

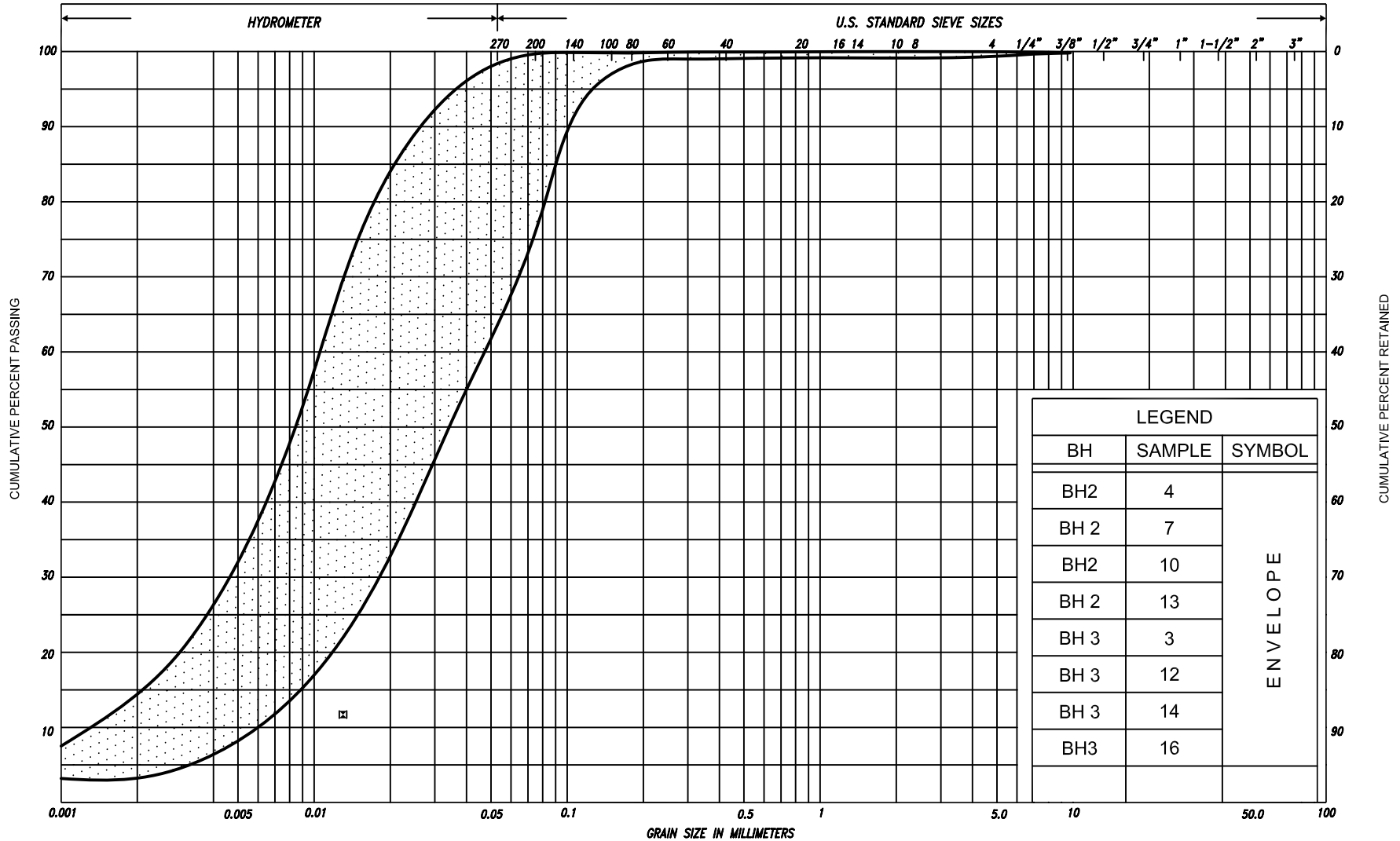


TABLE 1
SUMMARY OF SUBSURFACE CONDITIONS

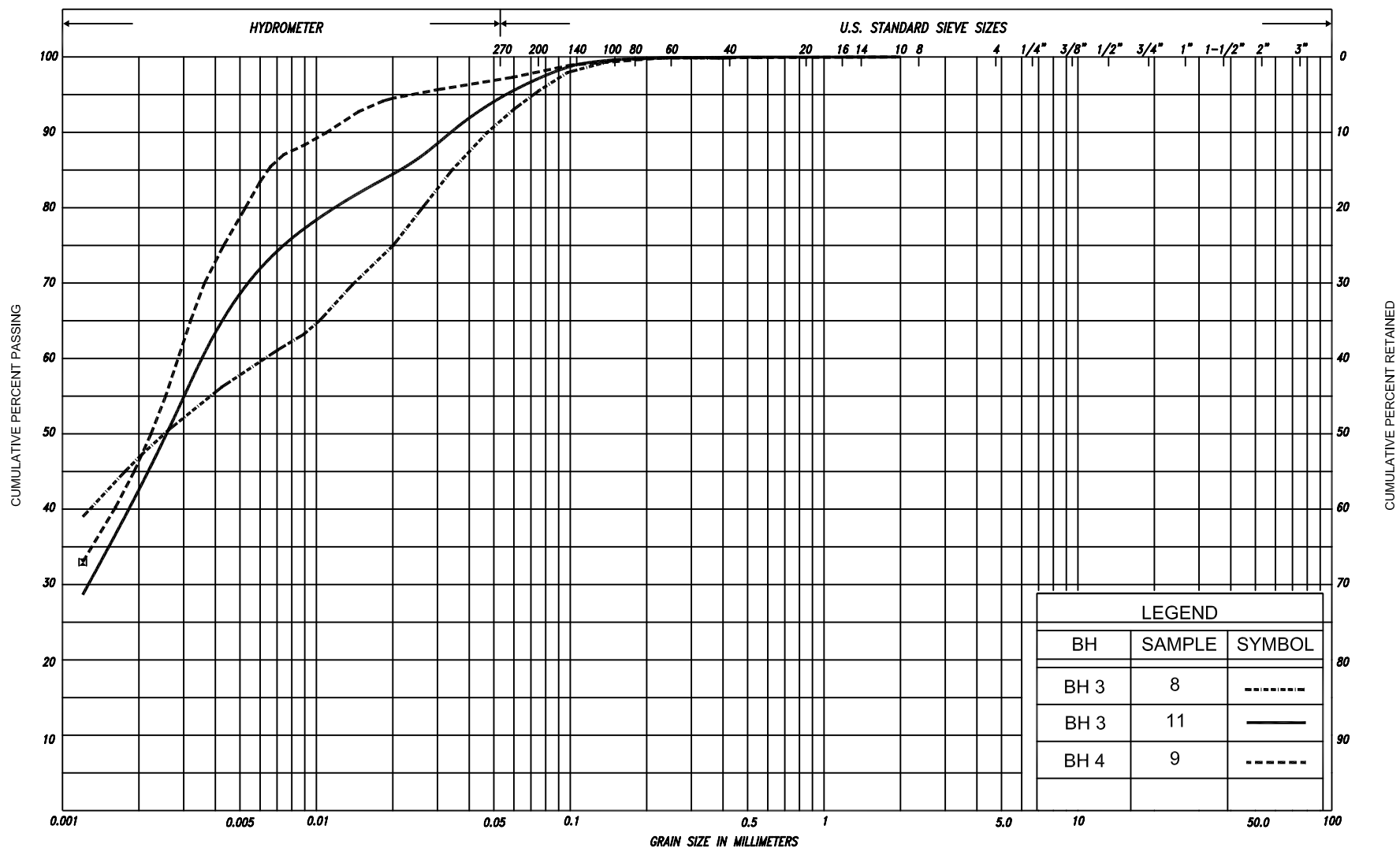
LOCATION AT THE BRIDGE SITE	SUMMARY OF SUBSURFACE CONDITIONS
East Abutment (Probe Hole 1)	Soil stratigraphy included a 300 mm thick topsoil over 800 mm cohesionless deposits of silt. Probable bedrock surface encountered at 1.1 m depth, elevation 291.0 m.
Centre Pier (Borehole 2)	Soil stratigraphy included 500 mm topsoil overlying 9.7 m thick silt unit which in turn underlain by 2.9 m thick cohesive silty clay matrix. A 22.9 m thick cohesionless silt unit was encountered below the silty clay, which mantled the probable bedrock at 36.0 m depth, elevation 253.9 m.
West Abutment (Borehole 3)	Soil stratigraphy encountered at the west abutment location included 600 mm fill overlying 500 mm thick topsoil unit which in turn overlying a 4.4 m thick silt matrix. A 6.4 m thick cohesive clayey unit is underlying the silt unit, which in turn is overlying 26.2 m thick cohesionless silt unit, which mantled the probable bedrock at 38.1 m depth, elevation 249.6 m.

