



November 27, 2014

FOUNDATION INVESTIGATION REPORT

**BIQUETTE CREEK CULVERT AT STA 13+350
HIGHWAY 17 REHABILITATION BETWEEN WARREN AND VERNER
FROM HIGHWAY 539 EASTERLY TO 0.2 KM EAST
OF WEST JUNCTION OF HIGHWAY 64
MINISTRY OF TRANSPORTATION, ONTARIO
GWP 300-98-00**

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REPORT





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PART A

**FOUNDATION INVESTIGATION REPORT
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1.0 INTRODUCTION

Golder Associates Ltd. (Golder) has been retained by Morrison Hershfield Limited (MH), on behalf of the Ministry of Transportation, Ontario (MTO), to provide foundation engineering services for the replacement of the Highway 17 Biquette Creek culvert at STA 13+350 in the Town of Verner in the Municipality of West Nipissing, Ontario. The Key Plan showing the general location of this section of Highway 17 and the location of the investigated area are shown on Drawing 1. The purpose of this investigation is to establish the subsurface conditions at the location of the culvert by borehole drilling, in situ testing and laboratory testing on selected soil samples.

2.0 SITE DESCRIPTION

The Biquette Creek culvert is located on Highway 17 in the Town of Verner immediately west of the west junction with Highway 64. In general, the topography in the area of the overall project limits consists of flat terrain with commercial and residential properties. The existing highway grade is at about Elevation 210 m with Biquette Creek crossing under the embankment about 10 m below the existing highway grade. The side slopes of the existing embankment are inclined at about 2 Horizontal to 1 Vertical (2H:1V) and the embankment side slopes are vegetated with grass and small trees/shrubs. The existing culvert consists of twin 1.1 m diameter Corrugated Steel Pipes (CSP), 59 m long.

3.0 INVESTIGATION PROCEDURES

The fieldwork for the investigation was carried out between November 27 and December 3, 2013, and between February 12 and 24, 2014, during which time a total of seven boreholes were advanced at the approximate locations shown on Drawing 1:

- four boreholes for the culvert alignment (Boreholes BI-1, BI-2, BI-5/5a and BI-6);
- one borehole for the proposed roadway protection (Borehole BI-3); and
- two boreholes for the proposed cofferdam (Boreholes BI-4 and BI-7).

Boreholes BI-1 to BI-3, located on the existing highway embankment, were advanced to depths between 15.8 m and 21.9 m below ground surface using a truck-mounted CME 55 drill rig outfitted with 108 mm inside diameter continuous flight hollow-stem augers and 'NW' casing with wash boring techniques, supplied and operated by Landcore Drilling Inc. of Sudbury, Ontario. Boreholes BI-4 to BI-7, located at or beyond the existing toe of slope, were advanced to a depth of 14.3 m below ground/ice surface using wash boring methods with portable equipment using NQ casing, supplied and operated by George Downing Estate Drilling Ltd. of Grenville-Sur-La-Rouge, Quebec. Borehole BI-5a was advanced adjacent to Borehole BI-5 to obtain Shelby Tube samples and to complete additional field vane testing. A Dynamic Cone Penetration Test (DCPT) was advanced adjacent to Boreholes BI-2 and BI-4 to BI-6 to depths between 15.2 m and 21.9 m below ground surface.

Soil samples were obtained at intervals of depths of about 0.75 m and 1.5 m, using a 50 mm outer diameter (O.D.) split-spoon sampler driven by an automatic hammer at Boreholes BI-1 to BI-3 and a manual hammer at



FOUNDATION REPORT HIGHWAY 17 BIQUETTE CREEK CULVERT

Boreholes BI-4 to BI-7, and performed in accordance with Standard Penetration Test (SPT) procedure (ASTM D1586). Selected samples of the cohesive soils were obtained using 76 mm O.D. thin-walled ‘Shelby’ tubes (ASTM D1587, Standard Practice for Thin-Walled Tube Sampling) for relatively undisturbed samples. Field vane shear tests were conducted in cohesive soils for determination of undrained shear strengths (ASTM D2573, Standard Test Method for Field Vane Strength Shear Test) using MTO Standard ‘N’ size vanes. The groundwater conditions and water levels in the open boreholes were observed during the drilling operations and are described on the Record of Borehole sheets in Appendix A. All boreholes were backfilled with bentonite upon completion of drilling in accordance with Ontario Reg. 903 (as amended).

The fieldwork was supervised throughout by members of our technical staff, who located the boreholes, arranged for the clearance of underground services, observed the drilling, sampling and in situ testing operations, logged the boreholes, and examined and cared for the soil samples. The samples were identified in the field, placed in appropriate containers, labelled and transported to our Sudbury laboratory where the samples underwent further visual examination and laboratory testing. All of the laboratory tests were carried out to MTO and/or ASTM Standards, as appropriate. Classification testing (water content, Atterberg limits and grain size distribution) was carried out on selected soil samples. The results of the laboratory testing are presented on the Record of Borehole sheets in Appendix A and are also included in Appendix B.

A sample of the creek water was obtained on March 10, 2014, using appropriate sampling protocols and submitted to a specialist analytical laboratory under chain of custody procedures for testing for a suite of parameters. The results of the analytical testing are summarized in Table B1 in Appendix B, together with the detailed analytical laboratory test results.

The as-drilled borehole locations and ground surface elevations were measured and surveyed by members of our technical staff, referenced to the marked stations and offsets on the highway or the ends of the culvert, as applicable. The MTM NAD 83 northing and easting coordinates, ground surface elevations referenced to Geodetic datum and borehole depth at each borehole are presented on the Record of Borehole sheets in Appendix A and are summarized below.

Borehole	Borehole Location		Ground Surface Elevation (m)	Borehole/DCPT Depth Below Ground/Ice Surface (m)
	Northing	Easting		
BI-1	5141606.9	256900.7	210.4	18.9
BI-2	5141600.0	256890.8	210.4	21.9/21.9
BI-3	5141612.0	256878.7	210.5	15.8
BI-4	5141633.4	256911.5	201.4	14.3/15.2
BI-5	5141631.0	256897.4	201.7	14.3/15.2
BI-5a	5141629.9	256897.0	201.7	8.2
BI-6	5141575.9	256881.4	201.3	14.3/15.2
BI-7	5141569.5	256888.3	199.4	14.3*

*includes 0.2 m thick layer of ice and 1.3 m column of water



4.0 SITE GEOLOGY AND SUBSURFACE CONDITIONS

4.1 Regional Geology

Based on terrain mapping (Ontario Geological Survey¹), the site is located on a glaciolacustrine plain in an area of sand and silt deposits with bedrock knobs/outcrops located to the north and south of the plain.

4.2 Subsurface Conditions

The detailed subsurface soil and groundwater conditions, as encountered in the boreholes advanced for this investigation, together with the results of the laboratory tests carried out on selected soil core samples, are given on the Record of Borehole sheets in Appendix A. The results of the in situ tests (i.e., SPT “N”-values and undrained shear strengths from the field vanes) as presented on the Record of Borehole sheets and in Section 4 are uncorrected. Detailed results of the laboratory testing of the soil samples are provided in Appendix B. The stratigraphic boundaries shown on the Record of Borehole sheets and on the stratigraphic profile and cross-section shown on Drawing 1 are inferred from non-continuous sampling, observations of drilling progress and the results of SPTs and in situ testing. These boundaries, therefore, represent transitions between soil types rather than exact planes of geological change. Further, subsurface conditions will vary between and beyond the borehole locations.

In general, the subsurface stratigraphy at the site consists of embankment fill (where encountered) or topsoil (where encountered) generally underlain by clayey silt to silty clay, which in turn is underlain by a silt to silt and sand deposit. A more detailed description of the subsurface conditions encountered in the boreholes is provided in the following sections.

4.2.1 Ice/Water

Borehole BI-7 was advanced from the surface of the ice near the outlet to the culvert at Elevation 200.9 m and encountered a 0.2 m thick layer of ice and 1.3 m column of water.

4.2.2 Fill

Boreholes BI-1 to BI-3 penetrated a layer of asphalt 225 mm thick at Elevation 210.4 m and 210.5 m, underlain by a fill deposit comprised of sand and gravel to sand between about 0.5 m and 2.9 m thick, underlain by clayey silt to silt fill between 6.5 m and 7.6 m thick.

The SPT ‘N’-values measured within the sand and gravel to sand fill range between 10 blows and 58 blows per 0.3 m of penetration indicating a compact to very dense relative density; and the ‘N’-values measured within the clayey silt to silt fill range between 5 blows and 24 blows per 0.3 m of penetration suggesting a firm to very stiff consistency.

¹ Southern Ontario Engineering Geology Terrain Study, 1980. Ontario Geological Survey.



Grain size analyses were carried out on two samples of the sand and gravel to gravelly sand fill and the results are presented on Figure B1 in Appendix B. Grain size analyses were carried out on two samples of the clayey silt to silt fill and the results are presented on Figure B2.

Atterberg limits tests were carried out on three samples of the cohesive fill and measured liquid limits ranging from about 21 per cent to 34 per cent, plastic limits ranging from about 17 per cent to 19 per cent, and plasticity indices ranging from about 4 per cent to 15 per cent. The results, which are plotted on a plasticity chart on Figures B3 in Appendix B, indicate that the tested samples of the overall deposit consist of clayey silt of low plasticity to silt of slight plasticity.

The natural moisture content measured on samples of the sand and gravel to sand fill is between 2 per cent and 4 per cent and samples of the clayey silt to silt fill is between 24 per cent and 32 per cent.

4.2.3 Topsoil

Borehole BI-4 encountered a 0.7 m thick layer of silty topsoil from ground surface at Elevation 201.4 m.

One SPT 'N'-value measured in the deposit is 3 blows per 0.3 m of penetration, suggesting a very loose consistency.

4.2.4 Sandy Silt to Silty Sand

Below the topsoil in Borehole BI-4 and below the water in Borehole BI-7, a deposit of sandy silt to silty sand was encountered at Elevation 200.7 m and 199.4 m, with a thickness of 1.5 m and 0.6 m, respectively.

Three SPT 'N'-values measured within this deposit are 9 blows and 10 blows per 0.3 m of penetration, indicating a loose to compact relative density.

4.2.5 Clayey Silt to Silty Clay

A deposit of clayey silt to silty clay was encountered below the fill in Boreholes BI-1 to BI-3, from ground surface in Boreholes BI-5 and BI-6 and below the sandy silt to silty sand deposit in Boreholes BI-4 and BI-7. The surface of the deposit was encountered between about Elevations 203.3 m and 198.8 m and the thickness of the deposit is between about 6.6 m and 10.5 m; Borehole BI-3 did not penetrate the deposit after exploring for 8.6 m. Silt laminations were observed within the majority of samples of this deposit. In Borehole BI-6, a 0.3 m layer of silty sand and gravel was encountered at a depth of 2.1 m below ground surface (Elevation 199.2 m).

The SPT 'N'-values measured within the clayey silt to silty clay deposit range between 2 blows and 8 blows per 0.3 m of penetration. In situ field vane testing measured undrained shear strengths ranging from 38 kPa to greater than 100 kPa, with sensitivities between 2 and 6. The in situ vane test results indicate that the deposit has a firm to very stiff consistency.

