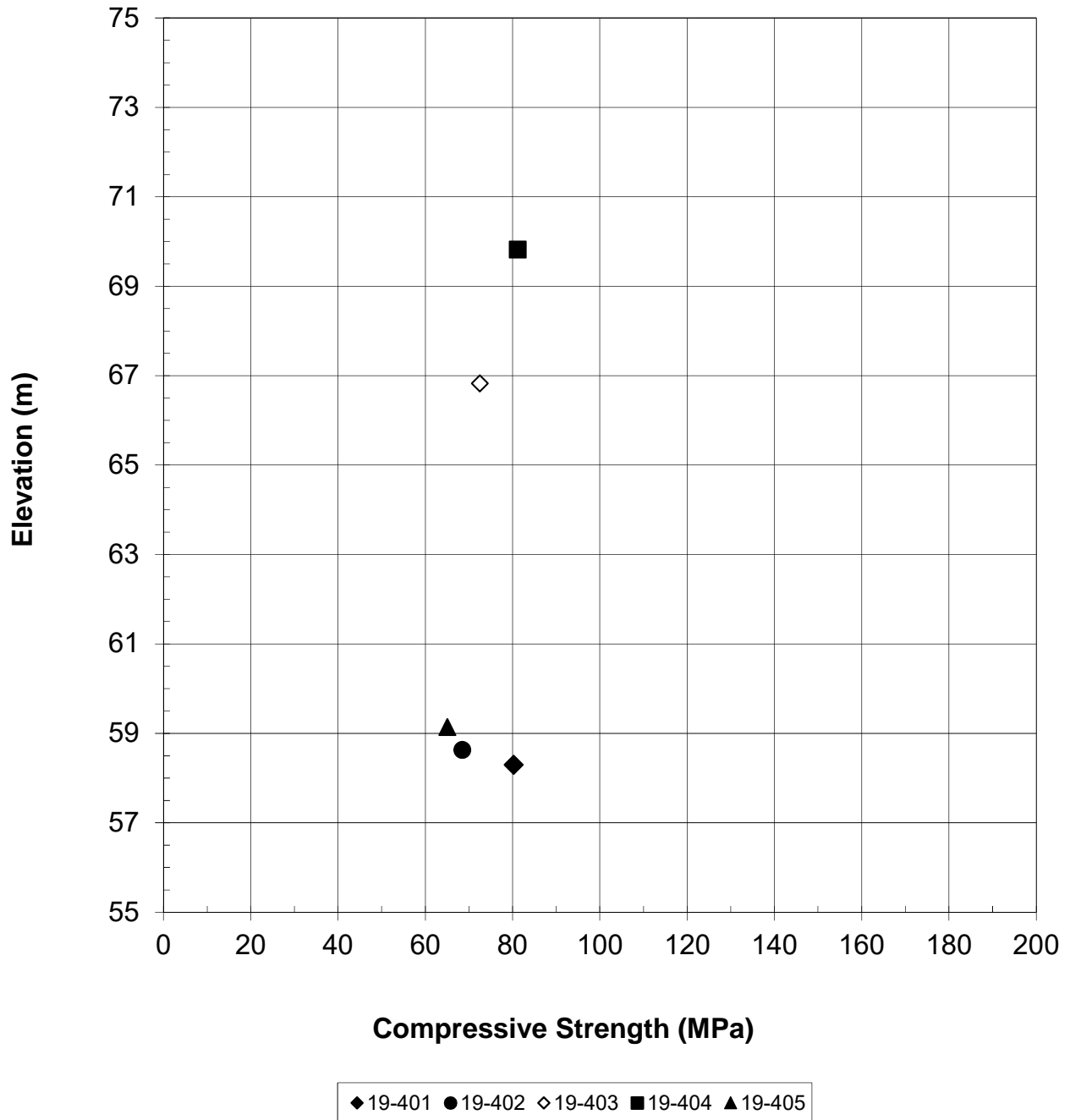
Borehole	Sample	Depth (m)
■ 19-409	10	6.86-7.47
◆ 19-410	9	6.86-7.47
▲ 19-410	11	9.14-9.75



