

CONTRACT NO. xxxx-xxxx

G.W.P. 3025-14-00

FOUNDATION INVESTIGATION REPORT

HIGHWAY 9, TEESWATER RIVER BRIDGE REHABILITATION

(SITE No. 2-256)

CONTRACT 5B
STRUCTURE REHABILITATION

Ministry Of Transportation





August 2017

DESKTOP FOUNDATION INVESTIGATION REPORT

**Teeswater River Bridge Rehabilitation
Site 2-256, Highway 9
Contract 5B Structure Replacements and Rehabilitation
GWP 3025-14-00
Ministry of Transportation, Ontario - West Region**

Submitted to:

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REPORT



Report Number: 1534424-5002C-R01

Geocres No.: 41A-244

Distribution:

8 Copies Stantec Consulting Ltd.
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1.0 INTRODUCTION

Golder Associates Ltd. (Golder Associates) has been retained by Stantec Consulting Ltd. (Stantec) on behalf of the Ministry of Transportation, Ontario (MTO) to carry out a desktop review of the subsurface information available for the Teeswater River bridge on Highway 9 as part of the detail design work for GWP 3025-14-00. The project involves the detailed design of the replacement and rehabilitation of thirty-nine structures along multiple highways in Southwestern Ontario. This report addresses the proposed rehabilitation of the Teeswater River bridge (Site 2-256) on Highway 9 in the Geographic Township of Greenock in Bruce County, Ontario.

The purpose of this report is to provide recommendations based on a site reconnaissance together with the available geotechnical and geological data available from the MTO Geocres Library. The terms of reference for the scope of work are outlined in the MTO's Request for Proposal and in Golder Associates' proposal P1534424 dated September 2, 2015. The work was carried out in accordance with our Quality Control Plan for Foundation Engineering dated October 26, 2015.

2.0 SITE DESCRIPTION

The subject site is located on Highway 9 approximately 140 metres east of Union Street in the community of Riversdale, in the Geographic Township of Greenock, Bruce County, Ontario. The approximate location of the bridge site is shown on the Key Plan, Figure 1.

This section of Highway 9 is currently a two lane, undivided highway with gravel shoulders. The bridge is oriented approximately east-west. The Teeswater River flows beneath the bridge generally from south to north. Highway 9 has a pavement surface elevation at about 277.5 metres at the bridge site. The existing precast concrete girder structure was constructed in 1969 as a replacement for the original structure. According to MTO's Structure Maintenance and Repair History Report¹, the bridge was rehabilitated in 1975, 1986, 2008 and 2012. The bridge has three spans with a total length of about 43 metres. The area immediately surrounding the site generally consists of flat-lying to gently rolling agricultural and forested lands to the east and the community of Riversdale to the west. Site photographs are provided in Appendix A.

3.0 INVESTIGATION PROCEDURES

The sources of information for this report included a site reconnaissance carried out at the site on February 14, 2017 together with a review of the available information from the MTO Geocres Library and the Ontario Geological Survey (OGS). No additional foundation investigations have been carried out for this assignment.

Geocres Report No. 41A-019 titled "Foundation Investigation Report For Proposed New Structure at Crossing Of Teeswater River and Highway #9, District #5 (Owen Sound), W.J. 67-F-19 – W.P. 101-64", dated April 18, 1967 was reviewed in conjunction with the preparation of this report. The Records of Boreholes and related laboratory test results are attached to this report in Appendix B. The Geocres report presented the results of the laboratory testing on the borehole logs and did not include separate figures illustrating the results.

¹ MTO, undated report: Structure Maintenance/Repair History (MRH Report) for Site Number 2-256, Highway 9 Teeswater River Bridge. This report contains the dates and summary details of rehabilitation works and inspections carried out at this site.



The borehole locations and ground surface elevations at the borehole locations are shown on the original Record of Borehole sheets in Appendix A and on Drawing 1, prepared by Golder. The table below summarizes the coordinates, ground surface elevations and depths of these previous boreholes.

Borehole	Location (m)		Ground Surface / Riverbed Elevation (m)	Depth of Water (m)	Borehole Depth# (m)
	Northing	Easting			
1	4 883 883	397 997	272.49	-	15.45
2*	4 883 870	398 002	273.01	-	4.27
3	4 883 884	398 013	270.45	3.20	10.67
4	4 883 879	398 050	273.50	-	15.24
5	4 883 888	398 031	271.27	1.89	14.84
6*	4 883 876	398 035	271.88	1.28	4.72
7*	4 883 891	398 046	273.01	-	5.15

*These boreholes contain records of dynamic cone penetration testing only.