TABLE 2
ADVANTAGES AND DISADVANTAGES, RELATIVE COSTS AND RISKS/CONSEQUENCES
ALLENSVILLE UNDERPASS

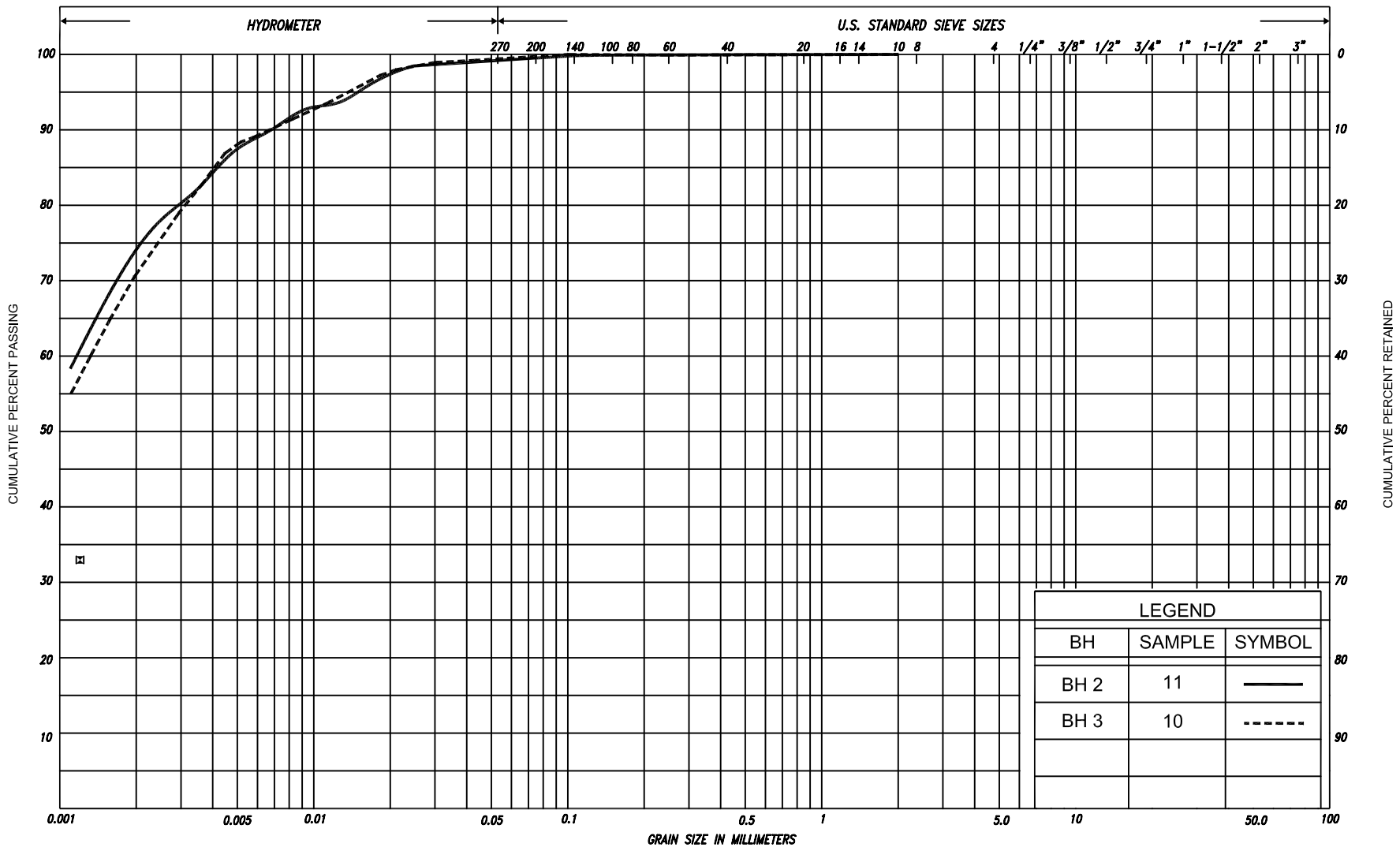
STRUCTURE FOUNDATION TYPE	ADVANTAGES	DISADVANTAGES	RELATIVE COSTS	RISKS/CONSEQUENCES	RANK
East Abutment Shallow Foundations - Spread footings	<ul style="list-style-type: none"> • Conventional construction methods • Spread footings on engineered fill may use higher bearing resistances 	<ul style="list-style-type: none"> • Low geotechnical resistances requires large footings 	<ul style="list-style-type: none"> • Less costly than deep foundations 	<ul style="list-style-type: none"> • Low risk 	1
	<ul style="list-style-type: none"> • Semi-integral abutment design is possible 	<ul style="list-style-type: none"> • Requires bedrock trench to provide adequate pile length 	<ul style="list-style-type: none"> • Costly than shallow foundations 	<ul style="list-style-type: none"> • Work with piling equipment near existing highway requires special care 	2
Centre Pier and West Abutment Deep Foundations - Steel H-Piles	<ul style="list-style-type: none"> • High load carrying capacities are obtained on piles to the bedrock • Integral abutment design is possible with pile foundations 	<ul style="list-style-type: none"> • Requires heavy pile driving equipment • Higher cost than shallow foundations • Requires surcharging of site to reduce negative skin friction 	<ul style="list-style-type: none"> • More costly than shallow foundations 	<ul style="list-style-type: none"> • Work with piling equipment near existing highway requires special care 	1
Deep Foundations - Caissons	<ul style="list-style-type: none"> • High load bearing capacity 	<ul style="list-style-type: none"> • Low soil resistances require deep installations below water table (<u>not practical</u>) 	<ul style="list-style-type: none"> • More costly than shallow foundations 	<ul style="list-style-type: none"> • Unwatering of caisson holes may not be feasible 	2 (not practical)
APPROACH EMBANKMENTS	ADVANTAGES	DISADVANTAGES	RELATIVE COSTS	RISKS/CONSEQUENCES	RANK
Surcharging without Soil Removal	<ul style="list-style-type: none"> • Excavation near existing embankment are not required • Post-construction settlements are mitigated 	<ul style="list-style-type: none"> • Requires preloading/surcharging to mitigate long-term settlement of approach embankment 	<ul style="list-style-type: none"> • Lower cost than soil removal option 	<ul style="list-style-type: none"> • Possible post-construction settlements of new roadway may need repair or maintenance 	1
Removal of Compressible Soils	<ul style="list-style-type: none"> • Reduced long-term settlements 	<ul style="list-style-type: none"> • Excavation of cohesive soil not practical 	<ul style="list-style-type: none"> • Higher cost than surcharge option 	<ul style="list-style-type: none"> • Excavation may cause instability to existing highway embankment 	2 (not practical)