Atterberg limits tests were carried out on fourteen samples of the cohesive deposit and measured liquid limits ranging from about 21 per cent to 47 per cent, plastic limits ranging from about 14 per cent to 25 per cent and plasticity indices ranging from about 5 per cent to 24 per cent. The results, which are plotted on a plasticity chart



on Figures B4.1, indicate that the tested samples of the overall deposit consist of clayey silt of low plasticity to silty clay of intermediate plasticity.

Atterberg limits tests were also carried out on one sample of the deposit that was separated into the silt lamina and the clay lamina and the test results are shown on Figure B4.2. The test results on the clay lamina indicate a liquid limit of about 87 per cent, a plastic limit of 27 per cent and a plasticity index of 60 per cent. The silt lamina has a liquid limit of about 23 per cent, a plastic limit of 17 per cent and a plasticity index of 7 per cent. The test results confirm that the 'silty' varves are classified as a silt of slight plasticity and the 'clayey' varves are classified as a clay of high plasticity.

The results of the grain size distribution testing completed on thirteen samples of this deposit, including those on the silt and clay laminae, are shown on Figure B5.

The natural moisture content measured on selected samples of this deposit generally ranges between about 24 per cent and 50 per cent; the moisture content measured on the clay lamina from Borehole BI-5a is 72 per cent.

4.2.6 Silt to Silt and Sand

A deposit of silt to sandy silt to silt and sand, some clay, was encountered below the clayey silt to silty clay deposit in Boreholes BI-1, BI-2 and BI-4 to BI-7. The surface of this deposit was encountered between Elevations 192.6 m and 189.7 m and sampled boreholes did not fully penetrate the deposit after exploring for thicknesses of between approximately 1.1 m and 5.6 m.

The SPT 'N'-values measured within this deposit range between 2 blows and 14 blows per 0.3 m of penetration, indicating a very loose to compact relative density.

Grain size distribution analyses were carried out on nine samples of this deposit and the results are represented on Figure B6.

Atterberg limits tests were carried out on six samples of this deposit: three samples indicate that the material is non-plastic; and three samples measured liquid limits ranging from about 18 per cent to 22 per cent, plastic limits ranging from about 15 per cent to 16 per cent and plasticity indices ranging from about 3 per cent to 6 per cent. The results, which are plotted on a plasticity chart on Figures B7, indicate that the three samples consist of silt of slight plasticity. Atterberg limits testing carried out on the natural moisture content measured on selected samples of this deposit ranges between about 20 per cent and 30 per cent.

4.2.7 Groundwater Conditions

Borehole BI-3 caved at a depth of about 9.8 m below ground surface (Elevation 200.7 m) upon completion of drilling and the borehole was noted to be dry to the cave depth. The unstabilized water level in Boreholes BI-1, BI-2 and BI-4 to BI-6 upon completion of drilling was between Elevation 201.8 m and 200.5 m. The creek ice surface on the south side of the embankment at Borehole BI-7 on February 23, 2014 was Elevation 200.9 m.

Groundwater levels encountered in the boreholes shortly after drilling may not be representative of static groundwater levels since the groundwater levels in the boreholes may not have stabilized on completion of



drilling. Groundwater levels are subject to seasonal fluctuations and to fluctuations after precipitation events and snowmelt.

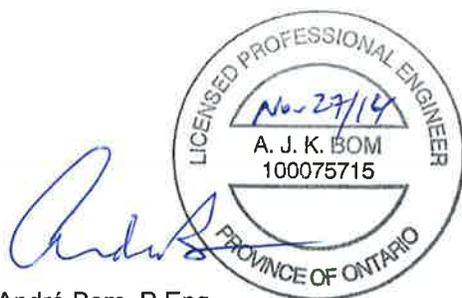
5.0 CLOSURE

The drilling program was supervised by Mr. Shane Albert and Mr. Mat Riopelle. This report was prepared by Mr. André Bom, P.Eng. Mr. Jorge M. A. Costa, P.Eng., Golder's Designated MTO Contact for this project and Principal with Golder, conducted an independent quality control review of the report



Report Signature Page

GOLDER ASSOCIATES LTD.



André Bom, P.Eng
Geotechnical Engineer

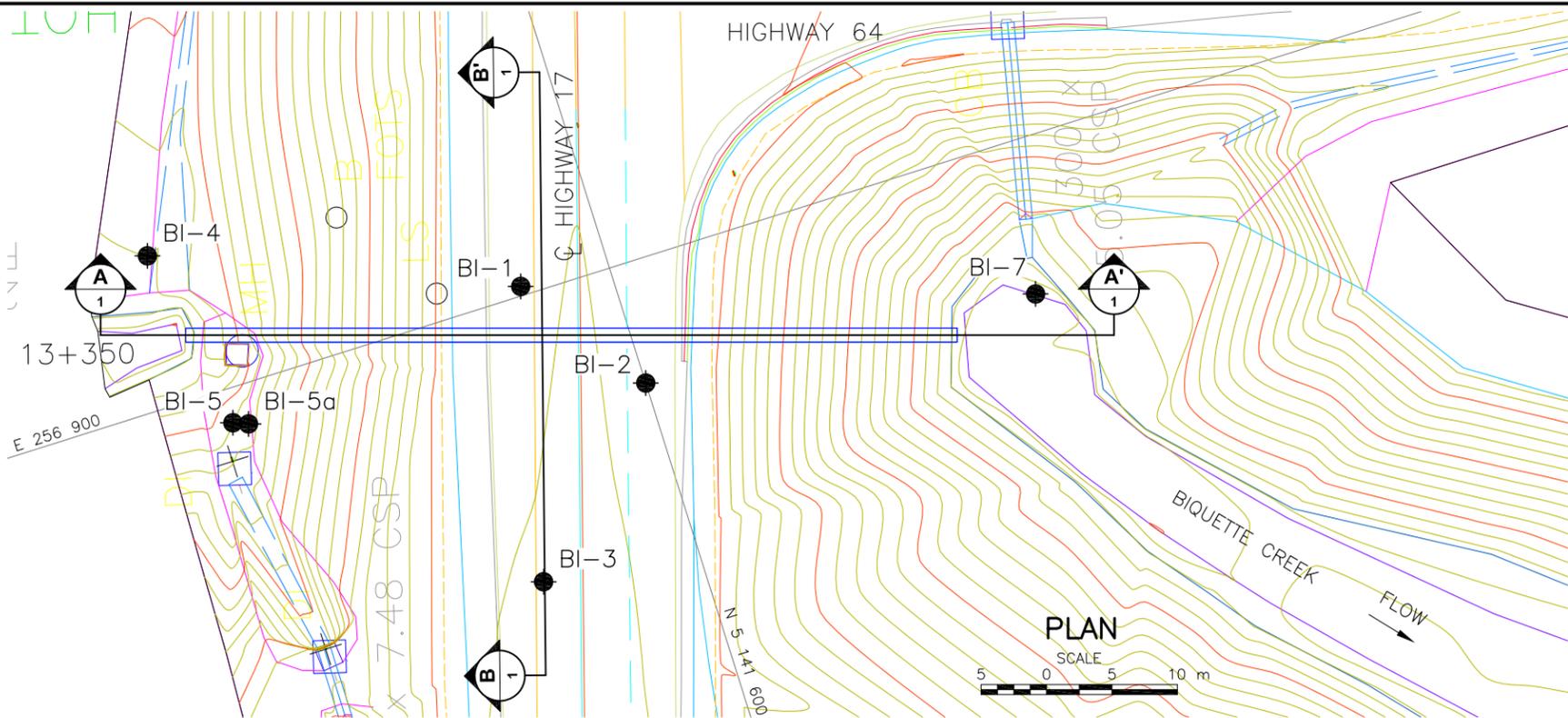


Jorge M.A. Costa, P.Eng
Designated MTO Contact, Principal

AB/JMAC/kp

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final fdr biquette creek.docx



METRIC
DIMENSIONS ARE IN METRES AND/OR MILLIMETRES UNLESS OTHERWISE SHOWN. STATIONS IN KILOMETRES + METRES.

CONT No. GWP No. 300-98-00



HIGHWAY 17
BIQUETTE CREEK CULVERT - STA 13+350
BOREHOLE LOCATIONS AND SOIL STRATA

SHEET



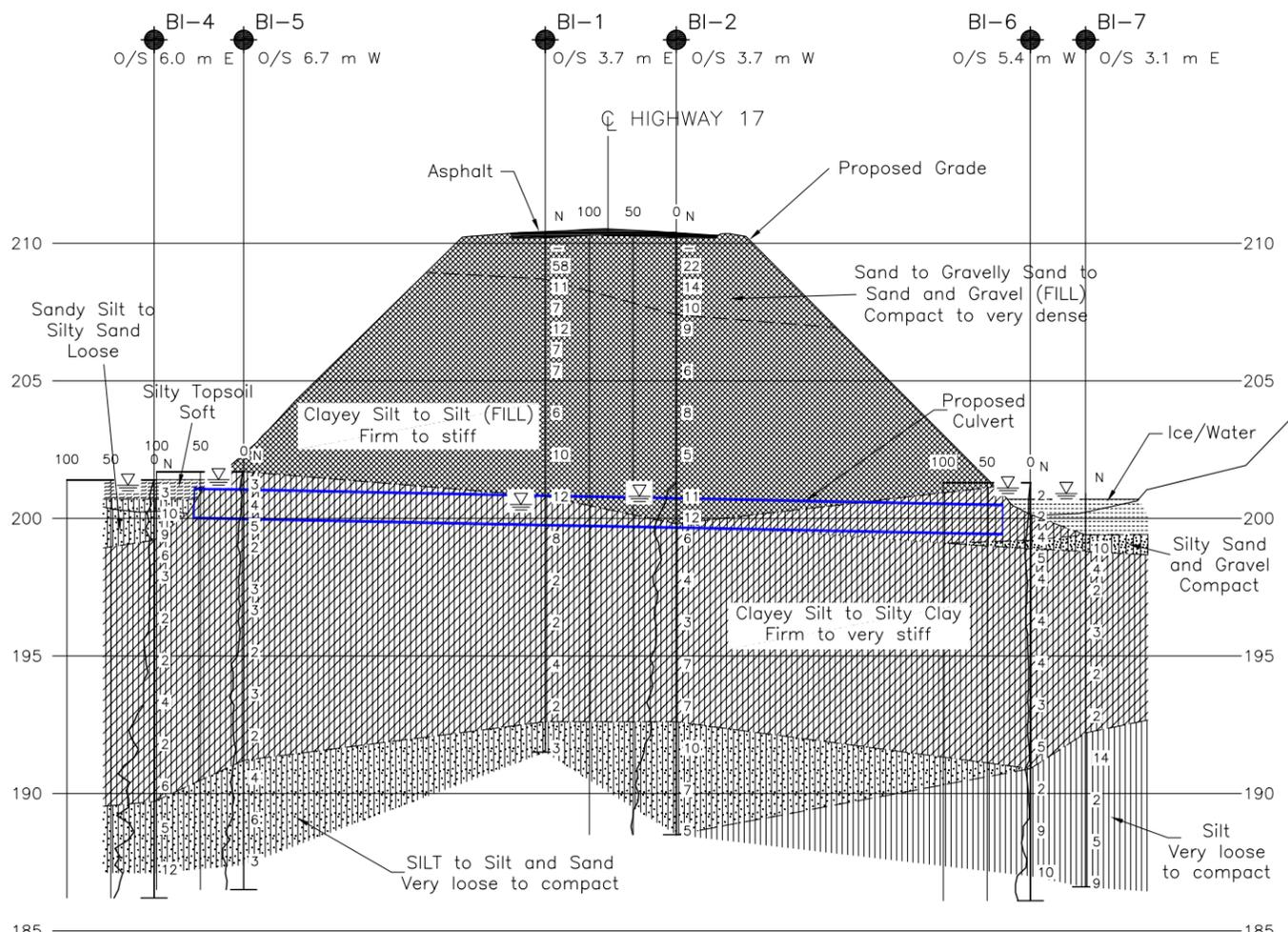
Golder Associates Ltd.
SUDBURY, ONTARIO, CANADA