#For boreholes 3, 5 and 6, the borehole depth includes the water column above the riverbed.

4.0 SITE GEOLOGY

The site lies within the Horseshoe Moraines physiographic region. This region is characterized by irregular, stony knobs and ridges which are composed mostly of till with some sand and gravel deposits as well as sand and gravel terraces and swampy valley floors². The quaternary geology mapping indicates that the surficial soils in the area of the site generally consist of modern alluvium containing silt, sand and gravel.³ Based on the available topographic bedrock mapping, the underlying bedrock surface is found at about elevation 256 metres⁴ corresponding to an overburden thickness of about 14 to 18 metres. The rock formation is mapped and described as limestone, dolostone and shale of the Detroit River Group of the Onondaga Formation of Middle Devonian age⁵.

5.0 SUBSURFACE CONDITIONS

The subsurface conditions encountered in the boreholes previously drilled at the site (Geocres Report No. 41A-019) are shown in detail on the Record of Borehole sheets in Appendix A. The following discussion has been simplified in terms of major soil or rock strata for the purposes of geotechnical design. The soil boundaries discussed in this report and illustrated on the Records of Boreholes have been inferred from non-continuous samples and observations of drilling resistance and represent a transition from one soil or rock type to another. The boundaries should not necessarily be interpreted to represent exact planes of geological change. Further, subsurface conditions should be expected to vary between and beyond the borehole locations. In addition, post-

² Chapman, L.J., and Putnam, D.F., 1984: Physiography of Southern Ontario; Ontario Geological Survey, Special Volume 2, 270p.

³ Cowan, W.R., and Pinch, J.J., 1986: Quaternary Geology of the Walkerton-Kincardine Area. Southern Ontario; Ontario Geological Survey, Map P.2956. Geological Series-Preliminary Map, scale 1:50 000. Geology 1975-1979.

⁴ Karrow, P.F. 1962, Bedrock Topography Series, Kincardine-Walkerton Sheet. Ontario Department of Mines, Preliminary Map P.165, Scale 1:50 000.

⁵ Ontario Geological Survey 2011. 1:250 000 scale bedrock geology of Ontario; Ontario Geological Survey, Miscellaneous Release---Data 126-Revision 1.



investigation construction activities at the site may have altered the subsurface conditions from those shown on the previous Records of Boreholes.

The soil descriptions on the previous Records of Boreholes have been interpreted to correspond to standard MTO soil descriptions, using the original laboratory data, where available. Although the majority of the descriptions provided on the Record of Boreholes from Geocres No. 41A-019 have been retained, materials described as sandy gravel have been classified as sand and gravel or silty sand and gravel for the purposes of this report. The sandy silt layer at elevation 264.6 metres in borehole 5 has been classified as silty sand. The standard MTO soil descriptions are used in the discussion below and in the profile on Drawing 1. The subsurface conditions encountered in the boreholes generally consisted of organic silt, granular deposits (silt, sandy silt, silty sand, and sand and gravel), interlayered with clayey silt and silty clay, overlying bedrock. Based on the elevation of the boreholes and dynamic cone penetration hole locations reported in Geocres No. 41A-019, the elevation of the ground surface at the abutments ranged from 272.5 to 273.5 metres at the time of the investigation. The pre-construction riverbed elevation ranged between elevation 270.4 and 271.8 metres at boreholes 3, 5 and 6. The depth of the river at these three borehole locations ranged between 1.3 and 3.2 metres.

Embankment fills were constructed when the existing structure was built. Currently, the nature of this fill is unknown but the grade was raised by approximately 5 m and 3 m to approximate elevation 277.3 and 276.8 metres at the west and east abutments, respectively.

5.1 Site Stratigraphy

A layer of sandy silt was found at ground surface or formed the river substrate at boreholes 1, 3, 4 and 5. The thickness of the sandy silt stratum varied between 0.8 and 2.1 metres. The sandy silt was very loose to compact with standard penetration test (SPT) N values ranging from 4 to 24 blows per 0.3 metres. The sandy silt is of low plasticity based on a single sample with liquid and plastic limits of 39 and 36 per cent, respectively.