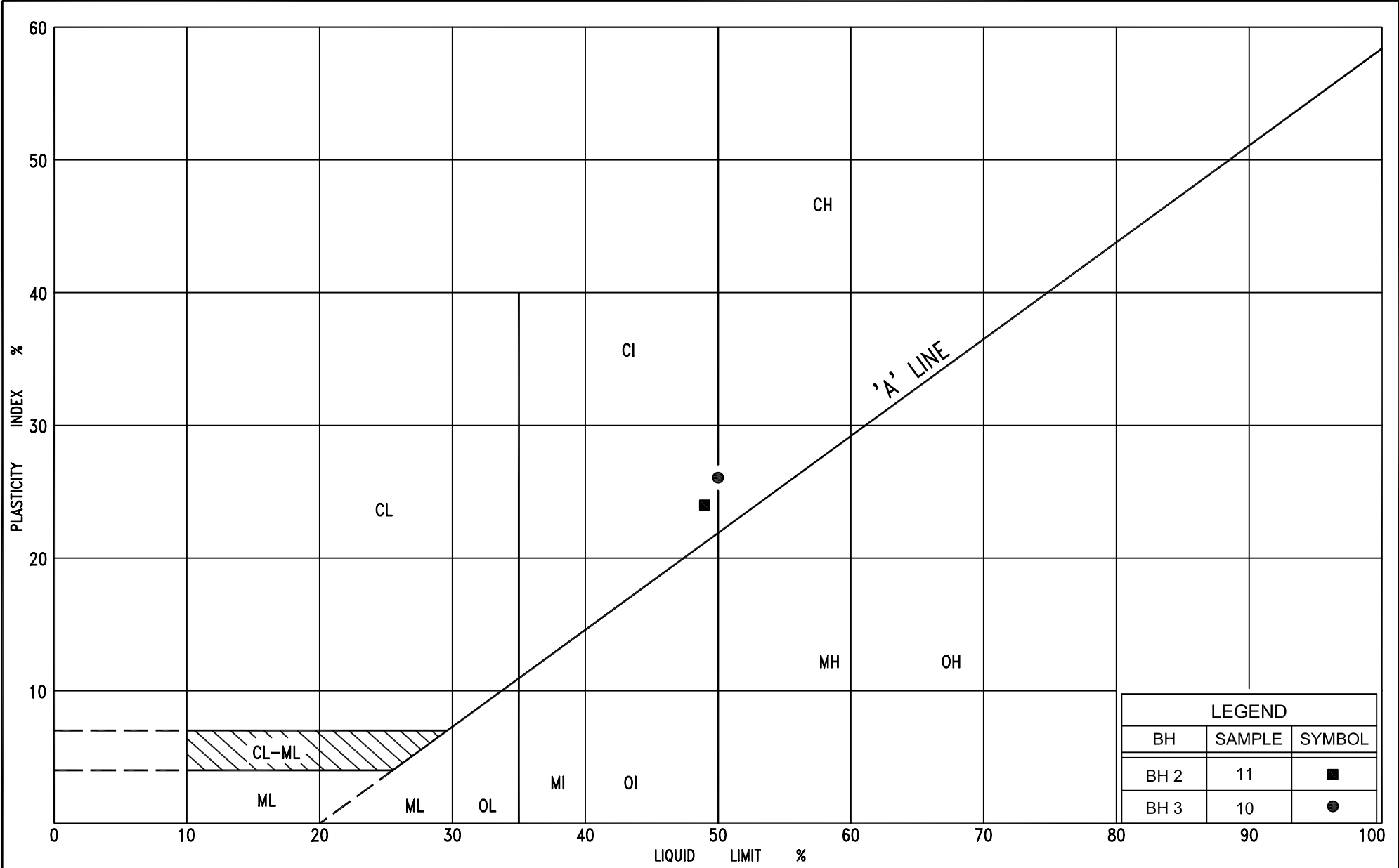
SILT & CLAY				FINE		MEDIUM		COARSE	GRAVEL			COB BLES	UNIFIED	
				SAND										
CLAY	FINE		MEDIUM	COARSE	FINE		MEDIUM	COARSE		GRAVEL			COBBLES	M.I.T.
	SILT													
CLAY		SILT			V. FINE	FINE	MED.	COARSE	GRAVEL					U.S. BUREAU
				SAND										



SILT & CLAY				FINE		MEDIUM		COARSE		GRAVEL			COBBLES	UNIFIED
CLAY	FINE	MEDIUM	COARSE	FINE		MEDIUM		COARSE		GRAVEL			COBBLES	M.I.T.
	SILT				SAND									
CLAY		SILT		V. FINE	FINE	MED.	COARSE	GRAVEL						U.S. BUREAU



SILT & CLAY					FINE		MEDIUM		COARSE	GRAVEL			COBBLES	UNIFIED	
					SAND										
CLAY	FINE		MEDIUM	COARSE	FINE		MEDIUM		COARSE		GRAVEL			COBBLES	M.I.T.
	SILT														
CLAY		SILT			V. FINE	FINE	MED.	COARSE	GRAVEL						U.S. BUREAU
					SAND										



Ministry of
Transportation
Ontario

PLASTICITY CHART
SILTY CLAY, trace sand

FIG No.	AR-PC-2
HWY:	11
W.P. No.	320-00-00

EXPLANATION OF TERMS USED IN REPORT

N VALUE: THE STANDARD PENETRATION TEST (SPT) N VALUE IS THE NUMBER OF BLOWS REQUIRED TO CAUSE A STANDARD 51mm O.D. SPLIT BARREL SAMPLER TO PENETRATE 0.3m INTO UNDISTURBED GROUND IN A BOREHOLE WHEN DRIVEN BY A HAMMER WITH A MASS OF 63.5kg, FALLING FREELY A DISTANCE OF 0.76m. FOR PENETRATIONS OF LESS THAN 0.3m N VALUES ARE INDICATED AS THE NUMBER OF BLOWS FOR THE PENETRATION ACHIEVED. AVERAGE N VALUE IS DENOTED THUS \bar{N} .