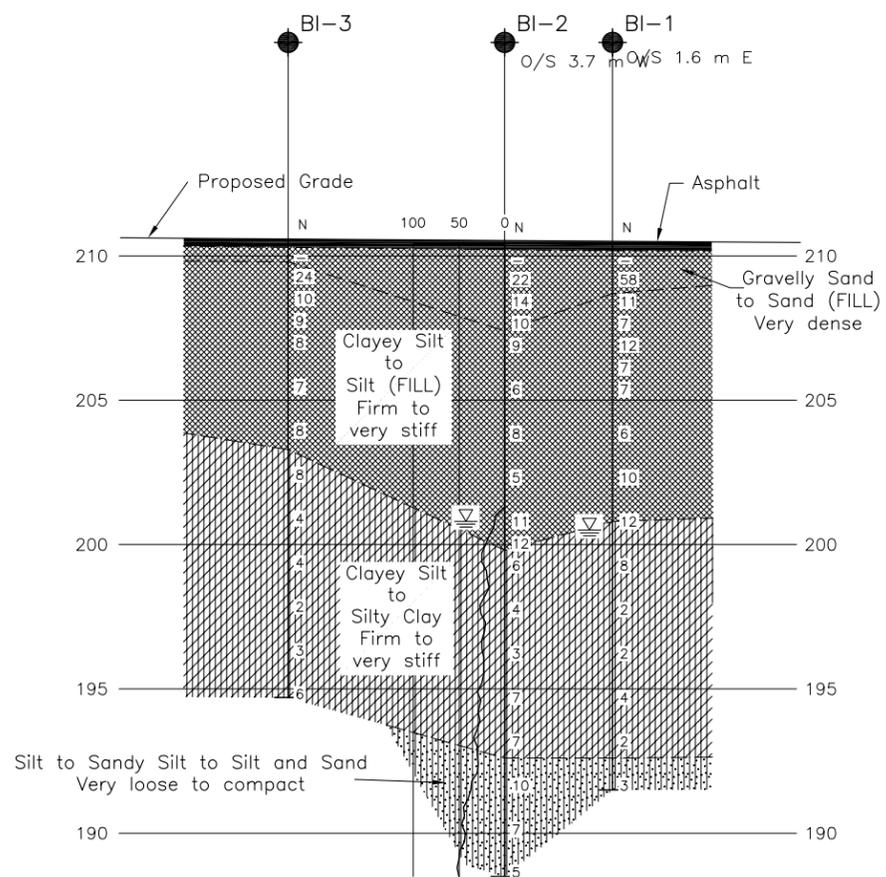
KEY PLAN
SCALE 8 0 8 km

LEGEND

- Borehole - Current Investigation
- N Standard Penetration Test Value
- 16 Blows/0.3m unless otherwise stated (Std. Pen. Test, 475 j/blow)
- ∇ WL upon completion of drilling



A-A'
1
CULVERT PROFILE
HIGHWAY 17
HORIZONTAL SCALE 5 0 5 10 m
VERTICAL SCALE 2.5 0 2.5 5 m



B-B'
1
CROSS-SECTION
HIGHWAY 17
HORIZONTAL SCALE 5 0 5 10 m
VERTICAL SCALE 2.5 0 2.5 5 m

BOREHOLE CO-ORDINATES

No.	ELEVATION	NORTHING	EASTING
BI-1	210.4	5141606.9	256900.7
BI-2	210.4	5141600.0	256890.8
BI-3	210.5	5141612.0	256878.7
BI-4	201.4	5141633.4	256911.5
BI-5	201.7	5141631.0	256897.4
BI-5a	201.7	5141629.9	256897.0
BI-7	200.9	5141569.5	256888.3

NOTES

This drawing is for subsurface information only. The proposed structure details/works are shown for illustration purposes only and may not be consistent with the final design configuration as shown elsewhere in the Contracts Documents.

The boundaries between soil strata have been established only at borehole locations. Between boreholes the boundaries are assumed from geological evidence.

The complete Foundation Investigation and Design Report for this project and other related documents may be examined at the Materials Engineering and Research Office, Downsview. Information contained in this report and related documents is specifically excluded in accordance with Section GC 2.01 of OPS General Conditions.

REFERENCE

Base plans provided in digital format by Morrison Hershfield, drawing file no. wp3009800a.dwg, received APR 7, 2014 and Biquette Creek Culvert and 11+600 culvert.dwg received on NOV 05, 2014.



NO.	DATE	BY	REVISION

Geocres No. 411-316

HWY. 17	PROJECT NO. 13-1184-0074	DIST.
SUBM'D. MT	CHKD.	DATE: NOV 2014
DRAWN: TB	CHKD. AB	APPD. JMAC
		SITE: 43-165/C
		DWG. 1



APPENDIX A

Record of Boreholes



LIST OF SYMBOLS

Unless otherwise stated, the symbols employed in the report are as follows:

I.	GENERAL	(a)	Index Properties (continued)
π	3.1416	w	water content
$\ln x$,	natural logarithm of x	w_l or LL	liquid limit
\log_{10}	x or log x, logarithm of x to base 10	w_p or PL	plastic limit
g	acceleration due to gravity	I_p or PI	plasticity index = $(w_l - w_p)$
t	time	w_s	shrinkage limit
FoS	factor of safety	I_L	liquidity index = $(w - w_p) / I_p$
		I_C	consistency index = $(w_l - w) / I_p$
		e_{max}	void ratio in loosest state
		e_{min}	void ratio in densest state
		I_D	density index = $(e_{max} - e) / (e_{max} - e_{min})$ (formerly relative density)
II.	STRESS AND STRAIN	(b)	Hydraulic Properties
γ	shear strain	h	hydraulic head or potential
Δ	change in, e.g. in stress: $\Delta \sigma$	q	rate of flow
ε	linear strain	v	velocity of flow
ε_v	volumetric strain	i	hydraulic gradient
η	coefficient of viscosity	k	hydraulic conductivity (coefficient of permeability)
ν	Poisson's ratio	j	seepage force per unit volume
σ	total stress	(c)	Consolidation (one-dimensional)
σ'	effective stress ($\sigma' = \sigma - u$)	C_c	compression index (normally consolidated range)
σ'_{vo}	initial effective overburden stress	C_r	recompression index (over-consolidated range)
$\sigma_1, \sigma_2, \sigma_3$	principal stress (major, intermediate, minor)	C_s	swelling index
σ_{oct}	mean stress or octahedral stress = $(\sigma_1 + \sigma_2 + \sigma_3)/3$	C_α	secondary compression index
τ	shear stress	m_v	coefficient of volume change
u	porewater pressure	C_v	coefficient of consolidation (vertical direction)
E	modulus of deformation	C_h	coefficient of consolidation (horizontal direction)
G	shear modulus of deformation	T_v	time factor (vertical direction)
K	bulk modulus of compressibility	U	degree of consolidation
		σ'_p	pre-consolidation stress
III.	SOIL PROPERTIES	OCR	over-consolidation ratio = σ'_p / σ'_{vo}
(a)	Index Properties	(d)	Shear Strength
$\rho(\gamma)$	bulk density (bulk unit weight)*	τ_p, τ_r	peak and residual shear strength
$\rho_d(\gamma_d)$	dry density (dry unit weight)	ϕ'	effective angle of internal friction
$\rho_w(\gamma_w)$	density (unit weight) of water	δ	angle of interface friction
$\rho_s(\gamma_s)$	density (unit weight) of solid particles	μ	coefficient of friction = $\tan \delta$
γ'	unit weight of submerged soil ($\gamma' = \gamma - \gamma_w$)	c'	effective cohesion
D_R	relative density (specific gravity) of solid particles ($D_R = \rho_s / \rho_w$) (formerly G_s)	C_u, S_u	undrained shear strength ($\phi = 0$ analysis)
e	void ratio	p	mean total stress $(\sigma_1 + \sigma_3)/2$
n	porosity	p'	mean effective stress $(\sigma'_1 + \sigma'_3)/2$
S	degree of saturation	q	$(\sigma_1 - \sigma_3)/2$ or $(\sigma'_1 - \sigma'_3)/2$
		q_u	compressive strength $(\sigma_1 - \sigma_3)$
		S_t	sensitivity

* Density symbol is ρ . Unit weight symbol is γ where $\gamma = \rho g$ (i.e. mass density multiplied by acceleration due to gravity)

Notes: 1
2

$\tau = c' + \sigma' \tan \phi'$
shear strength = (compressive strength)/2



LIST OF ABBREVIATIONS

The abbreviations commonly employed on Records of Boreholes, on figures and in the text of the report are as follows:

I. SAMPLE TYPE

AS	Auger sample
BS	Block sample
CS	Chunk sample
DS	Denison type sample
FS	Foil sample
RC	Rock core
SC	Soil core
SS	Split-spoon
ST	Slotted tube
TO	Thin-walled, open
TP	Thin-walled, piston
WS	Wash sample

II. PENETRATION RESISTANCE

Standard Penetration Resistance (SPT), N:

The number of blows by a 63.5 kg. (140 lb.) hammer dropped 760 mm (30 in.) required to drive a 50 mm (2 in.) drive open sampler for a distance of 300 mm (12 in.)

Dynamic Cone Penetration Resistance; N_d :

The number of blows by a 63.5 kg (140 lb.) hammer dropped 760 mm (30 in.) to drive uncased a 50 mm (2 in.) diameter, 60° cone attached to "A" size drill rods for a distance of 300 mm (12 in.).

PH: Sampler advanced by hydraulic pressure

PM: Sampler advanced by manual pressure

WH: Sampler advanced by static weight of hammer

WR: Sampler advanced by weight of sampler and rod

Piezo-Cone Penetration Test (CPT)

A electronic cone penetrometer with a 60° conical tip and a project end area of 10 cm² pushed through ground at a penetration rate of 2 cm/s. Measurements of tip resistance (Q_t), porewater pressure (PWP) and friction along a sleeve are recorded electronically at 25 mm penetration intervals.