Organic silt was encountered at elevation 271.5 metres in borehole 4 below the sandy silt deposit. The organic silt layer was about 1.7 metres thick and had SPT N values of 4 blows per 0.3 metres. The organic silt had water contents of 77 and 95 per cent.

Layers of clayey silt and/or silty clay were encountered beneath the sandy silt in boreholes 1, 3 to 5 and beneath the organic silt in borehole 4. These cohesive soils were encountered between elevation 269.2 and 271.5 metres and were 1.8 to 3.7 metres thick. The very stiff to hard cohesive soils had SPT N values of 15 to 41 blows per 0.3 metres and water contents of about 13 to 18 per cent. The cohesive deposits are of low to intermediate plasticity based on liquid limits of 18 to 38 per cent and plastic limits of 13 to 20 per cent.

Granular deposits, ranging in gradation from silt to sand and gravel, were encountered in boreholes 1 and 3 to 5 beneath the clayey silt from elevation 266.2 and 269.7 metres. The thickness of the granular layers ranged from about 6.9 to 7.3 metres thick.

Borehole 3 was terminated in a sand and gravel layer after exploring it for about 3.1 metres. The granular deposits had SPT N values of 15 to over 100 blows per 0.3 metres. The sand and gravel deposits below approximate elevation 263.7 metres were very dense while the overlying silt to silty sand deposits were loose to dense. Boulders were noted in the sand and gravel deposits. Water contents ranged between 8 to 25 per cent with silt layers having water contents of 21 per cent and above. The silt deposits contain clay layers and are of low plasticity based on liquid limits of 25 and 27 per cent and plastic limits of 19 and 20 per cent.



Limestone bedrock was encountered beneath the sand and gravel layer in borehole 1 at elevation 260.8 metres or a depth of 11.7 metres. Borehole 1 was terminated in the bedrock after it was cored to a depth of 3.7 metres below the bedrock surface. The bedrock in borehole 1 was described as weathered from elevation 259.0 to 260.8 metres, and sound from elevation 257.0 to 259.0 metres. Boreholes 4 and 5 were terminated in inferred bedrock at elevations 259.0 and 259.5 metres after penetrating the rock for 0.8 and 1.2 metres, respectively.

5.2 Groundwater Conditions

Based on the information provided in the Geocres report, artesian groundwater conditions were encountered in boreholes 1, 3, 4 and 5. The encountered groundwater elevation was not indicated on the borehole logs or in the report except to indicate that the water rose 1.2 m in borehole 1 and the water rose only 0.3 m in the other three boreholes. Based on our review of the borehole logs the groundwater level cannot be confirmed.

Borehole 3 was drilled in the river and the reported river water level during drilling on March 30, 1967 was elevation 273.6 metres. Boreholes 5 (drilled March 28 and 29, 1967) and 6 (drilled March 23, 1967) were advanced in the river floodplain and reported a river water level and an ice level above the ground surface, respectively, both corresponding to elevation 273.2 metres. A river water level of 271.8 metres in January 1967 was also reported in the Geocres report. The preliminary General Arrangement drawing provided by Stantec indicated a river water level of 272.4 metres in April 2016.

The reported water levels are not necessarily considered to be representative of the long-term, stabilized groundwater conditions. The groundwater levels should be expected to fluctuate seasonally and be higher during periods of sustained precipitation or during spring snow melt conditions.

6.0 SITE RECONNAISSANCE

A site reconnaissance was carried out at the site on February 14, 2017 by a member of our geotechnical engineering staff. In general, the approach embankments and abutment foreslopes appeared to be stable with no visible signs of movement. The foreslopes were covered with rip rap largely consisting of concrete pieces. The abutments appeared to be performing adequately with no observable movement(s) noted, although the east pile cap is partially exposed. Some concrete spalling and exposed rebar was noted at the abutment locations. The piers were in generally good condition although there appeared to be some exposed reinforcing steel in one of the columns at the east pier. Areas of delaminations and spalling were noted at the ends of some of the concrete girders. The bridge soffit is in generally good condition although some concrete spalling and exposed rebar was noted. The asphalt riding surface was in fair condition at the approaches, with some minor to moderate cracking, and in poor condition in the area of the bridge deck with more severe cracking. Photographs from the site reconnaissance are shown in Appendix B.