DYNAMIC CONE PENETRATION TEST: CONTINUOUS PENETRATION OF A CONICAL STEEL POINT (51mm O.D. 60° CONE ANGLE) DRIVEN BY 475 J IMPACT ENERGY ON 'A' SIZE DRILL RODS. THE RESISTANCE TO CONE PENETRATION IS MEASURED AS THE NUMBER OF BLOWS FOR EACH 0.3m ADVANCE OF THE CONICAL POINT INTO THE UNDISTURBED GROUND.

SOILS ARE DESCRIBED BY THEIR COMPOSITION AND CONSISTENCY OR DENSENESS.

CONSISTENCY: COHESIVE SOILS ARE DESCRIBED ON THE BASIS OF THEIR UNDRAINED SHEAR STRENGTH (c_u) AS FOLLOWS:

c_u (kPa)	0 - 12	12 - 25	25 - 50	50 - 100	100 - 200	> 200
	VERY SOFT	SOFT	FIRM	STIFF	VERY STIFF	HARD

DENSENESS: COHESIONLESS SOILS ARE DESCRIBED ON THE BASIS OF DENSENESS AS INDICATED BY SPT N VALUES AS FOLLOWS:

N (BLOWS/0.3m)	0 - 5	5 - 10	10 - 30	30 - 50	> 50
	VERY LOOSE	LOOSE	COMPACT	DENSE	VERY DENSE

ROCKS ARE DESCRIBED BY THEIR COMPOSITION AND STRUCTURAL FEATURES AND / OR STRENGTH.

RECOVERY: SUM OF ALL RECOVERED ROCK CORE PIECES FROM A CORING RUN EXPRESSED AS A PERCENT OF THE TOTAL LENGTH OF THE CORING RUN.

MODIFIED RECOVERY: SUM OF THOSE INTACT CORE PIECES, 100mm+ IN LENGTH EXPRESSED AS A PERCENT OF THE LENGTH OF THE CORING RUN. THE ROCK QUALITY DESIGNATION (R Q D), FOR MODIFIED RECOVERY, IS:

R Q D (%)	0 - 25	25 - 50	50 - 75	75 - 90	90 - 100
	VERY POOR	POOR	FAIR	GOOD	EXCELLENT

JOINTING AND BEDDING:

SPACING	50mm	50 - 300mm	0.3m - 1m	1m - 3m	> 3m
JOINTING	VERY CLOSE	CLOSE	MOD. CLOSE	WIDE	VERY WIDE
BEDDING	VERY THIN	THIN	MEDIUM	THICK	VERY THICK

ABBREVIATIONS AND SYMBOLS

FIELD SAMPLING

S S	SPLIT SPOON	T P	THINWALL PISTON
W S	WASH SAMPLE	O S	OSTERBERG SAMPLE
S T	SLOTTED TUBE SAMPLE	R C	ROCK CORE
B S	BLOCK SAMPLE	P H	T W ADVANCED HYDRAULICALLY
C S	CHUNK SAMPLE	P M	T W ADVANCED MANUALLY
T W	THINWALL OPEN	F S	FOIL SAMPLE
F V	FIELD VANE		

STRESS AND STRAIN

u_w	kPa	PORE WATER PRESSURE
u	1	PORE PRESSURE RATIO
σ	kPa	TOTAL NORMAL STRESS
σ'	kPa	EFFECTIVE NORMAL STRESS
τ	kPa	SHEAR STRESS
$\sigma_1, \sigma_2, \sigma_3$	kPa	PRINCIPAL STRESSES
ϵ	%	LINEAR STRAIN
$\epsilon_1, \epsilon_2, \epsilon_3$	%	PRINCIPAL STRAINS
E	kPa	MODULUS OF LINEAR DEFORMATION
G	kPa	MODULUS OF SHEAR DEFORMATION
μ	1	COEFFICIENT OF FRICTION

MECHANICAL PROPERTIES OF SOIL

m_v	kPa^{-1}	COEFFICIENT OF VOLUME CHANGE
C_c	1	COMPRESSION INDEX
C_s	1	SWELLING INDEX
C_α	1	RATE OF SECONDARY CONSOLIDATION
c_v	m^2/s	COEFFICIENT OF CONSOLIDATION
H	m	DRAINAGE PATH
T_v	1	TIME FACTOR
U	%	DEGREE OF CONSOLIDATION
σ'_{vo}	kPa	EFFECTIVE OVERBURDEN PRESSURE
σ'_p	kPa	PRECONSOLIDATION PRESSURE
τ_f	kPa	SHEAR STRENGTH
c'	kPa	EFFECTIVE COHESION INTERCEPT
ϕ'	-°	EFFECTIVE ANGLE OF INTERNAL FRICTION
c_u	kPa	APPARENT COHESION INTERCEPT
ϕ_u	-°	APPARENT ANGLE OF INTERNAL FRICTION
τ_R	kPa	RESIDUAL SHEAR STRENGTH
τ_r	kPa	REMOULDED SHEAR STRENGTH
S_t	1	SENSITIVITY = $\frac{c_u}{\tau_r}$

PHYSICAL PROPERTIES OF SOIL

ρ_s	kg/m^3	DENSITY OF SOLID PARTICLES	n	1, %	POROSITY	e_{max}	1, %	VOID RATIO IN LOOSEST STATE
γ_s	kN/m^3	UNIT WEIGHT OF SOLID PARTICLES	w	1, %	WATER CONTENT	e_{min}	1, %	VOID RATIO IN DENSEST STATE
ρ_w	kg/m^3	DENSITY OF WATER	S_r	%	DEGREE OF SATURATION	I_D	1	DENSITY INDEX = $\frac{e_{max} - e}{e_{max} - e_{min}}$
γ_w	kN/m^3	UNIT WEIGHT OF WATER	w_L	%	LIQUID LIMIT	D	mm	GRAIN DIAMETER
ρ	kg/m^3	DENSITY OF SOIL	w_p	%	PLASTIC LIMIT	D_n	mm	n PERCENT - DIAMETER
γ	kN/m^3	UNIT WEIGHT OF SOIL	w_s	%	SHRINKAGE LIMIT	C_u	1	UNIFORMITY COEFFICIENT
ρ_d	kg/m^3	DENSITY OF DRY SOIL	I_p	%	PLASTICITY INDEX = $w_L - w_p$	h	m	HYDRAULIC HEAD OR POTENTIAL
γ_d	kN/m^3	UNIT WEIGHT OF DRY SOIL	I_L	1	LIQUIDITY INDEX = $\frac{w - w_p}{I_p}$	q	m^3/s	RATE OF DISCHARGE
ρ_{sat}	kg/m^3	DENSITY OF SATURATED SOIL	I_C	1	CONSISTENCY INDEX = $\frac{w_L - w}{I_p}$	v	m/s	DISCHARGE VELOCITY
γ_{sat}	kN/m^3	UNIT WEIGHT OF SATURATED SOIL	DTPL		DRIER THAN PLASTIC LIMIT	i	1	HYDRAULIC GRADIENT
ρ'	kg/m^3	DENSITY OF SUBMERGED SOIL	APL		ABOUT PLASTIC LIMIT	k	m/s	HYDRAULIC CONDUCTIVITY
γ'	kN/m^3	UNIT WEIGHT OF SUBMERGED SOIL	WTPL		WETTER THAN PLASTIC LIMIT	j	kN/m^3	SEEPAGE FORCE
e	1, %	VOID RATIO						

METRIC

20
15 — 5 (%) STRAIN AT FAILURE
10

RECORD OF BOREHOLE No 2

1 of 3

METRIC

G.W.P. 320-00-00 LOCATION Highway 11 Coords: 5 011 823.5 N; 320 621.7 E ORIGINATED BY F.P.
DIST 54 HWY 11 BOREHOLE TYPE C.F.H.S.A. and Dynamic Cone Penetration Test COMPILED BY N.R.
DATUM Geodetic DATE April 13, 2009 CHECKED BY C.N.