III. SOIL DESCRIPTION

(a) Non-Cohesive (Cohesionless) Soils

Density Index	N
Relative Density	Blows/300 mm or Blows/ft
Very loose	0 to 4
Loose	4 to 10
Compact	10 to 30
Dense	30 to 50
Very dense	over 50

(b) Cohesive Soils Consistency

	kPa	C_u, S_u	psf
Very soft	0 to 12		0 to 250
Soft	12 to 25		250 to 500
Firm	25 to 50		500 to 1,000
Stiff	50 to 100		1,000 to 2,000
Very stiff	100 to 200		2,000 to 4,000
Hard	over 200		over 4,000

IV. SOIL TESTS

w	water content
w _p	plastic limit
w _l	liquid limit
C	consolidation (oedometer) test
CHEM	chemical analysis (refer to text)
CID	consolidated isotropically drained triaxial test ¹
CIU	consolidated isotropically undrained triaxial test with porewater pressure measurement ¹
D _R	relative density (specific gravity, G _s)
DS	direct shear test
M	sieve analysis for particle size
MH	combined sieve and hydrometer (H) analysis
MPC	Modified Proctor compaction test
SPC	Standard Proctor compaction test
OC	organic content test
SO ₄	concentration of water-soluble sulphates
UC	unconfined compression test
UU	unconsolidated undrained triaxial test
V	field vane (LV-laboratory vane test)
γ	unit weight

Note: 1 Tests which are anisotropically consolidated prior to shear are shown as CAD, CAU.

V. MINOR SOIL CONSTITUENTS

Per cent by Weight	Modifier	Example
0 to 5	Trace	Trace sand
5 to 12	Trace to Some (or Little)	Trace to some sand
12 to 20	Some	Some sand
20 to 30	(ey) or (y)	Sandy
over 30	And (non-cohesive (cohesionless)) or With (cohesive)	Sand and Gravel Silty Clay with sand / Clayey Silt with sand

PROJECT 13-1184-0074 **RECORD OF BOREHOLE No BI-1** 1 OF 2 **METRIC**
 G.W.P. 300-98-00 LOCATION N 5141606.9; E 256900.7 ORIGINATED BY SA
 DIST HWY 17 BOREHOLE TYPE 108 mm I.D. Continuous Flight Hollow Stem Augers COMPILED BY MT
 DATUM GEODETIC DATE November 27, 2013 CHECKED BY AB

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)						
ELEV. DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20						40	60	80	100	20	40
210.4	GROUND SURFACE																		
0.0	ASPHALT (225 mm)																		
0.2	Gravelly sand to sand, trace silt (FILL) Very dense Brown Moist	[Cross-hatched pattern]	1	AS	-														
			2	SS	58														
208.7	Clayey silt to silt, occasional organic pockets (FILL) Firm to stiff Brown to grey Moist	[Cross-hatched pattern]	3a	SS	11														
1.7			3b																
			4	SS	7														
			5	SS	12														
			6	SS	7														
			7	SS	7														
			8	SS	6														
			9	SS	10														
200.8	CLAYEY SILT to SILTY CLAY, silt laminations Firm to stiff Grey Wet	[Diagonal hatched pattern]	10	SS	12														
9.6			11	SS	8														
			12	SS	2														
			13	SS	2														

SUD-MTO 001 13-1184-0074.GPJ GAL-MISS.GDT 19/11/14 DATA INPUT:

Continued Next Page

 +³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE



PROJECT 13-1184-0074 **RECORD OF BOREHOLE No BI-1** 2 OF 2 **METRIC**
 G.W.P. 300-98-00 LOCATION N 5141606.9; E 256900.7 ORIGINATED BY SA
 DIST HWY 17 BOREHOLE TYPE 108 mm I.D. Continuous Flight Hollow Stem Augers COMPILED BY MT
 DATUM GEODETIC DATE November 27, 2013 CHECKED BY AB

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)		
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20	40	60	80						100	20
192.6	CLAYEY SILT to SILTY CLAY, silt laminations Firm to stiff Grey Wet		14	SS	4													
192.6																		
192.6			15	SS	2													
192.6																		
17.8	SILT and SAND, some clay Very loose Grey Wet		16	SS	3													
191.5																		
18.9	END OF BOREHOLE Note: 1. Water level at a depth of 9.9 m below ground surface (Elev. 200.5 m) upon completion of drilling.																	

SUD-MTO 001 13-1184-0074.GPJ GAL-MISS.GDT 19/11/14 DATA INPUT:

+³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE



PROJECT 13-1184-0074 **RECORD OF BOREHOLE No BI-2** 2 OF 2 **METRIC**
 G.W.P. 300-98-00 LOCATION N 5141600.0; E 256890.8 ORIGINATED BY SA
 DIST HWY 17 BOREHOLE TYPE 108 mm I.D. Continuous Flight Hollow Stem Augers COMPILED BY MT
 DATUM GEODETIC DATE November 28 and 29, 2013 CHECKED BY AB

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)				
ELEV. DEPTH	DESCRIPTION	STRAT. PLOT	NUMBER	TYPE			"N" VALUES	20						40	60	80	100
192.6	CLAYEY SILT, trace to some sand, silt laminations Stiff to very stiff Grey Wet		14	SS	7								1 10 64 25				
17.8	SILT to SAND, trace to some clay Loose to compact Grey Wet		15	SS	7												
17.8			16	SS	10								0 60 32 8				
			17	SS	7												
188.5			18	SS	5								0 5 79 16				
21.9	END OF BOREHOLE Note: 1. Water level at a depth of 9.6 m below ground surface (Elev. 200.8 m) upon completion of drilling. 2. Pre-drilled hole to 9.2 m depth immediately adjacent to Borehole BI-2 and advanced DCPT from 9.2 m to 21.9 m.																

SUD-MTO 001 13-1184-0074.GPJ GAL-MISS.GDT 19/11/14 DATA INPUT:

+³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

RECORD OF BOREHOLE No BI-3 1 OF 2 **METRIC**

PROJECT 13-1184-0074 G.W.P. 300-98-00 LOCATION N 5141612.0; E 256878.7 ORIGINATED BY SA

DIST HWY 17 BOREHOLE TYPE 108 mm I.D. Continuous Flight Hollow Stem Augers COMPILED BY MT

DATUM GEODETIC DATE December 3, 2013 CHECKED BY AB

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)					
ELEV. DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20						40	60	80	100	20
210.5	GROUND SURFACE																	
0.0	ASPHALT (225 mm)																	
0.2	Gravelly sand, some silt (FILL)		1	AS	-									23	59		(18)	
209.8	Brown Moist																	
0.7	Clayey silt to silt, trace sand (FILL)		2	SS	24													
	Firm to very stiff																	
	Grey Moist		3	SS	10													
			4	SS	9													
			5	SS	8													
			6	SS	7													
			7	SS	8													
203.3	CLAYEY SILT, some sand, silt laminations		8	SS	8													
7.2	Stiff to very stiff																	
	Grey Wet		9	SS	4									0	5	80	15	
			10	SS	4									0	6	73	21	
			11	SS	2													
			12	SS	3													

SUD-MTO 001 13-1184-0074.GPJ GAL-MISS.GDT 19/11/14 DATA INPUT:

Continued Next Page

+³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

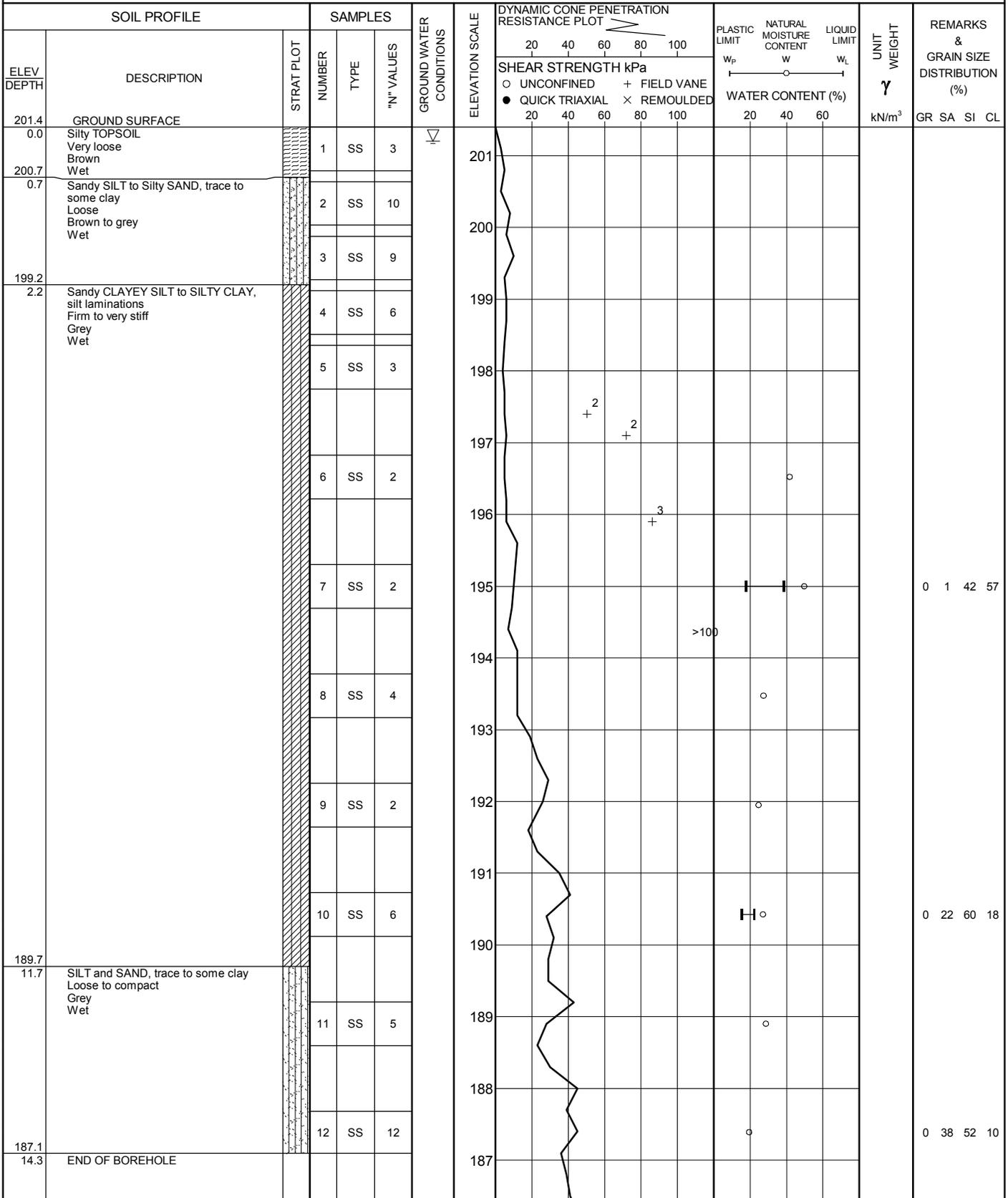
PROJECT <u>13-1184-0074</u>	RECORD OF BOREHOLE No BI-3	2 OF 2 METRIC
G.W.P. <u>300-98-00</u>	LOCATION <u>N 5141612.0; E 256878.7</u>	ORIGINATED BY <u>SA</u>
DIST <u> </u> HWY <u>17</u>	BOREHOLE TYPE <u>108 mm I.D. Continuous Flight Hollow Stem Augers</u>	COMPILED BY <u>MT</u>
DATUM <u>GEODETIC</u>	DATE <u>December 3, 2013</u>	CHECKED BY <u>AB</u>