7.0 MISCELLANEOUS

The site reconnaissance and preparation of the report was carried out by Mr. Daniel Hyland, E.I.T. under the direction of the Project Engineer, Ms. Dirka U. Prout, P.Eng. The report was reviewed by Mr. André Bom, P.Eng., an Associate with Golder Associates. Mr. Fintan J. Heffernan, P.Eng., the Designated MTO Contact and Quality Control Auditor for this assignment, conducted an independent quality review of the report.

GOLDER ASSOCIATES LTD.



Dirka U. Prout, P.Eng.
Senior Geotechnical Engineer


André Bom, P.Eng.
Associate



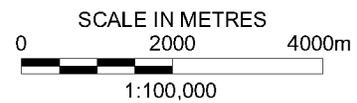
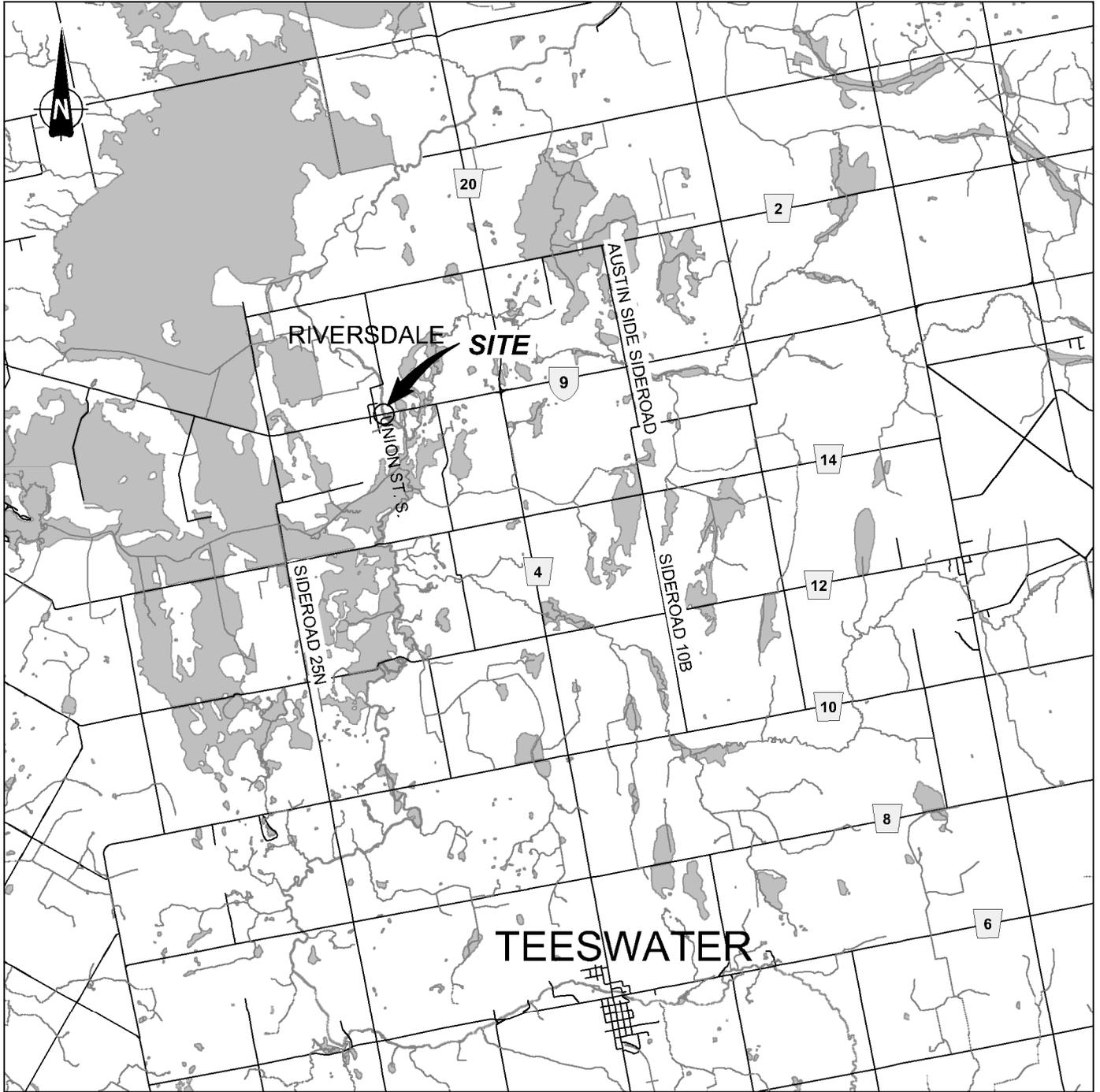
Fintan J. Heffernan, P.Eng.
MTO Designated Contact