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT NATURAL MOISTURE CONTENT LIQUID LIMIT			UNIT WEIGHT γ kN/m³	REMARKS & GRAIN SIZE DISTRIBUTION (%)
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			SHEAR STRENGTH kPa					w _p	w	w _L		
289.9							20	40	60	80	100						
0.0	Topsoil		1	SS	3												
289.4																	
0.5	Silt, trace to with sand trace clay organic inclusions		2	SS	6												
	Loose Brown Moist		3	SS	11												
	oxidized pockets		4	SS	10												
	Compact		5	SS	11												
			6	SS	12												
			7	SS	12												
	clayey silt layers		8	SS	6												
	Loose		9	SS	4												
	Grey		10	SS	6												
	some clay		11	SS	7												
279.7	Silty clay, trace sand clayey silt layers		12	SS	3												
10.2	Stiff Grey Wet		13	SS	23												
276.8																	
13.1	Silt some clay, trace sand																
	Compact Grey Moist																
274.9	Cont'd																

RECORD OF BOREHOLE No 2

2 of 3

METRIC

G.W.P. 320-00-00 LOCATION Highway 11 Coords: 5 011 823.5 N; 320 621.7 E ORIGINATED BY F.P.
DIST 54 HWY 11 BOREHOLE TYPE C.F.H.S.A. and Dynamic Cone Penetration Test COMPILED BY N.R.
DATUM Geodetic DATE April 13, 2009 CHECKED BY C.N.

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT				PLASTIC LIMIT w _p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w _L	UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL				
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			SHEAR STRENGTH kPa												
								○ UNCONFINED + FIELD VANE												
								● QUICK TRIAXIAL × LAB VANE												
							20 40 60 80 100					20 40 60								
274.9	Silt trace to some clay, trace sand Compact Grey Moist																			
15.0			14	SS	17															
			15	SS	20															
																</				

METRIC

20
15 — 5 (%) STRAIN AT FAILURE
10

RECORD OF BOREHOLE No 3

1 of 3

METRIC

G.W.P. 320-00-00 LOCATION Highway 11 Coords: 5 011 834.8 N; 320 586.9 E ORIGINATED BY F.P.
DIST 54 HWY 11 BOREHOLE TYPE C.F.H.S.A. + Wash Boring COMPILED BY N.R.
DATUM Geodetic DATE April 07 & 08, 2009 CHECKED BY C.N.

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT NATURAL MOISTURE CONTENT LIQUID LIMIT			UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%)		
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES			SHEAR STRENGTH kPa					w _p	w	w _L				
								○ UNCONFINED + FIELD VANE											
								● QUICK TRIAXIAL x LAB VANE											
WATER CONTENT (%)																			
20 40 60 80 100											20 40 60								
287.7	Sandy silt topsoil inclusions Brown Moist (FILL) Topsoil Silt, trace to some sand trace clay oxidized layers Compact Grey Wet Brown trace sand Loose Grey		1	SS	2														
0.0																			
287.1																			
0.6																			
286.6																			
1.1																			
		</																	

RECORD OF BOREHOLE No 3

2 of 3

METRIC

G.W.P. 320-00-00 LOCATION Highway 11 Coords: 5 011 834.8 N; 320 586.9 E ORIGINATED BY F.P.
 DIST 54 HWY 11 BOREHOLE TYPE C.F.H.S.A. + Wash Boring COMPILED BY N.R.
 DATUM Geodetic DATE April 07 & 08, 2009 CHECKED BY C.N.

SOIL PROFILE				SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT			PLASTIC LIMIT w _p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w _L	UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%)										
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	"N" VALUES	SHEAR STRENGTH kPa					WATER CONTENT (%)					GR	SA	SI	CL							
						○ UNCONFINED + FIELD VANE																				
						● QUICK TRIAXIAL × LAB VANE																				
272.7 15.0	Silt trace clay, trace sand Compact Grey Moist						20	40	60	80	100						0	6	90	4						
			14	SS	11								○													








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RECORD OF BOREHOLE No 4

1 of 2

METRIC

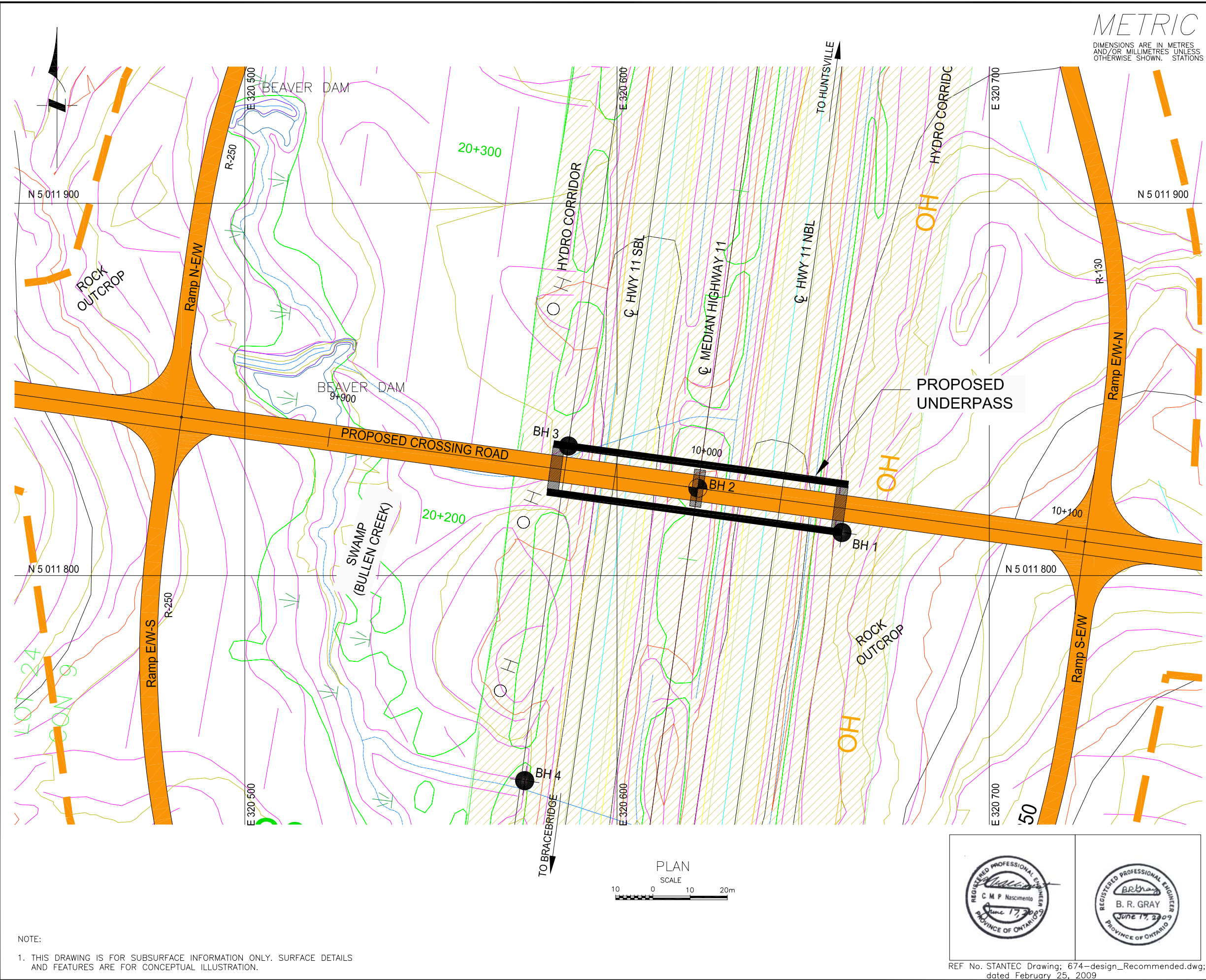
G.W.P. 320-00-00 LOCATION Highway 11 Coords: 5 011 744.9 N; 320 575.2 E ORIGINATED BY F.P.
DIST 54 HWY 11 BOREHOLE TYPE Continuous Flight Hollow Stem Augers COMPILED BY N.R.
DATUM Geodetic DATE April 09, 2009 CHECKED BY C.N.