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20	40	60	80					
	-- CONTINUED FROM PREVIOUS PAGE --															
194.7 15.8	END OF BOREHOLE Note: 1. Borehole caved at 9.8 m (Elev. 200.7 m) upon completion of drilling. Borehole dry to 9.8 m depth.		13	SS	6							○				

SUD-MTO 001 13-1184-0074.GPJ GAL-MISS.GDT 19/11/14 DATA INPUT:

+³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

PROJECT 13-1184-0074 **RECORD OF BOREHOLE No BI-4** 1 OF 2 **METRIC**
 G.W.P. 300-98-00 LOCATION N 5141633.4; E 256911.5 ORIGINATED BY MR
 DIST HWY 17 BOREHOLE TYPE NW Casing, Wash Boring COMPILED BY MT
 DATUM GEODETIC DATE February 20, 2014 CHECKED BY AB



SUD-MTO 001 13-1184-0074.GPJ GAL-MISS.GDT 19/11/14 DATA INPUT:

Continued Next Page

+ 3, × 3: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE



PROJECT 13-1184-0074 **RECORD OF BOREHOLE No BI-4** 2 OF 2 **METRIC**
 G.W.P. 300-98-00 LOCATION N 5141633.4; E 256911.5 ORIGINATED BY MR
 DIST HWY 17 BOREHOLE TYPE NW Casing, Wash Boring COMPILED BY MT
 DATUM GEODETIC DATE February 20, 2014 CHECKED BY AB

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)		
ELEV. DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20	40	60	80						100	20
186.2																		
15.2	END OF DCPT Note: 1. Water level at a depth of 0.2 m below ground surface (Elev. 201.2 m) upon completion of drilling. 2. DCPT advanced 0.5 m south of Borehole BI-4.																	

SUD-MTO 001 13-1184-0074.GPJ GAL-MISS.GDT 19/11/14 DATA INPUT:

+³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

RECORD OF BOREHOLE No BI-5 1 OF 2 **METRIC**

PROJECT 13-1184-0074 G.W.P. 300-98-00 LOCATION N 5141631.0; E 256897.4 ORIGINATED BY MR

DIST HWY 17 BOREHOLE TYPE NW Casing, Wash Boring COMPILED BY MT

DATUM GEODETIC DATE February 12 and 13, 2014 CHECKED BY AB

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)				
ELEV DEPTH	DESCRIPTION	NUMBER	TYPE	"N" VALUES			20	40						60	80	100	20
201.7	GROUND SURFACE																
0.0	CLAYEY SILT to SILTY CLAY Firm to very stiff Grey to brown Wet	1	SS	3	▽												
		2	SS	4		201								0	5	71	24
		3	SS	5		200											
	Silt laminations below 2.3 m depth.	4	SS	2		199											
		5	SS	3		198		2									
		6	SS	3		197											
		7	SS	2		196		4									
		8	SS	3		195								0	2	50	48
		9	SS	2		194											
		10	SS	4		193											
		11	SS	6		192											
		12	SS	3		191											
191.2	SILT to SILT and SAND, some clay Very loose to loose Grey Wet					190											
10.5						189								0	13	72	15
187.4	END OF BOREHOLE					188											
14.3						187											

SUD-MTO 001 13-1184-0074.GPJ GAL-MISS.GDT 19/11/14 DATA INPUT:

Continued Next Page

+ 3, × 3: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE



PROJECT 13-1184-0074 **RECORD OF BOREHOLE No BI-5** 2 OF 2 **METRIC**
 G.W.P. 300-98-00 LOCATION N 5141631.0; E 256897.4 ORIGINATED BY MR
 DIST HWY 17 BOREHOLE TYPE NW Casing, Wash Boring COMPILED BY MT
 DATUM GEODETIC DATE February 12 and 13, 2014 CHECKED BY AB

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)		
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20	40	60	80						100	20
186.5																		
15.2	END OF DCPT Note: 1. Water level at a depth of 0.3 m below ground surface (Elev. 201.4 m) upon completion of drilling. 2. DCPT advanced 0.4 m south of Borehole BI-5.																	

SUD-MTO 001 13-1184-0074.GPJ GAL-MISS.GDT 19/11/14 DATA INPUT:

+³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE



RECORD OF BOREHOLE No BI-5a 1 OF 1 **METRIC**

PROJECT 13-1184-0074 G.W.P. 300-98-00 LOCATION N 5141629.9; E 256897.0 ORIGINATED BY MR

DIST HWY 17 BOREHOLE TYPE NW Casing, Wash Boring COMPILED BY MT

DATUM GEODETIC DATE February 12 and 13, 2014 CHECKED BY AB

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)			
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20	40	60	80						100	20	40
201.7	GROUND SURFACE																		
0.0	CLAYEY SILT to SILTY CLAY Firm to very stiff Grey to brown Wet																		
	Silt laminations about 2 mm to 5 mm thick, spaced 5 mm to 20 mm apart in Samples 1 and 2.		1	TO	PH											0	3	63	34
			2 (s) 2 (c)	TO	PH											0	2	70	28
																0	0	15	85
	No recovery in Sample 3.		3	TO	PH														
	No recovery in Sample 4.		4	TO	PH														
193.5	END OF BOREHOLE																		
8.2	Note: 1. Borehole advanced 1.2 m south of Borehole BI-5.																		

SUD-MTO 001 13-1184-0074.GPJ GAL-MISS.GDT 19/11/14 DATA INPUT:

+³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE

PROJECT 13-1184-0074 **RECORD OF BOREHOLE No BI-6** **1 OF 2 METRIC**
G.W.P. 300-98-00 **LOCATION** N 5141575.9; E 256881.4 **ORIGINATED BY** MR
DIST HWY 17 **BOREHOLE TYPE** NW Casing, Wash Boring **COMPILED BY** MT
DATUM GEODETIC **DATE** February 24, 2014 **CHECKED BY** AB

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT		PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)
ELEV. DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	SHEAR STRENGTH kPa					
201.3	GROUND SURFACE												
0.0	Sandy SILTY CLAY, trace organics Soft Grey Wet		1	SS	2								
			2	SS	2							OC=3.5%	0 22 62 16
			3	SS	4								
199.2													
198.9	Silty SAND and GRAVEL Grey Wet		4	SS	5								
2.4	SILTY CLAY, trace sand, silt laminations Firm to very stiff Grey Wet		5	SS	4								
			6	SS	4								
			7	SS	4								0 2 57 41
			8	SS	3								
			9	SS	5								
			10	SS	2								
190.9	SILT, some clay, some sand Very loose to compact Grey Wet		11	SS	9								0 13 72 15
10.4	Silty clay laminations encountered below 10.4 m depth.		12	SS	10								
187.0	END OF BOREHOLE												
14.3													

SUD-MTO 001 13-1184-0074.GPJ GAL-MISS.GDT 19/11/14. DATA INPUT:

Continued Next Page

+ 3, × 3: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE



PROJECT 13-1184-0074 **RECORD OF BOREHOLE No BI-6** 2 OF 2 **METRIC**
 G.W.P. 300-98-00 LOCATION N 5141575.9; E 256881.4 ORIGINATED BY MR
 DIST HWY 17 BOREHOLE TYPE NW Casing, Wash Boring COMPILED BY MT
 DATUM GEODETIC DATE February 24, 2014 CHECKED BY AB

SOIL PROFILE		SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT W _p	NATURAL MOISTURE CONTENT W	LIQUID LIMIT W _L	UNIT WEIGHT γ	REMARKS & GRAIN SIZE DISTRIBUTION (%)		
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE			"N" VALUES	20	40	60	80						100	20
186.1																		
15.2	END OF DCPT Note: 1. Water level at 0.2 m below ground surface (Elev. 201.1 m) upon completion of drilling. 2. DCPT advanced 0.3 m west of Borehole BI-5.																	

SUD-MTO 001 13-1184-0074.GPJ GAL-MISS.GDT 19/11/14 DATA INPUT:

+³, ×³: Numbers refer to Sensitivity ○ 3% STRAIN AT FAILURE



APPENDIX B

Laboratory Test Results



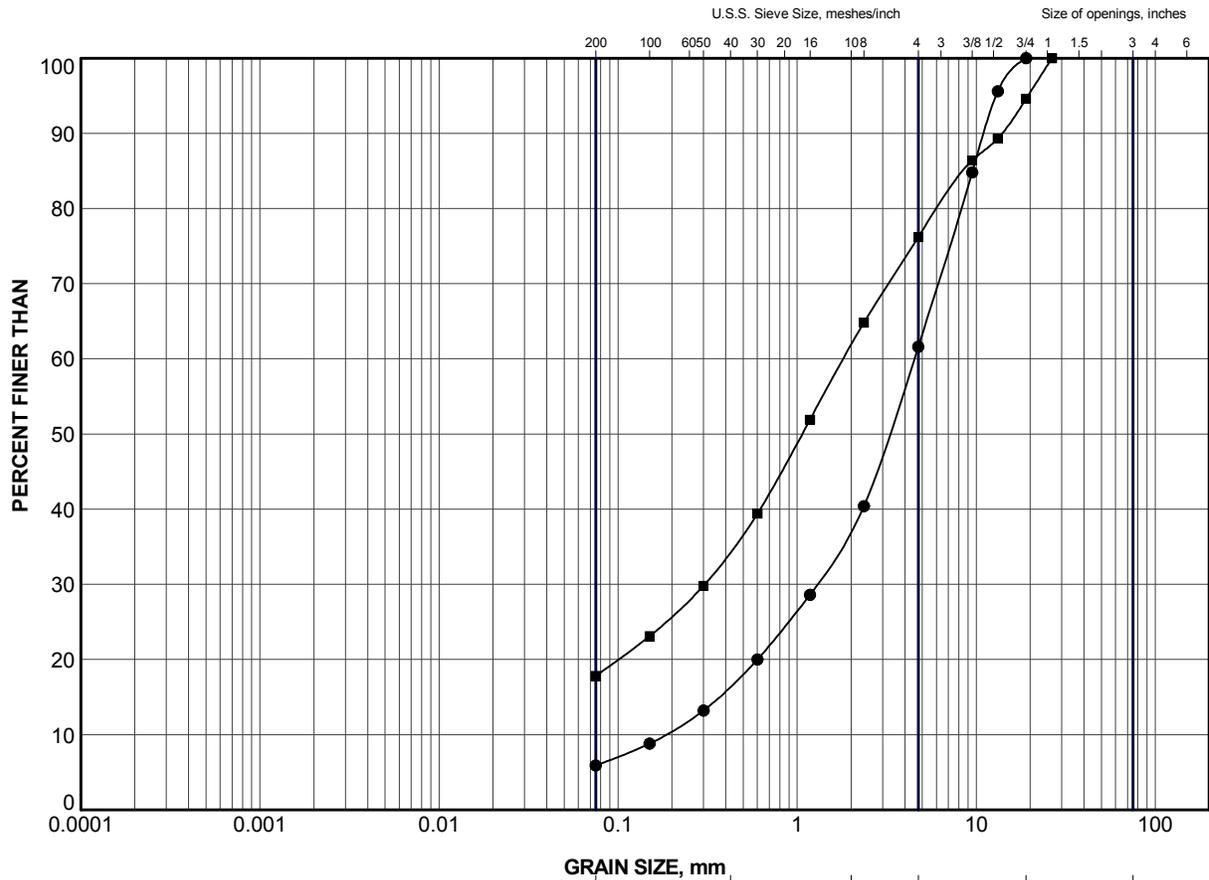
FOUNDATION INVESTIGATION AND DESIGN REPORT HIGHWAY 17 BIQUETTE CREEK CULVERT

Table B1 - Summary of Analytical Testing of Biquette Creek Water Sample

Parameter	Units	Reportable Detection Limit	Result
Dissolved Chloride	mg/L	1	5
Dissolved Sulphate	mg/L	1	Not Detected
Conductivity	$\mu\text{ohm/cm}$	1	71
Resistivity	ohm-cm	n/a	14,000
pH	n/a	n/a	6.97

- Notes: 1. Sample obtained on March 10, 2014.
2. Analytical testing carried out by Maxxam Analytics.