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MTO Designated Contact

DH/DUP/AB/FJH/cr

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part a&b fdns teeswater site 2-256.docx



REFERENCE

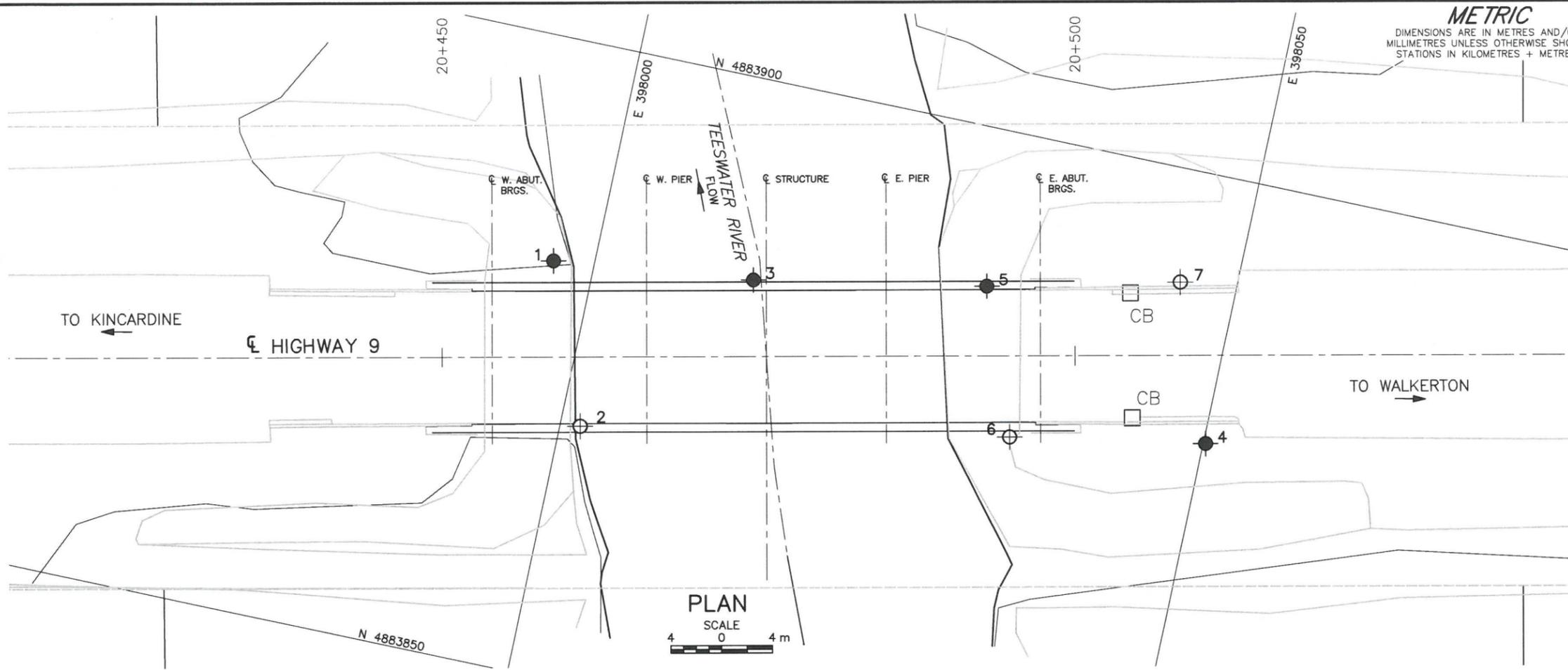
PLAN BASED ON CANMAP STREETFILES V.2008.4.

NOTES

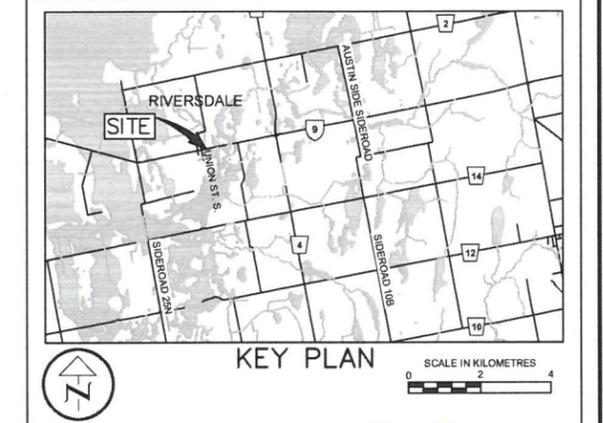
THIS DRAWING IS TO BE READ IN CONJUNCTION WITH ACCOMPANYING TEXT.
ALL LOCATIONS ARE APPROXIMATE ONLY.