SOIL PROFILE			SAMPLES			GROUND WATER CONDITIONS	ELEVATION SCALE	DYNAMIC CONE PENETRATION RESISTANCE PLOT					PLASTIC LIMIT w _p	NATURAL MOISTURE CONTENT w	LIQUID LIMIT w _L	UNIT WEIGHT γ kN/m ³	REMARKS & GRAIN SIZE DISTRIBUTION (%) GR SA SI CL			
ELEV DEPTH	DESCRIPTION	STRAT PLOT	NUMBER	TYPE	*N VALUES			SHEAR STRENGTH kPa												
								○ UNCONFINED + FIELD VANE												
								● QUICK TRIAXIAL × LAB VANE												
							WATER CONTENT (%)													
287.1 0.0	Peat		1	SS	1		287													
286.6 0.5	Silt, trace to some sand trace clay organic inclusions		2	SS	9		286													
	Loose Grey / Wet brown																			
	Compact Reddish Moist brown		3	SS	15															
							285													
			4	SS	13															
	Loose																			

Cont'd

METRIC

+⁷, ×⁵: Numbers refer to Sensitivity

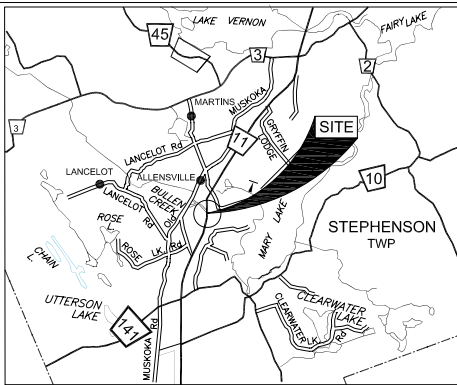


METRIC
DIMENSIONS ARE IN METRES
AND/OR MILLIMETRES UNLESS
OTHERWISE SHOWN. STATIONS

CONT No
GWP No 320-00-00
CROSSING ROAD I/C UNDERPASS
HIGHWAY 11
BOREHOLE LOCATIONS



SHEET



KEY PLAN
SCALE
0 2 4 6 km

LEGEND

- Borehole
- Dynamic Cone Penetration Test (Cone)
- Borehole & Cone
- N Blows/0.3m (Std. Pen Test, 475 J/blow)
- CONE Blows/0.3m (60 Cone, 475 J/blow)
- W L at time of investigation: April, 2009
- Head
- ARTESIAN WATER
- Encountered
- PIEZOMETER

BH No	ELEVATION	CO-ORDINATES	
		NORTHINGS	EASTINGS
1	292.1	5 011 811.6	320 660.4
2	289.9	5 011 823.5	320 621.7
3	287.7	5 011 834.8	320 586.9
4	287.1	5 011 744.9	320 575.2

NOTE
The boundaries between soil strata have been established only at Borehole locations. Between Boreholes the boundaries are assumed from geological evidence.

REVISIONS		DATE	BY	DESCRIPTION
Geocres No. 31E-295				
HWY No	11			DIST 52
SUBM'D	MN	CHECKED NR	DATE JUNE 17, 2009	SITE --
DRAWN	NA	CHECKED CN	APPROVED BRG	DWG AR-1

NOTE:
1. THIS DRAWING IS FOR SUBSURFACE INFORMATION ONLY. SURFACE DETAILS AND FEATURES ARE FOR CONCEPTUAL ILLUSTRATION.

PLAN
SCALE
10 0 10 20m



REF No. STANTEC Drawing; 674-design_Recommended.dwg;
dated February 25, 2009



APPENDIX A

SITE PHOTOGRAPHS



Photograph 1: Looking west from the west shoulder of Highway 11 SBL, approximate Station 20+215
Tip of a plastic culvert visible at the foreground of the photograph.



Photograph 2: Looking east from the median at about Sta. 20+215. A thick underbrush visible in the median of the Highway 11 lanes.



Photograph 3: Viewing east from the median to the east side of Highway 11 NBL at approximate Sta. 20+215. A hill is visible in the background of the photograph with bedrock outcrops exposed.



Photograph 4: Viewing east from the east shoulder of Highway 11 NBL at approximate Sta. 20+215. Bedrock outcrops exposed in the background of the photograph.