Checked by: AB



CLAY AND SILT	fine	medium	coarse	fine	coarse	Cobble Size
	SAND SIZE			GRAVEL SIZE		

LEGEND

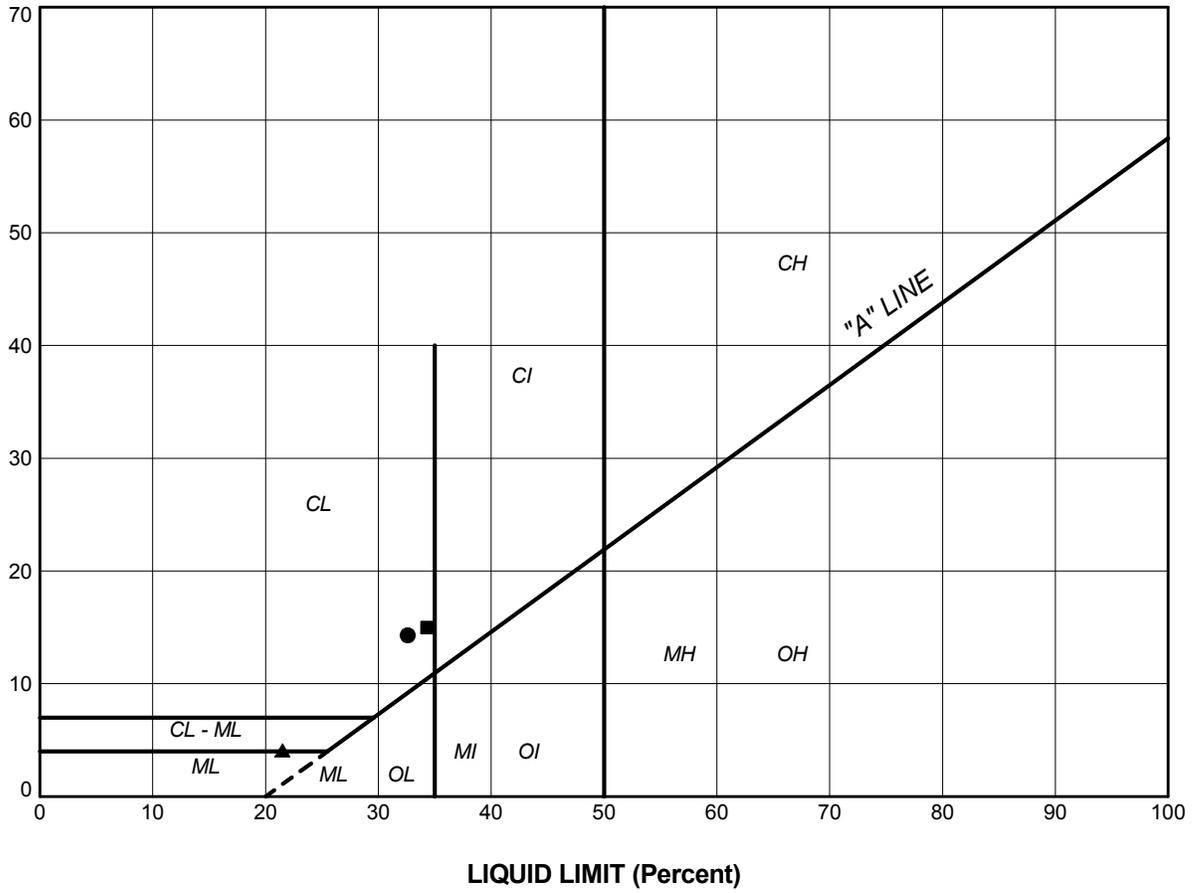
SYMBOL	BOREHOLE	SAMPLE	ELEV (m)
●	BI-2	3	208.6
■	BI-3	1	210.1

PROJECT HIGHWAY 17 BIQUETTE CREEK CULVERT - STA 13+350				
TITLE GRAIN SIZE DISTRIBUTION SAND and GRAVEL to GRAVELLY SAND (FILL)				
PROJECT No. 13-1184-0074		FILE No. 13-1184-0074.GPJ		
DRAWN	TB	Jun 2014	SCALE	N/A
CHECK	AB	Jun 2014	REV.	
APPR	JMAC	Jun 2014	FIGURE B1	



SUD-MTO GSD (NEW) GLDR_LDN.GDT

PLASTICITY INDEX (Percent)



SOIL TYPE
 C = Clay
 M = Silt
 O = Organic

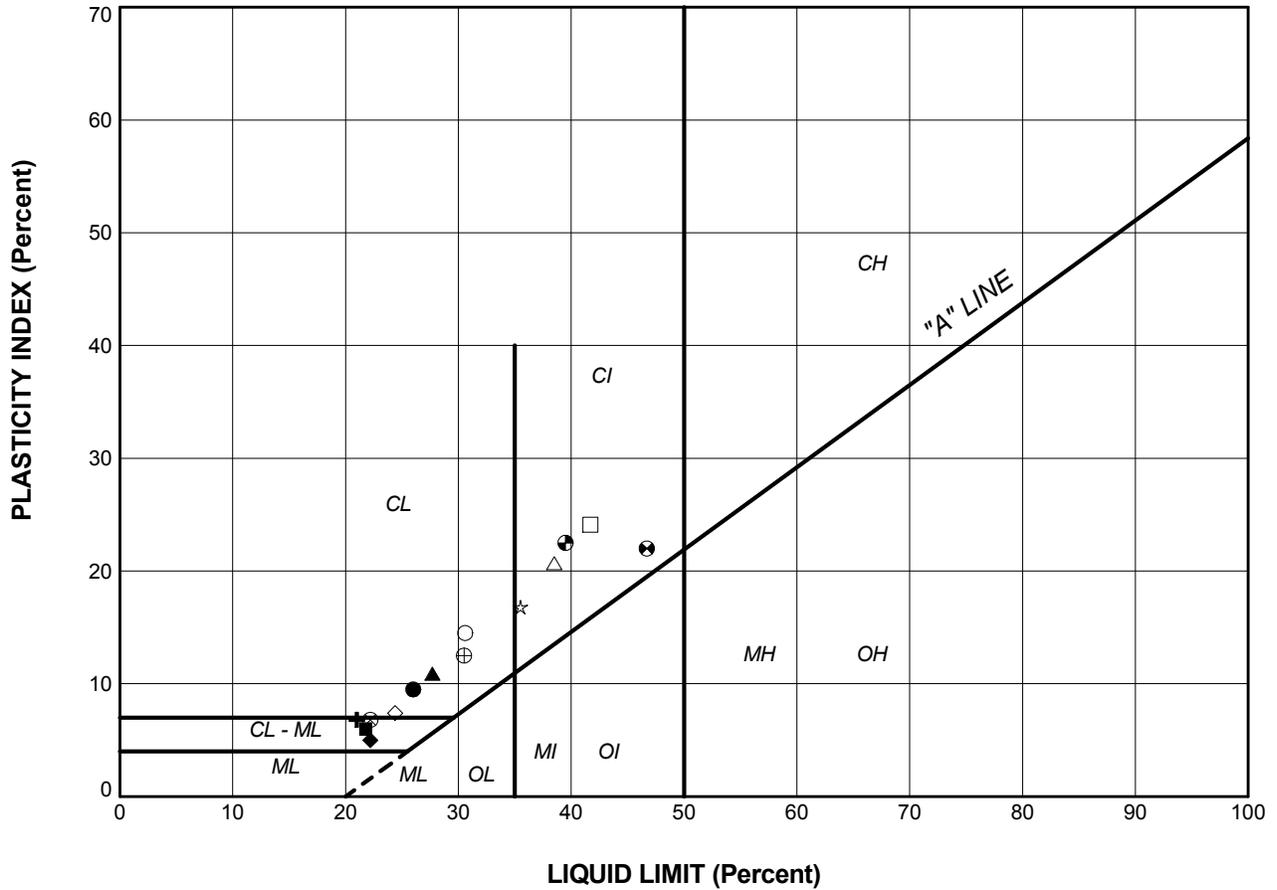
PLASTICITY
 L = Low
 I = Intermediate
 H = High

LEGEND

SYMBOL	BOREHOLE	SAMPLE	LL(%)	PL(%)	PI
●	BI-1	4	32.6	18.3	14.3
■	BI-2	8	34.3	19.3	15.0
▲	BI-3	6	21.5	17.4	4.1

PROJECT					HIGHWAY 17 BIQUETTE CREEK CULVERT - STA 13+350				
TITLE					PLASTICITY CHART SILT to CLAYEY SILT (FILL)				
PROJECT No.		13-1184-0074		FILE No.		13-1184-0074.GPJ			
DRAWN	TB	Jun 2014		SCALE	N/A	REV.			
CHECK	AB	Jun 2014		FIGURE B3					
APPR	JMAC	Jun 2014							