PROJECT						
TEESWATER RIVER BRIDGE REHABILITATION, SITE 2-256						
HIGHWAY 9						
GWP 3025-14-00						
TITLE						
KEY PLAN						
PROJECT No.		1534424		FILE No.	1534424-5002C-F01001	
CADD	LMK	May 30/17	SCALE	AS SHOWN	REV.	0
CHECK			FIGURE 1			

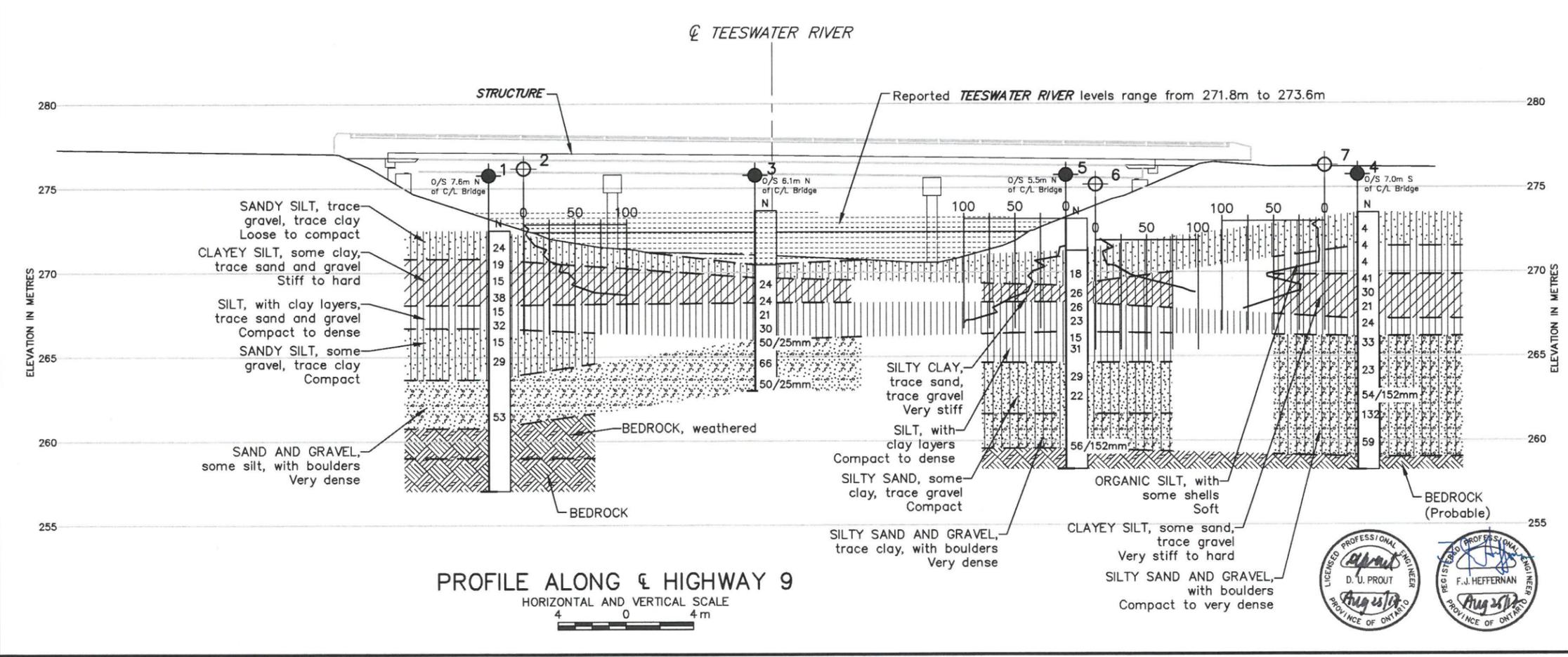




CONT No. WP No. 3025-14-00
 TEESWATER RIVER BRIDGE
 STRUCTURE REHABILITATION
 BOREHOLE LOCATIONS AND SOIL STRATA



- LEGEND**
- Borehole (from Geocres Report 41A-019)
 - ⊕ Cone Penetration (from Geocres Report 41A-019)
 - N Standard Penetration Test Value
 - 16 Blows/0.3m unless otherwise stated (Std. Pen. Test, 475 j/blow)
 - Dynamic Cone Penetration Test