APPENDIX B

Slope Stability Analyses Results

SLOPE STABILITY ANALYSIS RESULTS

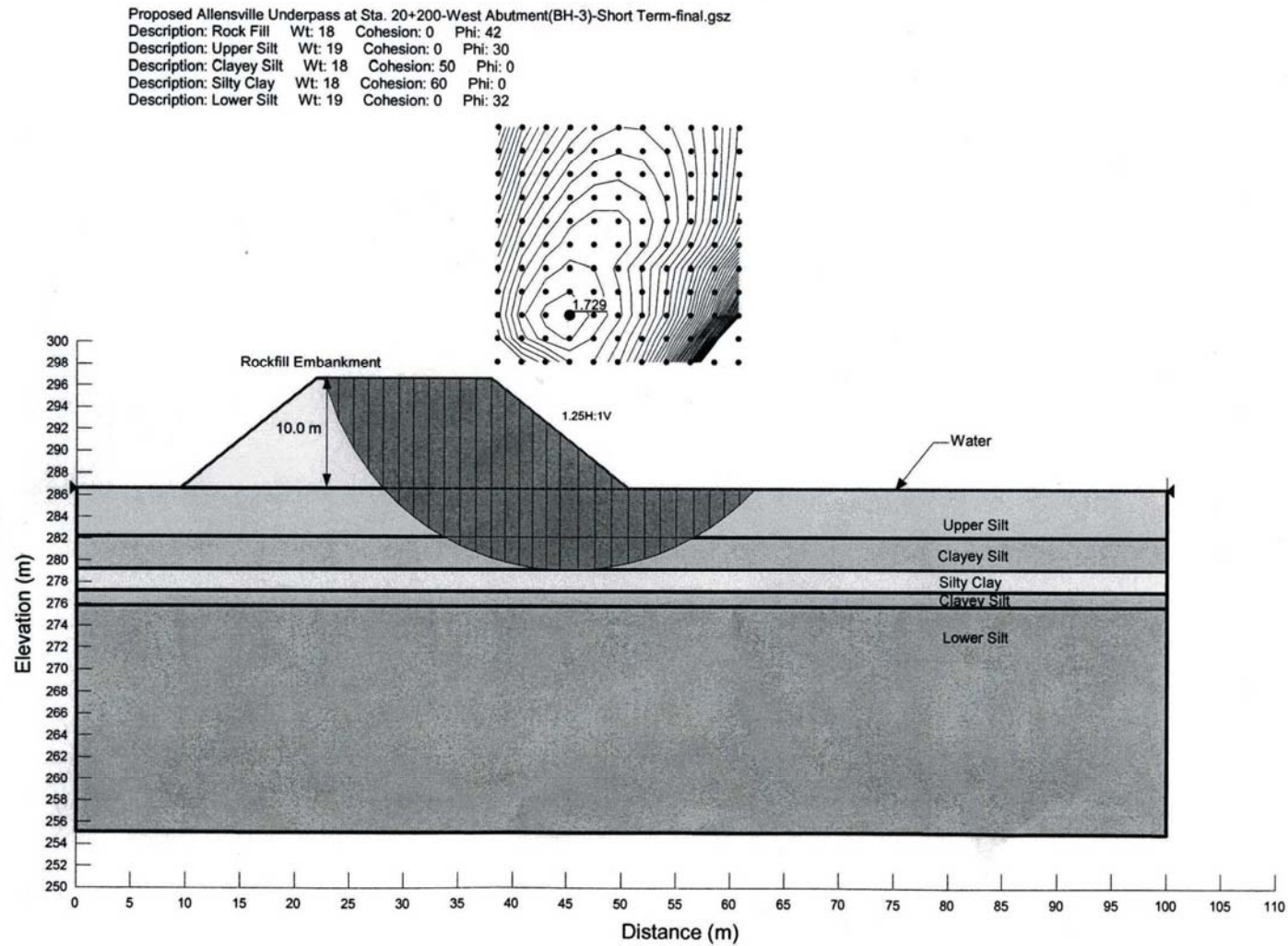


Figure 1

SLOPE STABILITY ANALYSIS RESULTS

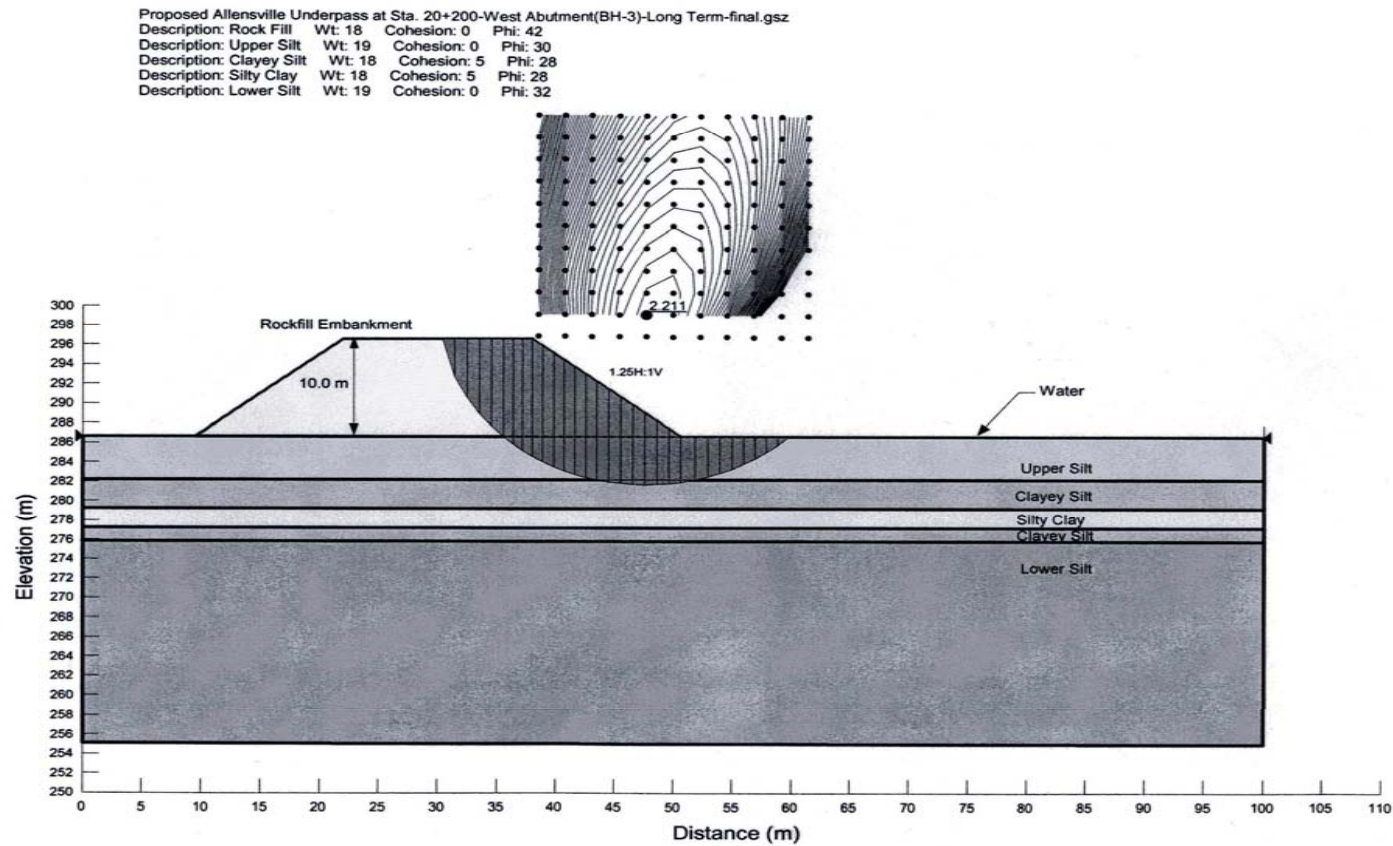
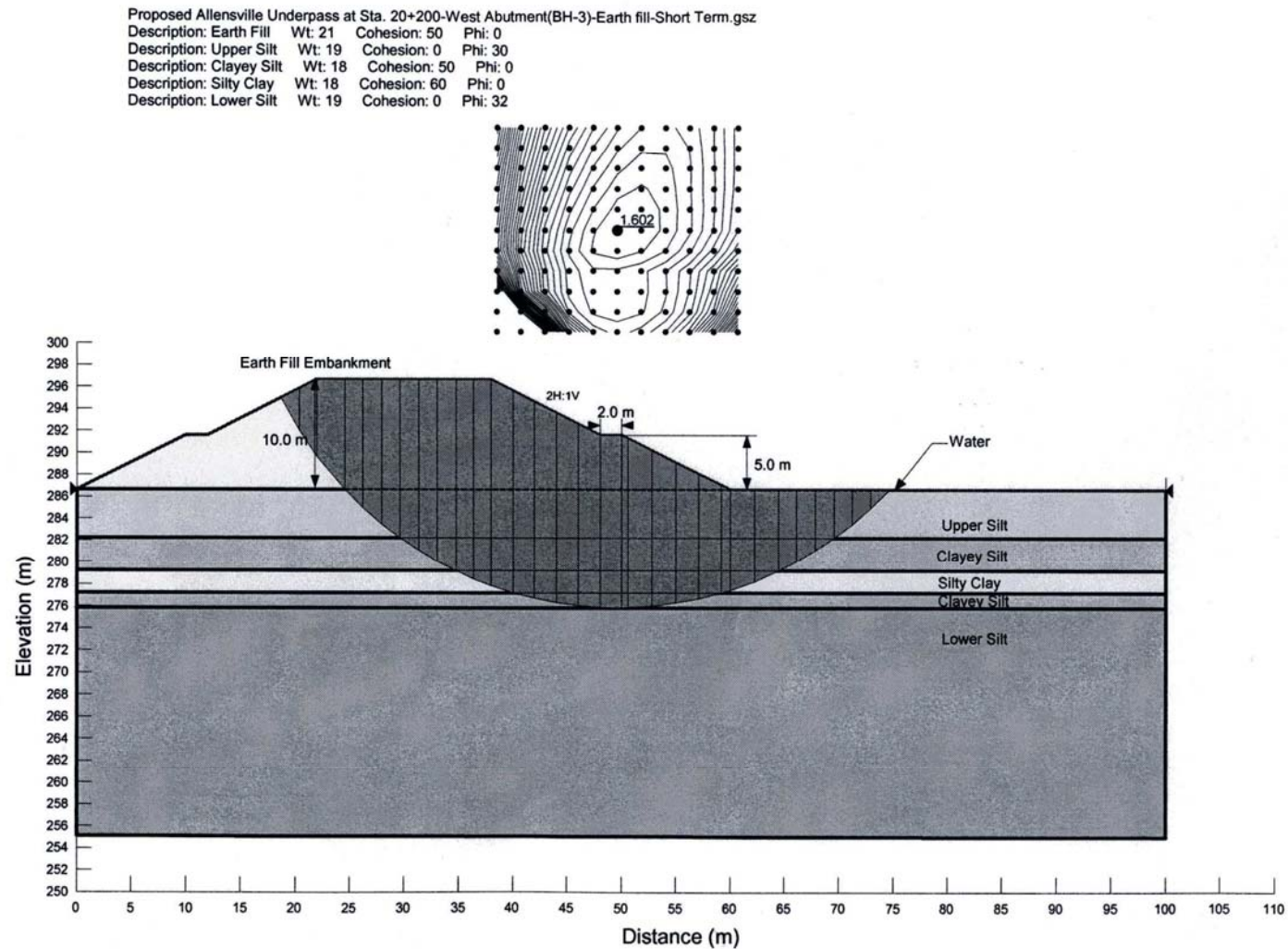