LEGEND		
SYMBOL	BH	SAMPLE
■	19-409	10
◆	19-410	9
▲	19-410	11

**SUMMARY OF LABORATORY COMPRESSIVE STRENGTH
UNCONFINED COMPRESSION TESTS**

FIGURE B22



APPENDIX C

Basic Chemical Analysis Results
Eurofins Report Numbers 1908450 and 1912180

Certificate of Analysis

Client: Golder Associates Ltd (Ottawa)
1931 Robertson Road,
Ottawa, Ontario

Attention: Kenton Power

PO#:

Invoice to: Golder Associates Ltd

Report Number: 1908450
Date Submitted: 2019-05-29
Date Reported: 2019-06-05
Project: 1655214/1400
COC #: 843943

Lab I.D.
Sample Matrix
Sample Type
Sampling Date
Sample I.D.

1429393
Soil
2019-05-13
14-405 sa8 17.5-19.5

Group	Analyte	MRL	Units	Guideline	
Anions	SO4	0.01	%		<0.01
Cl in Concrete	Cl	0.002	%		0.032
General Chemistry	Electrical Conductivity	0.05	mS/cm		0.56
	pH	2.00			8.31
	Resistivity	1	ohm-cm		1790

Guideline =

*** = Guideline Exceedence**

Results relate only to the parameters tested on the samples submitted.
Methods references and/or additional QA/QC information available on request.

MRL = Method Reporting Limit, AO = Aesthetic Objective, OG = Operational Guideline, MAC = Maximum Acceptable Concentration, IMAC = Interim Maximum Acceptable Concentration, STD = Standard, PWQO = Provincial Water Quality Guideline, IPWQO = Interim Provincial Water Quality Objective, TDR = Typical Desired Range

Certificate of Analysis

Client: Golder Associates Ltd (Ottawa)
1931 Robertson Road,
Ottawa, Ontario

Attention: Kenton Power
PO#:

Invoice to: Golder Associates Ltd

Report Number: 1912180
Date Submitted: 2019-07-11
Date Reported: 2019-07-18
Project: 1655214/1400
COC #: 846092

Group	Analyte	MRL	Units	Guideline	1440656 Soil 2019-06-16 19-401 sa 5	1440657 Soil 2019-06-19 19-404 sa 3	1440658 Soil 2019-06-20 19-406 sa 6	1440659 Soil 2019-06-17 19-407 sa 3
Anions	Cl	0.002	%		0.114	0.037	0.058	0.022
General Chemistry	Electrical Conductivity	0.05	mS/cm		0.35	0.18	0.15	0.18
	pH	2.00			8.29	9.22	8.46	9.08
	Resistivity	1	ohm-cm		2860	5560	6670	5560
Others	SO4	0.01	%		0.02	0.02	<0.01	0.01

Group	Analyte	MRL	Units	Guideline	1440660 Soil 2019-06-20 19-410 sa 5
Anions	Cl	0.002	%		0.038
General Chemistry	Electrical Conductivity	0.05	mS/cm		0.17
	pH	2.00			8.55
	Resistivity	1	ohm-cm		5880
Others	SO4	0.01	%		<0.01

Guideline = * = **Guideline Exceedence**

Results relate only to the parameters tested on the samples submitted.
Methods references and/or additional QA/QC information available on request.

MRL = Method Reporting Limit, AO = Aesthetic Objective, OG = Operational Guideline, MAC = Maximum Acceptable Concentration, IMAC = Interim Maximum Acceptable Concentration, STD = Standard, PWQO = Provincial Water Quality Guideline, IPWQO = Interim Provincial Water Quality Objective, TDR = Typical Desired Range



golder.com