SOIL TYPE
 C = Clay
 M = Silt
 O = Organic

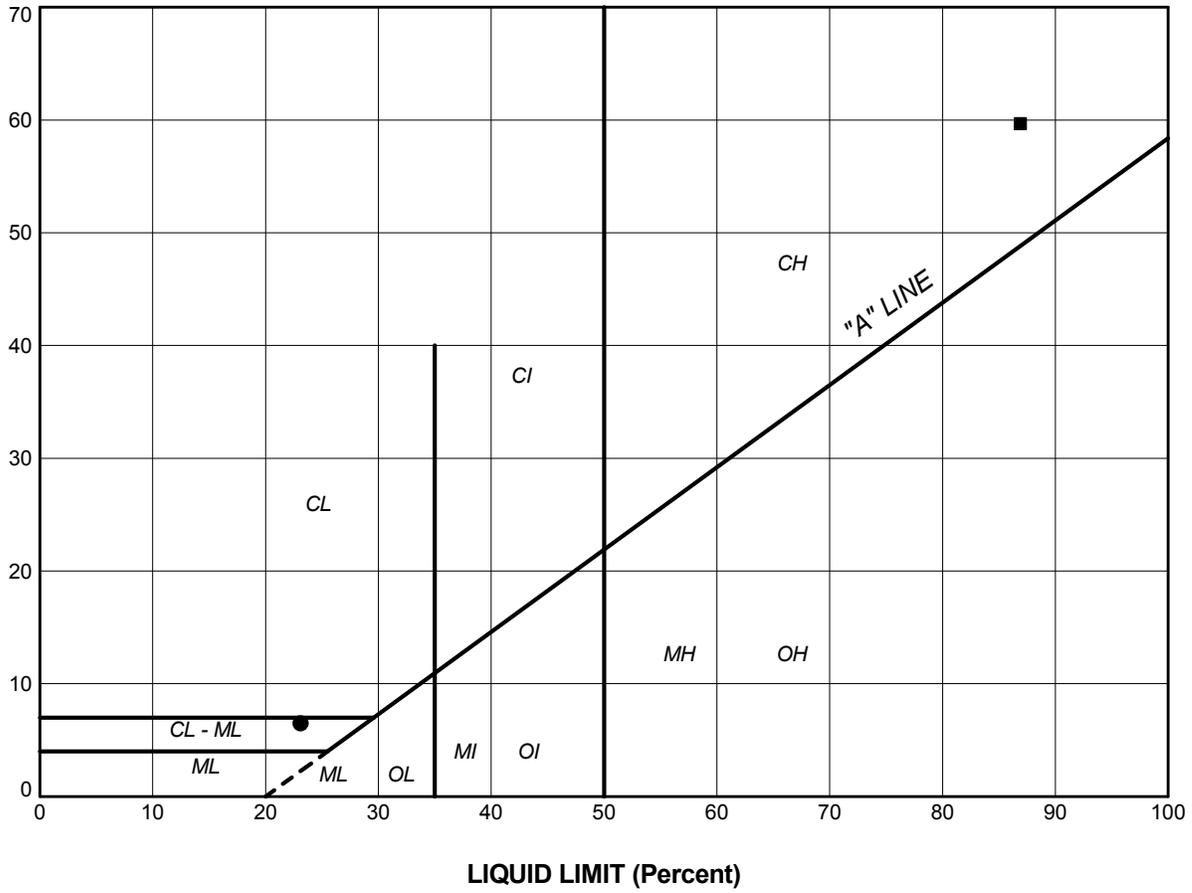
PLASTICITY
 L = Low
 I = Intermediate
 H = High

LEGEND

SYMBOL	BOREHOLE	SAMPLE	LL(%)	PL(%)	PI
●	BI-1	12	26.0	16.5	9.5
■	BI-2	11	21.8	15.8	6.0
▲	BI-2	13	27.7	16.8	10.9
+	BI-2	14	21.0	14.2	6.8
◆	BI-3	9	22.2	17.2	5.0
◇	BI-3	10	24.4	17.0	7.4
○	BI-3	12	30.6	16.1	14.5
△	BI-4	7	38.5	17.8	20.7
⊗	BI-4	10	22.2	15.4	6.8
⊕	BI-5	2	30.5	18.0	12.5
□	BI-5	7	41.7	17.6	24.1
⊗	BI-6	2	46.7	24.7	22.0
⊕	BI-6	7	39.5	17.0	22.5
☆	BI-7	4	35.5	18.7	16.8

PROJECT					HIGHWAY 17 BIQUETTE CREEK CULVERT - STA 13+350				
TITLE					PLASTICITY CHART CLAYEY SILT to SILTY CLAY				
PROJECT No.		13-1184-0074		FILE No.		13-1184-0074.GPJ			
DRAWN	TB	Jun 2014		SCALE	N/A	REV.			
CHECK	AB	Jun 2014		FIGURE B4.1					
APPR	JMAC	Jun 2014							
 Golder Associates SUDBURY, ONTARIO									

PLASTICITY INDEX (Percent)



SOIL TYPE
 C = Clay
 M = Silt
 O = Organic

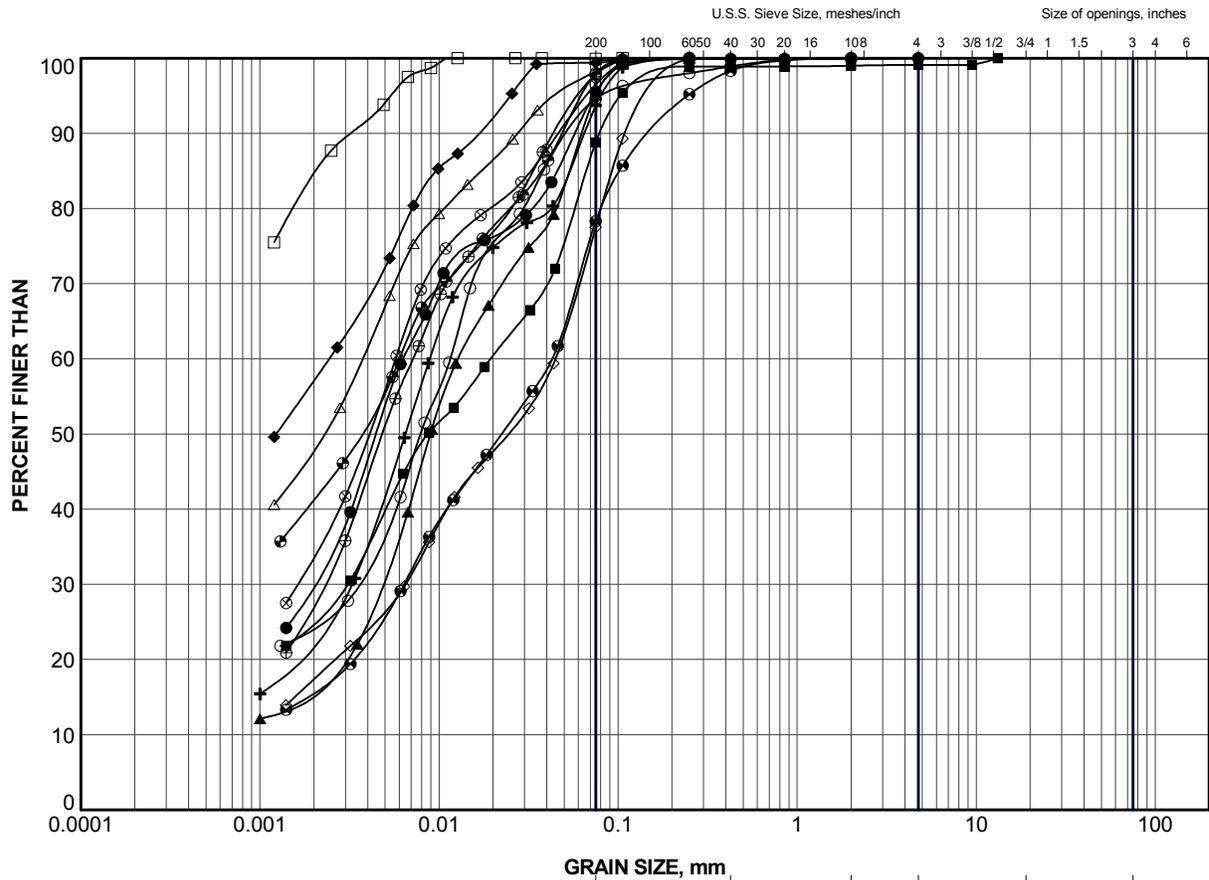
PLASTICITY
 L = Low
 I = Intermediate
 H = High

LEGEND

SYMBOL	BOREHOLE	SAMPLE	LL(%)	PL(%)	PI
●	BI-5a	2 (s)	23.1	16.6	6.5
■	BI-5a	2 (c)	86.9	27.2	59.7

Note:
 (s) silt lamina
 (c) clay lamina

PROJECT					HIGHWAY 17 BIQUETTE CREEK CULVERT - STA 13+350				
TITLE					PLASTICITY CHART SILT and CLAY LAMINAE				
PROJECT No.		13-1184-0074		FILE No.		13-1184-0074.GPJ			
DRAWN	TB	Jun 2014		SCALE	N/A	REV.			
CHECK	AB	Jun 2014		FIGURE B4.2					
APPR	JMAC	Jun 2014							
 Golder Associates SUDBURY, ONTARIO									

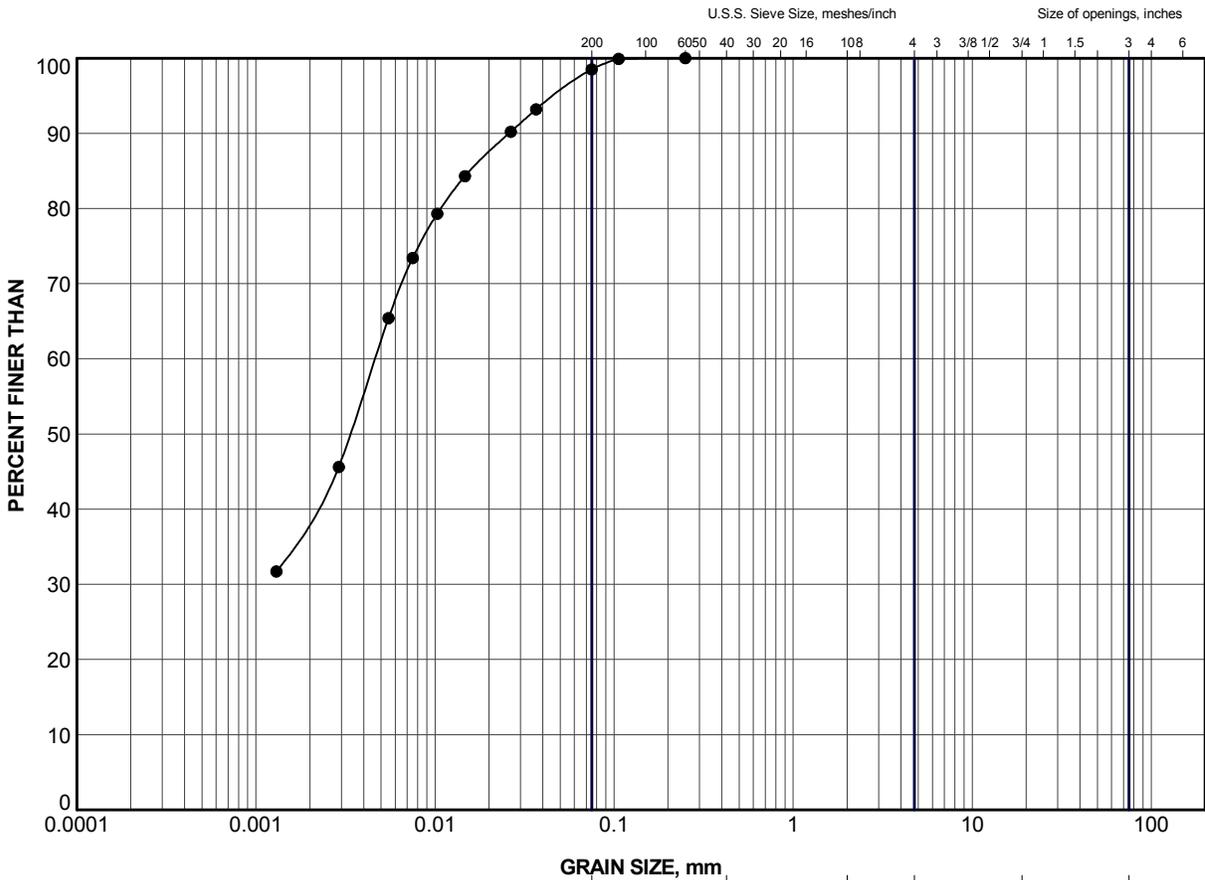


CLAY AND SILT	fine	medium	coarse	fine	coarse	Cobble Size
	SAND SIZE			GRAVEL SIZE		