Figure 2

SLOPE STABILITY ANALYSIS RESULTS



SLOPE STABILITY ANALYSIS RESULTS

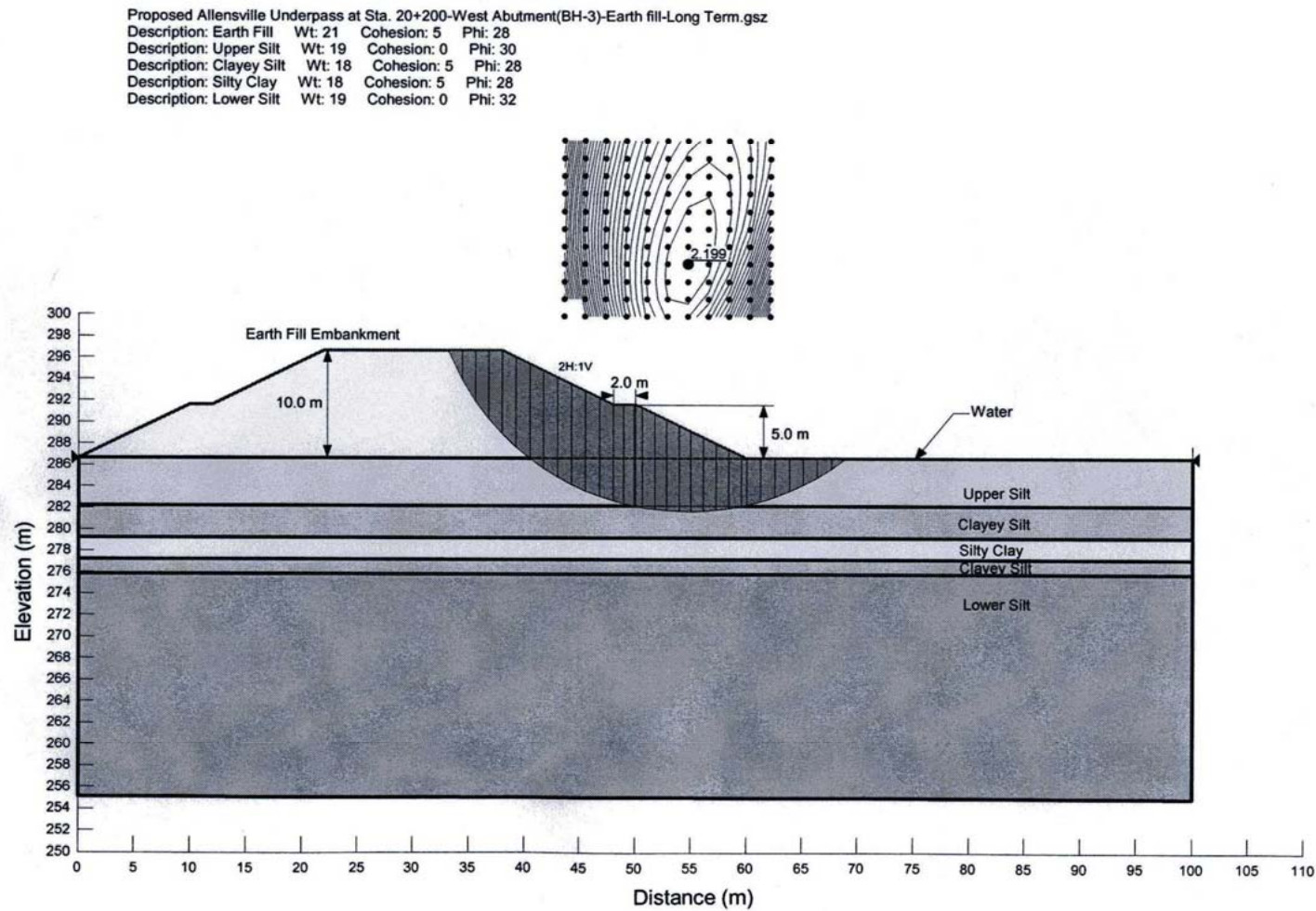


Figure 4