No.	ELEVATION	CO-ORDINATES (MTM NAD83 ZONE 11)	
		NORTHING	EASTING
GEOCRES NO. 41A-019			
1	272.49	4 883 882.5	397 996.8
2	272.86	4 883 870.1	398 001.6
3	273.65	4 883 884.3	398 012.5
4	273.50	4 883 879.1	398 050.2
5	273.16	4 883 887.6	398 030.7
6	271.88	4 883 876.3	398 034.9
7	273.01	4 883 891.1	398 045.6

NOTES

This drawing is for subsurface information only. Surface details and features are for conceptual illustration.

The boundaries between soil strata have been established only at borehole locations. Between boreholes the boundaries are assumed from geological evidence.

REFERENCE

Base plans provided by Stantec.

NO.	DATE	BY	REVISION
Geocres No. 41A-244			
HWY.	9	PROJECT NO.	1534424
DIST.		DATE:	Aug. 21/17
SUBM'D. DH	CHKD. DH	APPD. FJH	SITE: 2-256
DRAWN: LMK	CHKD. DUP	DWG.	1





APPENDIX A

Site Photographs



APPENDIX A

Site Photographs



Photograph 1: East end of bridge, looking west.



Photograph 2: East end of bridge, looking west.



APPENDIX A
Site Photographs



Photograph 3: South elevation.



Photograph 4: Embankment sideslope in northeast quadrant.



APPENDIX A

Site Photographs



Photograph 5: West abutment, looking north.



Photograph 6: Looking east under bridge.



APPENDIX A
Site Photographs



Photograph 7: East abutment, looking north.



Photograph 8: Partially exposed pile cap at east abutment.

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APPENDIX B

Records of Boreholes - Geocres Report No. 41A-019

DEPARTMENT OF HIGHWAYS - ONTARIO

RECORD OF BOREHOLE NO. 4

FOUNDATION SECTION

MATERIALS & TESTING DIVISION

JOB 67-F-19 LOCATION Sta. 64 + 73 @ Hwy.#9 and 20' o/s to Lt. ORIGINATED BY AMS
 W.P. 101-64 BORING DATE March 21, 22 and 23, 1967 COMPILED BY AMS
 DATUM Geodetic BOREHOLE TYPE NX, BX & AX Casing, EXL & AXT, R.C. CHECKED BY [Signature]

SOIL PROFILE		SAMPLES			ELEV. SCALE	DYNAMIC PENETRATION RESISTANCE				LIQUID LIMIT — WL PLASTIC LIMIT — WP WATER CONTENT — W			BULK DENSITY P.C.F.	REMARKS
ELEV. FEET	DESCRIPTION	NUMBER	TYPE	BLOWS / FOOT		SHEAR STRENGTH P.S.F.				WP	W	WL		
273.50m 897.3	GROUND LEVEL													
0.0	Sandy silt with traces of gravel. Very loose.	1	SS	4										
890.8	271.52m (1.98m)	2	SS	4	890									
6.5	Organic Silt with some shells. Very soft.	3	SS	4										
269.84m	(3.66m)	4	SS	41										
	Clayey silt with some sand and traces of gravel. Very stiff to hard.	5	SS	30	880									
		6	SS	21										
		7	SS	24										
873.3	266.18m (7.32m)	8	SS	33	870									
24.0	Sandy gravel, some silt, occ. boulders. Very dense.	9	SS	23										
		10	SS	54/6*	860									
		11	SS	132										
849.8	259.02m (14.48m)	14	SS	59	850									
47.5 817.3	Probable Bedrock													
50.0	End of Borehole													
258.26m (15.24m)														

Gr.1, Sa.20
Si.69, Cl.10

Gr.47, Sa.37
Si. & Cl.16

Gr.33, Sa.40
Si. & Cl.27

As a global, employee-owned organisation with over 50 years of experience, Golder Associates is driven by our purpose to engineer earth's development while preserving earth's integrity. We deliver solutions that help our clients achieve their sustainable development goals by providing a wide range of independent consulting, design and construction services in our specialist areas of earth, environment and energy.

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