LEGEND			
SYMBOL	BOREHOLE	SAMPLE	ELEV (m)
●	BI-1	12	197.9
■	BI-2	14	194.9
▲	BI-3	9	201.1
+	BI-3	10	199.5
◆	BI-4	7	195.0
◇	BI-4	10	190.4
○	BI-5	2	200.6
△	BI-5	7	195.3
⊗	BI-5a	1	198.4
⊕	BI-5a	2 (s)	197.0
□	BI-5a	2 (c)	196.9
⊙	BI-6	2	200.2
⊛	BI-6	7	194.9

PROJECT					HIGHWAY 17 BIQUETTE CREEK CULVERT - STA 13+350				
TITLE					GRAIN SIZE DISTRIBUTION CLAYEY SILT to SILTY CLAY				
PROJECT No.		13-1184-0074		FILE No.		13-1184-0074.GPJ			
DRAWN	TB	Jun 2014		SCALE	N/A	REV.			
CHECK	AB	Jun 2014		FIGURE B5.1					
APPR	JMAC	Jun 2014							





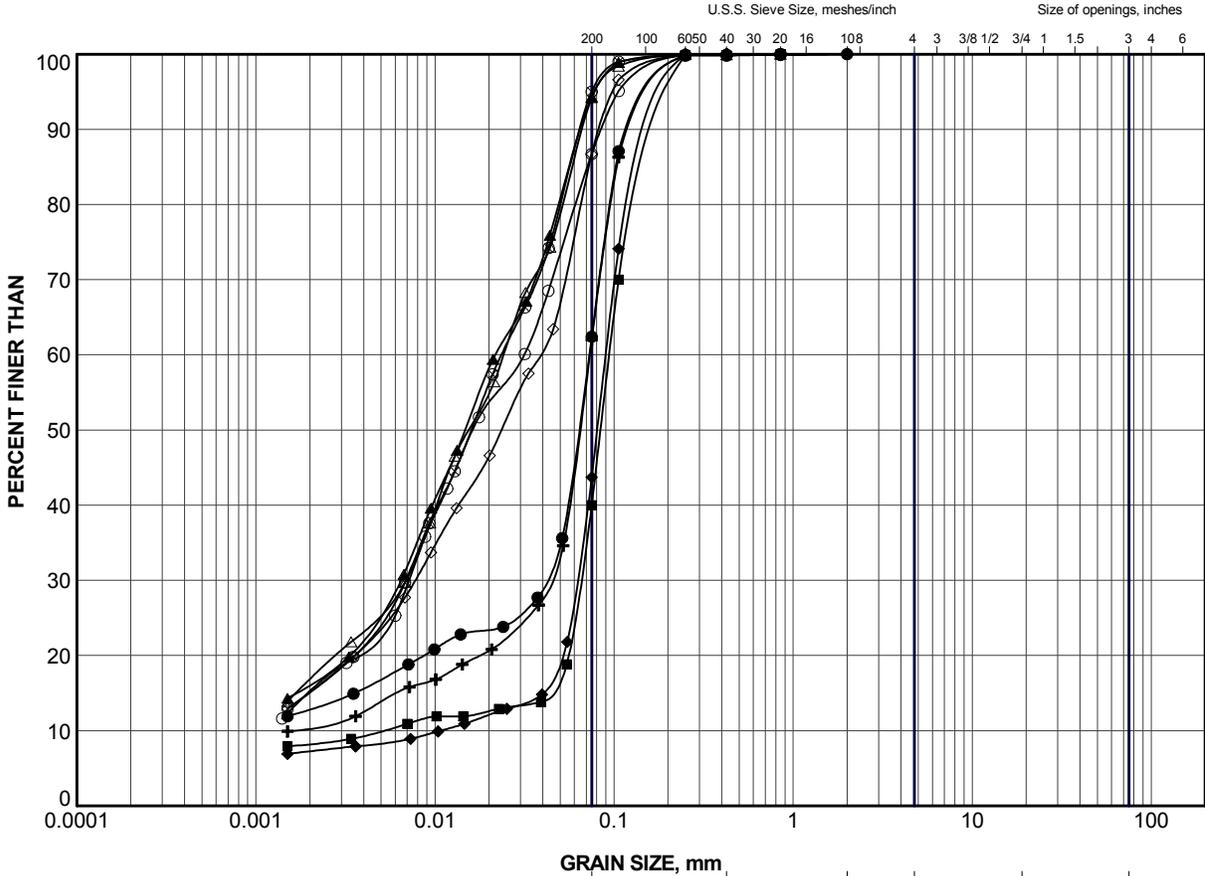
CLAY AND SILT	fine	medium	coarse	fine	coarse	Cobble Size
	SAND SIZE			GRAVEL SIZE		

LEGEND			
SYMBOL	BOREHOLE	SAMPLE	ELEV (m)
●	BI-7	4	196.0

PROJECT					HIGHWAY 17 BIQUETTE CREEK CULVERT - STA 13+350				
TITLE					GRAIN SIZE DISTRIBUTION CLAYEY SILT to SILTY CLAY				
PROJECT No.		13-1184-0074			FILE No.		13-1184-0074.GPJ		
DRAWN	TB	Jun 2014			SCALE	N/A	REV.		
CHECK	AB	Jun 2014			FIGURE B5.2				
APPR	JMAC	Jun 2014							



SUD-MTO GSD (NEW) GLDR_LDN.GDT



CLAY AND SILT	fine	medium	coarse	fine	coarse	Cobble Size
	SAND SIZE			GRAVEL SIZE		

LEGEND

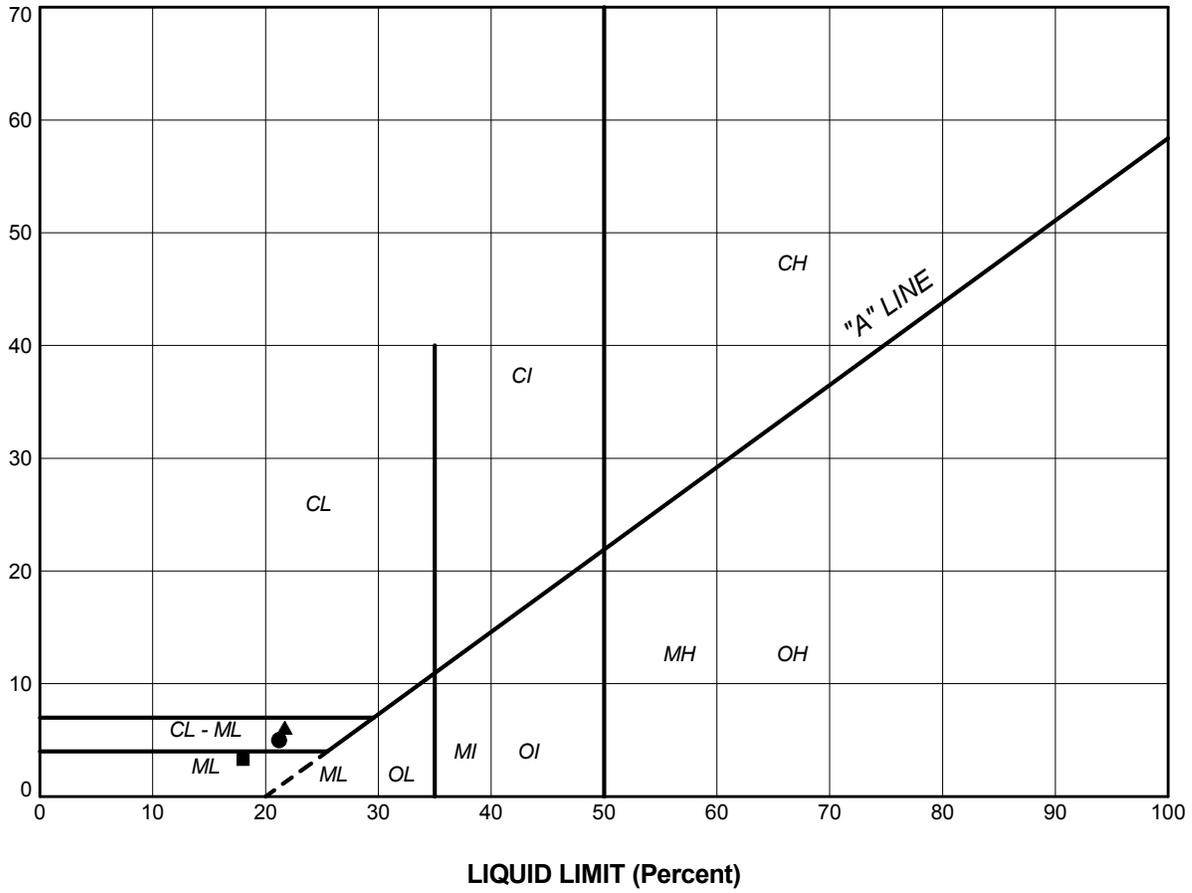
SYMBOL	BOREHOLE	SAMPLE	ELEV (m)
●	BI-1	16	191.8
■	BI-2	16	191.8
▲	BI-2	18	188.8
+	BI-4	12	187.4
◆	BI-5	10	190.7
◇	BI-5	11	189.2
○	BI-6	11	188.8
△	BI-7	7	191.5
⊗	BI-7	9	188.4

PROJECT HIGHWAY 17 BIQUETTE CREEK CULVERT - STA 13+350				
TITLE GRAIN SIZE DISTRIBUTION SILT to SILT and SAND				
PROJECT No. 13-1184-0074		FILE No. 13-1184-0074.GPJ		
DRAWN	TB	Jun 2014	SCALE	N/A
CHECK	AB	Jun 2014	REV.	
APPR	JMAC	Jun 2014	FIGURE B6	



SUD-MTO GSD (NEW) GLDR_LDN.GDT

PLASTICITY INDEX (Percent)



SOIL TYPE
 C = Clay
 M = Silt
 O = Organic

PLASTICITY
 L = Low
 I = Intermediate
 H = High

LEGEND

SYMBOL	BOREHOLE	SAMPLE	LL(%)	PL(%)	PI
●	BI-2	18	21.2	16.2	5.0
■	BI-5	11	18.0	14.7	3.3
▲	BI-6	11	21.7	15.6	6.1

PROJECT					HIGHWAY 17 BIQUETTE CREEK CULVERT - STA 13+350									
TITLE										PLASTICITY CHART SILT to SILT and SAND				
PROJECT No.			13-1184-0074			FILE No.			13-1184-0074.GPJ					
DRAWN		TB		Jun 2014		SCALE		N/A		REV.				
CHECK		AB		Jun 2014										
APPR		JMAC		Jun 2014										
 Golder Associates SUDBURY, ONTARIO					FIGURE B7									

As a global, employee-owned organisation with over 50 years of experience, Golder Associates is driven by our purpose to engineer earth's development while preserving earth's integrity. We deliver solutions that help our clients achieve their sustainable development goals by providing a wide range of independent consulting, design and construction services in our specialist areas of earth, environment and energy.

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